# Small size of recorded neuronal structures confines the accuracy in direct 1 axonal voltage measurements 2 3 Viktor János Oláh<sup>1,2</sup>, Gergely Tarcsay<sup>1</sup> and János Brunner<sup>1</sup> 4 <sup>1</sup> Laboratory of Cellular Neuropharmacology, Institute of Experimental Medicine, Budapest, Hungary 5 <sup>2</sup> János Szentágothai School of Neurosciences, Semmelweis University, Budapest, Hungary 6 7 Corresponding Author: János Brunner 8 Email: brunner.janos@koki.hu 9 10 Abstract 11 Patch-clamp instruments including amplifier circuits and pipettes affect the recorded voltage signals. We 12 hypothesized that realistic and complete *in silico* representation of recording instruments together with 13 detailed morphology and biophysics of small recorded structures will precisely reveal signal distortions 14 and provides a tool that predicts native signals from distorted voltage recordings. Therefore, we built a 15 model that was verified by small axonal recordings. The model accurately recreated actual action potential 16 measurements with typical recording artefacts and predicted the native electrical behavior. The 17 simulations verified that recording instruments substantially filter voltage recordings. Moreover, we 18

revealed that instrumentation directly interferes with local signal generation depending on the size of the recorded structures, which complicates the interpretation of recordings from smaller structures, such as axons. However, our model offers a straightforward approach that predicts the native waveforms of fast

voltage signals and the underlying conductances even from the smallest neuronal structures.

23

# 24 Introduction

25 Patch-clamp technique is affected by limitations that originate primarily from the physical properties of the 26 recording pipettes (Benndorf, 1995; Hamill, Marty, Neher, Sakmann, & Sigworth, 1981; Marty & Neher, 1995). Patch pipettes have significant resistance ( $R_{pip}$ ) and their glass wall represent a substantial capacitive surface ( $C_{pip}$ ) 27 as well. Limitations can be reduced by optimizing the recording conditions (that is, with the reduction of the R<sub>pip</sub>) 28 29 and C<sub>pip</sub>) and corrected by using compensatory mechanisms of the amplifiers. Under standard recording conditions in measurements from relatively large structures, such as neuronal somata, these optimizations and 30 corrections can sufficiently reduce distortions to an acceptable level. Therefore, the difference between the 31 recorded and native voltage signals are negligible during good current clamp conditions in most neuronal 32 structures. However, the reduction of instrumental distortions could became inherently insufficient in cases where 33 the recorded structures are small, such as most of the central synapses. Recording pipettes for small neuronal 34 structures must have small tip, which inevitably results in larger R<sub>pip</sub> values that substantial filters the recorded 35 signals (Benndorf, 1995; Novak et al., 2013; Ying, Bruckbauer, Rothery, Korchev, & Klenerman, 2002). 36 Consequently, the fast voltage signals such as the action potentials (APs) are particularly vulnerable to signal 37 distortion associated with direct recordings in small axonal structures. The shape of axonal APs is a key 38 39 determinant of neuronal signaling that affects neurotransmitter release and short-term dynamics in synaptic connections (Bean, 2007; Borst & Sakmann, 1999; Chao & Yang, 2019; Geiger & Jonas, 2000; Katz & Miledi, 40 1967; Kawaguchi & Sakaba, 2015; Zbili & Debanne, 2019). Therefore, accurate AP measurements are essential 41 to understand fundamental mechanisms of the neuronal information flow. Recent developments of the recording 42 apparatus allows collecting voltage signals from the finest axonal structures (Kawaguchi & Sakaba, 2015; Novak 43 et al., 2013; Ritzau-Jost et al., 2021; Rowan, DelCanto, Jianging, Kamasawa, & Christie, 2016; Vivekananda et 44 al., 2017). However, the interpretation of these signals are still limited because signal distortions caused by the 45 recording pipette and amplifier circuits remains elusive (Ritzau-Jost et al., 2021). We reasoned that as 46 computational modeling allows the precise reconstruction of the native electrical behavior of the most complex 47

48 neuronal structures (Henrik Alle, Roth, & Geiger, 2009; Beaulieu-Laroche & Harnett, 2018; Branco & Häusser,

49 2011; Jayant et al., 2017; Kwon, Sakamoto, Peterka, & Yuste, 2017) it should be similarly possible to simulate

50 the behavior of the recording instruments.

With these in mind, we built and tested a realistic model that considers not only the biological structures but also amplifier and pipette features. With this complex model we simulated actual recording conditions with the aim of subsequent, simulated removal of the instrumental contributions and distortions from the recorded signals. Thus, this complex model allowed the correction of the distortions caused by patch-clamp recording instruments and predict isolated biological signals. We tested the model by predicting the native action potential waveform of a directly recorded small axonal varicosity. Our simulations showed that recording instrumentation not only filters the signal, but it directly interferes with native signal generation in small neuronal structures.

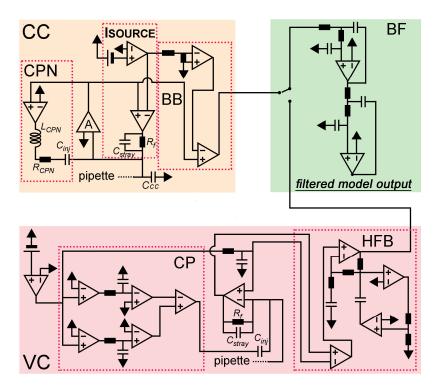
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# 59 **Results**

# 60 In silico implementation of amplifier features

We developed and validated a realistic amplifier model working both in voltage clamp (VC) and current clamp 61 (CC) mode using the NEURON simulation environment (Hines & Carnevale, 1997). The model needed to be 62 suitable for both VC and CC modes, because instrumental compensations are typically determined in VC mode 63 during seal formations and these settings are implemented for CC during voltage signals recordings. For precise 64 implementation of the components of the amplifier circuit, we examined their capacitive and resistive properties 65 using three test configurations (Supplementary Figure 1). The first test configuration was the isolated headstage 66 in open circuit (test #1), which allowed the characterization of the high frequency boost unit (see below) and the 67 capacitance compensation of the VC circuitry. Since open circuit measurements are not possible in CC mode, the 68 circuit was closed via known resistors in the second test configuration (test #2). This configuration allowed the 69 estimation of stray capacitance associated with the feedback resistor. The third test circuit was a modified model 70 cell (test #3, type 1U, Molecular Devices), which represents whole-cell recording conditions as it includes an 71

- 72 idealized cell and recording pipette with their resistive and capacitive components. In order to explore an extended 73 range of signal processing capacity of the amplifier, model cell components were varied using custom capacitors 74 and resistors. This test configuration allowed us to investigate the features of the capacitance neutralization of the 75 and resistors. This test configuration allowed us to investigate the features of the capacitance neutralization of the
- 75 CC circuitry.
- The construction of our model amplifier initially based on idealized circuit representations, namely a resistive feedback circuit (a current-to-voltage converter) typical for the VC and a voltage follower circuit (a unity gain voltage buffer) with an idealized current source for the CC (Sherman-Gold, 2012; Sigworth, 1995; Wilson &
- 79 Park, 1989) (**Figure 1**).



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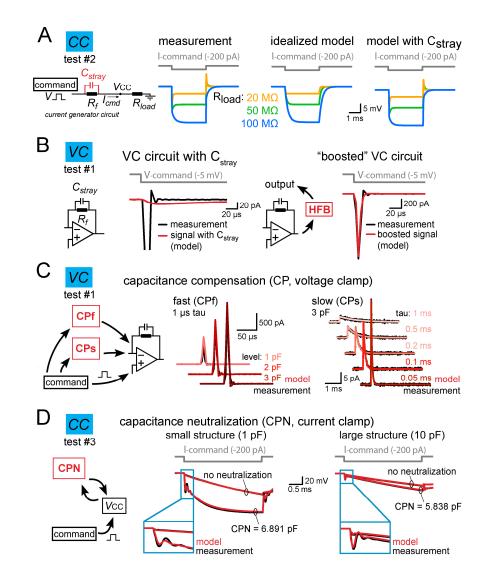
# 81 Figure 1. Model amplifier

Schematic circuit diagram of the model amplifier. The current clamp circuit (CC) consisted of a current source (ISOURCE),
an idealized voltage buffer (A), capacitance neutralization (CPN) and bridge balance (BB) circuits. The voltage clamp
circuit (VC) consisted of a resistive feedback amplifier with dual capacitance compensation (CP) and the high frequency
boost circuit (HFB). Outputs of the two amplifier modules are connected to a low-pass filter circuit (BF).

Operation of combined voltage- and current-clamp amplifiers requires a capacitor (C<sub>ini</sub>) for current injection in 87 both VC and CC modes and a resistor (Rf) used as current generator in CC and as feedback resistor in VC 88 (Strickholm, 1995) (Figure 1). To create realistic amplifier model, we first measured amplifier responses using 89 the three test circuits, which were subsequently simulated allowing individual tuning of elementary circuit 90 parameters. First, we measured C<sub>ini</sub>, assuming that the total capacitive load present in the isolated VC circuit (test 91 #1) corresponds to the injector capacitor. By recording voltage-step-evoked capacitive current responses in open 92 circuit configuration, we determined that the total capacitive load is 1.615 pF in our amplifier (MultiClamp700B). 93 As virtually all real resistors, Rf has a certain amount of parasitic capacitance (Cstray) which affects the 94 performance characteristics of the amplifier. We next determined the size of this parasitic capacitance. In CC 95 mode, the C<sub>strav</sub> connected in parallel with the R<sub>f</sub> (see ISOURCE circuit on Figure 1) acts as a capacitance-96 97 neutralizing element. However, this neutralizing effect appears only when the input load is considerably smaller than the  $R_f$  which was set to 500 M $\Omega$  in the real amplifier (Figure 2A left traces). To characterize the size of 98 C<sub>stray</sub> associated with the R<sub>f</sub>, we adjusted the C<sub>stray</sub> in the model to reproduce the evoked voltage responses recorded 99 100 with the amplifier in test #2 configuration with 20, 50 and 100 M $\Omega$  input loads (Figure 2A right traces). These simulations revealed 0.38 pF C<sub>strav</sub>, thus we used this value in the model. 101

Next, we added the remaining amplifier components to the model one-by-one. First, we focused on the VC 102 operations whose speed depends on a dedicated high frequency boost circuit (Sigworth, 1995). Amplifier are built 103 with this compensation mechanism because C<sub>stray</sub> substantially reduces the output bandwidth of the feedback 104 circuit in VC mode (time constant of the capacitive relaxation with the previously determined 0.38 pF C<sub>stray</sub>: 105 191.92 us, Figure 2B left). We added a simplified boosting unit tuned to accelerate model responses to the 106 experimentally observed amplifier speed (3.85 µs vs. 3.19 µs, real vs. boosted model, Figures 1 and 2B right). 107 Next, we implemented two pipette capacitance compensation circuits in the VC model. Fast capacitance 108 compensation (CPf, 0-16 pF, 0.5-1.8 µs) cancels the majority of C<sub>pip</sub>-induced current transients, while the slow 109 capacitance compensation (CPs, 0-3 pF, 10-4000 µs) reduces the slower instrumental capacitive components 110

- 111 (Sigworth, 1995) (not equivalent to whole-cell compensation that was not implemented in this model Figures 1
- 112 and 2C).



