

Adaptations for bipedal walking: Musculoskeletal structure and three-dimensional joint mechanics of humans and bipedal chimpanzees (*Pan troglodytes*)

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1 **Abstract**

2

3 Humans are unique among apes and other primates in the musculoskeletal design of their  
4 lower back, pelvis and lower limbs. Here, we describe the three-dimensional ground  
5 reaction forces and lower/hind limb joint mechanics of human and bipedal chimpanzee  
6 walking over a full stride and test whether: 1) the estimated limb joint work and power  
7 during stance phase, especially the single-support period, is lower in humans than bipedal  
8 chimpanzees, 2) the limb joint work and power required for limb swing is lower in  
9 humans than in bipedal chimpanzees, and 3) the estimated total mechanical power during  
10 walking, accounting for the storage of passive elastic strain energy in humans, is lower in  
11 humans than in bipedal chimpanzees. Humans and bipedal chimpanzees were compared  
12 at matched dimensionless and dimensional velocities. Our results indicate that humans  
13 walk with significantly less work and power output in the first double-support period and  
14 the single-support period of stance, but markedly exceed chimpanzees in the second-  
15 double support period (i.e., push-off). Humans generate less work and power in limb  
16 swing, although the species difference in limb swing power was not statistically  
17 significant. We estimated that total mechanical positive ‘muscle fiber’ work and power  
18 were 46.9% and 35.8% lower, respectively, in humans than bipedal chimpanzees at  
19 matched dimensionless speeds. This is due in part to mechanisms for the storage and  
20 release of elastic energy at the ankle and hip in humans. Further, these results indicate  
21 distinct heel strike and lateral balance mechanics in humans and bipedal chimpanzees,  
22 and suggest a greater dissipation of mechanical energy through soft tissue deformations  
23 in humans. Together, our results document important differences between human and  
24 bipedal chimpanzee walking mechanics over a full stride, permitting a more  
25 comprehensive understanding of the mechanics and energetics of chimpanzee bipedalism  
26 and the evolution of hominin walking.

27

28 **Keywords:** Force; Work; Power; Elastic Energy; Bipedalism; Locomotion

## 1 **1. Introduction**

2 As humans, we are unique among apes and other primates in the musculoskeletal  
3 design of our lumbar column, pelvis and lower limbs. In particular, we possess a mobile  
4 lower back, a short pelvis and long lower limbs with short feet. This is distinct from the  
5 relatively immobile lumbar column, tall pelvis and short hind limbs with long feet  
6 characteristic of living African apes (e.g., Schultz, 1930, 1961; Ward, 1993; Pilbeam and  
7 Lieberman, 2017). Our limb muscle masses are more proximally located and are made up  
8 of relatively short muscle fibers and long distal limb tendons as compared to African apes  
9 (e.g., Thorpe et al., 1999; O'Neill et al., 2013, 2017). Among other capabilities, these  
10 traits are thought to facilitate humans walking with a stable pelvis on adducted, extended  
11 lower limbs (O'Neill et al., 2015), using as much as 75% less energy per distance walked  
12 than a bipedal chimpanzee (Rodman and McHenry, 1980; Sockol et al. 2007).  
13 Understanding when and where in a full stride lower/hind limb mechanics differ between  
14 human and bipedal chimpanzee walking is important for elucidating how our  
15 interspecific differences in musculoskeletal structure affect joint loading, muscle-tendon  
16 behavior and the metabolic cost of walking.

17 Over a walking stride, humans generate a coordinated sequence of three-dimensional  
18 (3-D) moments and power that with some exceptions, are minimal near the middle single-  
19 support period and contribute to a burst in positive power during the second double-  
20 support period (i.e., push-off), with significant moments and power continuing  
21 throughout limb swing. At the hip, in particular, there are substantial non-sagittal plane  
22 moments, work and power over a stride (e.g., Eng and Winter, 1995), comprehensive  
23 measurements of which are needed for accurate determination of skeletal loading (e.g.,  
24 Stansfield et al., 2003), muscle-tendon force and fascicle length change (e.g., Arnold and  
25 Delp, 2011). Across the limb, the instantaneous 3-D joint moments, work and power  
26 reflect the net contributions from active muscle-tendon units and passive, soft tissues at  
27 each joint throughout the full gait cycle. While it is difficult to decompose the individual  
28 contributions of a mobile lower back, a short pelvis, and long lower limbs and short feet  
29 via joint-level analyses alone, these traits can be expected to act together to reduce the  
30 total mechanical work and power output of an erect human walking stride when  
31 compared to facultative bipeds, such as bipedal chimpanzees.

