

<b>Model for ring closure in ER tubular network dynamics</b>	1
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<b>Abstract</b>	10
Tubular networks of endoplasmic reticulum (ER) are dynamic structures whose steady-state	11
conformations are maintained by a dynamic balance between the persistent generation and	12
vanishing of the network elements. While factors producing the ER tubules and inter-tubular	13
junctions have been investigated, the mechanisms behind their elimination remained unknown.	14
Here we addressed the ER ring closure, the process resulting in the tubule and junction removal	15
through constriction of the network unit-cells into junctional knots followed by the knot	16
remodeling into regular junctions. We considered the ring closure to be driven by the tension	17
existing in ER membranes. We modeled, computationally, the structures of the junctional knots	18
containing internal nanopores and analyzed their tension dependence. We predicted an effective	19
interaction between the nanopores facilitating the knot tightening and collapse of additional	20
network unit cells. We analyzed the process of the pore sealing through membrane fission	21
resulting in formation of regular junctions. Considering the hemi-fission as the rate-limiting	22
stage of the fission reaction, we evaluated the membrane tensions guarantying the spontaneous	23
character of the pore sealing. We concluded that feasible membrane tensions explain all stages of	24
the ER ring closure.	25
	26

# Introduction

Endoplasmic reticulum (ER) is one of the most vital membrane bound organelles of eukaryotic cells serving as a platform for protein synthesis, folding, modification and transport to intracellular destination(Alberts et al., 2017, chap. 12). The ER functions determine its structure consisting of the double-membrane nuclear envelope, and the peripheral ER, which spans most of the cytoplasm of mammalian cells(Westrate et al., 2015). The peripheral ER includes 30-50nm thick flat membrane sheets and a highly intricate network of membrane tubules with 25-90 nm diameters interconnected by three-way junctions(Schroeder et al., 2018; Terasaki, 2018; Voeltz et al., 2002; Westrate et al., 2015). In spite of their complex architecture and topological features, the membranes of all ER elements are interconnected into a continuous system that encloses a common luminal space.

Several decade-long studies by the methods of diffraction-limited optical(Lee and Chen, 1988; Terasaki et al., 1986), electron(Palade, 1956), and, more recently, super-resolution(Nixon-Abell et al., 2016; Schroeder et al., 2018) microscopies have revealed a multiscale character of the peripheral ER architecture exhibiting a macroscopic and nanoscopic levels of organization(Westrate et al., 2015). The ER nanoscopic structures described so far include ER tubular matrices(Nixon-Abell et al., 2016), sheet nanoholes(Schroeder et al., 2018), and ER to Golgi transport intermediates(Weigel et al., 2021), all characterized by an intrinsic length scale in the range between few tens and 100 nm. The nanoscopic structures appear to represent mechanically equilibrium membrane conformations. The macroscopic ER structures include stacks of micron-large sheets interconnected by helicoidal junctions(Terasaki et al., 2013), and irregular polygonal networks of tubules with a typical unit-cell size of several microns that are in the focus of this study.

The macroscopic tubular networks, exhibit an, essentially, non-equilibrium dynamic behavior, 50  
which includes continuous emerging and disappearance of junctions and tubules on the 51  
background of their perpetual motion(Lee and Chen, 1988). The junctions and tubules are 52  
generated through the new tubule branching off and fusion with the tubules already existing 53  
within the network(Dabora and Sheetz, 1988; Lee and Chen, 1988). This leads to formation of 54  
new network unit-cells. Disappearance of the junctions and tubules is mediated by the process 55  
referred to as the ring closure, whose essence is a contraction followed by vanishing of the 56  
network unit-cells(Lee and Chen, 1988; Powers et al., 2017). The contraction stage results in 57  
transformation of a polygonal unit-cell, regardless of its initial size, into a small “knot”, which 58  
replaces one of the initial inter-tubular junctions. In the following, we will refer to this structure 59  
as the junctional knot. Normally, a junctional knot transforms into a regular junction with no 60  
noticeable swelling or discontinuity(Lee and Chen, 1988), thus, completing the ring closure. In 61  
addition to the ring closure, a direct scission of ER tubules has been reported(Espadas et al., 62  
2019), but appears to happen too rarely to play a considerable role in the network 63  
dynamics(Wang et al., 2016). In spite of the persistent generation and disappearance of the 64  
network elements, the overall numbers of the junctions, tubules and unit-cells in the macroscopic 65  
tubular network do not change in time. The steady-state conformations of ER macroscopic 66  
networks are commonly attributed to the dynamic balance between the tubule branching-fusion 67  
and the ring closure events(Lee and Chen, 1988). 68

Understanding the physical mechanisms behind the dynamics of the macroscopic ER networks, 69  
requires knowledge of a minimal set of physical factors, which drive the competing processes of 70  
creation and disintegration of the network elements. Based on the *in vitro* studies(Wang and 71  
Rapoport, 2019) and live cell observations, there are three such factors. The proteins of the 72

reticulum/REEP families generate and stabilize ER tubules by producing the required membrane 73  
curvature(Hu et al., 2008). The Atlastin family proteins create the network junctions by 74  
mediating fusion of ER tubules(Powers et al., 2017). Pulling forces applied to the ER membranes 75  
by the cytoskeleton appear to be necessary, on one hand, for the tubular branching, mobility, and 76  
maintenance of the overall extended network conformations, and, on the other, for the ring 77  
closure and the related elimination of the network elements. This is supported by the 78  
observations that disassembly of the intracellular force-generating machinery based on 79  
microtubules and the associated molecular motors results in stopping all kinds of movement of 80  
the ER network elements including the unit-cell contraction and the related ring closure(Terasaki 81  
et al., 1986). Also the reconstituted ER tubular networks, which exhibited the major structural 82  
and dynamic features of the intra-cellular ER networks including the ring closure(Powers et al., 83  
2017; Wang and Rapoport, 2019), were, most probably, subjected to pulling forces originating 84  
from such factors as the network adhesion to the external substrate and the thermal convection of 85  
the surrounding liquid(15). 86

While micromechanics of the protein-mediated membrane curving and fusion involved in 87  
generation of the ER network elements have been thoroughly investigated(Wang et al., 2021; 88  
Wang and Rapoport, 2019), the physical mechanisms behind the disintegration of the network 89  
tubules and junctions through the ring closure have never been addressed and represent the subject 90  
of this work. 91

Here we analyze the formation of the junctional knots and their remodeling into regular junctions 92  
as the crucial stages of the ER ring closure. We propose that the major factor driving all steps of 93  
these processes is the membrane tension. We computationally determine the experimentally 94

inaccessible configurations of the junctional knots containing internal pores and resulting from 95  
constriction of one or multiple network unit-cells. We analyze fission of the hourglass-like 96  
membrane necks forming the pores rims, which mediates the pore sealing and constitutes the 97  
essence of the knot remodeling into the regular junctions. We consider the fission to proceed 98  
through an intermediate stage of hemi-fission representing the rate-limiting stage of the process. 99  
We compute the energy of the hemi-fission structure determining the energy barrier of the fission 100  
reaction and evaluate the tensions necessary to eliminate this barrier. 101

## Model 102 103

We consider the process of ring closure illustrated in (Fig. 1A-H) as consisting of two stages: 104  
constriction of an ER network unit cell into a junctional knot (Fig. 1A-D), and transformation of 105  
the latter into a regular junction (Fig.1 E-H). 106

We assume the unit-cell constriction (Fig.1 A-D) to be driven by the membrane tension. This is 107  
based on the known dynamic property of random networks of stressed lines interconnected by 108  
mobile three-way junctions(Stavans, 1993). A simple balance analysis of the tension-related 109  
forces acting on the network junctions shows that all polygonal unit-cells with less than six 110  
vertices (i.e. pentagonal, quadratic and triangular) are mechanically unstable and tend to collapse 111  
by constriction(Stavans, 1993). The computational simulations of such network behavior 112  
demonstrated the events of the unit cell constriction and other features of the ER network 113  
dynamics(Lin et al., 2017). Examples of such simulations are presented in (Supplementary 114

Movie). As follows from these and other simulations, polygonal unit-cells transform into  
equilateral triangular unit cells, which then undergo collapse into junctional knots (Fig.1 A-D).