#### 113

114 Figure 2. Implementation of individual amplifier components with realistic parameters

115 (A) The stray capacitance ( $C_{stray}$ ) associated with the current passing resistor ( $R_f$ ) was predicted by simulating the voltage 116 responses recorded in test #2 configuration.  $C_{stray}$  acts as a capacitance neutralizing element in CC mode. Because the 117 capacitance neutralizing effect of  $C_{stray}$  depends on the load resistance ( $R_{load}$ ) attached to the amplifier input ( $V_{CC}$ ), we tested 118 three scenarios using 20, 50 and 100 M $\Omega$  resistors. The left traces show measured voltage responses evoked by brief current 119 injection in the presence of different  $R_{load}$ . Idealized (i.e.  $C_{stray}$  free) model responses are shown in the middle for comparison. 120 Right, model responses with 0.38 pF  $C_{stray}$  replicated the observed amplifier behavior.

121 (B)  $C_{\text{stray}}$  of  $R_f$  slows down the current responses in the VC model (red trace, left panel). This effect is compensated in the 122 actual amplifiers by using high frequency boost circuit (HFB). The implementation of a high frequency boost circuit in the 123 model restored the response speed (red trace, right panel).

(C) Capacitance compensation in the VC model (red) faithfully replicates the magnitude and the time course of amplifier generated compensatory currents (black, test circuit#1) for both the fast (CPf) and slow (CPs) compensations.

126 (D) Comparison of simulated (red) and recorded (black) voltage signals obtained with different capacitance neutralization

127 (CPN) in CC mode from a small structure (middle panel) and from a large structure (left panel). Notice that the instrumental

128 CC model faithfully replicates the neutralizing capability of the amplifier and the neutralization associated signal artefacts129 regardless of the applied CPN settings.

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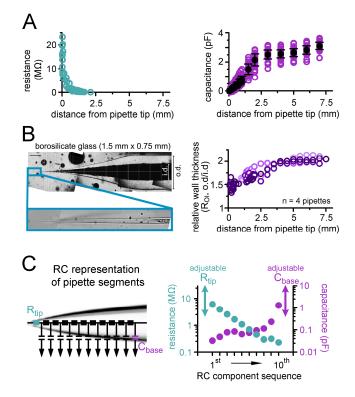
We also implemented two compensatory mechanisms for the CC mode, namely the capacitance neutralization 131 (CPN) and the bridge balance (BB) compensation (Figure 1). The CPN circuit is a positive feedback loop that 132 feeds the pipette voltage back to the input through the C<sub>ini</sub> in order to discharge the pipette capacitance (Sherman-133 Gold, 2012; Wilson & Park, 1989). Due to this positive feedback, the recordings are prone to oscillate as CPN 134 level approaches a fully compensated state. Such evolving oscillation carry information about the intrinsic 135 behavior of the CPN circuit. Therefore, the oscillating signal (dampening and frequency profile) can be employed 136 for determining a minimal set of passive circuit elements necessary the re-create the CPN behavior. Specifically, 137 we measured the maximal possible capacitance neutralization where the recording is still stable using test#3 138 circuit. Pipette parameters (10M $\Omega$ , 2.8 pF) and the cell-equivalent resistor (500 M $\Omega$ ) was fixed and only the 139 capacitance of the cell was varied from 0.75 pF to 46.7 pF. The model reproduced the recorded signal artefacts 140 when a resistor (1.49 M $\Omega$ ) and an inductor (18.3 H) was incorporated to the CPN circuit in series with the C<sub>ini</sub> 141 (Figures 1 and 2D). Amplifiers are typically supplied with BB compensatory mechanism to eliminate the voltage 142 drop across the access resistance (Araki & Otani, 1955; Sherman-Gold, 2012). In the model, we subtracted a 143 scaled version of the command signal from the recorded voltage (Figure 1). We also extended our model with a 144 four-pole low-pass Bessel filter unit with adjustable cutoff frequencies from 0.5 kHz to 100 kHz (Figure 1). 145

Altogether, by using a measurement-based approach we created an amplifier model, in which both the VC and
CC operation and their specific compensatory capabilities show realistic behavior.

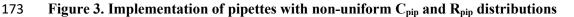
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#### 150 *Pipette implementation considers the observed nonuniform* $C_{pip}$ *and* $R_{pip}$ *distributions*

Next, we focused on the accurate implementation of patch pipettes. To properly characterize the distribution of 151 resistance along patch pipettes that are suitable for recordings from small axons, we repeatedly broke small pieces 152 153 from the end of the pipettes and determined the resistance as a function of tip distance (Figure 3A, n = 55resistance measurement). In agreement with the theoretical considerations (Benndorf, 1995; Ying et al., 2002), 154 we found that pipette resistance drops sharply after the tip, falling below one M $\Omega$  within the first millimeter (0.33) 155  $\pm 0.18$  M $\Omega$  for measurements with tip distance over 1 mm, n=20 measurement). To determine the capacitance 156 distribution of our pipettes we systematically varied the immersed length of the pipettes in the recording solution 157 and measured the capacitance, which corresponds to the cumulative capacitance of the dipped part (Cornwall & 158 Thomas, 1981) (Figure 3A, n = 656 capacitance measurement). The cumulative capacitance increased within the 159 first 3 mm from the tip, whereas the remaining part of the pipette had only moderate contribution to the total 160 capacitance suggesting inhomogeneous capacitance distribution along pipettes ( $0.03 \pm 0.07$  pF,  $2.52 \pm 0.3$  pF and 161  $3.1 \pm 0.25$  pF at 0.1 mm, 3 mm and 7 mm tip distances respectively, n=39, 40 and 38 measurements, Figure 3A). 162 A key parameter that defines the pipette capacitance is the ratio of the outer and inner pipette diameters (R<sub>OI</sub>) 163 (Benndorf, 1995; Cornwall & Thomas, 1981). One potential explanation for the inhomogeneous capacitance 164 distribution is that the R<sub>OI</sub> is not constant along the pipette but it decreases toward the tip. To test this possibility 165 and verify the predictions of the capacitance distribution measurement, we directly measured the Roi of the 166 recording pipettes. In order to precisely measure the edge of the pipette walls and avoid optical distortions by the 167 curved glass walls, we carefully split the pipettes using a custom-built grinding system and measured their inner 168 and outer diameters along the longitudinal axis (Figure 3B, see Methods section for details). Consistent with the 169 dipping measurements,  $R_{OI}$  decreased toward the tip ( $R_{OI} < 2mm = 1.6 \pm 0.02$  vs.  $R_{OI} > 5mm = 2.04 \pm 0.02$ , n = 4170 pipettes) explaining the larger contribution of the tip region to the total pipette capacitance. 171



#### 172



174 (A) Pooled data of  $R_{pip}$  (left graph) and  $C_{pip}$  (right graph) as a function of tip distance.

(B) A representative imaging plane that was used for the measurement of the relative wall-thickness (R<sub>oi</sub>) that is, the ratio
of outer and inner diameter (o.d. and i.d., respectively) of the pipettes. Scale bar: 0.5 mm. Graph on the right shows that the
wall of the pipettes is much thinner toward the tips (i.e. the inner diameter is larger than predicted from the R<sub>oi</sub> of the original
glass; the 4 measured pipettes are shown in different shades of purple).

(C) Pipettes were implemented as 10 independent RC units, a resistor (R<sub>tip</sub>, on the left) and a capacitor (C<sub>base</sub>, on the right).
The two latter components allow the adjustment of the model to fit the differences of R<sub>pip</sub> and C<sub>pip</sub> of individual pipettes.
Graph on the right indicates the actual capacitance (purple) and resistance (green) values of the 10 fixed RC motifs.

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Based on these measurements, we created the skeleton of a "prototypical" patch pipette model from 10 RC units to consider the inhomogeneous distribution of capacitance and resistance (**Figure 3C**). Model pipette parameters can be adjusted to account for variability across individual pipettes using an additional resistor placed to the tip and a capacitor placed to the back to tune the  $R_{pip}$  and  $C_{pip}$  of individual pipettes.

# 188 Reconstitution of the native electrical behaviour of a small axon

To test the efficacy of the complex instrumental model in predicting undisturbed fast neuronal membrane responses from distorted recordings, we used patch-clamp data from a small ( $<1 \mu m$ ) *en passant* axonal varicosity of an identified hippocampal mossy fiber axon (MF, **Figure 4A**). Recordings from submicron-sized neuronal structures are supposedly substantially distorted as they can be patched only with high access resistance and their capacitance is in the range of the remaining uncompensated instrumental capacitance.

- The experimental conditions needed to be realistically modeled, including the precise morphology and electrical properties of the biological structure and the instrumental conditions (**Supplementary Figure 2**, see Methods for details). First, we characterized the total instrumental capacitance ( $C_{tot}$ , the sum of all amplifier-, holder- and pipette-related capacitances) present in the actual recording (**Figure 4A**,  $C_{tot}$  : 7.097 pF from which 3.23 pF is the  $C_{pip}$  and 2 pF is the capacitance of the pipette holder). Target trace for this estimation was recorded using both fast and slow pipette capacitance compensation of the amplifier with the highest frequency resolution (output filter was bypassed) and we set the model accordingly.
- Next, we precisely reconstructed the morphology of the biocytin-labelled and fluorescently recovered MF axon because signal propagation strongly depends on the length, diameter and their inhomogeneties of the biological structures (Goldstein & Rall, 1974; Manor, Koch, & Segev, 1991) (**Figure 4B**). As it is characteristic for hippocampal mossy fibers the 519  $\mu$ m long reconstruction of the recorded MF included large (>3  $\mu$ m) terminals, filopodial extensions and small (<1.5  $\mu$ m) *en passant* varicosities within the *stratum lucidum* of the CA3 area (Acsady, Kamondi, Sık, Freund, & Buzsáki, 1998; Rollenhagen et al., 2007).
- We next determined the cable properties; specific membrane resistance ( $R_m$ ), membrane capacitance ( $C_m$ ), and intracellular resistivity ( $R_i$ ) of the particular axon. For this, we optimized the model to the experimentally recorded voltage responses evoked by short and long current stimuli (**Figure 4C**) (Nörenberg, Hu, Vida, Bartos, & Jonas, 2010; Roth & Häusser, 2001; Schmidt-Hieber, Jonas, & Bischofberger, 2007; Szoboszlay et al., 2016). The advantages of the complex (instrumental + biological) model became obvious in these fittings. Pipette artefacts

can markedly contaminate the onset of the evoked responses upon current injection (Major, Larkman, Jonas, Sakmann, & Jack, 1994). The incorporation of the complete experimental instrument to the model precisely reproduced these stimulus artefacts, therefore, allowing us to isolate biological contributions and obtain the passive cellular parameters. The predicted cellular parameters ( $R_m = 60.0 \text{ k}\Omega^*\text{cm}^2$ , a  $C_m = 0.65 \text{ }\mu\text{F}^*\text{cm}^{-2}$  and  $R_i$ = 147.3  $\Omega^*\text{cm}$ ) match with the data reported for MFs using recordings from large terminals (S. Hallermann, Pawlu, Jonas, & Heckmann, 2003). It is important to note that the similarities of the simulated and recorded fast voltage transients further verify our complex model.

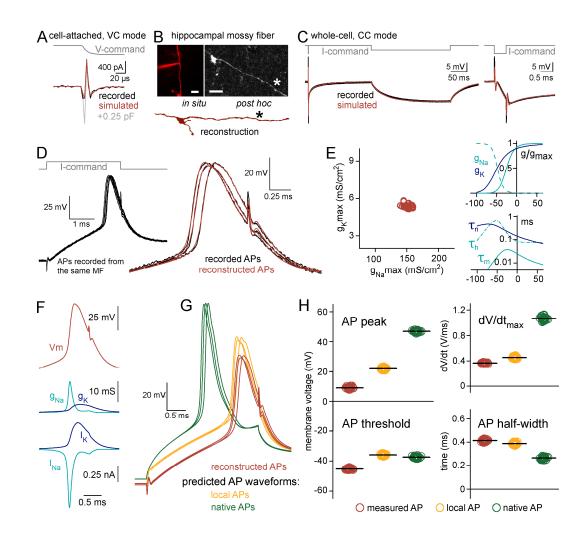




Figure 4. Reconstitution of the undisturbed membrane dynamics of a recorded axon

221 (A) Current responses to -20 mV voltage steps recorded from the axonal membrane in on-cell mode (black) and in the model 222 with 7.097 pF (red) and 7.347 pF (grey)  $C_{tot}$ . Notice the sensitivity of simulated responses to small differences in the

instrumental capacitance applied in the model.