1        In addition to our skeletal structure, our more proximal limb segment masses and  
2 long, thin distal limb tendons can be expected to further reduce the total mechanical work  
3 and power output in a walking stride. It has long been hypothesized that more proximal  
4 lower limb-mass distribution reduces the moment of inertia, and therefore the mechanical  
5 power required for limb swing (e.g., Gray, 1968; Hildebrand, 1985), including in fossil  
6 hominins (Jungers and Stern, 1988). Human limb mass perturbations provide some  
7 support for this view, demonstrating that a distal shift of the mass-specific moment of  
8 inertia increases the limb swing mechanical power and metabolic costs of walking (Royer  
9 and Martin, 2005; Browning et al., 2007). Still, the magnitude of these perturbations was  
10 large, and the resulting changes in limb segment inertial properties can exceed the  
11 difference between humans and African apes or some Old World monkeys (e.g., Isler et  
12 al., 2006; Supplementary Online Material [SOM] Table S1).

13        Long, thin tendons, as well as other soft tissues (e.g., ligaments, aponeuroses), have a  
14 significant capacity for passive elastic strain and reducing the mechanical work and  
15 power required of muscle fibers (e.g., Alexander, 1988; Roberts, 2016). While often  
16 associated with bouncing gaits, the storage and release of elastic strain energy in human  
17 walking is now well established. Direct measurements of ankle plantar flexor muscle-  
18 tendon behavior have shown that the Achilles tendon is stretched during single-support  
19 period and then recoils in the second double-support period, making a substantial  
20 contribution to positive ankle power at push-off (e.g., Fukunaga et al., 2001; Ishikawa et  
21 al., 2005). However, elastic mechanisms in human walking are not limited to the ankle.  
22 The hip joint produces a large component of the total limb mechanical work and power  
23 output in walking (e.g., Eng and Winter, 1995; Farris and Sawicki, 2012a; Schache et al.,  
24 2015), and a portion of this is derived from non-muscular tissues stretched during the  
25 single-support period, including hip joint ligaments, associated tissues and aponeuroses  
26 (e.g., Whittington et al., 2008; Eng et al., 2015). Although there is extensive quantitative  
27 data on human walking, little comparative data exist that permit a direct assessment of  
28 whether these presumed musculoskeletal adaptations interact to reduce the total  
29 mechanical work and power output as compared to a biped that lacks this lower back,  
30 pelvis and lower limb structure, such as bipedal chimpanzees. Indeed, the absence of  
31 comprehensive, speed-controlled comparisons has left the unique aspects of human

1 walking mechanics still not well defined, despite their critical significance for  
2 interpreting skeletal trait evolution in hominins.

3 This is not to suggest that data on bipedal chimpanzee walking mechanics are  
4 unknown. A seminal series of lab-based studies provided the first quantitative  
5 comparison of human and bipedal chimpanzee walking mechanics in the 1970s and  
6 1980s (i.e., Yamazaki et al., 1979; Okada, 1985; Yamazaki, 1985). These studies include  
7 important, initial insights into the ground forces and joint moments of human and  
8 facultative bipedal walking in chimpanzees and other taxa; however, the experimental  
9 design (i.e., mismatched speeds, markerless joint kinematics) as well as the absence of  
10 variance metrics permits only limited interspecific inferences. Indeed, forces and  
11 moments are velocity-dependent parameters (e.g., Farris and Sawicki, 2012a; Schache et  
12 al., 2015; see also SOM) and, as such, interspecific comparisons are well known to be  
13 sensitive to speed. More careful, speed-controlled comparisons of human and bipedal  
14 chimpanzee walking have examined two-dimensional (2-D) sagittal plane stance phase  
15 joint moments (Sockol et al. 2007; see also Pontzer et al., 2009), but exclude joint work  
16 and power as well as limb swing. Thus, a comprehensive characterization of the 3-D  
17 moments, work and power of human and bipedal chimpanzee walking over a full stride is  
18 still unavailable.