Here we focus on the second stage of the ring closure (Fig.1 E-H), the remodeling of the  
junctional knots into regular junctions. The analysis is based on comparison of the elastic energy  
of the junctional knot membrane with that of the structures formed at the intermediate and final  
steps of the remodeling process.

We consider the junctional knot energy and the energy of the final regular junction to consist of  
two contributions: the energy of membrane bending,  $F_B$ , and the energy of membrane tension,  
 $F_T$ ,

$$F_E = F_B + F_T . \quad (1)$$

The bending energy,  $F_B$ , is associated with the shape of the membrane midplane that is characterized at  
each point by the mean,  $J$ , and Gaussian,  $K$ , curvatures (Spivak, 1999). We use Helfrich model of  
membrane bending elasticity (Helfrich, 1973) according to which the membrane material  
parameters setting the value of the bending energy are the spontaneous curvature,  $J_S$ , the bending  
modulus,  $\kappa$ , and the modulus of Gaussian curvature,  $\bar{\kappa}$  (Helfrich, 1973). The spontaneous  
curvature,  $J_S$ , which accounts for the intrinsic tendency of the membrane to acquire a bent shape  
and determines the intra-membrane torque, is generated for ER tubular membranes by the  
curvature generating proteins of the reticulon/REEP family and has values in the  $0.01 - 0.1 \text{ nm}^{-1}$   
range, as inferred from the measurements of the ER tubule diameters (Schroeder et al., 2018;  
Terasaki, 2018; Voeltz et al., 2002). The bending modulus,  $\kappa$ , which sets the scale of the  
bending energy, while varying in a certain range (Dimova, 2014), has a typical value of,  $\kappa \approx$

$10^{-19}$  Joule (Dimova, 2014). The modulus of Gaussian curvature,  $\bar{\kappa}$ , whose direct measurements 136  
have been, largely, prohibited by geometrical restrictions, is, typically, negative and has been 137  
estimated to have values in the range between 0 and  $-\kappa$  [see e.g. (Templer et al., 1998; Terzi et 138  
al., 2019)]. 139

The tension energy,  $F_T$ , is associated with the membrane area,  $A$ , and the system parameter 140  
setting the scale of this energy is the tension value,  $\gamma$ . 141

We define the system energy as the thermodynamic work of creating the junctional knot (or the 142  
regular junction) out of an effective membrane reservoir represented by the surrounding tubular 143  
ER. Based on the ER structure, we consider the reservoir to consist of cylindrical membrane 144  
tubules characterized by a spontaneous curvature,  $J_S$ , and subject to a tension,  $\gamma$ . The radius,  $r_R$ , 145  
and the corresponding mean curvature,  $J_R$ , of the reservoir tubules are given by 146

$$r_R = \frac{1}{J_R} = \left[ \frac{1}{2} J_S \left( 1 + \sqrt{1 + 4 \frac{\gamma}{\kappa J_S^2}} \right) \right]^{-1}, \quad (2) \quad 147$$

as set by the mechanical equilibrium between the tension and the intra-membrane torque (see SI 148  
A)). We consider the junctional knot to be connected to the reservoir by three tubular arms, 149  
which merge with the reservoir along circular border-lines of radius,  $r_R$  (Eq. 2), and denote the 150  
distance from the border-lines to the unit-cell center by  $L$  (Fig. 1I). The boundary conditions 151  
imposed on membrane shape at the border-lines require a smooth transition between the 152  
membranes of the tubular arms and those of the reservoir. Taking the distance,  $L$ , to be 153  
substantially larger than the characteristic length-scale of the system,  $L \gg \sqrt{\frac{\kappa}{\gamma}}$  (see SI A)), we 154



guarantee a negligibly small influence of the boundary conditions on the junctional knot configurations. 155 156

The bending energy of shaping a unit area of the reservoir membrane into a unit area element of the junctional knot (or the regular junction) is given by 157 158

$$f_B = \frac{1}{2} \kappa [J^2 - 2 J_S (J - J_R) - J_R^2] + \bar{\kappa} K. \quad (3) \quad 159$$

The total bending energy,  $F_B$ , is obtained by integration of  $f_B$  over the system area  $A_T$ , which includes the area of the junctional knot (or the regular junction) and that of the connecting arms, 160 161

$$F_B = \oint f_B dA. \quad (4) \quad 162$$

The tension energy is given by, 163

$$F_T = \gamma A_T. \quad (5) \quad 164$$

It is convenient to relate the energy of the junctional knot (or the regular junction),  $F_E$ , to that of a hypothetical reference state,  $F_0$ , which we define as consisting of three homogeneous cylindrical membrane tubules of radius  $r_R$  (Eq. 2) pulled out of the reservoir through the boundary lines up to the center of the unit cell, i.e., each having the length  $L$  (Fig. 1J). The relative energy,  $F_R = F_E - F_0$ , does not depend on the arbitrarily chosen length,  $L$ , provided that the latter is sufficiently large, and characterizes solely the conformation of the knot membrane *per se*. 165 166 167 168 169 170 171

By considering the energy of the intermediate stage of the junctional knot remodeling emerging as a result of hemi-fission of the pore rim, we account, in addition to the elastic energy above, for 172 173

the energy of tilting and splaying the hydrocarbon chains of lipid molecules forming the  
membrane of the core of the hemi-fission structure. The description of the model used for  
evaluation of the tilt and splay energy and the related elastic moduli of the membrane is  
presented in (SI B).

## Results

### Configurations and energies of junctional knots and regular junction

The configurations and energies of the junctional knots (and the regular junctions) were obtained  
by numerical minimization of the relative energy,  $F_R$ , using the Brakke's Surface Evolver  
program(Brakke, 1992). The examples of the resulting configurations computed for a specific  
tension value are presented in (Fig. 2A), and (Fig.2B) for a junctional knot and a regular  
junction, respectively. Whereas the junctional knot and the regular junction have similar  
dimensions and shapes of their external contours (Fig. 2A,B), the former differs from the latter  
by an hour-glass pore in the middle (Fig. 2A). This pore is a remnant of the micron large space  
confined within the initial network unit-cell before its contraction. The equilibrium size of the  
pore is set by the interplay of two counter-acting factors, the tension and the bending energy. The  
bending energy of the membrane forming the pore rim increases in the course of the pore  
constriction and, hence, resists this process. By contrast, the tension favors the pore tightening.

Therefore, the radius of the pore waist decreases from 8nm to 4nm with increasing membrane tension from 0.1 mN/m to 0.5 mN/m (Fig.2C). For even larger tensions the pore radius tends to decrease beneath 4 nm which is the lower boundary of our calculation validity set by the membrane thickness.

We further analyzed the structures of junctional knots resulting from a sequential contraction of several triangular network unit-cells into the same junctional knot. To this end, we computed the optimal configurations of the junctional knots with various number of pores as presented in (Figs. 2D,E) for knots containing, respectively, three and five pores. As shown in (Fig.2 D,E), the pores are tightly packed in the center of the structure. The larger the pore number within a junctional knot, the smaller the pore radii under the same tension. This can be regarded as an effective tension-mediated attractive interaction between the pores within a junctional knot, which enables the pore contraction and tighter packing, and must facilitate embedding of additional pores.

Finally, we investigated the stability of the pore location within the junctional knot. For this purpose, we computed the change of the system energy resulting from displacement of one of the pores from the junctional knot into one of the tubules emerging from the junctional knot (Fig. 2F). As presented in (Fig. 2F), this event consumes energy irrespectively of the number of the pores within the junction meaning that the dense packing of the pores within a junctional knot is a stable configuration.

# **Transformation of junctional knots into regular junctions through sealing of intra-knot pores**

Here we analyze sealing of the intra-knot pores, which converts the junctional knots into regular junctions. This is a final step of the ring closure event, which reduces the overall number of junctions in the ER network. For a junctional knot containing one pore, the sealing completes the removal of two junctions from the network (Fig. 1E-H).

We consider the membrane fission mediating the sealing (Kozlovsky and Kozlov, 2003) to occur either within the hourglass-like membrane neck forming the rim of the pore, or within one of the short neck-like membrane elements forming the sides of the junctional knot and surrounding the pore. We propose that the factor driving the membrane fission is the membrane stress that accumulates within the junctional knot membrane under the tension-driven constriction of the pore and relaxes as a result of the pore sealing.