(B) Confocal z-stack images show the recorded axon at the end of the experiment (left) and after the anatomical recovery

225 (right). Bottom, part of the reconstructed morphology. Asterisks mark the recording position. Scale bars: 10 μm

(C) Voltage responses in the recorded axon (black) and in the passive cable model with the added instrument (red) to short

227 (3 ms, -50 pA) and long (250 ms, -2.5 pA) current stimuli. The short pulse is shown at an expanded timescale on the right.

(D) Recorded (black) and simulated APs (red) evoked by brief (3 ms, 86 pA) current stimuli. APs were simulated in the
 complex model that included the instrument, the passive cable and Hodgkin-Huxley type sodium and potassium
 conductances.

(E) Left, distribution of optimal maximal Na<sup>+</sup> (gNa<sub>max</sub>) and K<sup>+</sup> (gK<sub>max</sub>) conductance densities obtained from 30 recorded and independently fitted APs. Right, averaged gating properties and voltage dependence of the conductances that were resulted in by the fits that recreated the recorded APs.

(F) Simulated AP waveform (top) with the underlying conductances (middle,  $g_{Na}$  and  $g_K$ ) and the modeled ionic currents (bottom,  $I_{Na}$  and  $I_K$ ).

(G) The simulations with the confirmed conductance sets allowed to see the waveforms of the same APs not only within
the pipette (red, corresponding to measured APs) but also the simultaneous AP waveforms within the axon (orange,
corresponding to local APs) and, after the removal of the recording instrument from the model, the native, undisturbed AP
waveforms (green).

240 (H) Differences in waveform parameters of measured, local and native APs. Individual points show the peak, threshold, 241 maximum rate of the rise  $(dV/dt_{max})$  and half-width of 30 independently simulated APs in the three points of view. Horizontal 242 black lines indicate mean values.

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Next, we simulated the active ionic mechanisms underlying the recorded AP waveforms. APs were evoked with 244 brief current stimuli (Figure 4D and E, 3 ms, 86 pA). To simulate APs we tuned Hodgkin-Huxley-type sodium 245 and potassium conductances (Hodgkin & Huxley, 1952) (modified version of the built-in mechanism in the 246 NEURON simulation environment). Optimization of the density, kinetics and voltage dependence resulted in AP 247 waveforms closely matching to the recorded ones (absolute AP peak:  $9.0 \pm 0.12$  mV vs.  $9.28 \pm 0.12$  mV, recorded 248 vs. simulated APs, respectively, AP half-width:  $0.52 \pm 0.002$  ms vs.  $0.52 \pm 0.002$  ms, AP threshold: -45.28  $\pm$ 249  $0.07 \text{ mV vs.} -44.27 \pm 0.16 \text{ mV}$ , maximum rate of rise:  $363.26 \pm 0.93 \text{ vs.} 432.27 \pm 3.56$ , n = 30 APs; Figure 4D). 250 This suggest that the complex instrumental model in combination with traditional conductance functions is 251 sufficient to reconstruct the recorded AP waveforms from potentially distorted recordings. Importantly, although 252

each of the target APs was fitted independently, the optimal model conductance parameters were confined to a 253 narrow range within the parameter space (coefficient of variation = 3% for both the Na<sup>+</sup> and K<sup>+</sup> conductance 254 predictions, maximal  $g_{Na}$  density:  $151.7 \pm 5.23$  mS/cm<sup>2</sup>, maximal  $g_K$  density:  $5.41 \pm 0.16$  mS/cm<sup>2</sup>, n = 30; Figure 255 4E) indicating that the optimization provided a unique solution for the experimental data. Analysis of the error 256 between the fit and its target data in different Na<sup>+</sup> and K<sup>+</sup> conductance combinations also revealed a single 257 minimum that coincided with the best fit parameter combinations (Supplementary Figure 3). Furthermore, the 258 259 optimal conductance parameters (i.e. their maximal conductance levels, their voltage dependence, and their activation and inactivation time constants), as well as the resulted ionic currents, are similar to previously 260 described mechanisms underlying cortical axonal APs at near-physiological temperature (Henrik Alle et al., 2009; 261 Geiger & Jonas, 2000; Stefan Hallermann, De Kock, Stuart, & Kole, 2012; Schmidt-Hieber & Bischofberger, 262 2010) (H. Alle, Kubota, & Geiger, 2011; Engel & Jonas, 2005; Hu & Jonas, 2014) (Figure 4 E and F), confirming 263 the validity of our AP-reconstitution approach. 264

The relatively high series resistance ( $R_{access}$ ) in the recording (modeled  $R_{access}$ : 53.2 ± 1.02 M $\Omega$  in the AP 265 reconstitution simulations) can result in significant pipette filtering. The complex model, however, allowed us to 266 investigate not only the APs recorded through the pipette but also the local spike that occurred within the axon 267 while it was patched (Figure 4G). These local APs are not affected by the filtering effect caused by the pipette, 268 so we could directly quantify filtering effects by comparing the *local* and *recorded* axonal AP waveforms (Figure 269 4H). Because of the filtering, local spikes had larger peak amplitudes and faster time course than the recorded 270 APs (absolute peak:  $21.95 \pm 0.12$  mV vs.  $9.0 \pm 0.12$  mV, local vs. measured AP, respectively,  $p = 6.88 \times 10^{-60}$ , 271 t(29) = -552.75 paired sample t-test, n = 30 APs, half-width:  $0.48 \pm 0.002$  ms vs.  $0.52 \pm 0.002$  ms, local vs. 272 measured AP, respectively,  $p = 1.99 * 10^{-17}$ , t(29) = 18.23, paired sample t-test, n = 30 APs, Figure 4H). As 273 expected, the maximal rate of rise  $(dV/dt_{max})$  during the upstroke of spikes was the most different between local 274 and measured APs as it is the most sensitive to low-pass filtering introduced by the pipette ( $453.11 \pm 2.54$  V/s vs. 275  $363.26 \pm 0.93$  V/s, respectively,  $p=4.69 * 10^{29}$ , t(29) = -47.5, paired sample t-test, n = 30 APs, Figure 4H). 276

277 Altogether, these observations are in agreement with the expected filtering, which affects fast signals, such as the

axonal APs more prominently.

Our model predicts that APs of the small MF bouton had lower peak and slower kinetics than APs measured from 279 large MF terminals (Henrik Alle et al., 2009; Geiger & Jonas, 2000). These observed differences could derive 280 either from biological variability among the subcellular compartments or from the larger deteriorating 281 instrumental impact on the local membrane of the smaller axon. To discriminate between these possibilities, we 282 investigated the *native* AP parameters predicted by the model. In this arrangement, we run the modeled biological 283 structure with the reconstructed model conductances but the recording instruments was removed (Figure 4G and 284 H). Thus, we predict how the native APs would look if the recording instrument was not present. We found that 285 the native APs reached more depolarized peak potential  $(46.9 \pm 0.09 \text{ mV}, p = 2.27*10^{-48}, t(29) = 221.43, paired$ 286 sample t-test, n = 30 APs) and were significantly faster (half-width:  $0.33 \pm 0.002$  ms,  $p = 1.36*10^{-33}$ , t(29) = -287 68.3, paired sample t-test;  $dV/dt_{max}$ : 1064.81 ± 5.1 V/s,  $p = 3.75*10^{-45}$ , t(29) = 171.47, paired sample t-test, n = 1000288 30 APs) compared to the local spikes modeled with the experimental rig. The obtained native AP parameters were 289 similar to those reported from large MF boutons, suggesting that the different AP shape observed in the small MF 290 recording is primarily attributable to the presence of the measuring system. 291

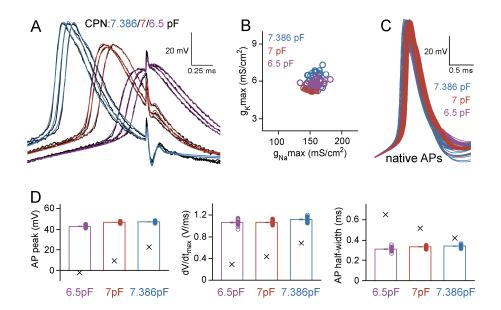
Altogether, these results show that it is possible to obtain the native and local AP properties and the plausible underlying mechanisms using a complex instrumental model.

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# 295 Modeling the recording instruments accurately predicts signal distortions and native AP shapes

We used additional experiments to verify the reliability and plausibility of the model predictions. Specifically, we recorded APs with three different capacitance neutralization settings from the same axon and tested whether it alters the output of the model (CPN=6.5, 7 and 7.384 pF **Figure 5A**). Sub-optimal CPN conditions affects the recorded signal in several ways (**Supplementary Figure 4**). The simulations reproduced the recorded APs with different level of distortions when the CPN in the model was adjusted accordingly (**Figure 5A**). In addition, the

- predicted underlying sodium and potassium conductances were also very similar ( $g_{Na}$  density: 159.02 ± 1.73
- 302 mS/cm<sup>2</sup>,  $151.7 \pm 0.95$  mS/cm<sup>2</sup>,  $160.03 \pm 1.47$  mS/cm<sup>2</sup>,  $g_K$  density:  $5.83 \pm 0.05$  mS/cm<sup>2</sup>,  $5.41 \pm 0.03$  mS/cm<sup>2</sup>, 6.32
- $\pm 0.09 \text{ mS/cm}^2$ ; n = 30, n = 30 and n = 28 for CPN = 6.5 pF APs, CPN = 7 pF APs and CPN = 7.386 pF APs,
- 304 respectively, Figure 5B and Supplementary Figure 5).



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# Figure 5. APs recorded and simulated from the same axon under different instrumental distortions predicted similar native spike shapes

(A) Representative target APs (black) and their best-fit representations in the complex instrument+axon model with
standard CPN settings (red, 7 pF), with slightly reduced CPN (purple, 6.5 pF) or with the highest attainable CPN level (blue,
7.386 pF).

(B) The best-fit  $gNa_{max}$  and  $gK_{max}$  were similar from APs with different CPN levels (n=30, 30 and 28 target APs).

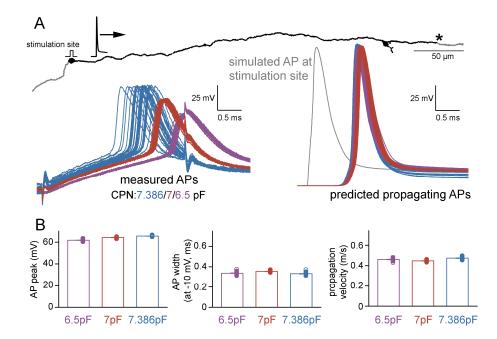
312 (C) The native AP waveforms retrieved from APs with different CPN levels were also similar.

313 (D) Peak, maximal dV/dt and half-width of the native APs predicted based on recordings with three different CPN settings.

Columns show the averages of the native APs, while X denotes the averages of the experimentally measured parameters (n=30,30 and 28 APs) which were distorted by the instruments.