19 Here, we evaluate how human and bipedal chimpanzee musculoskeletal structure  
20 affects their 3-D moments, work, and power output. Specifically, we provide the first  
21 comprehensive description and direct, speed-controlled comparisons of stride-to-stride  
22 and intraspecific variation of human and bipedal chimpanzee ground reaction forces, as  
23 well as the lower/hind limb joint moment and power profiles of each species over a full  
24 walking stride. Based on their differences in musculoskeletal structure, we then test  
25 whether: 1) the estimated limb joint work and power during stance phase, especially the  
26 single-support period, is lower in humans than bipedal chimpanzees, 2) the limb joint  
27 work and power required for limb swing is lower in humans than in bipedal chimpanzees,  
28 and 3) the estimated total mechanical power during walking, accounting for the storage of  
29 passive elastic strain energy in humans, is lower in humans than in bipedal chimpanzees.  
30 For completeness, the 3-D mechanics of bipedal chimpanzees and humans were  
31 compared at matched dimensionless (i.e., relative-speed match) and dimensional (i.e.,

1 absolute-speed match) speeds. Matched dimensionless speed comparisons minimize the  
2 effects due to differences in body size or walking speed, while emphasizing those arising  
3 specifically from differences in musculoskeletal design between humans and  
4 chimpanzees. The dimensional comparison, in contrast, permits an assessment of how  
5 sensitive the interspecific differences in 3-D mechanics are to walking speed.

6

## 7 **2. Materials and methods**

### 8 *2.1. Human and chimpanzee subjects*

9 Three-dimensional kinematic and ground force data were collected for three humans  
10 (*Homo sapiens*: age =  $24.3 \pm 2.3$  years, mass =  $M_b$ :  $79.2 \pm 6.2$  kg) and three chimpanzees  
11 (*Pan troglodytes*: age =  $5.5 \pm 0.2$  years, mass =  $M_b$ :  $26.5 \pm 6.7$  kg) during bipedal  
12 walking. All subjects were male. Bipedal chimpanzees walked across an 11 m rigid, level  
13 runway at self-selected speeds, following an animal trainer offering a food reward.  
14 Human data were then collected during walking along a 20 m rigid, level runway at  
15 speeds matching the chimpanzee dataset in dimensionless (i.e., relative-speed match) and  
16 dimensional (i.e., absolute-speed match) forms (Fig. 1; Table 1; SOM Table S2) using an  
17 instantaneous speed. Bipedal chimpanzees were trained for 1 hour  $d^{-1}$ , 3–5 days  $wk^{-1}$ , for  
18 at least six months prior to the start of data collection. The University of Massachusetts  
19 Amherst Institutional Research Board and the Stony Brook University Institutional  
20 Animal Care and Use Committee approved all human (SPHHS-HSRC-13-36) and  
21 chimpanzee (2009-1731-FAR-USDA) experiments, respectively. Prior to data collection,  
22 the human subjects each provided written informed consent.

23

### 24 *2.2. Three-dimensional marker and ground reaction force data*

25 The procedures used for marker data collection and 3-D joint kinematic  
26 measurements in humans and chimpanzees have been detailed in O'Neill et al. (2015). In  
27 brief, marker positions were recorded using synchronized high-speed video cameras.  
28 Marker data for the humans were collected using an eleven-camera system recording at  
29 240 Hz (Qualisys, Inc.; Gothenburg), while chimpanzee data were collected using a four-  
30 camera system recording at 150 Hz (Xcitex, Inc., Woburn). The calibrated video  
31 recording volume for the humans was created using a wand-based nonlinear

1 transformation approach, while the recording volume for the chimpanzees was  
2 established using direct linear transformation and a custom-built calibration frame.  
3 Marker locations were digitized using Qualisys Track Manager software (Qualisys, Inc.;  
4 Gothenburg) for the humans and ProAnalyst software (Xcitex, Inc., Woburn) for the  
5 chimpanzees.