*Favorability of the pore sealing.* We start with analyzing the conditions required for the pore sealing to be energetically favorable, i.e., leading to decrease of the system energy. To this end we compare the energy,  $F_{E0}$ , of a three-way tubular junction with no pores (Fig. 2B) with the energy,  $F_{E1}$ , of a junctional knot with one pore (Fig. 2A).

The computational results for  $F_{E0}$ ,  $F_{E1}$  and for the energy released by the pore sealing,  $\Delta F_S = F_{E1} - F_{E0}$ , are presented in (Fig. 3A,B) in dependence on the membrane tension,  $\gamma$ . According to (Fig. 3B), for non-vanishing tensions, the released energy,  $\Delta F_S$ , is positive and, hence, the sealing event is favorable within the considered parameter ranges. The energy release is a consequence of relaxation, as a result of the pore sealing, of the elastic stresses accumulated

initially, within the junctional knot upon its tension-driven constriction. The tension reinforces 235  
the energetic favorability of the pore sealing since the amount of the released energy,  $\Delta F_S$ , 236  
increases with  $\gamma$  (Fig. 3B). 237

*Dependence of the rate-limiting stage of the pore sealing on the membrane tension.* Finally, we 238  
address a possible kinetic hindrance of the pore sealing by an energy barrier represented by an 239  
intermediate state of the reaction. To this end, we consider a specific pathway of the membrane 240  
structural transformations leading from a junctional knot with one pore (Fig. 2A) to a regular 241  
junction (Fig. 2B). 242

First, we find the site within the junctional knot in which membrane fission occurs with a highest 243  
probability. We require the fission site to be a region encircling the membrane shape and 244  
characterized by a relatively high surface density of the elastic energy,  $f_E$ , which includes the 245  
contributions from the bending energy,  $f_B$  (Eq.2), and the reservoir tension,  $\gamma$ , such that 246

$$f_E = \frac{1}{2} \kappa (J^2 - 2 J J_S) + \bar{\kappa} K + \gamma. \quad (6) \quad 247$$

The computed distribution of  $f_E$  along the surface of a junctional knot with one pore is presented 248  
in (Fig. 4A) for two limiting sets of the elastic parameters. In both cases, a continuous ring-like 249  
region of high or elevated energy density forms around the waist of the pore rim rather than the 250  
membrane necks surrounding the pore. Thus, we suggest that fission occurs in the middle of the 251  
membrane neck forming the pore rim. 252

Based on the previous work(Kozlovsky and Kozlov, 2003), we consider the fission reaction to 253  
proceed via an intermediate stage of hemi-fission at which only the internal monolayer of the 254  
pore rim undergoes splitting, while the external monolayer remains intact, as illustrated in (Fig. 255

1E-F). The intermediate structure formed at this stage is referred to as the hemi-fission stalk(Kozlovsky and Kozlov, 2003) (Figs. 1F). The fission is completed by splitting of the hemi-fission stalk (Figs. 1G,H). Since, as shown above, the full fission results in a decrease of the system elastic energy, we consider the hemi-fission stalk to represent the potential rate-limiting step of the fission process. The activation energy of fission,  $\Delta F_A$ , is thus the difference between the energy of a junctional knot with the hemi-fission stalk,  $F_{EHF}$ , and that of the initial junctional knot with a pore,  $F_{E1}$ , such that  $\Delta F_A = F_{EHF} - F_{E1}$ .

The computation of the configuration and the energy of the hemi-fission stalk is based on the previous works (Hamm and Kozlov, 2000) and, as already mentioned, uses the elastic model of tilt, splay and saddle-splay deformations of lipid monolayers described in (SI B). The monolayer resistance to the three deformations is characterized by the elastic moduli of tilt,  $\kappa_t$ , splay,  $\kappa_m$ , and saddle-splay,  $\bar{\kappa}_m$  (SI B). As described in (SI C), the computational procedure we used here is similar to that developed previously for modeling intermediate structures of different reactions of membrane fusion and fission(Golani et al., 2021; Kozlovsky et al., 2002; Kozlovsky and Kozlov, 2002), but accounts for the specific geometry of a junction between three tubules.

Our main goal was to examine the dependence of the activation energy,  $\Delta F_A$ , on the membrane tension,  $\gamma$ , which we took to vary in the range between 14 and  $770 \frac{\mu N}{m}$ . We also explored the dependence of the activation energy,  $\Delta F_A$ , on the monolayer elastic parameters whose values have not been directly measured and can vary within estimated ranges. Specifically, we computed  $\Delta F_A$  for different values of the dimensionless ratio between the monolayer modulus of Gaussian curvature and the bending modulus,  $\chi = \frac{\bar{\kappa}_m}{\kappa_m}$ , varying in the feasible range between 0 and -1(Templer et al., 1998). Another parameter is the characteristic decay length of the tilt

deformation,  $l$ , which is determined by the ratio between the monolayer bending and tilt moduli 278

by,  $l = \sqrt{\frac{\kappa_m}{\kappa_t}}$ , and was taken to change between 1 and 2nm(Golani et al., 2021). 279

The results for the energy of the hemi-fission intermediate,  $F_{EHF}$ , are shown in (Fig. 3A), and for 280  
the activation energy,  $\Delta F_A$ , are presented in (Fig. 3B, 4B-C), where the energy values are scaled 281  
by the bilayer bending modulus  $\kappa \approx 10^{-19}$ Joule(Dimova, 2014) , the reference system is the 282  
same as used for computations of the junctional knot energy (Fig. 1J), and the tension varies 283  
within a biologically feasible range. 284

The dependence of  $\Delta F_A$  on the tilt decay length,  $l$ , is shown in (Fig. 4B) for  $\chi = -0.5$ . The 285  
activation energy is decreasing with increasing,  $l$ , which means that the smaller the tilt modulus, 286  
 $\kappa_T$ , the smaller the activation energy of fission. 287

The dependence of  $\Delta F_A$  on  $\chi$  is presented in (Fig. 4C) for  $l = 1.5$  nm. The activation energy 288  
decreases with  $\chi$ , and, consequently, with the monolayer modulus of Gaussian curvature  $\bar{\kappa}_m$ , 289  
becoming more negative. For sufficiently negative values of  $\chi$ , the activation energy is predicted 290  
to be small or vanishing. 291

The effects of the elastic parameters and tension on the activation energy are summarized in (Fig. 292  
4D), where each line represents the parameter combinations for which the activation energy 293  
vanishes meaning that the fission process happens spontaneously. According to this diagram, for 294  
fission to be spontaneous, the tension has to be large, the monolayer modulus of Gaussian 295  
curvature has to be as negative as possible, and the tilt modulus has to be small. 296

The computed membrane configurations formed along the full pathway of the junctional knot 297  
remodeling into a regular junction are presented in (Fig. 5A-C). 298

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## Discussion

300

Here we considered the critical final stages of the ER ring closure, the process of constriction 301  
and vanishing of polygonal unit-cells of the ER tubular networks. The ring closure reduces the 302  
number of the network three-way junctions, which dynamically equilibrates the persistent 303  
process of new junction generation by the ER tubule branching and fusion. We computationally 304  
analyzed the experimentally inaccessible structures of the junctional knots, which result from 305  
constriction of one or several triangular unit-cells of a tubular network and contain internal 306  
pores. We analyzed the pore sealing by membrane fission, which completes the ring closure, and 307  
determined the conditions necessary for vanishing of the activation energy related to the hemi- 308  
fission intermediate of the fission reaction. 309

The major message of our analysis is that the ER ring closure can be driven by tension existing 310  
in the ER tubular membranes. The distribution of the membrane tension in ER appears to be 311  
highly variable. According to the ER images in live cells, there are regions where the ER tubules 312  
look loose and undergoing thermal undulations(Georgiades et al., 2017; Nixon-Abell et al., 2016; 313  
Westrate et al., 2015), which implies that they are subjected to either vanishing or extremely low 314  
tensions(Georgiades et al., 2017). At the same time, the ER tubules, which undergo sliding and 315  
ring closure look stretched(Lee and Chen, 1988; Powers et al., 2017), as expected for membranes 316  
exposed to considerable tensions. Substantial tensions in reconstituted ER networks were 317  
determined by direct measurements(Upadhyaya and Sheetz, 2004). Altogether, these 318  
observations suggest that different parts of the ER network are subject to various tensions, which 319  
is counterintuitive given the 2D-fluidity of the interconnected ER membranes. Yet such 320



situations are feasible provided that not the whole ER tubular network but only certain parts of it  
are stretched between the sites of contact with cytoskeleton in which pulling forces are applied to  
the ER tubules. While these ER areas must be exposed to tension, the other ER regions, which  
are outside of the zones of the pulling force action, are expected to remain tension free.