- 316
- 317 Importantly, not only the predicted AP shapes matched but the native APs were also similar despite of the different
- levels of distortions in the three independent original recording conditions (absolute AP peak:  $43.0 \pm 0.17$  mV,
- $46.9 \pm 0.09 \text{ mV}, 47.2 \pm 0.14 \text{ mV}, \text{AP half-width: } 0.31 \pm 0.003 \text{ ms}, 0.33 \pm 0.002 \text{ ms}, 0.34 \pm 0.003 \text{ ms}; n=30, n=$

n=28 for CPN=6.5 pF APs, CPN=7 pF APs and CPN=7.386 pF APs, respectively; Figure 5C and D). For an 320 additional verification, we tested whether the model provides consistent predictions of AP propagation across 321 conductance sets derived from different recording configurations. Specifically we simulated the natural AP 322 conduction of distally evoked APs to the original recording site (423 µm away, Figure 6A) and measured the 323 324 speed of propagation and the shape of the incoming APs. The incoming propagating APs were similar (absolute AP peak:  $61.73 \pm 0.13$  mV,  $64.22 \pm 0.07$  mV,  $65.48 \pm 0.08$  mV, AP width at -10 mV:  $0.34 \pm 0.003$  ms,  $0.36 \pm 0.003$  ms, 0.003 m 325 0.002 ms,  $0.33 \pm 0.002 \text{ ms}$ ; n=30, n=30, n=28 for CPN=6.5 pF APs, CPN=7 pF APs and CPN=7.386 pF APs, 326 327 respectively; Figure 6).



328

#### 329 Figure 6. Characteristics of propagating native APs

(A) The reconstructed and simulated axonal structure with the position at which native AP parameters were captured (indicated with asterisk) after distal AP initiation (stimulation site) in individual models that were optimized for different recording conditions. Left, 88 original AP recordings that were used for the AP optimization in the models and recorded individually with three different CPN settings (n=30, 30 and 28 with 6.5, 7 and 7.368 pF CPN, respectively). The retrieved conductance sets were applied to the complete axon individually in all 88 cases. The right panel shows the 88 native, propagating simulated APs at the indicated distal point along the axon. The color is as for the measured APs on the left. A simulated AP at the stimulation site is shown in gray.

(B) Peak, width at -10 mV and propagation velocity of the distally initiated propagating APs retrieved from 88 individual
simulations. Note that conventional AP half-width measurements can not be applied for propagating APs because of the
altered apparent threshold.

340

- The prediction of AP propagation velocity is particularly sensitive to model parametrization as the speed of axonal spike propagation strongly depends both on the morphological properties of the axon and the specific passive and active mechanisms of the axonal membrane. Consistent with previous measurements in hippocampal MFs (Henrik Alle et al., 2009; Kress, Dowling, Meeks, & Mennerick, 2008), all model configuration predicted similar propagation speed ( $0.46 \pm 0.002 \text{ m}^*\text{s}^{-1}$ ,  $0.45 \pm 0.001 \text{ m}^*\text{s}^{-1}$ ,  $0.47 \pm 0.002 \text{ m}^*\text{s}^{-1}$ ; **Figure 6B**).
- Taken together, these results confirm that complete representation of the recording instruments in a model is sufficient for generating plausible native signals and underlying membrane mechanisms from signals that are distorted by the recording apparatus.

349

# 350 Instrumental and structural parameters jointly define signal distortion in recordings from small neuronal 351 structures

In addition to providing a useful tool for predicting and correcting instrumental distortions our simulations 352 confirmed that complete elimination of the instrumental disturbance was not possible during recordings (Ritzau-353 Jost et al., 2021), since substantial difference persists between the measured and native APs, even when the 354 capacitance compensation reached the maximally attainable level (see Figure 5C). The model raised the 355 possibility that inadequate local signal generation also significantly contribute to the alterations in AP shapes in 356 addition to filtering that affects recordings through patch pipettes. We refer to this effect as observer effect based 357 on the analogy with the concept introduced in the field of physics for situations where the measurement inevitably 358 changes the measured parameter. The observer effect can be quantified as the difference between local APs 359 (signals in the structure when pipette is present) and native APs (signals without the presence of any instrument, 360 Figure 4G and H). We quantified the relative contribution of filtering and observer effects to the total 361

instrumental distortion in different experimental situations. Specifically, we varied pipette parameters, compensation settings and the size of the recorded cell (size was set to as  $C_{cell} = 1 \text{ pF}$  and 10 pF, corresponding to the size of axons or small caliber dendrites and small cell bodies, respectively) in a reduced model which included only a single neuronal compartment with the instrumentation and compared the half-widths of APs (**Figure 7**). First, we isolated the filter effect by comparing simultaneous AP signals in the pipette and in the cell (measured versus local AP).

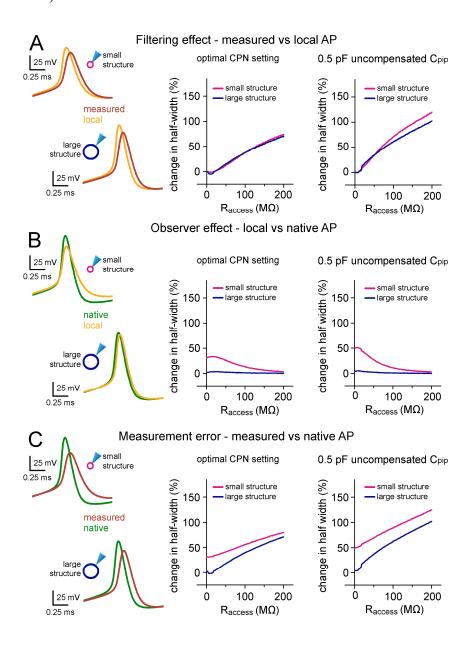


Figure 7. Instrumental and structural parameters cooperatively determine signal distortions in recordings from small neuronal structures

(A) On the left, the differences between the waveforms of the same APs within the pipette (measured) and in the two hypothetical cells (local) highlight the filtering effect of 70 M $\Omega$  R<sub>access</sub>. Only the size of the membrane surface were different in the two spherical structures, resulting in 1 and 10 pF biological capacitance, which correspond to small axonal and small somatic recordings. Graph in the middle summarizes the filtering effect quantified as the difference in AP half-width over a wide range of R<sub>access</sub> in the small and large spherical cells. The right graph summarizes the filtering effect in simulations where suboptimal capacitance neutralization was applied (6.3 pF instead of 6.8 pF).

(B) Using the same simulation environment as in panel A, the observer effect was quantified as the difference between the
local AP and the native AP waveform. Thus, this data represents the isolated influence of the instrument on local signal
generation.

(C) To quantify the measurement error we demonstrate the difference between the measured AP and the native AP waveformin the same conditions as above. Thus, this is the sum of the filtering and observer effects.

382

In accordance with the general notion (Barbour, 2014), high  $R_{access}$  significantly filters fast voltage transients and allowed faithful measurement only in a confined  $R_{access}$  range ( $R_{access}$  that causes 10% AP signal widening: 47 M $\Omega$  for small cell and 41 M $\Omega$  in case of larger cell; **Figure 7A**, left). Furthermore, when uncompensated capacitance was added to the circuit by reducing the applied capacitance neutralization (-0.5 pF), the recording became more vulnerable and reliable recordings needed better  $R_{access}$  ( $R_{access}$  with 10% distortion: 20 M $\Omega$  for small cell and 17 M $\Omega$  in case of larger cell; **Figure 7A**, right).

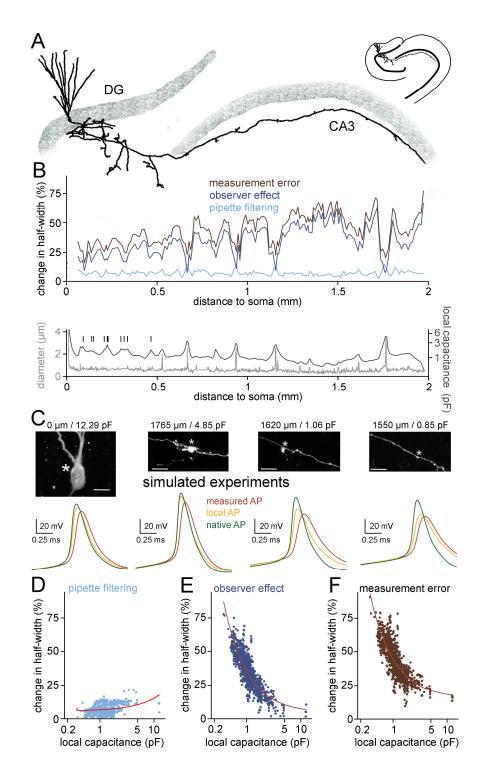
Next, we isolated the observer effect by comparing the local and native AP shapes with or without the presence 389 of the recording instrument (Figure 7B). The observer effect was always negligible in the case of the larger 390 simulated biological structure as the capacitance added by the pipette was insignificant compared to the cellular 391 parameters. In contrast, when the structure was smaller the structure had to discharge the remaining instrumental 392 capacitance, which was in in this case in the range of C<sub>cell</sub>, resulting in significant observer effect on the recorded 393 AP shape (Figure 7B). Consistent with this hypothesis, observer effect was larger in simulations with additional 394 uncompensated  $C_{pip}$  (mean change in AP half-width in the R<sub>access</sub> range of 1-50 M $\Omega$ : 31.03±0.32 % vs. 40.54±1.14 395 %, optimal CPN vs. CPN with 0.5 pF uncompensated  $C_{pip}$ , respectively; Figure 7B). Intriguingly, the observer 396 effect showed a reversed dependence on the Raccess. It was the most pronounced when Raccess was low. The larger 397

R<sub>access</sub> presumably isolates the residual instrumental capacitance from the cell and consequently weakens the
 instrumental impact.

Finally, by comparing the measured and native signals we assessed the overall measurement error. In case of the 400 larger simulated structure, the overall measurement error is dominated by the filtering effect (Figure 7C). In 401 contrast, when C<sub>cell</sub> is small, the observer effect contributes significantly to the total error. Interestingly, the 402 complementary changes in the two effects make these recordings less sensitive to changes of Raccess and the error 403 is similar when the Raccess is low or high (Figure 7C left). The results confirm that residual uncompensated pipette 404 capacitance further deteriorate the difference between native and measured AP signals (Figure 7C left). Similar 405 conclusions can be drawn regarding other AP parameters as well (Supplementary Figure 6). Altogether, these 406 model simulations demonstrated that measurement errors in patch-clamp recordings depend not purely on the 407 pipette parameters but the size of the recorded structure itself has influence on the signal distortion. 408

Finally, to confirm the above findings on the error sources in a native biophysical structure we repeated the above 409 tests in a reconstructed MF that was labeled during somatic recording that ensured more intact axonal arborization 410 (Figure 8A). In this case the simulations ran with fixed instrumental parameters (6.74 pF  $C_{tot}$  and 60 M $\Omega$  R<sub>access</sub>. 411 with 6.8 pF capacitance neutralization and 60 M $\Omega$  bridge balance correction; Figure 8A, B and C). We evoked 412 APs along the axon and compared the pipette measured, local and native AP waveforms to determine the 413 contribution of the observer and filtering effects to the instrumental signal distortion and their dependence on the 414 local biophysical environment (Figure 8A, B and C). In agreement with the single compartment simulations 415 (Figure 7), observer effect had a major contribution to the overall measurement error (change in AP half-width: 416  $7.02 \pm 1.02$  %,  $34.03 \pm 4.59$  % and  $43.26 \pm 4.51$  % for pipette filtering, for observer effect and for total 417 measurement error, respectively, n=941 locations; Figure 8A, B and C). As it is expected from the fixed 418 instrumental parameters, pipette filtering was similar in small and large diameter sections of the axon. In contrast, 419 the size of the observer effect was much larger in smaller axonal structures. Consequently, the measurement error 420 was also the largest in the smallest diameter sections (Figure 8B). Importantly, minima in observer effect coincide 421 with larger local capacitance, which originate from the large mossy fiber boutons in the CA3 area and branching 422

- 423 points in the hilus. Indeed, the overall measurement error showed similar inverse correlation to local capacitance
- 424 ( $R^2=0.68$ , power) as the observer effect ( $R^2=0.75$ , power) while the pipette filtering was structure-independent
- 425 (Figure 8D-F). These findings confirm that measurement error critically depends on the local biophysical
- 426 environment.