6 Ground reaction forces were collected using floor-mounted force platforms set into  
7 the runway flush to its surface, within the calibrated video recording volume. Two force  
8 platforms (AMTI, Watertown) sampling at 2400 Hz were used to record individual limb  
9 forces from humans, whereas an array of four force platforms (AMTI, Watertown)  
10 sampling at 1500 Hz were used to collect individual limb forces in chimpanzees  
11 throughout a bipedal walking stride. Marker data and force platform data were collected  
12 using a manual trigger that started and stopped video and force platform recording  
13 simultaneously. The  $x$ -,  $y$ -, and  $z$ - force data were low pass filtered with a cut-off  
14 frequency set to 60 Hz, while the marker data were filtered at 4–6 Hz. The force data  
15 were then downsampled to 240 or 150 Hz to match the synchronous video data for each  
16 species using MATLAB v. R2015 (The Mathworks, Inc., Natick). The  $x$ -,  $y$ -, and  $z$ - data  
17 from each force platform was transformed into the marker global coordinate system using  
18 markers positioned on the corner of each platform during the calibration of the video  
19 recording volume, prior to the start of an experiment. This permitted spatial  
20 transformations between the global coordinate system and the local force plate coordinate  
21 systems.

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### 23 *2.3. Musculoskeletal models and inverse dynamics*

24 Three-dimensional kinematics and ground force data were processed using generic  
25 musculoskeletal models of the pelvis and lower/hind limbs of an adult human (Delp et al.,  
26 1990) and an adult chimpanzee (O'Neill et al., 2013) scaled to the size of each subject  
27 using anatomical segment markers (O'Neill et al., 2015). All models included skeletal  
28 geometry of the pelvis and lower/hind limbs relevant to determining 3-D mechanics of  
29 the hip, knee, and ankle (talocrual) joints.

30 An inverse kinematics algorithm was used to determine the 3-D coordinates of the  
31 scaled model of each subject of each species over the full gait cycle (O'Neill et al., 2015).

1 This was done through a least-squares minimization of the discrepancy between the  
2 experimentally determined marker positions and the corresponding marker positions on  
3 the scaled model, subject to constraints enforced by the anatomical models of the joints  
4 (Lu and O'Connor, 1999; Delp et al., 2007). The 3-D kinematics and force data were  
5 combined with the scaled musculoskeletal model of each subject and used to calculate the  
6 net joint moments and mechanical power associated with the joint moments. Inverse  
7 dynamics combines rigid-segment linear and rotational motion, ground reaction forces,  
8 and limb segment inertial parameters to calculate net forces and moments at each joint.  
9 Detailed limb segment inertial parameters are provided for the adult human and adult  
10 chimpanzee models in the supplemental materials (SOM Table S1). These generic  
11 parameters were scaled to the size of each subject based on subject-specific  
12 measurements of body mass and segment lengths.

13 The instantaneous joint powers were computed at the  $j^{\text{th}}$  joint over both the stance and  
14 swing phase of walking as the dot product of the  $j^{\text{th}}$  joint moment and joint angular  
15 velocity vectors. Because the joint angles and joint moments were both expressed in the  
16 anatomically relevant but non-orthogonal joint reference frames, the moment and angular  
17 velocity vectors were both transformed into a common orthogonal reference frame before  
18 computing the dot product. This transformation is especially critical when the segments  
19 forming a joint are not closely aligned with the global reference frame, as in the  
20 abducted, flexed-limb walking of bipedal chimpanzees (O'Neill et al., 2015). The hip,  
21 knee, and ankle powers were then multiplied by two to represent the work done by both  
22 limbs over a full stride:

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$$24 \quad W_j^+ = 2 \cdot \int_{t_1}^{t_2} P_j^+ dt \quad (1)$$

$$25 \quad W_j^- = 2 \cdot \int_{t_1}^{t_2} P_j^- dt \quad (2)$$

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27 The positive and negative mechanical work of the  $j^{\text{th}}$  joint was computed by integrating  
28 over the time duration  $t_1$  to  $t_2$  of a walking stride, where  $t_1$  and  $t_2$  are the start and end of  
29 the first double-support period (ds1), single-support period (ss), second-double support



1 period (ds2) of stance phase or the limb swing phase (sw). The total limb positive and  
2 negative work in the  $i^{\text{th}}$  period or phase of a stride were calculated as the sum of the  
3 positive and negative work at each of the  $n$  joints ( $n = 3$  for each species):

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$$5 \quad W_i^+ = \sum_{j=1}^N W_j^+ dt \quad (3)$$

$$6 \quad W_i^- = \sum_{j=1}^N W_j^- dt \quad (4)$$

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8 Total positive and negative mechanical work for the complete stride ( $W_{\text{tot}}^+$ ,  $W_{\text{tot}}^-$ ) were  
9 calculated as the sum of the positive or negative work for the first double-support period  
10 ( $W_{\text{ds1}}^+$ ;  $W_{\text{ds1}}^-$ ), single-support period ( $W_{\text{ss}}^+$ ;  $W_{\text{ss}}^-$ ), second double-support period ( $W_{\text{ds2}}^+$ ;  $W_{\text{ds2}}^-$ )  
11 and limb swing ( $W_{\text{sw}}^+$ ;  $W_{\text{sw}}^-$ ). The positive and negative work terms were  
12 subsequently divided by the stride time to determine average power output ( $P_i^+$ ;  $P_i^-$ ).