According to our results, the spontaneous pore sealing corresponding to a vanishing activation  
energy of the membrane fission reaction can be driven by small membrane tensions generated by  
pulling forces as little as  $f = 2 \text{ pN}$  if the absolute value of the membrane modulus of Gaussian  
curvature is large, e.g.  $\bar{\kappa} = -0.6 \cdot 10^{-19} \text{ Joule}$ , while the tilt modulus is small such as  $\kappa_t =$   
 $10^{-11} \frac{N}{nm}$ . Such parameters values correspond to the limits of the currently estimated ranges for  
 $\bar{\kappa}$  and  $\kappa_t$ . For the mid-range values of,  $\bar{\kappa} = -0.2 \cdot 10^{-19} \text{ Joule}$  and  $\kappa_t = 1.8 \cdot 10^{-11} \frac{N}{nm}$ , the  
spontaneous fission requires large tensions corresponding to pulling forces of about  $f = 40 \text{ pN}$ .  
Such tensions could be generated by more than 10 molecular motors acting on each membrane  
tubule, which must be, biologically, a seldom situation. This implies that special fission proteins  
might be required to facilitate the junctional knot conversion into the regular junctions.

Another prediction of our results is that in ER network regions exposed to ultralow tensions, the  
transition of the junctional knots to regular junctions should not occur. In this case, one might  
expect the accumulation of pores within the junctional knots leading to formation of sieve-like  
structures such as ER matrices(Nixon-Abell et al., 2016).

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## Figure legends 436

### Figure 1 437

Model for the pathway of the ER ring closure. (A-D) Formation of a junctional knot as a result of 439  
the ring constriction. (A) Segment of macroscopic network of ER tubules. (B) A network unit- 440  
cell with four junctions. (C) Formation of a triangular unit cell as a result of dynamic evolution 441  
of the four-junction unit cell. (D) Constriction of the triangular unit cell into a junctional knot. 442  
(E-H) Transformation of a junctional knot into a regular junction through the pore sealing 443  
mediated by membrane fission. (E) View of the junctional knot cross-section indicated in (H). 444  
(F) View of the cross-section through the hemi-fission stalk. (G) and (H) represents sequential 445  
stages of post fission relaxation. (I) The system under consideration in contact with the reservoir 446  
with the dashed circle indicating the reservoir boundary,  $r_R$  is the radius of the reservoir tubules, 447  
 $L$  is the distance from the system center to the boundaries with the reservoir. (J) The hypothetical 448  
reference system. 449

### Figure 2 450

Computed configurations of junctional knots with different number of pores. (A) One pore. (B) 451  
No pore, which represents a regular junction. (C) The tension dependence of the pore radius in 452  
one-pore junctional knot. (D) Three pore junctional knot. (E) Five pore junctional knot. (F) The 453  
energy of transition of one pore from the junctional knot to a tubule as a function of the initial 454  
number of pores in the junction. The used parameters:  $\kappa = 0.8 \cdot 10^{-19}$  Joule;  $J_S = \frac{1}{25 \text{ nm}}$ ;  $\gamma =$  455  
 $140 \frac{\mu\text{N}}{\text{m}}$  (except for (C));  $r_R = 15\text{nm}$  (except for (C));  $L = 8.5 \cdot r_R$ . 456  
457

### Figure 3

Energies of the intermediate stages of the ring closure as functions of tension. (A) The energies of the junctional knot with one pore (black line), the hemi-fission stage of the pore sealing (red line), the regular junction (dashed line). (B) The energy released as a result of the pore sealing,  $\Delta F_S$ , (black line), and the fission activation energy,  $\Delta F_A$ , (red line).  $\kappa = 0.8 \cdot 10^{-19}$  Joule;

$$J_S = \frac{1}{25 \text{ nm}}; \chi = \frac{\bar{\kappa}}{\kappa} = \frac{\bar{\kappa}_m}{\kappa_m} = -0.5; l = \sqrt{\frac{\kappa_m}{\kappa_{t,m}}} = 1.$$

### Figure 4

**Hemi-fission stage of the pore sealing in a junctional knot.** (A) The excess stress distribution along the membrane of a junctional knot for two characteristic values of the ratio between the membrane modulus of Gaussian curvature and bending modulus,  $\chi = \frac{\bar{\kappa}}{\kappa}$ , and other elastic parameters as in (Fig.2). Left panel,  $\chi = -1$ ; right panel  $\chi = 0$ . (B) The activation energy of hemi-fission as a function of the membrane tension,  $\gamma$ , for  $l = \sqrt{\frac{\kappa_m}{\kappa_{t,m}}} = 1$ , and different values of  $\chi = \frac{\bar{\kappa}_m}{\kappa_m}$ . (C) The activation energy of hemi-fission as a function of the membrane tension,  $\gamma$ , for  $\chi = -0.5$  and different values of  $l$ . (D) The relationships between  $\chi = \frac{\bar{\kappa}_m}{\kappa_m}$  and  $l = \sqrt{\frac{\kappa_m}{\kappa_{t,m}}}$  corresponding to a vanishing activation energy of hemi-fission,  $\Delta F_A = 0$ , for different values of the tension.



# Figure 5

Computed configurations of all stages of a junctional knot transition into a regular junction with the top and plain views presented, respectively, in the left and right panels. (A) Junctional knot with one pore. (B) Hemi-fission stage of the pore sealing. (C) Regular junction.  $\kappa = 0.8 \cdot$

$$10^{-19} J; \chi_G = \frac{\bar{\kappa}_m}{\kappa_m} = -0.5; l = \sqrt{\frac{\kappa_m}{\kappa_{t,m}}} = 1 \text{ nm}; \gamma = 290 \frac{\mu\text{N}}{\text{m}}; r_R = 12\text{nm}; L = 6 \cdot r_R.$$

