

Sub-optimal Discontinuous Current-Clamp switching rates lead to deceptive mouse neuronal firing

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Abstract Intracellular recordings using sharp micro-electrodes often rely on a technique called Discontinuous Current-Clamp to accurately record the membrane potential while injecting current through the same micro-electrode. It is well known that a poor choice of DCC switching rate can lead to under- or over-estimation of the cell potential, however, its effect on the cell firing is rarely discussed. Here, we show that sub-optimal switching rates lead to an overestimation of the cell excitability. We performed intracellular recordings of mouse spinal motoneurons, and recorded their firing in response to pulses and ramps of current in bridge and DCC mode at various switching rates. We demonstrate that using an incorrect (too low) DCC frequency lead not only to an overestimation of the cell conductance, but also, paradoxically, to an artificial overestimation the firing of these cells: neurons fire at lower current, and at higher frequencies than at higher DCC rates, or than the same neuron recorded in Bridge mode. These effects are dependent on the membrane time constant of the recorded cell, and special care needs to be taken in large cells with very short time constants. Our work highlights the importance of choosing an appropriate DCC switching rate to obtain not only accurate membrane potential readings, but also accurate representation of the firing of the cell.

Keywords

Electrophysiology, Technique, DCC, intracellular recording, sharp micro-electrodes, neuronal excitability, firing frequency

1 Introduction

2 Neurons, by virtue of their plasma membrane and the numerous ion channels that
3 can be found therein, behave—to a first approximation— like RC circuits. Conse-
4 quently, a stationary electrical (ionic) current flowing through the membrane causes
5 a change of voltage proportional to the resistance of the cell. This is Ohm’s law:
6 $V = I \times R$, where V is sometimes called voltage drop or IR drop. When performing
7 intracellular recordings with microelectrodes, or whole cell recordings using patch
8 electrodes, electrophysiologists can control the current flowing through their elec-
9 trode (“current clamp”) to change the membrane potential of the cell and thereby
10 study its excitability. However, the electrode itself, because of its very small tip,
11 acts as an additional RC circuit, and therefore also experiences an IR drop when
12 current is applied. In these conditions, it is essential to be able to separate the
13 physiological response of the cell from a change of voltage caused by the resistance
14 of the very electrode used to perform the recording. Two main techniques have
15 been developed over the years to overcome this problem. The first one, the so-
16 called “bridge” mode, consists (broadly speaking) in subtracting the voltage drop
17 caused by the current injection through a variable resistor set to a value close to
18 the estimated electrode resistance from the voltage measured by the electrode. This
19 technique works well if the resistance of the electrode can be assumed to be con-
20 stant over a large range of current intensity. Unfortunately, that is often not the
21 case, particularly with small intracellular microelectrodes, which can exhibit strong
22 non-linearities. A second technique was invented in the early 1970s, which consists
23 in injecting current and measuring the potential at separate times, hence the name
24 “discontinuous current clamp” (DCC) (Brennecke and Lindemann, 1971; Finkel and
25 Redman, 1984). Instead of injecting a continuous current, the amplifier will alter-
26 nate at a high frequency between injecting a pulse of current (scaled appropriately
27 so as to conserve the same charge transfer) for a very short duration (classically

28 1/3 of the DCC period), while no current is injected for the remainder of the DCC
29 period. The membrane potential is sampled at the end of the period, when no cur-
30 rent is injected through the microelectrode. If the time constant of the electrode
31 is fast enough compared to the time constant of the membrane, then the IR drop
32 through the electrode has had time to vanish when the potential is sampled, while
33 the IR drop through the membrane would have barely decayed. In theory, these
34 two recording modes (bridge and DCC) should yield the same values of membrane
35 potential, as long as they are used in the proper conditions. One important aspect
36 parameter is the DCC switching rate, which needs to be high enough so that the
37 membrane time constant can smooth out the short pulses of current, but not so high
38 as to prevent the IR drop through the electrode to vanish before the end of the sam-
39 pling period. An incorrectly set DCC rate should, in theory, only lead to under- or
40 over-estimating the membrane potential. Yet, a recent study (Jensen et al., 2020) il-
41 lustrates that the firing behaviour of a spinal motoneuron in response to a triangular
42 ramp of current can change drastically depending on the DCC switching rate set by
43 the experimenters, suggesting that the choice of the DCC switching rate is a critical
44 parameter to take into consideration not only in order to obtain accurate readings
45 of the membrane potential, but also when studying the firing rates of the cell. In
46 this paper, We demonstrate that using a sub-optimal (too low) DCC frequency lead
47 not only to an overestimation of the cell conductance, but also, paradoxically, to an
48 artificial overestimation the firing of these cells: neurons fire at lower current, and
49 at higher frequencies than at higher DCC rates, or than the same neuron recorded
50 in Bridge mode.

51 **2 Results**

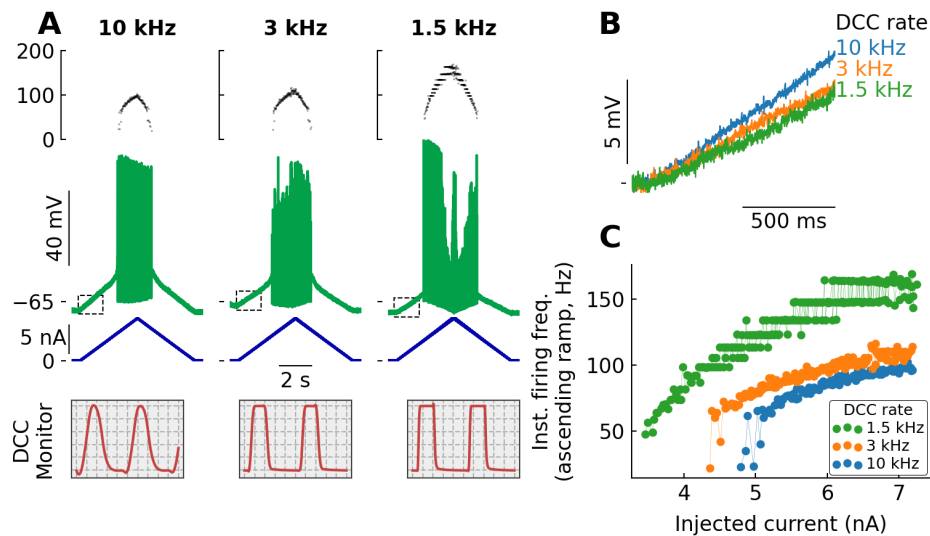


Figure 1. Typical example showing how DCC rates alter the response of a motoneuron to a stationary input. **A.** Response of a triceps Surae motoneuron ($R_{in}=3.8\text{ M}\Omega$; $\tau_m=3.3\text{ ms}$) to a slow (1 nA/s) triangular ramp of current, recorded in DCC mode with switching rates 10, 3 and 1.5 kHz. Bottom traces: injected current. Middle traces: voltage response. Top traces: instantaneous firing frequency. The boxes on the bottom represent the monitoring traces used to check the settling of the electrode, recorded at the top of the ramp. Time bases from left to right: $20\text{ }\mu\text{s}$, $67\text{ }\mu\text{s}$, and $133\text{ }\mu\text{s}$ per division. **B.** Expansions of the regions delimited with the dashed box in A. **C.** F-I curves showing the instantaneous firing frequency plotted against the injected current at the time of each spike.

52 2.1 Case study

53 Let us start by observing the effect of changing the DCC rate on the response of a
54 motoneuron to a triangular ramp of current. When recorded with a DCC rate of
55 10 kHz, the motoneuron depolarized progressively until it started to fire repetitively
56 (Figure 1A). The initial firing was irregular and accelerated very steeply over the
57 first few spikes. Then, the firing became more regular and increased approximately
58 linearly with the injected current (Figure 1C). This is the classical response of mouse
59 spinal motoneurons to this kind of current injected: a brief sub-primary range, fol-
60 lowed by a linear primary range (Manuel et al., 2009; Iglesias et al., 2011). When
61 recorded with a DCC rate of 3 kHz, the response was similar, but quantitative differ-
62 ences were visible. First, the rate of rise of the membrane potential before the onset
63 of firing was slower than at 10 kHz (Figure 1B). Since the current increases linearly,

64 the rate of rise of the membrane potential is directly proportional to the resistance
65 of the cell. At 3 kHz, the cell thus appears to have a higher conductance than at
66 10 kHz. Paradoxically, even though the conductance was seemingly increased, the
67 cell started firing at a lower current intensity, and at higher frequencies than at
68 10 kHz (Figure 1C). These effects were even more pronounced at lower DCC rates.
69 At 1.5 kHz, the apparent conductance was larger than at 10 and 3 kHz (lower rate
70 of rise of the potential, Figure 1B) and the firing started even sooner (Figure 1C).
71 In addition, at 1.5 kHz, the firing frequency increased very steeply with the injected
72 current and reached much higher values (> 100 Hz) than with higher DCC rates.
73 Moreover, when the firing frequency increased beyond 100 Hz, the firing acquired
74 a very distinctive step-like pattern, where the firing frequency had a tendency to
75 oscillate back and forth between two discrete values (Figure 1C).