428 Figure 8. Measurement error along the axon is inhomogeneous and depends on the local biophysical environment

(A) Morphology of a somatically labeled complete granule cell that was used for simulating hypothetical recordings alongits axon.

(B) Top, observer- and filtering effects (dark blue and light blue, respectively) together with the overall measurement error (brown) in simulated axonal measurements plotted against the somatic distance of the recording position. Each value represent average of 5 individual measurements in each 10 µm segments. Bottom, axonal diameter (grey) and local capacitance (black) as a function of somatic distance. Vertical bars indicate the branch points of hilar axon collaterals. Notice that signals that derive from axonal segments that are closer to the soma are less affected by the observer effect due to the capacitive "load" of the somatic membrane.

437 (C) Representative simulated recordings from the soma and different axonal sites and confocal images of the simulated
438 recording site (same cell as in panel A). Corresponding somatic distances and local capacitances are indicated on the top.
439 Asterisks mark the recording positions in the simulations. Scale bar=10 µm.

(D) The filtering effect showed only weak correlation with the local axonal capacitance (n = 941 simulated recordings,  $R^2$ = 0.13, linear fit). Circles represent the filtering effect at independent measurement sites along the same axon. Note the

441 = 0.13, linear fit). Circles represent the filtering effect at independent measurement sites along the same axon. Note the
 442 logarithmic scale of the x-axis.

(E) The observer effect showed significant correlation with local axonal capacitance (n = 941 simulated recordings,  $R^2 = 0.75$ , fitted with power function).

(F) Correlation between the total measurement error and the local axonal capacitance (n = 941 simulated recordings,  $R^2 = 0.68$ , fitted with power function).

447

# 448 **Discussion**

Here we developed a measurement-based, highly realistic model representation of the recording instrument that faithfully replicates actual patch-clamp recordings when combined with the detailed morphological reconstruction of the recorded structure. Simulation of the complete experimental condition allows for eliminating the instrumental distortions that are inevitably contaminates signals from small neuronal processes, such as axons. This realistic model also enabled us to determine the extent and sources of perturbations that contaminate electrophysiological signals. The results showed that physical parameters of the measuring instrument and the local biophysical properties of the recorded structure and their quantifiable interactions define the errors in voltage

456 measurements. Consequently, signal deterioration potentially arise from the altered local signal generation instead457 of pipette filtering in small axonal recordings.

The core hypothesis behind our study is that realistic in silico representation of recording instruments together 458 with the detailed morphology and biophysics of the recorded structure provide a better understanding of signal 459 distortions present in direct voltage recordings and offers an applicable offline approach to predict native signals 460 from distorted recordings. The combined simulation of the experimental conditions and the morphology was 461 proved previously to be an ideal tool to describe technical limitations associated with VC measurements and to 462 correct the recorded signals from those distortions (Beaulieu-Laroche & Harnett, 2018; Major et al., 1994; 463 Schaefer, Helmstaedter, Sakmann, & Korngreen, 2003; Silver, Traynelis, & Cull-Candy, 1992; Spruston, Jaffe, 464 Williams, & Johnston, 1993). However, these simulations have not included the complete recording instruments, 465 which are known to impose significant distortions on the recorded signals, especially when the biological source 466 is physically small, such as small axons. Other efforts corrected distortions of measured voltage signals by 467 estimating the transfer functions of the specific recording instrument (Brette et al., 2008; Jayant et al., 2017; 468 Magistretti, Mantegazza, de Curtis, & Wanke, 1998). Although such formulations are computationally efficient. 469 they could not be applied to the variable individual contribution of circuit components (e.g. pipettes, C<sub>pip</sub> and 470 R<sub>access</sub> compensatory elements), which imposes different signal distortions, such as filtering or instrumental 471 capacitive load. Here, we implemented the pipette and all amplifier elements as individual circuits as they were 472 actually built in the complete system and showed that the idealized instrument is sufficient to replicate the 473 behavior of the complete measuring instrument and its compensatory capabilities (Figures 1, 2 and 3). Thus, we 474 assume that implementing these components will allow adapting the model to other amplifier types. One of the 475 unexpected findings of our study is the uneven capacitance distribution of recording pipettes (Benndorf, 1995). 476 Majority of the total C<sub>pip</sub> originate from the first two and a half mm from the tip (Figure 3). The gradual increase 477 of relative wall thickness from the tip explains the larger contribution of the tip. Although the relative wall 478 thickness was found to be constant previously for borosilicate glass capillaries (Benndorf, 1995) we observed 479 decreased relative wall thickness toward the tip that explains the larger capacitive contribution of the tip. 480

To outline a feasible application, we utilized the complete instrumental model to correct the shape of APs directly 481 recorded from a small axon terminal of a hippocampal mossy fiber. The size of this bouton (largest diameter: 0.7 482 µm) was in the range of typical cortical axon terminals and was much smaller than the famous large mossy fiber 483 terminals. The complete instrumental model in combination with the realistic axonal morphology and biophysics 484 faithfully replicated the measured voltage signals (Figures 4, 5 and 6), including the signal artefacts and distorted 485 fast APs. The simulation resulted in ionic currents and conductances that matched with previous results obtained 486 with direct MF recordings from large boutons (Figure 4E and F) (H. Alle et al., 2011; Henrik Alle et al., 2009; 487 488 Geiger & Jonas, 2000). Consequently, the retrieved native axonal APs were brief events with large amplitude (Figures 4, 5 and 6) whose shape closely resembled to the spike waveforms reported for the large axon terminals 489 of the same axon (Henrik Alle et al., 2009; Geiger & Jonas, 2000). The simple Hodgkin-Huxley type conductance 490 models with six free parameters were sufficient to restore the experimentally recorded MF AP waveforms. 491 Although APs in the distal MFs can be described with a similar standard Hodgkin-Huxley type gating (Engel & 492 Jonas, 2005; Ohura & Kamiya, 2018), AP simulation in other neuron types or in other subcellular elements 493 required more detailed kinetic schemes (Stefan Hallermann et al., 2012; Ritzau-Jost et al., 2014; Ritzau-Jost et 494 al., 2021; Schmidt-Hieber & Bischofberger, 2010). Therefore, implementation of more elaborated conductance 495 models and inclusion of additional conductances can further improve our simulations and adapt to multiple 496 activity regimes, such as the plasticity of AP shapes during sustained activity (Geiger & Jonas, 2000). 497

The complex model allowed us to dissect the sources of errors that contaminate recordings from small biological 498 structures. As previously described for small, electrotonically compact neurons (D'Angelo, De Filippi, Rossi, & 499 Taglietti, 1995; Goodman, Hall, Avery, & Lockery, 1998; Rohrbough & Broadie, 2002), we found that even with 500 careful capacitance neutralization, the capacitive load added by the recording instrument substantially altered the 501 intrinsic electrical behavior of the axon (Figures 4 and 5). Using a simplified neuronal representation, we 502 confirmed with that instrumental capacitance effectively attenuates the action potentials in small neuronal 503 structures (Figure 7) emphasizing again that C<sub>pip</sub> reduction can substantially improve the accuracy of the 504 measured voltage signal (Dudel, Hallermann, & Heckmann, 2000; Levis & Rae, 1993; Ogden & Stanfield, 1994; 505

Ritzau-Jost et al., 2021; Sakmann & Neher, 1983). Interestingly, we have shown that increase in the Raccess reduced 506 the instrumental impact on the cellular electrogenesis (probably due to effective electrical isolation of the neuronal 507 structure from the recording pipette) suggesting that high impedance recording can have also advantages when 508 experimental subject is small. The high impedance recordings may reduce the complexity of post hoc AP 509 reconstitution as in this case the predicted AP shape depends only on the pipette filtering (Javant et al., 2017). 510 One of the major findings of our study is that instrumental and cellular factors define the accuracy of CC 511 experiments not in isolation from each other, but their interaction is equally important. This was the most apparent 512 513 when we examined the cellular contribution of the overall measurement error along a reconstructed MF which forms varicosities with different diameter. Thus, the differently sized axon segments provides different local 514 biophysical conditions (Figure 8). In this arrangement, which is characteristic to all axons at a various degree 515 (i.e. the size of the terminals and axonal shaft varies), the observed inverse relationship between local capacitance 516 and the measurement error highlight the importance of structural details on direct axonal recordings. 517

A more general consideration is that the target-size-dependent effects are not specific to the axonal recordings. Experiments that target small cellular structures, whose electrical parameters are comparable to the capacitance introduced by the measuring instrument, are potentially subject to the distortions quantified in our study. The target-dependent measurement errors are not specific to the action potential firing either. In fact, the typically high conductance densities in axons (Hu & Jonas, 2014; Ritzau-Jost et al., 2014) can partly compensate for the observer effect. Depending on the local biophysical environment, the recording instruments can induce substantial observer error in dendritic membrane potential as well.

525

#### 526 Methods

Experimental procedures were made in accordance with the ethical guidelines of the Institute of Experimental
Medicine Protection of Research Subjects Committee (MÁB-7/2016, PE/EA/48-2/2020).

529

530 *Constraining the amplifier model* 

The model cell. Electrical components of the customized model cell (test#3 circuit, modified type 1U, Molecular 531 Devices) were connected through conductive metal slots taken from a circuit breadboard allowing the change of 532 circuit components without the need for soldering that would introduce variable stray capacitance (Supplementary 533 Figure 1). We used non-inductive, low-noise resistors: resistors either originally present in the 1U model cell, 534 10M $\Omega$  and 500 M $\Omega$ , or Ohmite SLIM-MOX10203 series, 20-100M $\Omega$ . Stray capacitance of each elements of the 535 test circuits (including the resistors and their slots) was characterized in VC mode by measuring the capacitive 536 load associated with the introduction of the given circuit element. All capacitors were considered ideal, that is, 537 without any resistive component. 538

*Boosting unit.* We implemented a simplified boosting unit (Sigworth, 1995) in which capacitors were fixed (100 pF and 120 pF) while resistors were directly fitted to reproduce the capacitive current response in the test#1 configuration. Late phase of the response profile (starting 24  $\mu$ s after the stimulus onset) has particular importance because artefacts in that temporal domain can contaminate measured biological signals, therefore, this part of the signal was heavily weighted (850x) during the adjustment of the boosting unit.

*VC capacitance compensation:* Both CPf and CPs circuits were designed as described previously (Sigworth,
1995).

Stray capacitance of the CC circuit. To optimize the circuitry of CC model, we performed measurements with test#3 circuit, where pipette parameters ( $10M\Omega$ , 2.8 pF) and the size of the cell-equivalent resistor ( $500 M\Omega$ ) were fixed, only cellular capacitance varied from 0.75 pF to 46.7 pF. We applied short current stimuli (-50 to -200 pA, 3 ms) to elicit voltage responses with the maximal attainable capacitance neutralization or without CPN. Traces recorded in the absence of CPN allowed us to characterize the total capacitive load of the CC circuitry. The model most accurately reproduced the real voltage responses when a 0.76 pF stray capacitance was added at the amplifier input node (C<sub>CC</sub> on Figure 1).