Figure 1

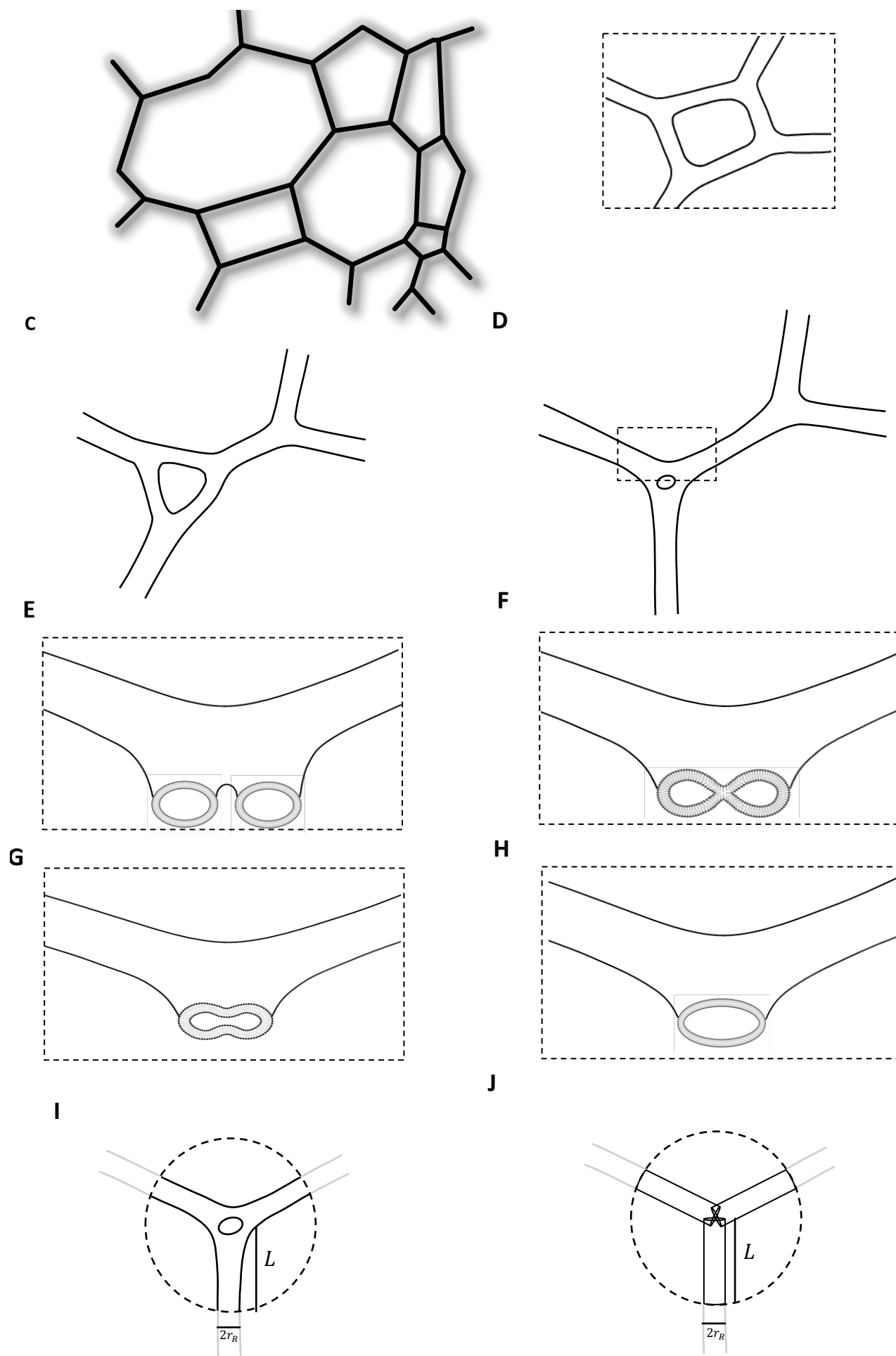


Figure 2

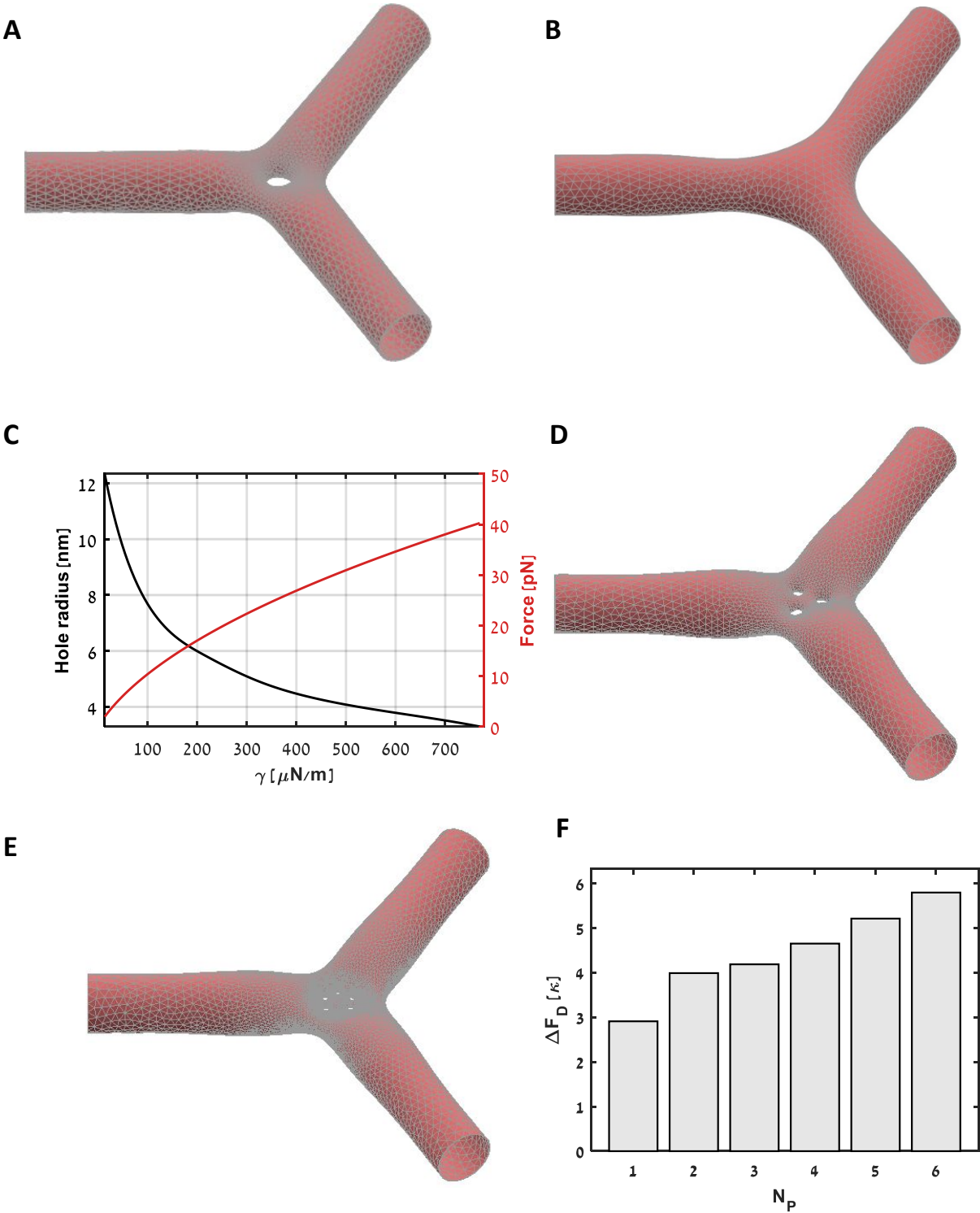


Figure 3