76 **2.2 DCC switching rate affects the apparent cell conductance**

77 The first effect outlined above, namely the increase in cell conductance at low DCC
78 rate, is fairly straightforward to explain. By design, in DCC mode, the amplifier
79 injects a short pulse of current, then stops the injection to allow the voltage drop
80 through the electrode to vanish before the membrane potential is sampled. How-
81 ever, during that time of no current injection, the membrane potential will also de-
82 cay. The technique only works if the electrode time constant (adjusted to be as
83 fast as possible using the capacitance compensation circuit of the amplifier) is much
84 faster than the membrane time constant. In these conditions, the DCC frequency
85 can be set high enough that the membrane potential has barely decayed by the time
86 the voltage is sampled, and the membrane potential recorded in DCC mode is very
87 close to the membrane potential that would be recorded with a perfectly balanced
88 bridge (Figure 2B). If the DCC rate is too low, however, then the membrane potential
89 has time to decay in between the end of the current pulse and the sampling time
90 (Figure 2A). Consequently, the membrane potential recorded in DCC mode is lower

91 than it would be when recorded in bridge mode. Since the current intensity ap-
92 plied by the amplifier is the same in all cases, an underestimation of the membrane
93 potential produces an apparent increase of the cell conductance at low DCC rates.
94 Conversely, if the DCC rate is too high, then the IR drop through the electrode does
95 not have time to vanish by the time the potential is sampled (Figure 2C). Therefore
96 the value of the membrane potential of the cell is contaminated by a fraction of the
97 IR drop through the electrode, leading to an overestimate of the potential, and thus
98 an apparent decrease in cell conductance (Figure 2C).

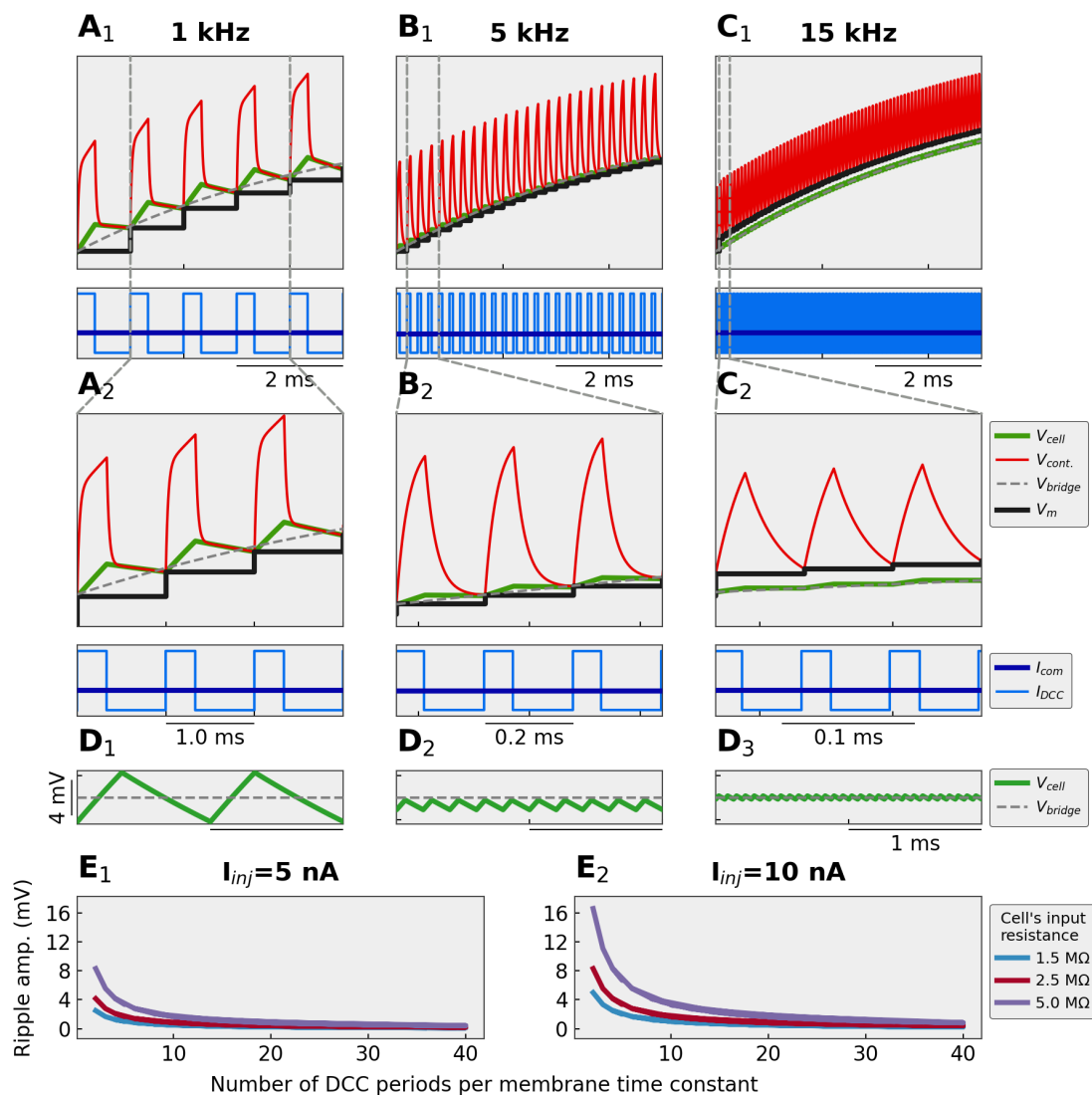
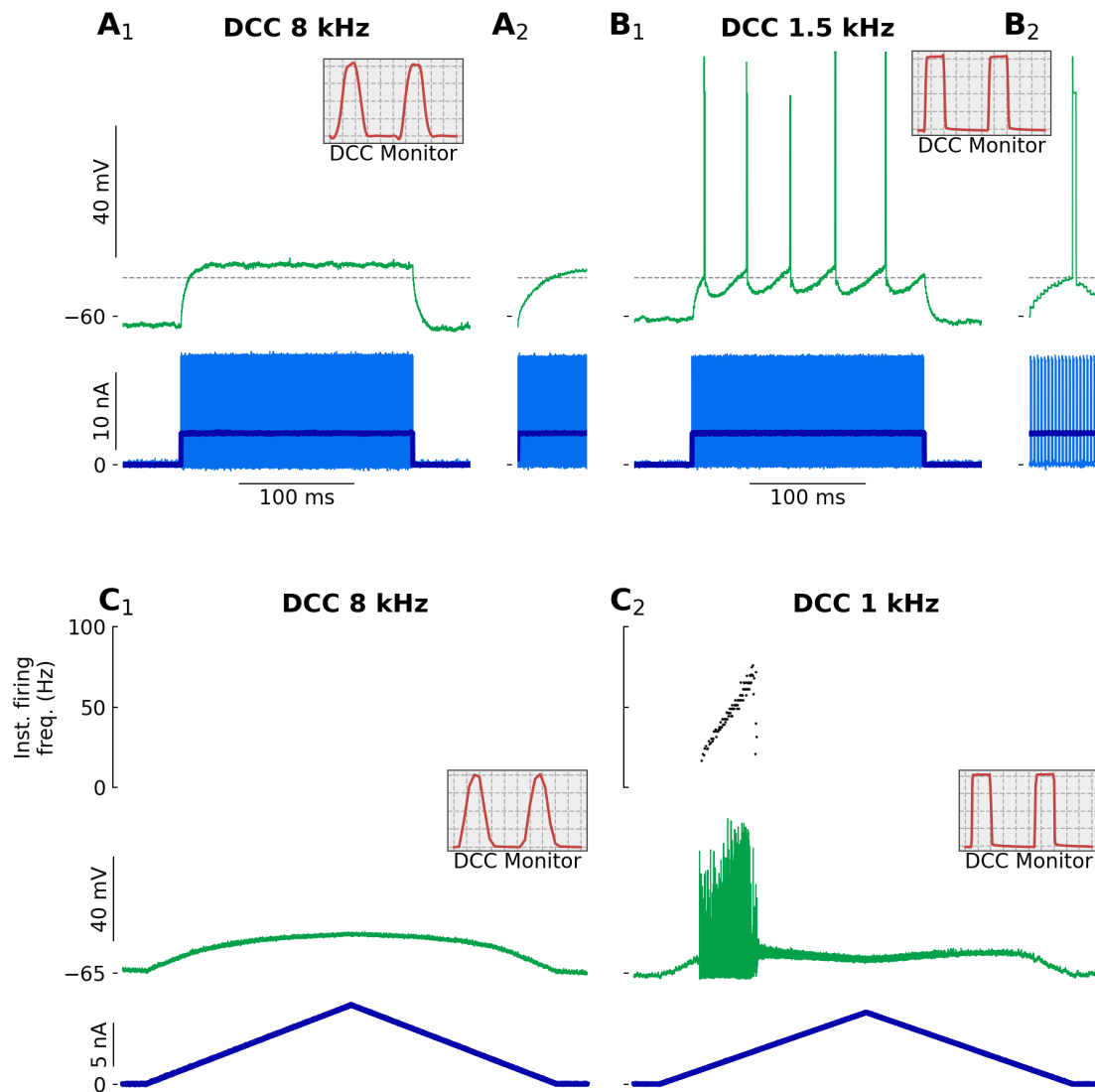