Capacitance neutralization (CPN). We implemented CPN in two steps. First, we added an idealized positive 553 feedback loop, where the compensation through the C<sub>ini</sub> can be modulated with the gain of an operational 554 amplifier. This simple circuit representation was sufficient to reproduce the neutralizing capability of the real 555 amplifier, that is, equal CPN settings resulted in the same level of compensation in the model as in the real 556 experiments. Next, we reproduced the characteristic CPN-related stimulus artefacts that are present in typical 557 current clamp measurements. We placed a resistor (R<sub>CPN</sub>) and an inductor (L<sub>CPN</sub>) to the CPN path (Figure 1) and 558 559 tuned their parameters by direct fitting of the model voltage responses to the experimental data (examples are 560 shown on Figure 2D).

561 *Bridge balance compensation (BB)*. To recreate the BB circuit, we created a reference signal from the command 562 equivalent to the voltage drop caused by 1 M $\Omega$  load resistance (Figure 1). Scaled version of that reference signal 563 was then subtracted from the pipette voltage for the correction.

*Bessel filters*. We added filters to the amplifier model to match of our actual biological recordings. We added an active linear filter consisting of two cascaded Sallen-Key filter stages (Figure 1). Filter parameters were set according to an available filter design tool (<u>https://www.analog.com/designtools/en/filterwizard/</u>) to produce output with four pole low-pass Bessel filter characteristics. All recordings were made with bypassed filtering mode and we applied 100 kHz lowpass filter throughout the simulations.

# 569 *Pipette parameter measurements*

We used typical borosilicate glass capillaries (BF150-75-10, Sutter Instruments, Novato, CA) to fabricate pipettes that are suitable for recordings from small axons. To implement these high impedance pipettes into the model we measured their actual parameters. First, we assessed the actual pipette capacitance as a function of the tip distance by dipping known part of the recording pipettes into the recording solution. Pipette position was measured by the x axis values of the motorized micromanipulator (SM5 controller with Mini unit, Luigs und Neumann, Ratingen, Germany). First, we recorded the total capacitance of the instrumentation in open circuit VC mode when the pipette was out of the solution. Then, we gently moved the pipette to a position where the tip intermittently

reached the surface of the fluid characterized by the appearance of short conductive periods in the recorded VC signal. Then, the pipette was pushed forward to the solution to reach a position where the conductive state became stable (typically  $<5 \,\mu$ m forward movement). Starting from this tip position point, we systematically increased the length of the dipped part and quantified the capacitance in VC by integrating the first 50 µs of the transient response to a -20 mV voltage step. Integrated area was divided by the voltage step amplitude to convert the electric charge to capacitance.

To measure distribution of resistance along the pipettes, we broke off a known length of the pipette and measured the resistance of the remaining part in VC mode. First, we moved the pipette tip to a defined position under the objective and recorded its resistance. After withdrawal of the pipette, we broke the tip by gently touching it with a piece of lens cleaning tissue. The newly formed pipette tip was then positioned back to the reference position on the image. We determined the length of the broken pipette parts by reading the difference of the positioning motor. Resistance was measured in VC mode using -2 to -20 mV steps. We repeated the breaking process for each pipettes several times (1x-8x, using 22 pipettes in total).

We visualized the outer/inner diameter ratio ( $R_{OI}$ ) of the recording pipettes using a grinding system that gradually 590 cut them in half. This measurement allowed to avoid the optical distortions caused by the lens effect of the 591 cylindrical glass. The recording pipettes (the first 8-12 mm from the tip) were embedded into epoxy resin on a 592 microscope slide. Pipettes were longitudinally grinded with a coarse-grained aluminium-oxide abrasive disc (grit 593 size=600) until we reached the surface of the pipettes. Then, the grinding was occasionally interrupted to check 594 the surface and cross-section of the pipette under a transmitted light microscope (Leica DM2500 microscope, 5X-595 100X magnifications). As the plane of the pipette tip was approached, we switched to fine-grained abrasive discs 596 (grit size=6000). The images obtained from different cross section levels were then used to measure the pipette 597 diameters (Adobe Photoshop 5.0). The diameter data were included only from those focal planes for distinct 598 segments of the pipette tips, where the outer diameter was the largest and the relative wall thickness was the 599 smallest. We assumed infinite pipette wall resistivity in the model. 600

# 601 *Slice preparation and electrophysiology*

Hippocampal slice was prepared from a 29 days old Wistar rat as previously described (Brunner & Szabadics, 602 2016). In brief, the animal was deeply anaesthetized with isoflurane. After decapitation, the 350 µm thick slice 603 was cut with Leica VT1200S vibratome in ice-cold cutting solution (85 mM NaCl, 75 mM sucrose, 2.5 mM KCl, 604 25 mM glucose, 1.25 mM NaH<sub>2</sub>PO<sub>4</sub>, 4 mM MgCl<sub>2</sub>, 0.5 mM CaCl<sub>2</sub>, and 24 mM NaHCO<sub>3</sub>) in an orientation 605 optimized to preserve the mossy fibre tract in the hippocampal CA3 area (Bischofberger, Engel, Li, Geiger, & 606 Jonas, 2006). The slice was incubated at 32 °C for 60 minutes after sectioning, and was stored at room temperature 607 until the experiment. The recording solution was composed of 126 mM NaCl, 2.5 mM KCl, 26 mM NaHCO<sub>3</sub>, 2 608 mM CaCl<sub>2</sub>, 2 mM MgCl<sub>2</sub>, 1.25 mM NaH<sub>2</sub>PO<sub>4</sub>, and 10 mM glucose (equilibrated with 95% O<sub>2</sub> and 5% CO<sub>2</sub> gas 609 mixture). The pipette was filled with an intracellular solution containing 90 mM K-gluconate, 43.5 mM KCl, 1.8 610 mM NaCl, 1.7 mM MgCl<sub>2</sub>, 0.05 mM EGTA, 10 mM HEPES, 2 mM Mg-ATP, 0.4 mM Na<sub>2</sub>-GTP, 10 mM 611 phosphocreatine, 8 mM biocytin and 20 µM Alexa Fluor 594 hydrazide (pH=7.25). The recordings were 612 performed at 35 °C. For patching, axon was visualized with an upright IR-DIC microscope (Eclipse FN-1; Nikon) 613 equipped with high-numeric aperture objective (Nikon 1.1 NA, Apo LWD 25 W), oil condenser (Nikon D-CUO 614 DIC Oil Condenser, 1.4 NA) and a sCMOS camera (Andor Zyla 5.5). After the recordings the Alexa Fluor 594-615 labelled structure was visualized in situ using a confocal system (Nikon Eclipse C1 Plus). Then, the slice was 616 fixed for further morphological experiments (see below). 617

To record from the individual small MF terminal, we searched for visually identifiable axonal structures under 618 the guidance of the DIC optics in the *stratum lucidum* of the CA3 area, whose size was smaller than those of the 619 typical large mossy fiber boutons. The patch pipette was pulled from borosilicate glass capillary (inner diameter: 620 0.75 mm, outer diameter: 1.5 mm, Sutter Inc.). After the seal formation, we manually carefully compensated the 621 C<sub>pip</sub> in VC mode. Compensated capacitive responses to -20 mV step command were then recorded and the average 622 of 164 sweeps served as target for tuning the C<sub>pip</sub> in the model. After establishing the whole-cell configuration by 623 applying sudden negative pressure, we switched to CC mode to record the passive and active membrane responses 624 from the axon with different CPN compensation. All recordings were collected with a MultiClamp 700B amplifier 625

(Molecular Devices) without filtering (filter bypassed) and digitized with Digidata1440 A/D board (Molecular Devices) at 250 kHz sampling rate using the pClamp10 software package (Molecular Devices). At the end of the experiment, we collected preliminary morphological data by imaging the Alexa Fluor 594 signal with the confocal system. The obtained z stack image was then used to confirm the MF identity (evidenced by the presence of a large MF terminal along the recorded axon, Figure 4B) and for the documentation of the recording position.

# 631 3D morphological reconstruction

- After the recording, slice was fixed overnight at 4°C in 0.1 mM phosphate buffer containing 2% PFA and 0.1%
- 633 picric acid. The slice was then re-sectioned (to 60 μm) and the sections were incubated overnight with Alexa
- Fluor 594-conjugated streptavidin in 0.5% Triton X-100 and 2% normal horse serum to reveal the biocytin signal.
- To investigate the detailed morphology, the recorded axon was imaged with a confocal system (60X objective,
- 636 Plan Apo VC, NA=1.45, Nikon C2, x-y pixel size:0.08-0.1 μm, z-step: 0.1-0.15 μm). High resolution
- reconstructions were done automatically by the Vaa3D software (Peng, Bria, Zhou, Iannello, & Long, 2014; Peng,
  Ruan, Long, Simpson, & Myers, 2010; Peng, Tang, et al., 2014).
- 639 Implementation of the seal in the model
- The seal was represented as a single resistor ( $R_{seal}$ ) connected in parallel to the cell. To estimate the  $R_{seal}$  in the axonal recording, first we calculated the ratio ( $R_{ratio}$ ) between the cellular input resistance ( $R_{cell}$ ) and the  $R_{seal}$ based on the voltage shift produced by the shunt conductance of seal (Perkins, 2006):

$$V_{\text{measured}}/V_{\text{rest}} = R_{\text{ratio}}/(1 + R_{\text{ratio}})$$

644 where  $V_{\text{measured}}$  is the recorded voltage,  $V_{\text{rest}}$  is the native resting membrane potential.  $R_{\text{seal}}$  and  $R_{\text{cell}}$  were then 645 calculated from the measured input resistance ( $R_{\text{in,measured}}$ ) and from the  $R_{\text{ratio}}$  using the equations:

$$1/R_{cell} = 1/R_{in,measured} - 1/R_{seal}$$

647 where:

$$R_{seal} = ratio * R_{cell}$$

649 The apparent resting membrane potential of the recorded MF axon was -75.2 mV, close to the resting membrane potential previously reported for the somata and axons of granule cells (~ -80 mV (Brunner & Szabadics, 2016; 650 Martinello, Giacalone, Migliore, Brown, & Shah, 2019; Ruiz, Campanac, Scott, Rusakov, & Kullmann, 2010; 651 Schmidt-Hieber, Jonas, & Bischofberger, 2004; Staley, Otis, & Mody, 1992)). This moderate shift, caused by the 652 leak through the seal, suggests orders of magnitude larger R<sub>seal</sub> compared to the axonal input resistance. Indeed, 653 we calculated 65.64 G $\Omega$  R<sub>seal</sub> and 3.94 G $\Omega$  R<sub>cell</sub> for the recording assuming -80 mV resting membrane potential. 654 Accordingly, we applied 65.64 GQ Rseal in the AP reconstitution model (Figures 4, 5 and 6), while Rseal was set 655 to 50 G $\Omega$  in all other simulations. To compensate for the seal-induced depolarizing voltage shift, baseline 656 membrane potential in the model was adjusted by constant current injection to match those of the experimental 657 data. 658

## 659 *General simulation parameters*

660 Cellular membrane parameters were assumed to be spatially uniform, unless stated otherwise. Potassium and 661 sodium equilibrium potentials were set to -77 mV and +70 mV, respectively and we assumed -80 mV reversal 662 potential for the leak conductance in active models. Simulations ran with 4 µs and 0.5 µs temporal resolution, in 663 CC mode and in VC mode, respectively.