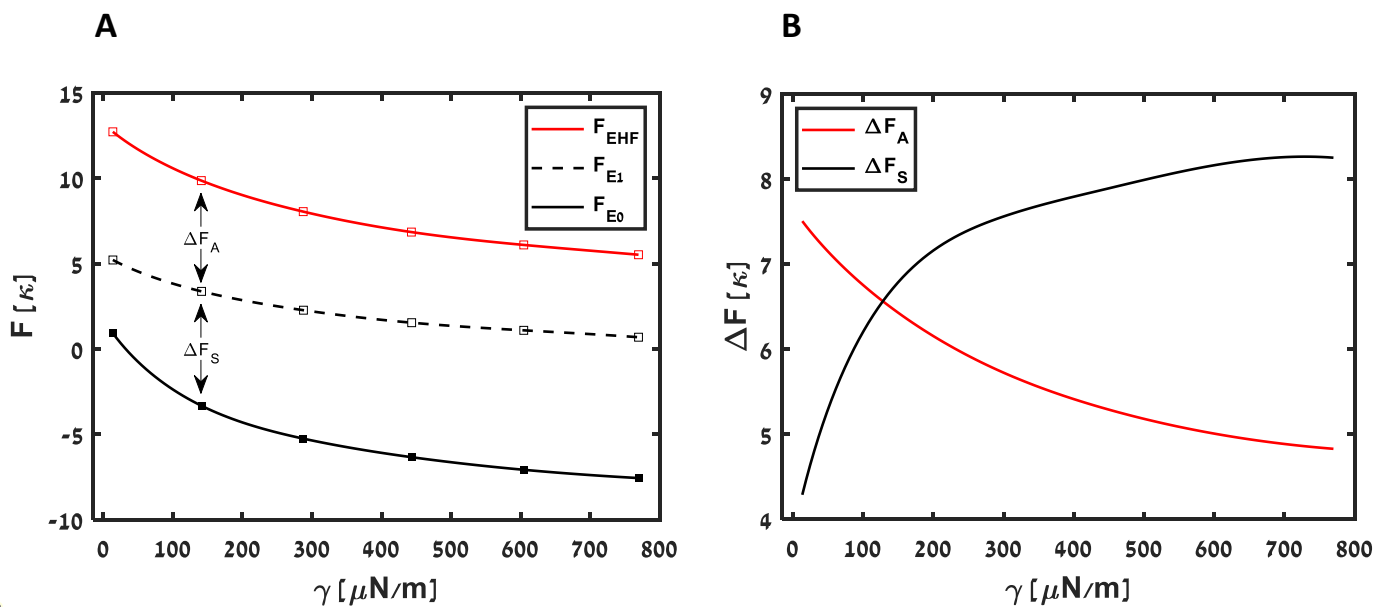


Figure 4

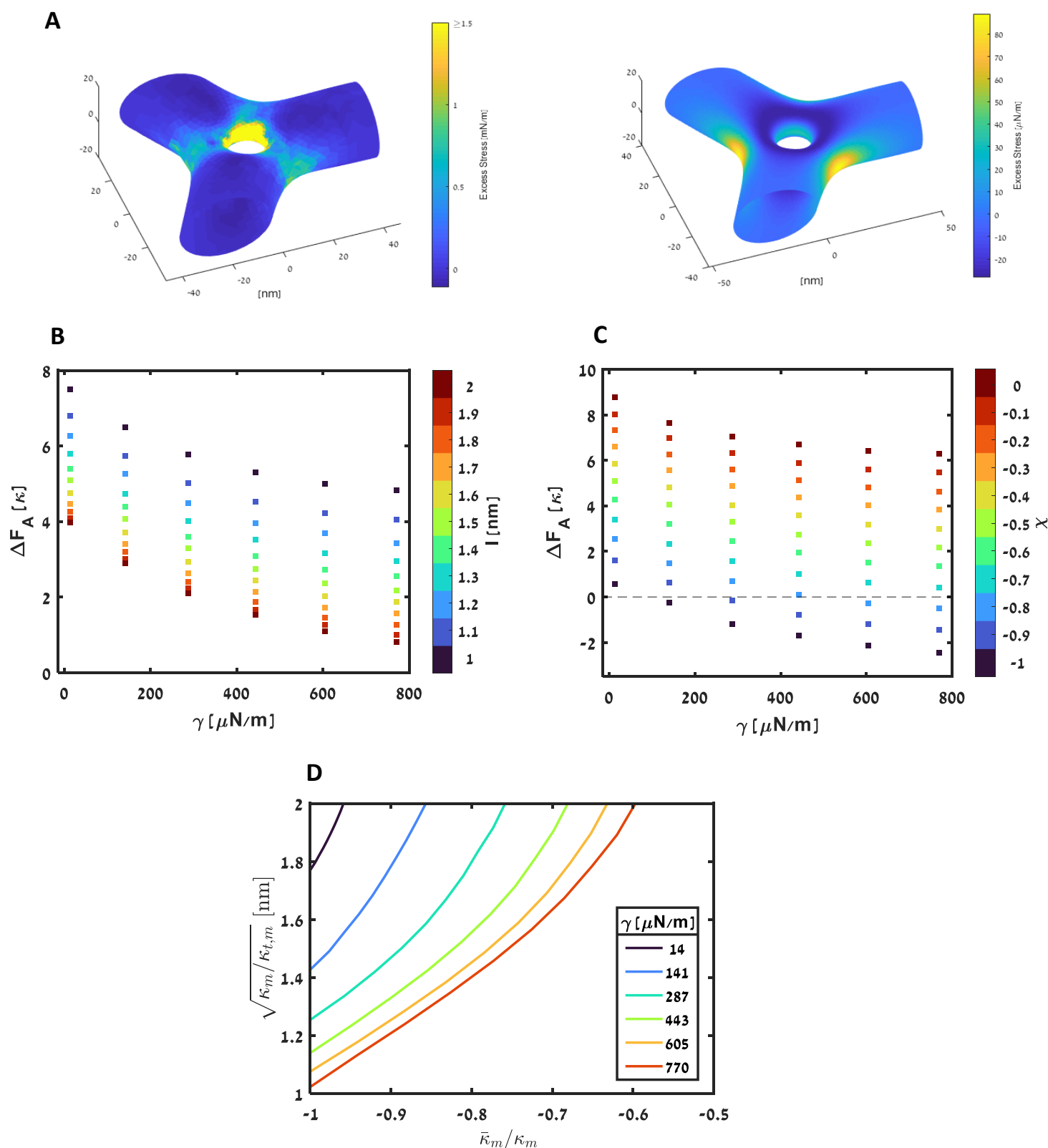
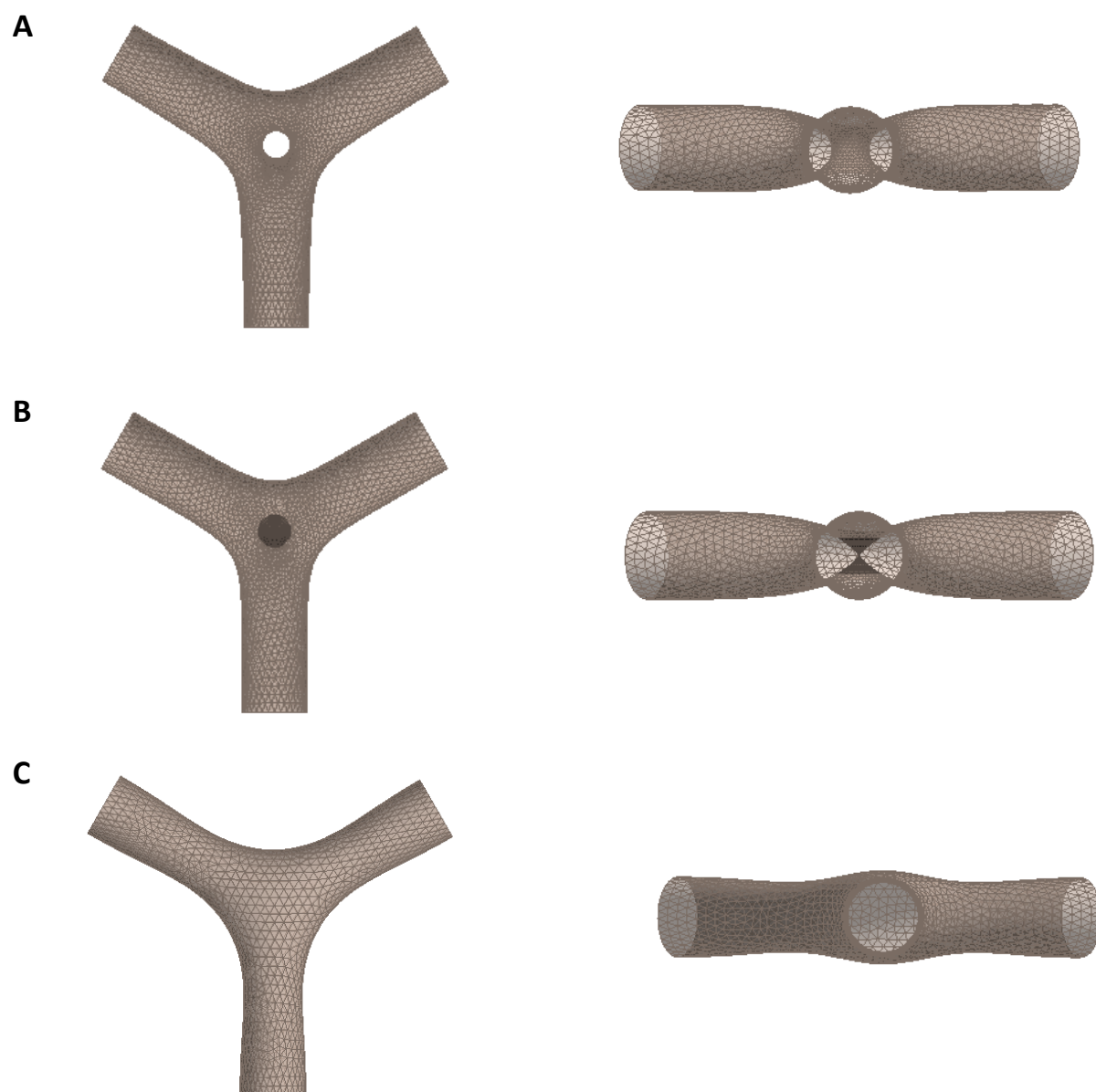