Figure 2 (previous page). Effect of DCC rate on the recording of the membrane potential. Numerical simulations showing the response of a neuron to a square pulse of current. The simulated cell had a resistance of $5\text{ M}\Omega$ and a time constant of 5 ms . The electrode had a resistance of $1\text{ M}\Omega$ and an effective time constant $200\times$ faster than the membrane time constant. **A.** recording with a DCC rate of 1 kHz (5 cycles per time constant). The arrowheads point to sharp oscillations in the membrane potential. **B.** recording with a DCC rate of 5 kHz (25 cycles per time constant). **C.** recording with a DCC rate of 15 kHz (75 cycles per time constant). **D.** Traces showing the steady-state amplitude of the membrane potential ripples in a cell with an input resistance of $2.5\text{ M}\Omega$, time constant 3 ms , and injected current 10 nA when recorded in DCC mode at 1 kHz (D_1), 5 kHz (D_2), and 15 kHz (D_3). **E.** Plots showing the amplitude of the ripples as a function of the normalized DCC frequency (number of DCC cycles per membrane time constant). The response was measured in steady-state for two current intensities that are routinely reached during our recordings in mouse spinal motoneurons ($5\text{ nA } E_1$, and $10\text{ nA } E_2$) and for three values of the cell's input resistance (which correspond to typical values for FF $1.5\text{ M}\Omega$, FR $2.5\text{ M}\Omega$, and S motoneurons $5\text{ M}\Omega$). V_{bridge} : response of the cells to the continuous current as would be observed in an ideal situation where the electrode resistance was perfectly compensated for by the bridge circuit. $V_{cont.}$: continuous voltage recorded at the tip of the electrode that includes the voltage drop through the electrode and the cell membrane. V_m : output of the amplifier, which is the value of $V_{cont.}$ sampled at the end of each DCC period (diamonds) and stored in a sample-and-hold circuit. V_{cell} : calculated membrane potential excluding the contribution of the electrode resistance. I_{com} : stationary current that the experimenter is imposing to the cell. I_{DCC} : actual current injected in the cell. That current is $3\times$ the amplitude of I_{com} , but injected for only $1/3$ of the time.

99 **2.3 Low DCC switching rates can drive firing**

100 The effect of the DCC on the F-I curves is more subtle. Although the amount of charge
101 transferred to the cell is the same in DCC and in Bridge, the frequency content of
102 the input is not the same. By chopping the current injection in short pulses, the DCC
103 introduces harmonics of the DCC frequency in the input signal (Brette and Destexhe,
104 2012). This is particularly problematic at low DCC rates, where the membrane po-
105 tential has time to increase during the pulse injection and then has time to decay
106 substantially in between each current injection, creating "ripples" in the membrane
107 potential (Finkel and Redman, 1984) (Figure 2). Note that although these ripples
108 are present in the membrane potential, they are hidden to the experimenter by the
109 DCC sample-and-hold circuit, which samples the potential at the end of the DCC
110 period and holds the amplifier output constant at that value until the next sampling
111 time. We therefore relied on numerical simulations to investigate these ripples. Fig-
112 ures 2D₁₋₃ show examples of steady-state ripples experienced by a model of a typical
113 FR motoneuron when injected with 10 nA of current in DCC mode at 1, 3, and 8 kHz.
114 Because the actual current injected during the DCC pulses are 3× the intensity of
115 the desired current, these ripples can be quite large. The amplitude of these rip-
116 ples depends not only on the DCC frequency, but also on the time constant of the
117 membrane (as well as, of course, the resistance of the cell and the intensity of the
118 injected current). We therefore normalized the DCC rate by the membrane time
119 constant (number of DCC periods per time constant). Figures 2E₁₋₂ show how the
120 amplitudes of the ripples change with DCC rate for three values of the motoneu-
121 ron input resistance (1.5 MΩ, 2.5 MΩ, and 5 MΩ, corresponding to typical values
122 for, respectively, FF, FR and S mouse motoneurons (Martínez-Silva et al., 2018)),
123 and two values of injected current (5 and 10 nA, which are values that are typically
124 reached when injecting ramps of current in mouse motoneurons). These figures
125 show that the amplitudes of the ripples increase steeply when the DCC switching



126 rate is decreased, particularly under 10 DCC periods per time constant. However,
127 even for reasonable rate (10–20 DCC periods per time constant), the ripples can
128 reach several millivolts in amplitude.

129 As discussed above, using a low DCC frequency becomes equivalent to injecting a
130 series of short pulses of current. This kind of stimulus is highly efficient to trigger
131 motoneuron firing, much more than a continuous current injection (Delestrée et al.,
132 2014; Martínez-Silva et al., 2018). Figure 3A shows the response of a motoneuron
133 to the same 200 ms-long 4 nA pulse of current, recorded in DCC mode with a rate of

Figure 3 (previous page). Spurious firing elicited by low DCC rates. A–B. Recording from a Triceps Surae motoneuron ($R_{in}=3.5\text{ M}\Omega$; $\tau_m=4.9\text{ ms}$) following the injection of a 200 ms-long 4 nA pulse of current. A. Response recorded with a DCC rate of 8 kHz. The inset in A2 is a zoom over the first 15 ms following the onset of the pulse. B. Response recorded with a DCC rate of 1.5 kHz. The inset in B2 is a zoom over the first 15 ms following the onset of the pulse. The horizontal dashed line represents the voltage threshold measured at the foot of the first spike of the response in B. The grey boxes in A and B represent the monitoring traces used to check the settling of the electrode, recorded at the top of the ramp. Time bases from left to right: 25 μs (C_1), and 133 μs (C_2) per division. **C.** Response of a Triceps Surae motoneuron ($R_{in}=5.0\text{ M}\Omega$; $\tau_m=4.7\text{ ms}$) to the injection of a triangular ramp of current (1 nA/s) with a DCC rate of 8 kHz (C_1) or 1 kHz (C_2). The bottom trace is the injected current, the middle trace is the membrane potential and the top graph is the instantaneous firing frequency. The inserts represent the monitoring traces used to check the settling of the electrode, recorded at the top of the ramp. Time bases from left to right: 25 μs (C_1), and 200 μs (C_2) per division.

134 1.5 kHz and 8 kHz. With a DCC at 8 kHz, this pulse of current was not able to reach
135 firing threshold (Figure 3A₁). At lower DCC rate, however, although the amount
136 of current injected is the same, the motoneuron responded with a strong repetitive
137 discharge (Figure 3B₁). Interestingly, the voltage threshold for the first spike was
138 below the steady-stage potential reached with a DCC of 8 kHz (compare dashed
139 lines in Figure 3A₂ and B₂), suggesting that the appearance of firing at 1.5 kHz
140 was not due to a larger depolarisation (in fact, the depolarisation is smaller, see
141 above), but rather due to the strong sensibility of the cell to transient currents and
142 ripples in their membrane potential. In the extreme case, a low DCC rate can turn
143 a motoneuron that was not able to fire repetitively in response to a stationary input
144 (Figure 3C₁) into a motoneuron that elicits a bout of repetitive firing to the same
145 ramp (Figure 3C₂). Observation of the DCC monitoring trace on the oscilloscope
146 (inserts in Figure 3C) confirms that the inability to fire repetitively was not due to the
147 electrode becoming blocked. The IR drop through the electrode had fully vanished
148 by the end of the DCC period, and the membrane potential was therefore accurately
149 measured. With a DCC at 1 kHz, however, the DCC period was so long that not
150 only the IR drop through the electrode had time to settle to zero, the membrane
151 potential also rose and decayed during each DCC period. The net effect is a series

152 of large amplitude membrane potential ripples (which are hidden by the sample-
153 and-hold circuit of the amplifier), superimposed to the slow depolarization of the
154 quasi-stationary ramp. The spiking observed in these conditions is caused by this
155 mixed dynamic and stationary input, rather than a response to the stationary input
156 alone.