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#### 14 *2.4. Elastic and ‘muscle fiber’ work and power estimates*

15 In human walking, passive elastic energy is stored at the ankle and hip joints during  
16 the single-support period and released in the second-double-support period as well as,  
17 perhaps, in early limb swing (e.g., Fukunaga et al., 2001; Ishikawa et al., 2005;  
18 Whittington et al., 2008; Eng et al., 2015). The structures most responsible for this are the  
19 Achilles tendon at the ankle and the joint capsule ligaments and iliotibial tract at the hip.  
20 A similar mechanism is not expected at the knee joint due to the opposite phasing (i.e.,  
21 positive power in single-support and negative power in the second-double-support  
22 period) of the joint power during late stance phase. We estimated that elastic energy was  
23 stored during the portion of the single-support period in which the relevant joint power  
24 curve was negative. We assumed that the elastic energy storage equaled the negative  
25 work, and that all of the elastic energy stored was supplied to the subsequent period of  
26 positive power generation. At both the dimensionless and dimensional walking speeds,  
27 the positive power generation occurred during the double-support period for the ankle, or  
28 the double-support period and early limb swing for the hip. As such, the net positive  
29 elastic work during the single-support period was estimated as:

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$$W_{el,j} = 2 \cdot \left| \int_{t_{ss1}}^{t_{ss2}} P_j^- dt \right| \quad (5)$$

where  $W_{el,j}$  is the elastic work absorbed at the  $j^{\text{th}}$  joint ( $a$ : ankle;  $h$ : hip) during the single-support period of the stance phase of a walking stride, and used to generate positive elastic recoil. The positive elastic power output was computed by dividing the positive elastic work by stride time. Therefore, the total ‘muscle fiber’ work and power were the estimated positive elastic work at the ankle ( $W_{el,a}$ ) and hip ( $W_{el,h}$ ) subtracted from the total positive mechanical work ( $W_{\text{tot}}^+$ ). The positive mechanical power attributable to ‘muscle fiber’ was computed by dividing the ‘muscle fiber’ work by stride time.

## 2.5. Analysis and statistics

Four strides per subject were analyzed for the humans (H) and chimpanzees (C). All 3-D moment and power data were normalized to 101 points over one full stride, facilitating comparisons of multiple strides. This also permitted the mean  $\pm$  standard deviation (s.d.) of the moment and power curves to be determined per species.

For the chimpanzees, walking speed was calculated as the average of the instantaneous forward velocity of four markers (i.e., 3 pelvis, 1 hip marker) over the full stride, while for humans a marker placed over the sacrum was used. To account for differences in body size among subjects and species, analyses were performed with dimensionless variables, using the base units of body mass  $M_b$ , gravitational acceleration  $g$ , and average lower/hind limb length  $L$ . Lower/hind limb length was measured as the average height of the greater trochanter marker from the ground during quiet standing for humans and during the middle of the single-support period for chimpanzees ( $H = 0.92 \pm 0.05$ ,  $C = 0.39 \pm 0.02$  m). Velocity ( $v$ ) was made dimensionless by the divisor  $(gL)^{0.5}$  and as the Froude number ( $Fr = v^2/gL$ ). Force was made dimensionless by the divisor  $M_b g$ , moment and work by  $M_b g L$  and power by  $M_b g^{1.5} L^{0.5}$ . In all cases, stance, swing, and stride duration were determined based on the ground reaction forces.

To compare the stride-to-stride, intraspecific, and interspecific variation of the ground reaction forces of our human and chimpanzee samples, the adjusted coefficient of

1 multiple correlation (CMC) was used (Kadaba et al. 1989,  $r_a^2$ ). The CMC represents the  
2 correlation of the ground reaction force among strides for each individual (i.e., stride-to-  
3 stride variation) or among the individuals (i.e., intraspecific variation). The balanced  
4 human and chimpanzee datasets permit a direct, interspecific comparison of CMCs  
5 computed using the species means.