Figure 5



## Supplementary Information

### A. Relationship between the radius and tension of a reservoir tubule

To derive the relationship between the radius,  $r_R$ , the tension,  $\gamma$ , and the spontaneous curvature,  $J_S$ , of a tubular membrane given by (Eq. 2) of the main text, we use the equation of mechanical equilibrium of a curved membrane (see “Some aspect of membrane elasticity”(Poon and Andelman, 2006, pp. 79–96)) Since the mean curvature,  $J$ , of a cylindrical membrane is homogeneous so that its gradient along the membrane surface vanishes,  $\nabla J = 0$ , and the Gaussian curvature vanishes as well,  $K = 0$ , the equilibrium equation adopts a simple form,

$$\gamma J - \tau J^2 = \Delta P, \quad (\text{A1})$$

where  $\tau$  is the membrane torque related to the membrane spontaneous curvature,  $J_S$ , and bending modulus,  $\kappa$ , by the relationship

$$\tau = \kappa (J - J_S), \quad (\text{A2})$$

and  $\Delta P$  is the trans-membrane pressure difference. Substituting (Eq.A2) into (Eq.A1) and taking into account that,  $\Delta P = 0$ , for ER tubules, we obtain the equation for the tubule mean curvature

$$J^2 - J_S J - \frac{\gamma}{\kappa} = 0. \quad (\text{A3})$$

Solution of this equation for the tubule mean curvature,  $J$ , and cross-sectional radius,  $r$ , gives

$$J = \frac{1}{r} = \frac{1}{2} J_S \left( 1 + \sqrt{1 + 4 \frac{\gamma}{\kappa J_S^2}} \right). \quad (\text{A4})$$

For vanishing spontaneous curvature,  $J_S = 0$ , the expression (Eq.2) takes a simple form

$$J = \frac{1}{r} = \sqrt{\frac{\gamma}{\kappa}}. \quad (\text{A5})$$

The relationships (Eqs. A4,A5) describe the curvature,  $J_R$ , and the cross-section radius,  $r_R$ , of the reservoir given by (Eq. 2) of the main text.

## B. Elastic energy of splay and tilt of membrane monolayer

Hemi-fission and hemi-fusion intermediates of membrane remodeling introduce deformations of inhomogeneous tilting of the hydrocarbon chains of lipid molecules (Hamm and Kozlov, 2000, 1998). Since the in-plane distributions of these deformation are different for the two monolayers, the elastic energy has to be computed separately for each monolayer, which can be done by using the generalized Helfrich model accounting for the tilt, splay, and saddle splay of the hydrocarbon chains as introduced in detail in the earlier works (Kozlovsky et al., 2004, 2002; Kozlovsky and Kozlov, 2003, 2002). Here we sketch the main features of this model.

To describe the monolayer geometry, we use the dividing surface coinciding with the interface between the regions of the polar heads and hydrocarbon tails of the monolayer. The local orientation of the lipid molecules at each point of the dividing surface is characterized by the lipid director,  $\vec{n}$ , which is defined as a unit vector pointing from the locally averaged position of the ends of the hydrophobic lipid tails to those of the polar heads (Fig. S1). Lipid tilt, splay, and saddle splay are defined based on the variation of  $\vec{n}$  along the dividing surface and the deviation of  $\vec{n}$  from the unit normal vector to the dividing surface,  $\vec{N}$ .

The lipid tilt is defined as

$$\vec{t} = \frac{\vec{n}}{\vec{n} \cdot \vec{N}} - \vec{N}, \quad (\text{B1})$$

and its consequence for the monolayer internal structure can be understood as shearing of the lipid hydrocarbon chains in the direction perpendicular to the monolayer plane (Hamm and Kozlov, 2000, 1998; May et al., 2004) (Fig. S1).

Lipid splay,  $\tilde{J}$ , referred also to as the modified mean curvature, is defined as the two-dimensional divergence of the lipid director,  $\vec{\nabla} \cdot \vec{n}$ , determined along the, generally, curved dividing surface. In covariant form, the lipid splay is the trace of the tensor,  $\tilde{b}_\alpha^\beta = \nabla_\alpha n^\beta$ , where the sub and superscripts denote, respectively, the co- and contravariant components in the local coordinate basis of the surface.  $\tilde{b}_\alpha^\beta$  is referred to as the modified curvature tensor. Therefore,



$$\tilde{J} = \vec{\nabla} \cdot \vec{n} = \tilde{b}_\alpha^\alpha. \quad (B2)$$

Lipid saddle splay is the determinant of the modified curvature tensor,

$$\tilde{K} = \det \tilde{b}_\alpha^\beta. \quad (B3)$$

In the absence of the tilt deformation, the lipid director and the surface normal are aligned,  $\vec{n} = \vec{N}$ , so that the splay,  $\tilde{J}$ , is reduced to the two-dimensional divergence of the surface normal,  $J = \vec{\nabla} \cdot \vec{N}$ , whose geometrical meaning is the mean curvature of the dividing surface,  $J = c_1 + c_2$ , where  $c_1$  and  $c_2$  are the two principal curvatures of the surface. Saddle splay,  $\tilde{K}$ , is reduced in this case to Gaussian curvature of the surface,  $K = c_1 \cdot c_2$ , the product of the two principle curvatures.

The elastic energy of the tilt, splay and saddle-splay deformations per unit area of the membrane plane is given by (Hamm and Kozlov, 2000),

$$f_m = \frac{1}{2} \kappa_m (\tilde{J} - J_{s,m})^2 - \frac{1}{2} \kappa_m J_{s,m}^2 + \bar{\kappa}_m \tilde{K} + \frac{1}{2} \kappa_{t,m} \vec{t}^2. \quad (B4)$$

where  $\kappa_m$  is the monolayer bending modulus whose value was measured for pure lipid monolayers and varies in the range between  $5 - 20 k_b T$  (Dimova, 2014; Niggemann et al., 1995; Pontes et al., 2013) ( $k_b T \approx 4.11 \cdot 10^{-21}$  Joule is the product of the Boltzmann constant,  $k_B$ , and the absolute room temperature);  $\bar{\kappa}_m$  is the monolayer saddle splay modulus, which has been estimated to be negative and have an absolute value smaller but of the same order of magnitude as the bending modulus;  $\kappa_{t,m}$  is the monolayer tilt modulus;  $J_{s,m}$  is the monolayer spontaneous splay, which equals the molecular intrinsic curvature of the constituting lipids. We define the ratio between the bending and saddle splay moduli as  $\chi = \bar{\kappa}_m / \kappa_m$ , which can have values in the range between -1 and 0 (Templer et al., 1998; Terzi et al., 2019). As a measure of the tilt modulus, we use  $l = \sqrt{\kappa_m / \kappa_{t,m}}$ , which has a meaning of a characteristic decay length of the tilt deformation and whose estimated values vary in the range between 1nm and 2nm (Doktorova et al., 2017; Hamm and Kozlov, 1998; May et al., 2004; Nagle et al., 2015; Terzi et al., 2019). The ER membrane is composed mostly of phosphatidylcholine (PC) and phosphatidylethanolamine (PE) (Zambrano et al., 1975), both having negative intrinsic molecular curvature (Chen and Rand, 1997; Leikin et al., 1996; Szule et al., 2002), and a small amount of lysolipids, such as lysophosphatidylcholine (LPC), characterized by positive intrinsic molecular curvature (Fuller and Rand, 2001; Zambrano

et al., 1975). We estimate the ER monolayers spontaneous splay by calculating the weighted average of the intrinsic molecular curvatures of the constituting lipids to be  $J_{s,m} = -0.1 \text{ nm}^{-1}$  (Kozlov and Helfrich, 1992). Since, to the best of our knowledge, there is no evidence for asymmetrical distribution of lipids components between cytosolic and luminal monolayers of ER membrane, we assume the two monolayer compositions to be identical.