# 664 *Fitting procedures*

We fitted the model responses to the experimental data to minimize the sum of squared error between them using the Brent's PRAXIS optimization algorithm embedded in NEURON. For  $C_{pip}$  estimation, a 5 ms long trace was considered with 2.5 ms baseline before the stimulus. For passive parameter estimations, we weighted the voltage response evoked by short current stimulus (25.8 ms from the stimulus onset, 3X) in order to equalize the contribution of short- and long pulse responses to the total error. For AP reconstruction, fitting interval started with 2.6 ms long baseline period before the stimulus onset. The actual APs were weighted eight-fold, starting 0.5 ms before the peak. The optimization ended 1.5 ms following the AP peak to avoid the contamination of the

parameter estimation with afterdepolarization related mechanisms not implicated in the model (Martinello et al.,

673 2019; Ohura & Kamiya, 2018).

We used sodium and potassium conductance mechanisms with canonical Hodgkin-Huxley gating scheme, in 674 675 which not only the density can be freely adjusted but also the kinetics and the voltage dependence of the two types of conductance. For this, we modified the built-in Hodgkin-Huxley mechanisms of NEURON by 676 introducing rate-scaling factors (scNa and scK) to adjust the speed of model channel operation. The originally 677 implemented temperature scaling was removed from the mechanisms. In addition, we used global voltage shifts 678 (vsNa and vsK) to modulate the voltage dependence of the channels. Altogether, free parameters (gmaxNa, gmaxK, 679 scNa, scK, vsNa, vsK) were constrained to obtain an ideal model of the AP waveform measured in our various 680 experimental settings. Because the Raccess can change during the recordings, this parameter was set individually 681 for each target trace. Optimization of the individual AP fits was initiated from four parameter sets that allows 682 exploration substantial part of the parameter space (Supplementary Figure 3A). The parallelized codes for AP 683 reconstitution were run on the Comet supercomputer through the Neuroscience Gateway portal (Sivagnanam et 684 al., 2013). To assess the quality of individual fits, their mean squared error was normalized to the baseline variance 685 of the actual target trace. Of the results of the four parallel optimizations, the solution where the normalized error 686 was the smallest was accepted as the best fit. Fit was rejected when the normalized error was larger than 10. 687 Fitting of 2 of the original 90 target APs did not resulted in solutions, which met this criterion. These APs were 688 excluded from the analysis (both were obtained with 7.386 pF CPN). 689

690

# 691 Assessments of the reliability of optimizations

692 *In silico* reconstruction of the complete experiment consisted of subsequent optimization steps (Supplementray 693 Figure 2A). First, we used VC data to set actual pipette parameters (1). After adding the model instrumentation 694 and the detailed morphology of the recorded structure to the model, we tuned the passive cellular parameters 695 together with the  $R_{access}$  (2). Next, we equipped the model structure with active sodium and potassium

- conductances and adjusted their properties to match model responses the experimentally recorded AP waveform
  (3). Finally, having established the appropriate conductance sets, we obtained the native behavior of the axon (4).
  The reliability of the fitting procedures were tested with artificial traces with Gaussian noise.
- To assess the accuracy of  $C_{tot}$  estimation, we generated target traces by simulating on-cell VC experiments. The model always recovered correct  $C_{tot}$  value (proportion of fitting estimations within 10% error to the correct value:
- 100 %, n=990 optimizations, Supplementary Figure 2A and B) irrespective to the C<sub>tot</sub> (5.8-13.7 pF) and noise
- level (SD=0-35.3 pA) of the targets, which confirms the high sensitivity of VC based C<sub>pip</sub> estimation.
- To test the reliability of cellular passive parameter and R<sub>access</sub> prediction, we created a hypothetical axon with 703 biologically plausible diameter distribution (log-normal distribution with mean of 0.6 µm and variance of 0.4 704 um<sup>2</sup>). We attached the model axon to the pipette and generated hypothetical CC measurements with long and 705 short current stimuli ( $C_m$  range: 0.5 - 1.5 uF/cm<sup>2</sup>,  $R_m$  range: 10 - 100 k $\Omega/cm^2$ ,  $R_i$  range: 50 - 250  $\Omega^*$ cm,  $R_{access}$ : 50 706 - 400 MΩ, noise SD = 1.73 mV). We fitted these synthetic targets from a single initiation parameter set ( $C_m$ : 1 707 pF/cm<sup>2</sup>, R<sub>m</sub>: 50 k $\Omega$ /cm<sup>2</sup>, R<sub>i</sub>: 150  $\Omega$ \*cm, R<sub>access</sub>: 150 M $\Omega$ ). 75 % of optimizations resulted in acceptable results, 708 that is, the fit error was less than 10-times the baseline variance of its target. In those successfully fitted cases the 709 predicted parameters were close to their predefined values (proportion of fitting estimations within 10% error to 710 the correct value: C<sub>m</sub>: 90.83 %, R<sub>m</sub>: 97.66 %, R<sub>i</sub>: 81.88 %, R<sub>access</sub>: 82.3 % n= 469 optimizations, Supplementary 711 Figure 2C). 712
- We also verified the reliability of the prediction of native AP shapes in independent simulations (Supplementary Figure 2D and E). For this we generated diverse AP waveforms using independent, sophisticated sodium and potassium conductance mechanisms (using 8-state kinetic schemes obtained from (Stefan Hallermann et al., 2012; Schmidt-Hieber & Bischofberger, 2010) in a single compartment neuron ( $R_{access}$ =100 MΩ,  $C_{pip}$ =6.74 pF, BB compensation=100 MΩ, CPN compensation= 6.85 pF,  $R_{seal}$ =50 GΩ, noise SD: 0.45 mV). Our standard fitting routine reliably retrieved the shapes of APs.
- 719 Systematic errors in model predictions

We also examined the potential impact of systematic error sources on model predictions. Such potential error can 720 originate from inaccuracies of the morphological reconstruction. Post hoc anatomical processing can result in 721 considerable tissue shrinkage. Additionally, diameter of thin axonal processes is close to the resolution limit of 722 light microscopy. To evaluate the potential effects of inaccurate anatomical representation of the recorded axon, 723 we artificially altered the reconstructed morphologies and tested how the recovered native APs were affected. 724 The axonal diameters were either homogeneously increased by 160 nm or reduced by 180 nm (axons were not 725 allowed to shrink below 100 nm). As expected, recovered passive parameters and active conductance densities 726 727 scaled with the diameter to compensate for the altered morphological dimensions (Table 1). However, as the model re-adjusted the local electrical environment by scaling the membrane properties, the predicted intra-axonal 728 and native AP waveforms remained remarkably similar in spite of the large changes in the morphology and 729 passive membrane parameter. 730

 $R_{seal}$  provides an additional error source because its calculation depends on the native resting membrane potential, which can not be assessed directly (i.e. measurements start in cell attached mode). Therefore, we defined the theoretical lower limit for the R<sub>seal</sub> in the direct axonal recording; when native resting membrane potential equals with the potassium equilibrium potential (-93 mV with the solutions used in the experiment) R<sub>seal</sub> would be only 20.58 GΩ. Re-optimization of the model using this small R<sub>seal</sub> caused only minor alterations in the predicted conductances and AP parameters (reduced R<sub>seal</sub> model, Table 1). Altogether, these control simulations suggest that potential systematic errors have marginal impact on the primary results of the manuscript.

		standard model	reduced Rseal	thick morphology	thin morphology
		mouer	Tystai	morphology	morphology
Passive parameters	$\mathbf{R}_{\mathbf{m}}(\mathbf{k}\Omega/\mathbf{cm}^2)$	60.01	72.92	62.97	38.88
	$C_m(\mu F/cm^2)$	0.65	0.62	0.62	0.99
	$\mathbf{R}_{i}(\Omega^{*}\mathrm{cm})$	147.3	141.54	208.08	56.78
	normalized error	2.96	3.05	2.95	3.18
	L		·		
active conductances for APs recorded with CPN=6.5 pF	gNa(mS/cm <sup>2</sup> )	159.02±1.73	160.24±2.1	150.24±1.86	229.79±3.57
	$gK(mS/cm^2)$	5.83±0.46	5.46±0.04	5.33±0.04	12.74±0.56
	normalized error	5.2±0.16	5.09±0.16	5.22±0.16	5.72±0.19
active conductances for APs recorded with CPN=7 pF	gNa(mS/cm <sup>2</sup> )	151.7±0.95	150.29±1.06	142.27±0.97	232.6±1.5
	$gK(mS/cm^2)$	5.41±0.03	5.08±0.03	5.08±0.03	9.23±0.08
	normalized error	5.89±0.17	5.92±0.17	6.36±0.18	6.04±0.19
active conductances for APs recorded with CPN=7.386 pF	gNa(mS/cm <sup>2</sup> )	160.03±1.47	142.26±1.17	144.38±1.23	249.13±2.44
	$gK(mS/cm^2)$	6.32±0.09	6.08±0.44	5.87±0.07	11.24±0.146
	normalized error	6.8±0.28	8.22±0.34	8.1±0.3	7.35±0.3
n=30 AP reconstitution	L	·	· · ·		
AP parameters (reconstructed measurement)	dV/dt <sub>max</sub> (mV/ms)	363.26±0.93	369.87±6.04	$354.99 \pm 0.8$	372.7±0.96
	peak(mV)	9.01±0.12	9.01±0.49	8.98±0.12	9.24±0.12
	threshold(mV)	$-45.28 \pm 0.07$	-45.29±0.06	-45.17±0.07	-45.69±0.06
	half-width(ms)	$0.52{\pm}0.002$	0.52±0.004	$0.51 \pm 0.002$	0.52±0.002
AP parameters (local in the axon)	dV/dt <sub>max</sub> (mV/ms)	453.11±2.54	453.82±2.53	450.44±2.34	481.59±3.06
	peak(mV)	21.96±0.12	21.23±0.12	22.13±0.12	22.34±0.11
	threshold(mV)	$-35.88 \pm 0.09$	-35.92±0.09	$-36.01 \pm 0.09$	-36.97±0.09
	half-width(ms)	$0.48 \pm 0.002$	0.49±0.002	$0.48 \pm 0.002$	0.49±0.002
AP parameters (native, I-step evoked)	dV/dt <sub>max</sub> (mV/ms)	1064.81±5.1	1111.03±5.76	865.03±4.65	914.95±6.32
	peak(mV)	46.85±0.09	47.34±0.09	40.06±0.12	40.26±0.15
	threshold(mV)	-37.36±0.09	-37.64±0.09	$-35.93{\pm}0.09$	-36.7±0.09
	half-width(ms)	$0.33 \pm 0.002$	0.33±0.002	$0.33 \pm 0.002$	0.34±0.002
AP parameters (native, propagating)	dV/dt <sub>max</sub> (mV/ms)	1605.96±9.75	1671.34±10.82	1609.7±10.18	1549.38±12.2
	peak(mV)	64.21±0.07	64.71±0.07	64.16±0.08	63.29±0.11
	AP width @-10 mV (ms)	0.36±0.002	0.35±0.002	0.36±0.002	0.36±0.002
	propagation velocity(ms)	0.45±0.001	0.48±0.002	0.46±0.002	0.43±0.002

739 Table 1. Summary of parameters obtained from different model configurations

740

741 Simulations to explore the correlations between signal distortions and recording conditions (Figure 7)

742 We used a single compartment with fixed  $10 \,\mu\text{m}^2$  surface area to represent neuronal structure in these simulations.