6 To compute the difference in dimensionless work and power between humans and  
7 bipedal chimpanzees, the percent difference was calculated as  $|(s_1 - s_2)| / [(s_1 + s_2) / 2] \cdot 100$ ,  
8 where  $s_1$  (species 1) and  $s_2$  (species 2) are the species mean work and power parameters.  
9 Because the sample was balanced, a two-level nested analysis of variance (ANOVA) was  
10 used to compare work and power output in each period or phase of a walking stride (i.e.,  
11 double-support 1, single support, double-support 2, limb swing; Fig. 1), as well as the  
12 total mechanical work and power output over a full stride to test hypotheses 1-3. A two-  
13 level nested approach allowed repeated individual subject trials to be incorporated as  
14 random effects and was therefore preferred to an independent samples t-test based on  
15 subject means. Statistical significance was set at  $\alpha = 0.05$ . The nested ANOVA was  
16 computed in R v. 4.0.2 using the base package for Mac OS (R Development Core Team,  
17 2020).

18 Due to the small sample sizes for each species, omega-squared ( $\omega^2$ ) was also used to  
19 assess the effect size of the difference between chimpanzees and human comparisons  
20 outlined in hypotheses 1-3. Effect size descriptive thresholds were  $\omega^2 \leq 0.01 =$  ‘small’,  
21  $\omega^2 \leq 0.06 =$  ‘medium’,  $\omega^2 \leq 0.14 =$  ‘large’ (Field, 2013). Effect size calculations were  
22 implemented in R v. 4.0.2 using the ‘effectsize’ package (R Development Core Team,  
23 2020).

24

### 25 **3. Results**

26 The average walking speeds of humans and chimpanzees were  $1.66 \pm 0.06$  and  $1.09 \pm$   
27  $0.10 \text{ m s}^{-1}$ , respectively. These correspond to similar dimensionless velocities ( $v'$ ; H =  
28  $0.56 \pm 0.01$ , C =  $0.56 \pm 0.06$ ) and  $Fr$  numbers (H =  $0.31 \pm 0.02$ , C =  $0.31 \pm 0.06$ ) (Table  
29 1). These speeds are close to—but a bit faster than—the preferred overground speeds for  
30 human walking, and well below the expected walk-run transition speed for terrestrial  
31 mammals (i.e.,  $v' = 0.7$ ;  $Fr = 0.5$ ; Alexander, 1989; Kram et al., 1997).

1 Here, we describe the three-dimensional ground reaction forces, lower/hind limb joint  
2 moment and power profiles of humans and bipedal chimpanzees walking over a full  
3 stride at matched dimensionless speeds. The limb-joint work and power in stance, swing  
4 and over a full stride are determined to test hypotheses 1-3.

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### 6 *3.1. Ground reaction forces, stride-to-stride, and intraspecific variation*

7 The ground reaction forces of humans and chimpanzees were different in both  
8 magnitude and pattern (Fig. 2). The vertical force was monophasic in bipedal  
9 chimpanzees, lacking the second peak from the single-support period into the second  
10 double-support period that is characteristic of human walking. The bipedal chimpanzee  
11 anterior-posterior force was distinct from humans, as it exhibited a smaller peak force in  
12 both posterior and anterior directions, while the mediolateral force was larger, most  
13 notably during the single-support period.

14 The CMCs were smaller between strides than between individuals for both humans  
15 and bipedal chimpanzees (Table 2). This indicates that there is more variation among  
16 humans and chimpanzees in ground reaction forces than there is within a given individual  
17 from one stride to the next. Among individuals, the medio-lateral force was the most  
18 variable in chimpanzees ( $r^2_a = 0.847 \pm 0.012$ ) and humans ( $r^2_a = 0.916 \pm 0.038$ ). Directly  
19 comparing the CMC values of human and chimpanzee samples indicates that, on average,  
20 chimpanzees are more variable in their ground reaction force stride-to-stride than humans  
21 at matched dimensionless speeds ( $H = r^2_a = 0.985$ ,  $C = r^2_a = 0.922$ ).