157 As hinted above (Figure 1), this effect can profoundly affect the shape of the frequency-
158 current relationship of a motoneuron in response to a triangular ramp of current,
159 but which F-I curve is the most physiological? Figure 4 illustrates the response of
160 a motoneuron to a series of ramps of current recorded in DCC mode at various fre-
161 quencies. Because this motoneuron had a fairly low rheobase and did not require a
162 lot of current to fire, we were able to record the response in Bridge mode as well.
163 That response is free of artefacts due to DCC switching, and we will therefore use
164 it as the control firing for this cell. As can be seen, the response recorded in DCC
165 mode at 8 kHz is almost indistinguishable from the one recorded in Bridge mode
166 (Figure 4B). However, when the DCC frequency is too low, the curve is shifted to the
167 left (lower recruitment current), the slope is steeper, and a distinctive “step” pattern
168 appears on the instantaneous frequency.

169 This effect is seen consistently across motoneurons. Figure 5A–D shows how the
170 current intensity required to start firing (onset current), the current intensity when
171 the cell stopped firing (offset current), the slope of the ascending phase of the F-I
172 relationship (F-I gain), and the voltage threshold measured on the first spike of the
173 ramp vary with DCC frequency. It is clearly apparent that values measured at low
174 DCC rates are usually very different than the ones measured at higher rates, and that
175 the values tend to converge to a stable value when the DCC rate is increased past
176 a critical point. Moreover, in the motoneurons in which we were able to record the
177 response in Bridge mode (Figure 4), the values measured with the highest DCC rates
178 agree well with the values recorded in bridge mode (diamonds), with the exception
179 of the voltage threshold, which cannot be measured accurately in bridge mode since

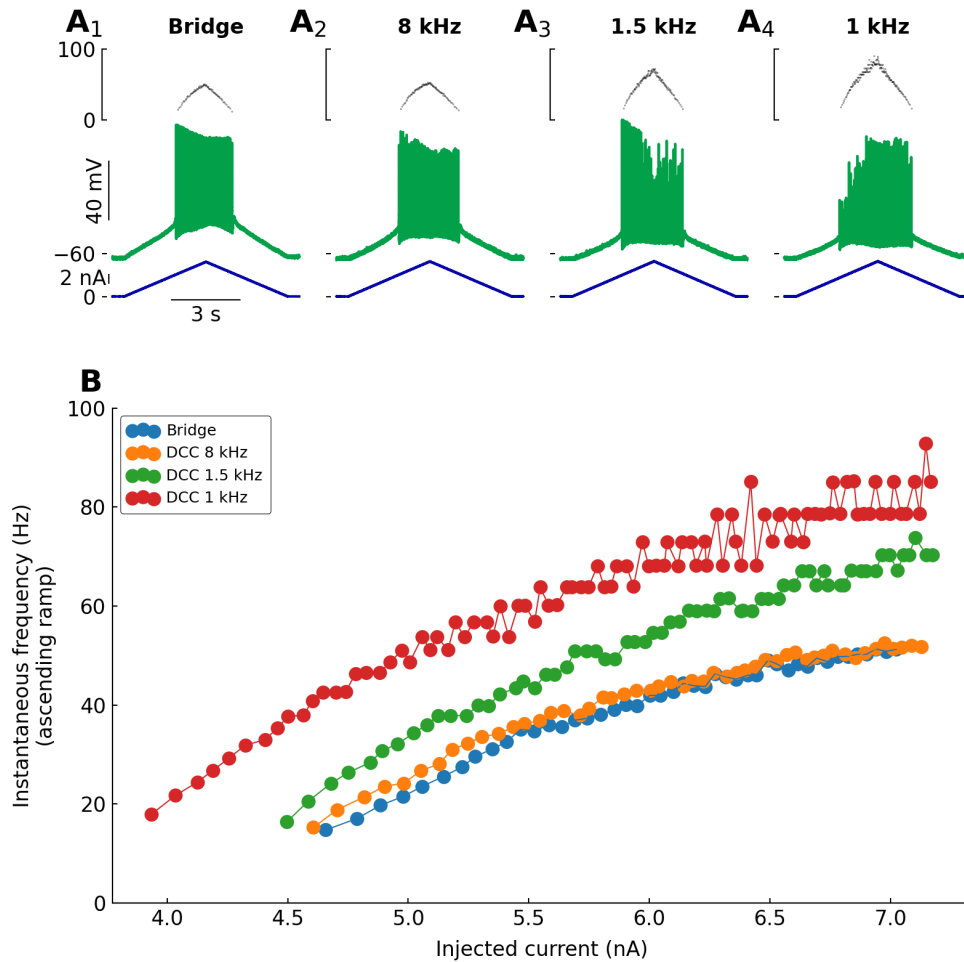


Figure 4. Effect of DCC switching rate on the response to a ramp of current. **A.** Same motoneuron as Figure 3A–B, injected with a triangular ramp of current (2 nA/s) and recorded either in Bridge mode (A₁), or in DCC mode at various switching rates (A₂: 8 kHz, A₃: 1.5 kHz, A₄: 1 kHz). **B.** The instantaneous firing frequency on the ascending ramp is plotted against the current intensity.

180 one cannot completely get rid of the IR drop through the electrode in this mode.
181 Because the effect of the DCC rate depends on the time constant of the cell, the
182 plateau value is reached for different DCC rates in each motoneuron. We therefore
183 normalized the DCC rate in each cell by the membrane time constant (number of
184 DCC periods per time constant), and we normalized the measured value to the value
185 estimated at the highest DCC rate (Figure 5E–F). These curves clearly show that
186 all measurements converge towards the same value as the DCC switching rate is
187 increased. However, these curves demonstrate that the rate of 10 cycles per time
188 constant recommended in the Axoclamp manual is not high enough. Rates of at least
189 15–20 cycles per time constant are necessary to get good estimates of the value of
190 most of these measurements.

191 **2.4 Low DCC rates entrain firing at discrete intervals**

192 As shown above, using a low DCC switching rate not only leads to cells firing at
193 lower current, but also at higher frequencies. For instance, in the cell exemplified
194 in Figure 6A, lowering the DCC rate from 8 to 3 kHz led to both a leftward and
195 upward shift of the F-I curve. Reducing it further to 1 kHz led to the appearance of
196 marked “plateaus” in the instantaneous firing frequency. This behavior can be repro-
197 duced in a simple integrate-and-fire model (Figure 6B). These plateaus correspond
198 to interspike intervals (ISI) that are multiples of the DCC switching period. The cell
199 no longer fires at its natural interspike interval, but instead is driven to fire on the
200 crest of the membrane potential ripples when the after-hyperpolarization from the
201 preceding spike has relaxed sufficiently for the membrane potential to come close
202 to the voltage threshold (Figure 6C). Because a significant amount of current has
203 to be injected in spinal motoneurons to reach firing threshold, the ripples can get
204 quite large (Figure 2E), which is why they can entrain firing with shorter ISI (higher
205 frequency) than what would be observed for the same current intensity in Bridge
206 mode (Figure 6C).