The total elastic energy of the membrane is calculated by integrating the energy density (Eq. 4) over the areas of the luminal and cytosolic monolayers,

$$F_B = \int f_c dA_c + \int f_l dA_l, \quad (\text{B5})$$

where the subscripts  $c$  and  $l$  denote the cytosolic and luminal monolayers of the ER tubule, respectively. The energy of membrane tension,  $F_T$ , is given by a product between the lateral tension of each membrane monolayer,  $\gamma_m$ , and its area, which is  $A_c$  and  $A_l$  for the cytosolic and luminal area respectively,

$$dF_T = \gamma_m (dA_c + dA_l). \quad (\text{B6})$$

The total elastic energy is:

$$F_E = \int (f_c + \gamma_m) dA_c + \int (f_l + \gamma_m) dA_l. \quad (\text{B7})$$

### C. Structure and energy of the hemi-fission stage of the pore sealing.

We consider the pore sealing to proceed through an intermediate stage of hemi-fission of the membrane neck constituting the rim of the pore (Fig.1E-H of the main text). The hemi-fission intermediate includes a non-bilayer structure in the middle (Fig.1F of the main text) referred to as the membrane stalk. Our goal here was to compute the elastic energy of the hemi-fission intermediate,  $F_{EHF}$ , which could be compared to the energies of a junctional knot with one pore,  $F_{E1}$ , and of a regular junction with no pore,  $F_{E0}$ , as described in the main text.

To perform the computation of  $F_{EHF}$ , we used the results of the previous works (Kozlovsky and Kozlov, 2003, 2002) in which the structure and energy of a membrane stalk were computed for various processes of membrane remodeling: abscission of an endocytic vesicle (Kozlovsky and

Kozlov, 2003), hemi-fusion of flat(Kozlovsky et al., 2002; Kozlovsky and Kozlov, 2002) and curved(Martens et al., 2007) membranes. In spite of different overall configurations of these systems, the computed structure of the membrane stalk had a common feature: the middle part of the stalk could be considered as a localized sub-system referred to as the stalk-core (Fig.S1). The tilt angles in the stalk-core monolayers were equal  $\frac{\pi}{4}$  in the middle of the structure, and relaxed along the mid-plane over a characteristic length of few nanometer(Kozlovsky and Kozlov, 2003), which sets the stalk-core boundary (Fig.S1).

Based on that, we approximated the hemi-fission intermediate of the pore sealing as the stalk-core embedded into the three-way tubular junction. The boundary between the stalk-core and the surrounding membrane was chosen to lie on a sphere co-centered with the stalk-core, having a radius as  $R_b = 8 \text{ nm}$ , and called below as the boundary sphere. According to the earlier works(Kozlovsky and Kozlov, 2003, 2002) and verified by the present computations for the stalk-core monolayers, at this boundary the lipid tilt, practically, vanishes and the monolayer curvatures becomes small with respect to the monolayer width.

The computation of the configuration and energy of the hemi-fission intermediate included the calculation of the stalk-core energy and the energy of the surrounding membrane of the junction and minimization of the sum of the two energies with respect to the position of the interface between the stalk-core and the surrounding membrane on the boundary sphere.

By computing the stalk-core energy, we assumed that reticulons are excluded from the stalk-core because of the small dimension and non-bilayer structure of the latter so that the spontaneous splay of the stalk-core monolayers is determined solely by its constituting lipids. We further assumed that the monolayer hydrocarbon moiety is incompressible and that the monolayers dividing planes are parallel to the membrane mid-plane, meaning the lipid tail length is related to the tilt by the relationship  $\delta = \delta_0 \sqrt{1 + t^2}$ . The computation of the stalk-core energy consisted in integration of the monolayer energy density along the monolayer surfaces (Eq. B7) and minimization of the obtained overall energy with respect to the tilt distribution in each monolayer upon a requirement of the monolayer tilt angles remaining equal  $\frac{\pi}{4}$  in the center of the structure (Fig.S1). The details on the parametrization of the monolayer shapes and tilt distributions we used here can be found in(Golani et al., 2021).

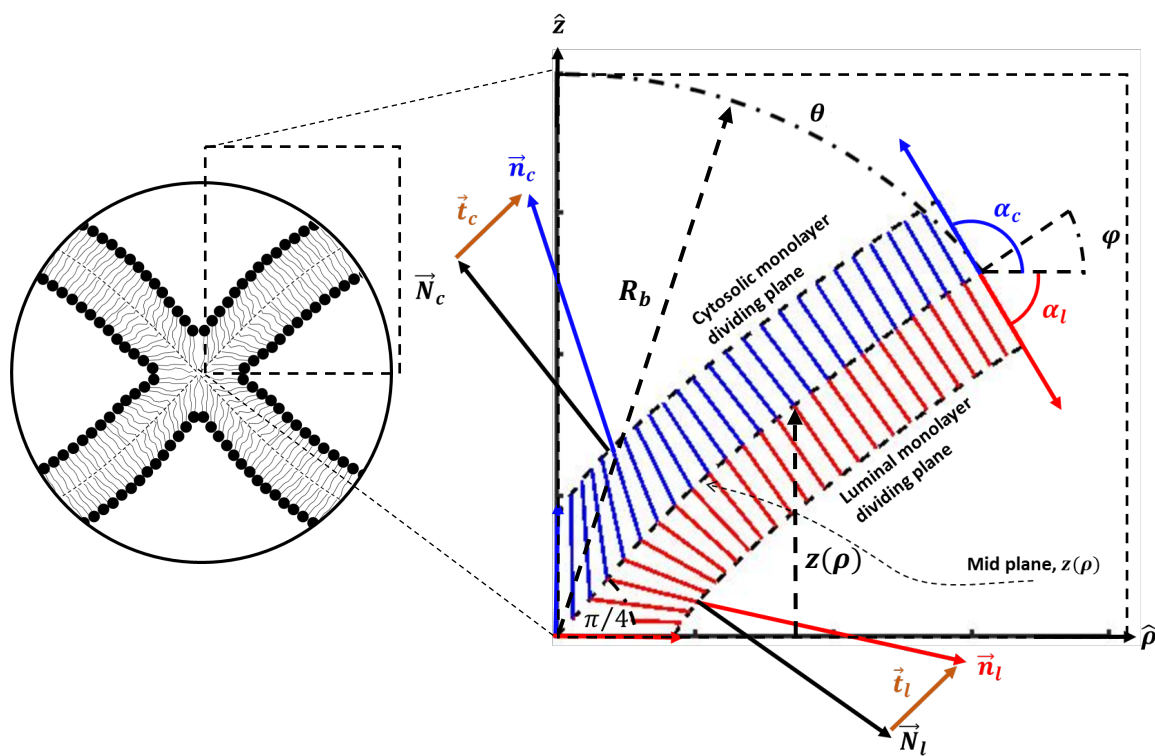
The computation of the energy of the surrounding membrane was performed analogously to that of the junctional knot or a regular junction, i.e. by integration of the regular density of the bilayer elastic energy ((Eq.3) of the main part) and minimization of the result with respect to the membrane shape using the Brakke's Surface Evolver(Brakke, 1992).

The computations of the stalk-core and the surrounding membrane energies were coupled through fulfillment of the boundary conditions at the interface between these two parts of the system, which included the requirement of smoothness of the membrane mid-plane profile, the continuity of the mid-plane curvature and the vanishing of the lipid tilt in the two monolayers of the stalk-core.

## Figure legend

Hemifission stalk and definitions. The vertical,  $Z$ , axis represents the axis of rotational symmetry. Left – drawing of a cross section of a hemifission stalk, bordered with by a sphere representing the interface  $e$  between the stalk-core and the surrounding membrane. right – computation results of stalk core shape. Blue and red lines represent averaged lipid director of cytosolic and luminal monolayers, respectively. Definitions:  $\vec{n}$  lipid director,  $\vec{N}$  Normal to dividing plane,  $\vec{t}$  tilt vector,  $\alpha$  angle lipid director and  $\hat{\rho}$  and  $\varphi$  angle between tangent vector to mid-plane and  $\hat{\rho}$ . The subscript  $c$  and  $l$  represent the cytosolic and luminal monolayers, respectively. Right panel represent the minimal energy configuration for the parameters:  $= 1.5nm$ ,  $\chi = -0.5$ ,  $J_m = -0.1nm^{-1}$ ,  $\theta_b = 50^\circ$ ,  $\varphi_b = 31^\circ$  and  $R_b = 8nm$ .

Figure S1



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