22

### 23 *3.2. Limb-joint moment profiles*

24 As expected, humans and chimpanzees were quite different in the magnitude and  
25 pattern of the limb joint moments over a full stride (Fig. 3; Table 3). At the hip,  
26 chimpanzees exhibit the largest joint moments in hip flexion-extension, with peak hip  
27 extension moment occurring in the first double-support period and continuing throughout  
28 the single-support period of stance. Unlike humans, for whom the net flexion moment  
29 begins near midstance, the net flexion moment does not occur until the second-double  
30 support period in bipedal chimpanzee walking. Humans and chimpanzees were opposite  
31 in phase in the frontal plane, where chimpanzees exhibit a net hip adduction moment

1 throughout stance that peaks in the second-double support period. Near the middle of the  
2 single support period, the hip adduction-abduction moment approaches zero in both taxa.  
3 Chimpanzees exhibit substantial hip rotational moments, with a large internal rotation  
4 moment throughout the single-support and second double-support periods. During limb  
5 swing, chimpanzees exceed humans in the magnitude of internal and external rotational  
6 moments.

7 Humans and chimpanzees both exhibit an initial knee flexion moment in the first  
8 double-support period, and then rapidly shift to a large net extension moment at the start  
9 of the single-support period. Unlike humans, chimpanzees have a net knee extension  
10 moment throughout the single and second double-support periods. The pattern and  
11 magnitude of knee flexion-extension moments in limb swing are similar for both species.

12 The chimpanzee exhibits a net ankle plantar flexion moment throughout stance phase,  
13 including during the first double-support period. This differs from humans, who exhibit a  
14 net dorsiflexion moment in the first double-support period, likely associated with our  
15 distinct ‘heel strike’. Whereas chimpanzees maintain a near-constant ankle plantar  
16 flexion moment throughout the remainder of stance, there is an increase in the magnitude  
17 of the net plantar flexion moment throughout the single and second double-support  
18 periods in humans, which peaks in the second-double support period. For both species,  
19 there is a small net dorsiflexion moment throughout limb swing, on average.

20

### 21 *3.3. Limb-joint power profiles*

22 The magnitude as well as pattern of joint powers differed between humans and  
23 bipedal chimpanzees (Fig. 4; Table 4). In both humans and chimpanzees, there was  
24 negative hip power in the first double-support period. In the single-support period, there  
25 is an initial period of hip energy generation followed by hip energy absorption in humans,  
26 whereas chimpanzee hips generate energy throughout this period. In the second-double  
27 support period, there was positive power in human hips, whereas there was negative  
28 power in chimpanzee hips. For humans, the second double-support period positive power  
29 continues into limb swing, ending with a small burst of energy absorption. Chimpanzees  
30 generate substantial positive hip power in the first half of limb swing, ending with a small  
31 burst of energy generation.

1 At the knee joint, there was a substantial positive power peak in the first double-  
2 support period in both chimpanzees and humans, followed by complex, cyclical pattern  
3 of energy absorption and generation through the single-support and second double-  
4 support periods. In the middle of the single-support period, chimpanzees have a small  
5 burst of energy generation, whereas humans are near zero power output. Throughout limb  
6 swing, there was substantial negative power at the knee in both species, especially in the  
7 second half of swing phase.

8 The ankle joint in chimpanzees is characterized by energy absorption followed by  
9 energy generation over the stance phase. This is distinct from humans, where a small  
10 amount of energy absorption occurs in the first double-support period, followed by a  
11 period of negative power at the end of the single-support period and then substantial  
12 positive power output in the second-double support period. The peak dimensionless  
13 positive power in the second-double support period is almost three times greater in  
14 humans than chimpanzees at matched dimensionless walking speeds, on average (Table  
15 4). For both species, there is a relatively small amount of energy generation from the  
16 ankle throughout limb swing.