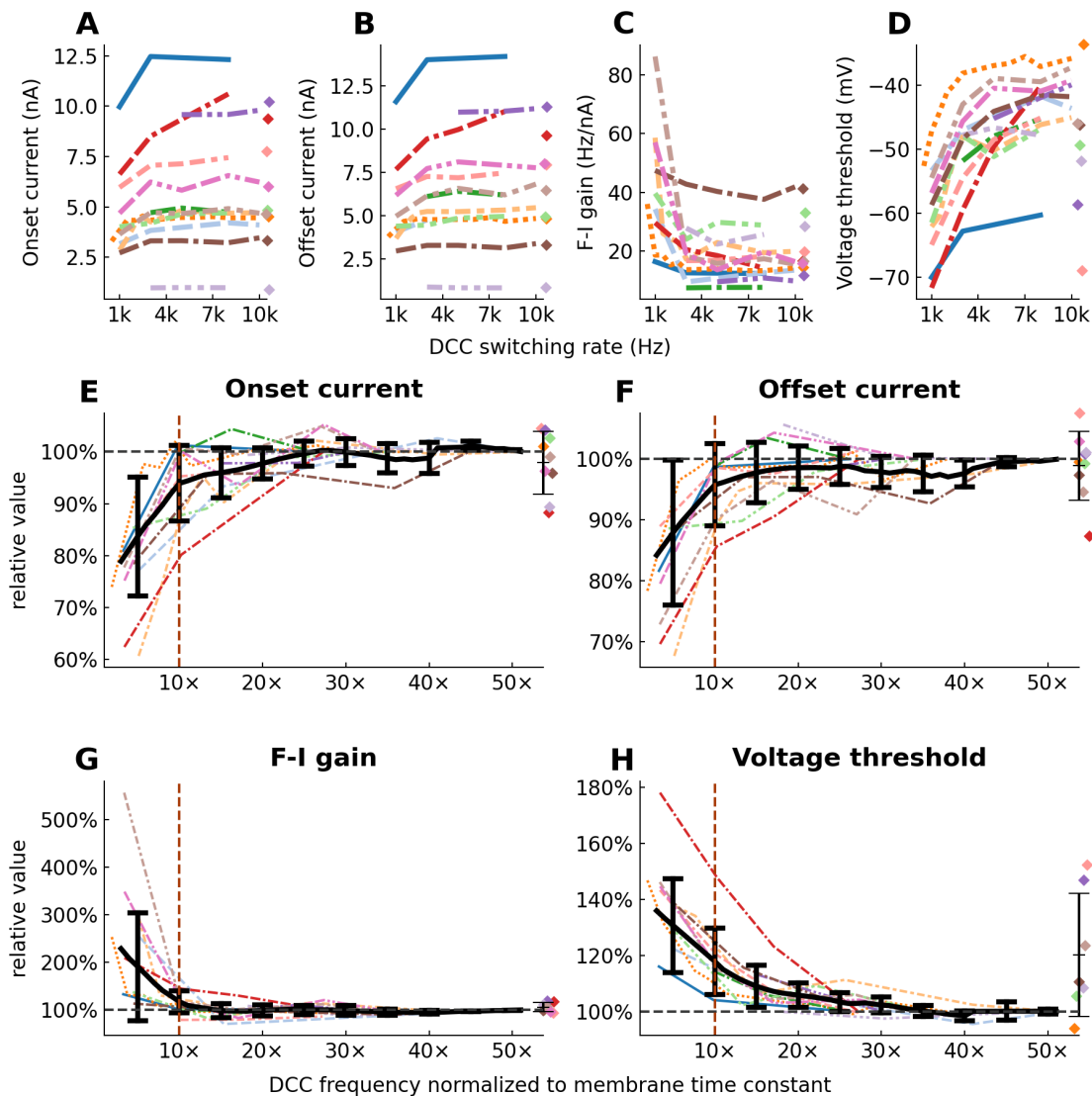


Figure 5. Relationship between parameters measured on the F-I curves and the DCC frequency used during the recording. In all panels, each line represents one motoneuron. The green dotted lines correspond to the motoneuron shown in Figure 4, and the parameters extracted from the trace recorded in bridge mode are represented by a green diamond on the right side of each plot. Onset current: current required to elicit the first spike on the ascending ramp. Offset current: current at which the firing stops on the descending ramp. F-I gain: slope of the F-I relationship measured on the ascending part of the ramp. Voltage threshold: voltage measured at the foot of the first spike elicited on the ascending ramp. **A–D.** Absolute value of each of the parameters plotted against the DCC rate used during the recording. **E–F.** Value of each of the parameters normalized to the value measured at the highest DCC rate achieved in each motoneuron (dashed horizontal line) plotted against the DCC rate normalized by the time constant of each motoneuron. The thick black trace represents the average values across motoneurons with error bars representing average \pm SD. The vertical dotted line shows the recommended minimal DCC rate of 10 cycles per membrane time constant.