Electrical behavior of small and larger cells was set by scaling the active and passive biophysical parameters of

the compartment (for small cell:  $C_m = 10 \ \mu F/cm^2$ ,  $R_m = 2 \ k\Omega/cm^2$ ,  $g_{Na}$  density=1.5 S/cm<sup>2</sup>,  $g_K$  density=0.4 S/cm<sup>2</sup>; for

145 larger cell: C<sub>m</sub>=100 μF/cm<sup>2</sup>, R<sub>m</sub>=0.2 kΩ/cm<sup>2</sup>, g<sub>Na</sub> density=15 S/cm<sup>2</sup>, g<sub>K</sub> density=4 S/cm<sup>2</sup>). To keep R<sub>seal</sub>/R<sub>cell</sub> ratio
146 constant between the two conditions, R<sub>seal</sub> was set to 50 GΩ and 5 GΩ, for small and larger cell, respectively.
147 The pipette capacitance was fixed to 6.74 pF while R<sub>access</sub> was systematically varied in the range of 1-200 MΩ.
148 To mimic optimal recording configuration, the applied CPN settings (6.8 pF) closely matched with C<sub>pip</sub>. APs were
149 elicited with 3 ms long current stimuli (30 pA and 160 pA for small and larger cell, respectively).

750 Simulations to explore the correlations between signal distortions and axonal morphology (Figure 8)

The detailed morphology of a somatically labeled granule cell was imported to the NEURON. Dendritic spines 751 were implemented by scaling two-fold the C<sub>m</sub> and the leak conductance in dendrites. Passive parameters (R<sub>i</sub>:150 752  $\Omega^*$ cm, C<sub>m</sub>:1 µF/cm<sup>2</sup>, R<sub>m</sub>:50 k $\Omega$ /cm<sup>2</sup>) were constant otherwise. Active conductances (g<sub>Na</sub> density=300 mS/cm<sup>2</sup>), 753  $g_{K}$  density=15 mS/cm<sup>2</sup>) were homogenously distributed along the cell, except the initial part of the axon where 754 we applied higher channel densities ( $g_{Na}$  density=1200 mS/cm<sup>2</sup>,  $g_K$  density=75 mS/cm<sup>2</sup>) with left-shifted 755 activation and inactivation (10 mV in the hyperpolarized direction). To explore the distortions in axonal AP 756 recordings, position of recording electrode ( $C_{tot}=6.74 \text{ pF}$ ,  $R_{access}=60 \text{ M}\Omega$ ,  $R_{seal}=50 \text{ G}\Omega$ , applied CPN=6.8 pF) was 757 systematically changed along the main axon (n=942 recording positions). APs were evoked by 3 ms long current 758 stimuli at each recording position. Amplitude of the injected current was automatically adjusted to evoke APs 759  $\sim$ 1.5 ms (1.33 ± 0.01 ms delay, n=942 APs) after stimulus onset. Local capacitance was determined for each 760 recording position using idealized VC simulations in the absence of experimental instrumentation (built-in 761 SEClamp mechanism with 10 M $\Omega$  series resistance). For quantification, we integrated the first 100  $\mu$ s of the 762 763 transient capacitive response to -20 mV voltage step. The resulted charge was divided by the voltage step amplitude. 764

765 *Data analysis and statistics* 

AP threshold was determined as membrane voltage where depolarization rate exceeded 20 mV/ms. AP amplitude was calculated as the voltage difference between the absolute peak potential and the threshold. AP half-width was

- defined as the spike duration at half of its amplitude. AP conduction velocity was determined by measuring the
   temporal difference between AP peaks at the initiation and at the recording site.
- 770 Data were analyzed using pClamp (Molecular Devices), OriginPro (OriginLab) and Excel (Microsoft) Photoshop

(Adobe) and custom written NEURON or Python scripts. The relevant NEURON codes are available on GitHub

772 (<u>https://github.com/brunnerjanos/amplifier-model</u>). Voltage values are presented without correction for the liquid

- junction potential. Normality of the data was assessed with Shapiro-Wilks test. Population data are presented as
- mean  $\pm$  s.e.m.
- 775

# 776 Acknowledgements

- 777 This work was carried out with the full support of János Szabadics' laboratory. We are grateful to János Szabadics
- for his continuous support, advices on the project and constructive comments on the manuscript. This work was
- funded by ERC-CoG 772452 (nanoAXON) grant to János Szabadics and the János Bolyai Research Fellowship
- of the Hungarian Academy of Sciences (to JB). We are thankful for the computational resources provided by the
- 781 Neuroscience Gateway. We thank László Barna, the Nikon Microscopy Center at the Institute of Experimental
- 782 Medicine, Nikon Europe B.V., Nikon Austria GmbH, and Auro-Science Consulting Ltd, for kindly providing
- 783 microscopy support and Dóra Kókay and Andrea Szabó for technical assistance.
- 784

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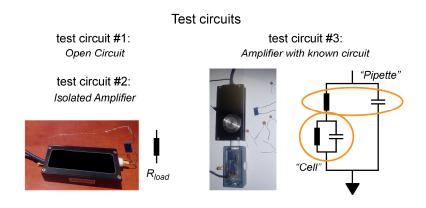
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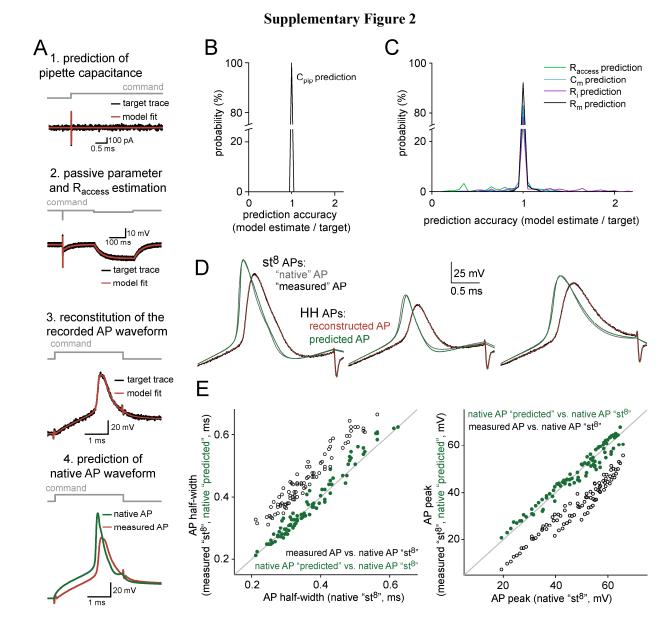
## **Supplementary Figure 1**





939

940 Supporting data for Figures 1 and 2. Test circuits used for the characterization of the circuit components





944 Figure S2. Supporting data for Figure 4. Parameter extraction from recorded VC and CC data

945 (A) Outline of the consecutive optimization steps that were used to retrieve the instrumental parameters.

946 (B) Distribution of the relative error in C<sub>pip</sub> estimations.

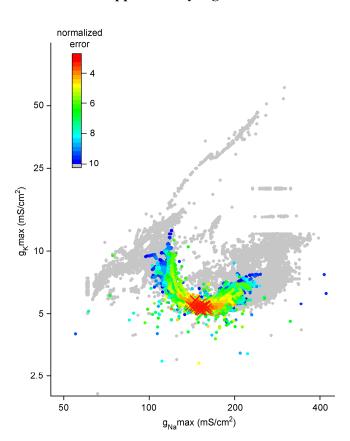
947 (C) Distribution of the relative errors present in the R<sub>access</sub> and passive parameter estimations.

948 (D) Overlay of representative APs (native and measured, gray and black traces, respectively) generated using 8-state active

949 conductance models and corresponding best-fit APs generated with the standard conductances used in our final model950 (reconstructed and predicted, red and green traces, respectively).

951 (E) Comparison of measured AP half-width and peak values (black) and the corresponding predicted native parameters
952 (green) with the original value (n=90 simulated experiments). The line indicates equality.

#### Supplementary Figure 3



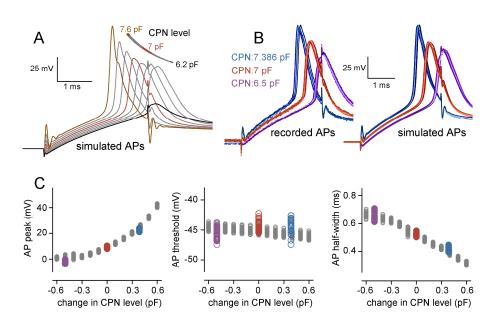
#### 954

# 955 Supporting data for Figure 4. Uniqueness of the fit results

956 The explored parameter space during the optimization of the conductances needed to reconstruct the recorded APs (30 fitted

APs started from 120 initializations). Each dot represent single run during the fit (n=142605 runs). The optimization error
of the each run is color coded. Red crosses mark best-fit solutions.

#### **Supplementary Figure 4**



#### 960

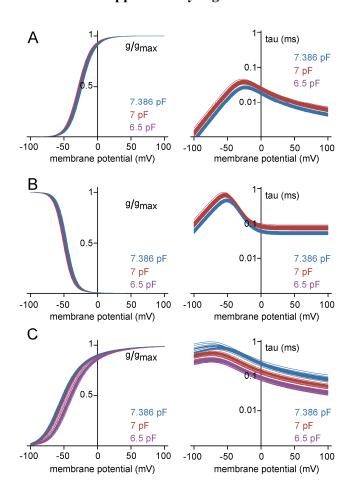
# 961 Supporting data for Figure 5. Critical influence of the applied CPN on the recorded AP waveforms

962 (A) Model AP waveforms simulated using the same conductance set but different CPN settings. Notice the AP failure at
963 CPN=6.2 pF (black) and the oscillation at CPN=7.6 pF (brown).

964 (B) Representative APs recorded (left) and simulated (right) in the same axon with different CPN settings (n=6 APs in each965 CPN conditions).

966 (C) Effects of different CPN level on AP peak (left), threshold (middle) and half-width (right). Gray circles show the AP
967 parameters simulated with the 30 different conductance sets (the same set as in Figure 4). Purple, red and blue symbols
968 show the experimentally recorded AP parameters obtained with three different CPN settings (n=30 APs in each conditions).
969 Zero on x-axis represents the originally set 7 pF capacitance neutralization.

# Supplementary Figure 5

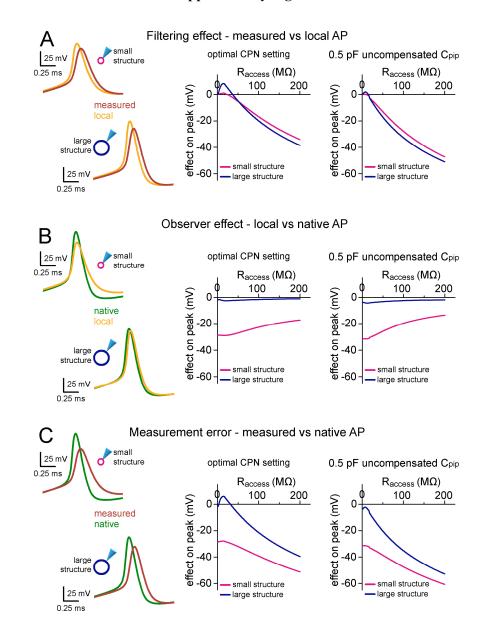


#### 971

# 972 Supporting data for Figure 5. Gating profile of model conductances obtained from fitting of AP waveforms with 973 different levels of distortions

- 974 (A) Voltage dependence (left) and kinetic profile (right) of the activation in Na<sup>+</sup> conductance models obtained by the 975 reconstruction of the APs recorded with different CPN settings (CPN = 6.5 pF in purple, CPN = 7 pF in red and CPN = 976 7.386 pF in blue). Each line represent single model conductance (n=30/30/28 models).
- 977 (B) Same as in panel (A) but for the inactivation of the Na<sup>+</sup> conductance models.
- 978 (C) Same as in panel (A) but for the K<sup>+</sup> conductance models

#### **Supplementary Figure 6**



980

979

#### 981 Supporting data for Figure 7. Instrumental and structural parameters cooperatively determine signal distortions in

# 982 recordings from small neuronal structures

983 The results of the same simulations as in Figure 7, are shown for effects on AP peak.