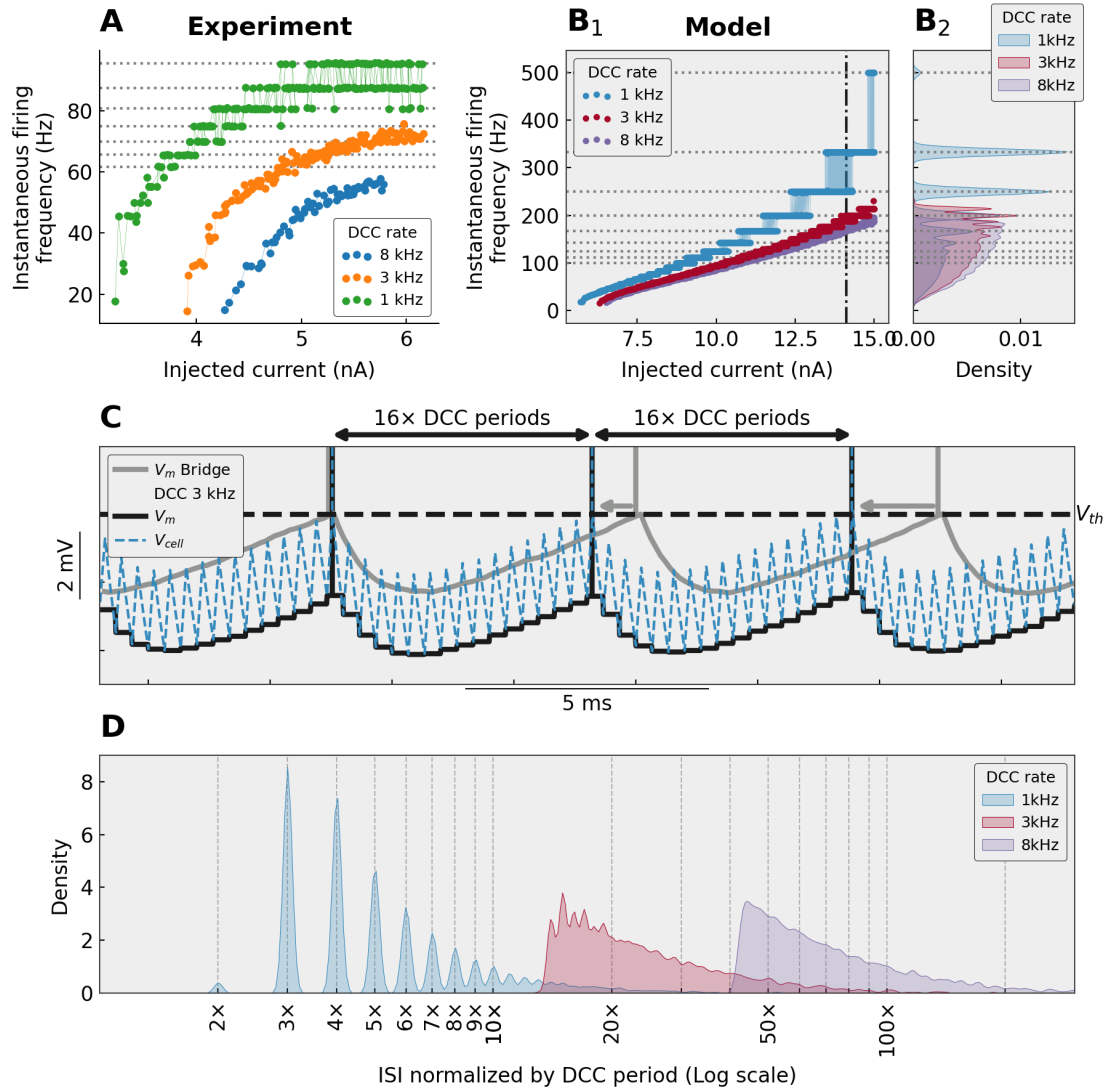


Figure 6 (previous page). Stepwise pattern is a sign of sub-optimal DCC rate **A.** F-I curves from a Triceps Surae motoneuron ($R_{in}=2.0\text{ M}\Omega$; $\tau_m=3.8\text{ ms}$), injected with a triangular ramp of current (1 nA/s) and recorded in DCC mode at three different DCC switching rates. At low DCC rates, a clear stepwise pattern is apparent, which corresponds to multiples of the switching rate (1050 Hz in this instance): 95.5 Hz (or 1 spike every 11 DCC periods), 87.5 Hz (1:12), 80.8 Hz (1:13), 75.0 Hz (1:14), 70.0 Hz (1:15), 65.6 Hz (1:16), etc. **B.** The same phenomenon can be observed in a simple integrate-and-fire motoneuron model. The model was that of a typical FF motoneuron ($R_{in}=1.5\text{ M}\Omega$; $\tau_m=2.0\text{ ms}$), injected with a 10 nA slow ramp of current (1 nA/s), and recorded in DCC mode at 8, 3, and 1 kHz. A stepwise pattern is apparent at the top of the F-I curve at 3 kHz, and is clearly present at 1 kHz (see distinct peaks in the distributions of the firing frequencies in B₂). The horizontal dotted line represent the multiples of the period of the 1 kHz switching rates. The vertical dash-dotted line represent the region zoomed in in C. **C.** Comparison of the behavior of the model recorded in bridge mode (grey line) and in DCC at 3 kHz. The black line represent the V_m output of the amplifier, while the dashed line represent the true membrane potential V_{cell} which is hidden from the experimenter by the sample-and-hold circuit. The membrane potential ripples created by the DCC shorten the interspike intervals (grey arrows) and entrain the firing with interspike intervals that are multiples of the DCC period. **D.** Distribution of the interspike intervals obtained in DCC mode at 1, 3, and 8 kHz. The intervals have been normalized by the DCC period (1 ms, 0.33 ms, and 0.125 ms, respectively) and plotted on a logarithmic scale. At 1 kHz, the interspike intervals are concentrated at multiples of the DCC period.

207 The plateaus are characteristic of recordings with sub-optimal DCC rates for two
208 reasons. Firstly, the amplitude of the ripples decreases with increasing DCC rates
209 (Figure 2D), therefore they are less likely to "stick out" from the noise and entrain
210 firing. Secondly, the plateaus are only apparent when the firing rate of the cell ap-
211 proaches the fundamental frequency of the DCC. Consider the behavior of the model
212 in Figure 6B with a sub-optimal DCC frequency of 1 kHz (2 DCC cycles per mem-
213 brane time constant). Firing starts at a low frequency then increases linearly without
214 visible plateaus until the frequency reaches 50–60 Hz where they are barely visible
215 but become much more prominent above 100 Hz. In this case, the plateaus appear
216 when the firing is entrained at about one spike every 10 DCC cycles, and become
217 more and more prominent as the firing frequency gets closer to the DCC rate: the
218 distribution of the interspike intervals become more and more peaked at multiples
219 of the DCC period (Figure 6D). Below 20 DCC cycles, even if entrainment happens,
220 the difference between being entrained at one spike per e.g. 30 or 31 DCC cycles

221 is drowned in the variability of the discharge. Therefore, at higher DCC frequen-
222 cies, not only do the ripples become smaller, but the range of firing frequencies over
223 which plateaus are apparent is pushed higher and higher. For instance, in the model
224 (Figure 6B), even though the firing frequencies largely overlap with DCC rates of 1,
225 3, and 8 kHz, firing rates reach one spike every 15 DCC cycles at 3 kHz (plateaus
226 are clearly visible, Figures 6B₁₋₂,D), but barely reach one spike every 45 DCC cycles
227 at 8 kHz (Figure 6D), and no plateaus are visible (Figure 6B).

228 Interestingly, this entrainment effect at sub-optimal DCC rates is able to induce an
229 apparent increase in the slope in the F-I relationship, particularly when the firing
230 frequency reaches high values. This phenomenon is illustrated Figure 7 where a
231 motoneuron was stimulated with a high-amplitude (13 nA), fast ramp of current
232 (5 nA/s), expressly for the purpose of pushing the motoneuron to high firing fre-
233 quencies. At DCC rates 5 and 8 kHz, the resulting F-I curves are almost indistin-
234 guishable, with a first range of current where the frequency was increasing steeply,
235 followed by a region where the frequency increased at a smaller rate (~ 7 Hz/nA,
236 dashed grey line). When recorded with a DCC rate of 3 kHz, the F-I curve was shifted
237 upward to higher firing frequencies. The slope of the initial linear phase was slightly
238 higher (~ 10 Hz/nA, black dashed line) than with higher DCC rates. When the fir-
239 ing reached frequencies above 150 Hz, a clear step-wise pattern became apparent
240 and the F-I curve became steeper (~ 20 Hz/nA), creating the illusion of a “secondary
241 range”, even though this change of slope is not present in the data recorded with
242 higher DCC rates for the same current intensities. This effect is due to the fact that,
243 when the DCC frequency is sub-optimal, ISI are entrained at multiple of the DCC pe-
244 riod (Figure 6D). As the injected current and the frequency increases, the ISI shorten
245 linearly by discrete steps (e.g. 1 spike every 10 DCC periods, then 1 spike every 9
246 DCC periods, then every 8 periods, etc...). Since the frequency is the inverse of the
247 ISI, the firing frequency is increasing very steeply as it jumps from plateau to plateau
248 (Figure 7B).

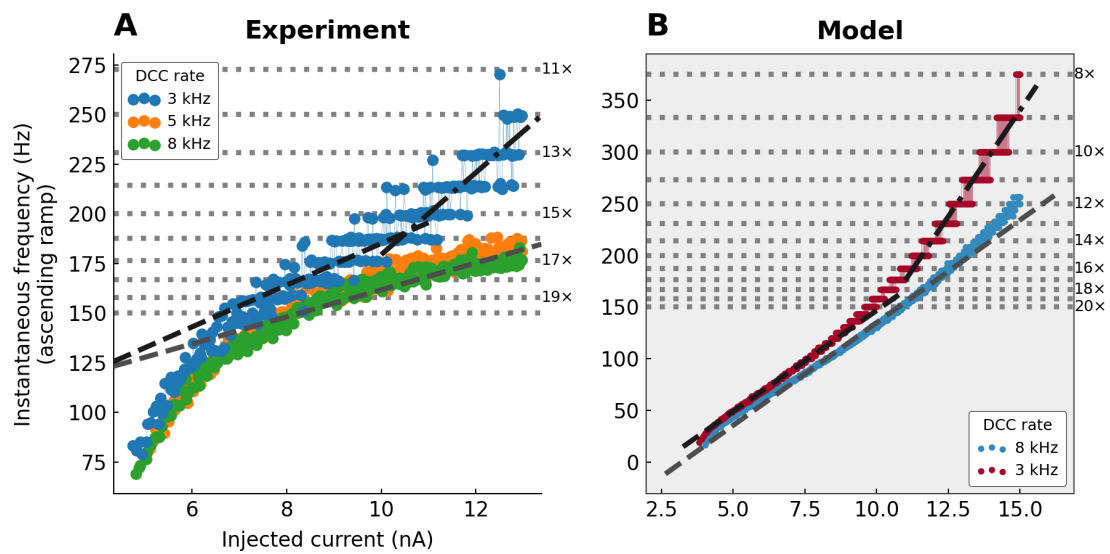


Figure 7. Apparent change of slope in the F-I curve associated with discrete firing intervals. **A.** F-I curves from a Triceps Surae motoneuron ($R_{in}=4.1\text{ M}\Omega$; $\tau_m=3.3\text{ ms}$). A fast triangular ramp of current (amplitude 13 nA, 5 nA/s) was injected to drive the firing at high frequency. The instantaneous firing frequency is plotted against the ascending ramp current intensity. Grey dashed line: slope of the F-I curve recorded at 8 kHz measured in the second half of the curve. Black dashed line: slope of the F-I curve recorded at 3 kHz, measured over the range 7–10 nA. Black dash-dotted line: slope of the F-I curve recorded at 3 kHz, measured over the range 11–13 nA. Horizontal dotted lines: subharmonics of the 3 kHz DCC rate as indicated on the right of the plot. **B.** F-I curves obtained in a model with $R_{in}=2.5\text{ M}\Omega$ and $\tau_m=2.0\text{ ms}$. Compared to the F-I curve obtained with a high DCC rate of 8 kHz, which is mostly linear (grey dashed line), the F-I curve obtained with a DCC rate of 3 kHz clearly changes slope at $\sim 10\text{ nA}$, from a slope roughly equal to the one measured at 8 kHz to a much steeper slope.

249 3 Discussion

250 This paper describes the effect of an incorrectly set DCC rate on the firing properties
251 of spinal motoneurons. Although a low DCC rate lead to an underestimation of the
252 membrane potential, and therefore an apparent increase in cell conductance, we
253 show that, paradoxically, it has the potential to artificially drive the cells to fire a
254 lower currents and higher frequency, as well as to profoundly alter the shape of the
255 F-I relationship.

256 Although there are no theoretical upper limits to the DCC cycling rate, in practice,
257 one is limited by the time constant of the electrode and the capacitance neutraliza-
258 tion circuit of the amplifier. Indeed, if the voltage drop through the micro-electrode

259 has not relaxed to zero at the sampling time, the membrane potential recorded is
260 contaminated by an unknown fraction of the electrode resistance. More importantly,
261 there is a lower limit to the DCC rate. For instance, the Axoclamp manual states that
262 the rate must be such that “that there are ten or more cycles per membrane time
263 constant. This enables the membrane capacitance to smooth the membrane voltage
264 response to the current pulses” (Axon Instruments, 2003). There must be a theo-
265 retical “optimal” DCC rate in between those two extremes, but finding that optimal
266 frequency is difficult in practice (Brette and Destexhe, 2012). Instead, electrophysi-
267 ologists observe the continuous electrode potential on an oscilloscope synchronized
268 to the DCC sampling clock. The goal is to adjust the electrode capacitance com-
269 pensation circuit and the DCC switching rate to reach the highest DCC rate possible
270 while ensuring that the response shown on the oscilloscope appears flat, that is to
271 say, that the contribution of the electrode resistance to the recorded potential has
272 dropped down to zero before the time when the voltage is sampled.

273 While it is fairly straightforward to check that the DCC rate is not too high based
274 on the settling time of the electrode observed on the monitoring oscilloscope, it
275 is difficult to know whether the DCC rate is fast enough to not distort the firing
276 of the cell. Our experiments show that the minimum value of ten cycles per time
277 constant commonly recommended is too conservative. We show that DCC rates
278 of at least 15–20 cycles per time constant are required to produce measurements
279 that match the ones obtained in bridge mode. More importantly, above 15 cycles
280 per time constants, the measurements become largely insensitive to the exact DCC
281 rates, and therefore small differences in DCC rates (relative to the cell’s membrane
282 time constant) between cells should not impact their respective firing behavior.

283 Compared to the Bridge mode, the DCC transforms the input signal from a contin-
284 uous variation in current intensity to a discontinuous situation, where the current
285 can only be injected as short square pulses. This difference is almost negligible
286 when the DCC rate is high enough for the membrane potential to barely move dur-

287 ing the current injection and the subsequent inter-pulse interval. However, at lower
288 DCC frequencies, the membrane potential exhibit substantial ripples (Figure 2). It
289 should be noted that, although these ripples are present across the membrane of the
290 recorded cell, they are hidden from the experimenter since the output of the am-
291 plifier is held constant at the level of the previous sampled value during that time
292 (thick black line in Figure 2A). When considering slow ramps of current, like in the
293 present study, decreasing the DCC rate from a high frequency to a lower frequency
294 therefore amounts to transitioning from a situation where the membrane potential
295 is increasing slowly, to a situation where sharp voltage ripples are superimposed
296 to a slow depolarisation. These ripples are particularly efficient at triggering ac-
297 tion potentials, particularly when the membrane potential is very close to the firing
298 threshold. Moreover, it has been shown in many neuronal types that the faster the
299 rate of rise of the membrane potential, the more reliably a spike will be generated
300 (Mainen and Sejnowski, 1995; Azouz and Gray, 2000; Agrawal et al., 2001; Kuo et
301 al., 2006). This high dynamic sensitivity explains why motoneurons recorded with
302 a low DCC rate fire at lower current despite reaching lower membrane potentials. In
303 addition, it also accounts for the fact that, at low DCC rate, firing becomes entrained
304 by the DCC. Membrane potential ripples trigger a spike more reliably than the slow
305 decay of the after-hyperpolarization that follows the preceding spike. The interspike
306 intervals thereby can only take values that are multiples of the DCC period, leading
307 to the characteristic step-like pattern observed in the F-I curves.

308 Interestingly, motoneurons have a natural regime of firing where a similar step-like
309 pattern can be observed in response to very slow current ramps. We have shown
310 previously that, for a narrow range of current motoneurons exhibit subthreshold os-
311 cillations which alternate with spikes, producing a very irregular firing. This regime,
312 called mixed-mode oscillations (MMOs) is responsible for the sub-primary firing
313 range. These oscillations naturally emerge from a sodium to potassium ratio too
314 weak to generate full blown spikes with high reliability; but when a spike is finally

315 generated, it is locked to one of the oscillations (Iglesias et al., 2011). However,
316 since the frequency of the MMOs is much lower (100–125 Hz, Manuel et al., 2009;
317 Iglesias et al., 2011), and disappear when the firing reaches past the transition fre-
318 quency between the sub-primary and the primary range (Iglesias et al., 2011), the
319 resulting plateaus in the F-I curve are only apparent over the sub-primary range.

320 As shown above, the distortions caused by the DCC rate are primarily dependent
321 on the time constant of the membrane. In spinal motoneurons, there is a strong
322 relationship between membrane time constant and cell size, such that small, Slow-
323 type (S) motoneurons have a longer membrane time constant than the larger, fast
324 fatigable (FF) motoneurons (Gustafsson and Pinter, 1984). Consequently, FF mo-
325 toneurons require an even higher DCC frequency than S motoneurons to obtain
326 accurate measurements of their excitability. We have previously shown that mouse
327 motoneurons have shorter time constants than cats (Manuel et al., 2009). Mouse
328 FF motoneurons have an average time constant of 2.1 ± 0.2 ms, FR motoneurons
329 2.9 ± 0.9 ms, while S motoneurons have a time constant of 4.0 ± 0.7 ms (unpublished
330 data from Martínez-Silva et al., 2018). Based on our present results, which show
331 that a DCC frequency corresponding to at least 15 cycles per time constant is re-
332 quired to measure the excitability of the cell, FF motoneurons should be recorded
333 with a DCC at at least 7 kHz, while S motoneurons can accommodate DCC frequen-
334 cies as low as 3.75 kHz. Because of their size, FF motoneurons are also the cells
335 that require the most current to fire. The impedance of the electrode is often highly
336 non-linear, and both the resistance and the time constant of the electrode have a
337 tendency to increase with the amount of injected current. Consequently, It is often
338 difficult to record the firing of these cells at high DCC rates. Instead, it would be
339 tempting, particularly in these cells, to lower the DCC rate to obtain proper settling
340 of the electrode's IR drop, but, as we demonstrate here, doing so would lead to an
341 overestimation of the cell's firing and excitability parameters. Moreover, in a mouse
342 model of Amyotrophic Lateral Sclerosis, we have shown that the largest motoneu-

343 rons become incapable of firing repetitively in response to a slow ramp of current
344 (Martínez-Silva et al., 2018). Given the membrane time constants of these cells, it
345 was essential to perform these recordings at high DCC rates (all of our recordings
346 were performed in DCC at 7–9 kHz), since lower DCC rates have the potential to dis-
347 tort the firing of these cells, and even mistakenly transform a non-repetitively-firing
348 motoneuron into a repetitively-firing motoneuron (Jensen et al., 2020).

349 **4 Conclusions**

350 In conclusion, the effects of inappropriate DCC switching rates on the apparent con-
351 ductance of the cells is well known. However, the effect on the firing characteristics
352 of the neurons are not often discussed. We show here that choosing a sub-optimal
353 DCC rate may dramatically distort parameters that are classically used to define the
354 “excitability” of neurons: lower current onset, lower current offset, higher firing
355 frequencies, higher F-I gains, and even the appearance of an artifactual “secondary
356 range” of firing. Low DCC rates can therefore lead to a misrepresentation of neu-
357 ronal excitability.

358 **5 Methods**

359 **5.1 Animals**

360 All procedures were approved by the Paris Descartes University ethics committee
361 (CEEA34; authorization number 2018052100307589) and followed the European
362 Directives (86/609/CEE and 2010-63-UE) and the French legislation on the protec-
363 tion of animals used for scientific purposes. Three C57BL/6 and four B6SJL male
364 mice (weight 25–31 g; 27.9 ± 2.3 g; $N=7$) were used in this study.

365 5.2 Experimental procedure

366 The surgical procedures have been described previously (Manuel et al., 2009; Manuel
367 and Heckman, 2012). Briefly, atropine (0.20 mg/kg; Aguetant) and methylpred-
368 nisolone (0.05 mg; Solu-Medrol; Pfizer) were given subcutaneously at the onset of
369 experiment, to prevent salivation and oedema, respectively. Fifteen minutes later,
370 anaesthesia was induced with an intraperitoneal injection of sodium pentobarbitone
371 (70 mg/kg; Pentobarbital; Sanofi-Aventis). A tracheotomy was performed, and the
372 mouse was artificially ventilated with pure oxygen (SAR-830/AP ventilator; CWE).
373 The end tidal CO₂ level was maintained around 4% (MicroCapstar; CWE). The heart
374 rate was monitored (CT-1000; CWE), and the central temperature was kept at 37°C
375 using an infrared heating lamp and an electric blanket. A catheter was introduced in
376 the external jugular vein, allowing us to supplement the anaesthesia whenever nec-
377 essary (usually every 20–30 min) by intravenous injections (sodium pentobarbitone,
378 6 mg/kg). The adequacy of anaesthesia was assessed on lack of noxious reflexes and
379 on the stability of the heart rate (usually 400–500 bpm) and end-tidal PCO₂. A slow
380 intravenous infusion (50 µL/h) of a 4% glucose solution containing NaHCO₃ (1%)
381 and gelatine (14%; Plasmagel; Roger Bellon) helped maintain the physiological pa-
382 rameters. The animal was paralyzed after the surgery with atracurium besylate
383 (Kalceks; initial bolus was 0.1 mg, followed by a continuous infusion 0.01 mg/h).
384 Additional doses of anaesthetics were then provided at the same frequency as be-
385 fore the paralysis, and adequacy of anaesthesia was assessed on the stability of the
386 heart rate and of PCO₂. The vertebral column was immobilized with two pairs of
387 horizontal bars (Cunningham Spinal Adaptor; Stoelting) applied on the Th12 and
388 L2 vertebral bodies, and the L3–L4 spinal segments were exposed by a laminectomy
389 at the Th13–L1 level. The Triceps Surae nerve (containing the branches innervating
390 the Medial Gastrocnemius, the Lateral Gastrocnemius and the Soleus) was dissected
391 and placed on a bipolar electrode for stimulation. All other branches of the sciatic

392 nerve were cut. The tissues in the hindlimb and the spinal cord were covered with
393 pools of mineral oil. At the end of the experiments, animals were killed with a lethal
394 intravenous injection of pentobarbitone (200 mg/kg).

395 **5.3 Electrophysiological recordings**

396 The motoneurons were impaled with micro-pipettes (tip diameter, 1.0–1.5 μm) filled
397 with either 3 M KCl or 3 M K-Acetate (resistance $23.1 \pm 5.9 \text{ M}\Omega$ [16.0–33.0 $\text{M}\Omega$],
398 $N=13$). Recordings were performed using an Axoclamp 2B amplifier (Molecular
399 Devices) connected to a Power1401 interface and using the Spike2 software (CED).
400 The current (I_m) and voltage output ($10V_m$) of the amplifier were low-pass filtered
401 at 10 kHz and sampled at 20 kHz. When recorded, the continuous output I_1 and
402 V_1 , and the DCC monitor output were sampled at 100 kHz. After impalement, iden-
403 tification of motoneurons rested on the observation of antidromic action potentials
404 in response to the electrical stimulation of their axon in the triceps nerve. All care
405 was taken to compensate for the microelectrode resistance and capacitance. No
406 bias current was used to maintain the resting membrane potential. All cells kept
407 for analysis had a resting membrane potential more hyperpolarized than -50 mV
408 and an overshooting antidromic spike. As fully described previously (Manuel et
409 al., 2009), the input resistance was measured using the peak response of a series
410 of small-amplitude square current pulses (-3 to $+3 \text{ nA}$, 500 ms) recorded in DCC
411 mode (8 kHz). The membrane time constant was measured on the relaxation of the
412 membrane potential after injection of small hyperpolarizing current pulses (-5 nA ,
413 1 ms), recorded in Bridge mode. Slow triangular ramps of current were injected
414 in DCC mode (switching rates as described in the text). A recovery period of at
415 least 30s was left in between each repetition. Using an offline automated script, the
416 timing of each spike was recorded along with the current intensity at that time to
417 construct the F-I curve. At switching rates $<3 \text{ kHz}$, the DCC voltage trace was often
418 too distorted to identify spikes reliably. In these cases, the continuous voltage trace

419 was carefully scanned manually to identify spikes. The onset current was defined
420 as the value of the injected current at which the first action potential was generated
421 one the ascending phase of the ramp. The offset current was the current intensity
422 corresponding to the last action potential on the descending phase of the ramp. The
423 F-I gain was measured as the slope of the F-I relationship in the most linear part
424 of the ascending phase of the ramp (“primary range”). The voltage threshold was
425 measured at the point when the slope of the membrane voltage crosses 10 mV/s
426 (Sekerli et al., 2004) just prior to the first spike of the ascending phase of the ramp.

427 **5.4 Numerical simulations**

428 Numerical simulations were conducted using the Brian2 simulator (v.2.4.1) in Python
429 v.3.8 and using the SciPy ecosystem (v.1.5.0; Virtanen et al., 2020).

430 For investigating membrane potential ripples (Figure 2), both the cell and the elec-
431 trodes are modeled as passive RC circuits with equations:

$$C * \frac{dV}{dt} = G * (V_0 - V) + I_{inj} \quad (1)$$
$$C = G * \tau$$

432 For the cell, G_{in} was set to 0.2 μS and $\tau_m=5$ ms. To model the IR drop through the
433 electrode, parameters were chosen so that the electrode was 200 \times faster than the
434 membrane time constant ($\tau_e=\tau_m/200=25$ μs). The equation above was solved with
435 $G_e=1$ μS . Although not quite realistic, this value was chosen so that the response of
436 the electrode would not completely dominate the graphs in Figure 2. Note however
437 that the value of the resistance of the electrode is only relevant at high DCC rates,
438 when the IR drop through the electrode does not have time to vanish by sampling
439 time (Figure 2). At lower switching rates, the resistance of the electrode is irrelevant
440 since its contribution has fully dropped to zero at the end of the DCC period.

441 For investigation of the effect of the DCC rate on firing, we used as simple integrate-

442 and-fire model with a passive leak conductance and an after-hyperpolarization (AHP)
443 current (Meunier and Borejsza, 2005; Manuel et al., 2006). The membrane poten-
444 tial (V_m) is governed by the equations:

$$\begin{aligned} C * \frac{dV_m}{dt} &= G_{in} * (V_r - V_m) + I_{AHP} + I_{inj} + \sigma \xi \\ C &= G_{in} * \tau_m \\ I_{AHP} &= \bar{g}_{AHP} * z * (E_k - V_m) \\ \frac{dz}{dt} &= \frac{-z}{\tau_{AHP}} \end{aligned} \tag{2}$$

445 G_{in} is the input conductance of the cell (we used the values 0.2 μ S, 0.4 μ S, and
446 0.67 μ S for S, FR and FF motoneurons, respectively, see text). τ_m is the membrane
447 time constant (varied between 2 and 5 ms, see text). V_r is the resting membrane
448 potential (0 mV). $\sigma \xi$ is a noise term. I_{AHP} is the AHP current. \bar{g}_{AHP} is the maximum
449 conductance of the AHP (2 μ S), E_k is the reversal potential of the AHP (-5 mV). z
450 is the fraction of the AHP conductance open at any point in time, and τ_{AHP} is the
451 relaxation time constant of the AHP (10 ms). For simplicity, the dynamic of the
452 AHP during the spike is not modeled, and instead, the parameter z is incremented
453 instantaneously at each spike (elicited when $V > V_{thr}$, $V_{thr}=10$ mV) according to
454 $z_{after} = (1 - \alpha) * z_{before} + \alpha$, where α is the fraction of the AHP recruited by a single
455 spike ($\alpha=0.25$) (Meunier and Borejsza, 2005), z_{before} is the value of z just prior to
456 the spike and z_{after} the value of z just after the spike. I_{inj} is the current injected by
457 the amplifier in bridge mode. In DCC mode, this current is chopped and scaled with
458 a duty cycle of 1/3. DCC rates range from 1 to 8 kHz.

459 5.5 Code availability

460 All figures were drawn using matplotlib v.3.2.2 (Hunter, 2007). The code for analy-
461 sis and production of figures is available at <https://doi.org/10.5281/zenodo.4139701>.

462 **Competing interests**

463 The author declares no conflict of interests.

464 **Grant information**

465 This work was financed by NIH NINDS R01 NS110953.

466 **Acknowledgements**

467 The author wishes to thank Drs. Daniel Zytnicki, Rob Brownstone, and Marco Beato
468 for their valuable comments and discussions. This work has benefited from the
469 support and expertise of the animal facility and microscopy platform of BioMedTech
470 Facilities at Université de Paris (INSERM US36/UMS2009).

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