17

### 18 *3.4. Limb-joint work and power in stance (hypothesis 1)*

19 Humans generate less dimensionless positive mechanical work ( $W_{ds1}^+$ :  $F_{1,18} = 21.38$ ,  $p$   
20  $= 0.0099$ ;  $\omega^2 = 0.77$ ) and power ( $P_{ds1}^+$ :  $F_{1,18} = 12.67$ ,  $p = 0.0236$ ;  $\omega^2 = 0.66$ ) than  
21 chimpanzees during the first double-support. The same was true for the single-support  
22 period positive mechanical work ( $W_{ss}^+$ :  $F_{1,18} = 27.58$ ,  $p = 0.0063$ ;  $\omega^2 = 0.82$ ) and power  
23 ( $P_{ss}^+$ :  $F_{1,18} = 13.51$ ,  $p = 0.0213$ ;  $\omega^2 = 0.68$ ). In the second double-support period, humans  
24 generate much more positive mechanical work ( $W_{ds2}^+$ :  $F_{1,18} = 38.15$ ,  $p = 0.0035$ ;  $\omega^2 =$   
25  $0.86$ ) and power than chimpanzees ( $P_{ds2}^+$ :  $F_{1,18} = 76.51$ ,  $p = 0.0009$   $\omega^2 = 0.93$ ; Fig. 5). In  
26 all cases, the effect sizes were ‘large’. This provides partial support for our first  
27 hypothesis.

28

### 29 *3.5. Limb-joint work and power in swing (hypothesis 2)*

30 Humans generate less dimensionless positive mechanical work ( $W_{sw}^+$ :  $F_{1,18} = 16.71$ ,  $p$   
31  $= 0.0016$ ;  $\omega^2 = 0.72$ ) and power ( $P_{sw}^+$ :  $F_{1,18} = 6.649$ ,  $p = 0.0614$ ;  $\omega^2 = 0.48$ ) than

1 chimpanzees in limb swing. The difference in positive work was significant, but the  
2 difference in power only near significant; however, in both cases the effect size was  
3 ‘large’ (Fig. 6). This provides partial support for our second hypothesis.

### 4 5 *3.6. Total mechanical work and power (hypothesis 3)*

6 The total dimensionless positive mechanical work ( $W_{\text{tot}}^+$ ) and power ( $P_{\text{tot}}^+$ ) was  
7 23.3% and 12.0% smaller in humans than chimpanzees, respectively. The difference in  
8 mechanical work was ‘large’ and significant ( $F_{1,18} = 11.55$ ,  $p = 0.0273$ ;  $\omega^2 = 0.64$ ), while  
9 the difference in power was a ‘medium’ effect, and not statistically significant ( $F_{1,18} =$   
10  $1.372$ ,  $p = 0.3070$ ;  $\omega^2 = 0.06$ ). The modest differential in total mechanical power is due to  
11 the substantial positive power output in the second double-support period of a human  
12 walking stride. However, when the mechanical work and power attributable to elastic  
13 storage and release at the human ankle and hip were accounted for, the estimated total  
14 positive ‘muscle fiber’ work and power percent differential between species increased to  
15 46.9% and 35.8%, respectively. The differences in estimated total positive ‘muscle fiber’  
16 work ( $F_{1,18} = 33.19$ ,  $p = 0.0045$ ,  $\omega^2 = 0.84$ ) and power ( $F_{1,18} = 10.56$ ,  $p = 0.0314$ ,  $\omega^2 =$   
17  $0.61$ ) between species were both significant, and the effect sizes were ‘large’ (Fig. 7),  
18 supporting our third hypothesis.

### 19 20 *3.7. Distribution of work across limb joints*

21 In human walking, the stance phase work is predominately from the ankle ( $47.0 \pm$   
22  $6.5\%$ ), and from the hip in swing phase ( $82.9 \pm 3.2\%$ ). This contrasts with chimpanzees  
23 in which most of their positive mechanical work is from the hip in both stance ( $49.1 \pm$   
24  $3.7\%$ ) and swing ( $88.5 \pm 1.9\%$ ) phases (Fig. 8).

25 In stance phase, human negative work is predominately absorbed at the knee ( $46.6 \pm$   
26  $3.0\%$ ), whereas chimpanzees absorb most of their mechanical work at the ankle ( $42.4 \pm$   
27  $2.0\%$ ). In swing phase, the knee accounts for nearly all of the negative work in both  
28 species ( $H = 91.2 \pm 4.6\%$ ;  $C = 93.0 \pm 2.1\%$ ).

### 29 30 *3.8. Dimensional vs. dimensionless walking mechanics*



1 For the comparison at matched dimensional speeds (i.e., absolute-speed match), the  
2 average human walking speed was  $1.08 \pm 0.02 \text{ m s}^{-1}$ . This corresponds to a  $v'$  of  $0.36 \pm$   
3  $0.01$  and  $Fr$  of  $0.13 \pm 0.02$  (SOM Table S2), which are slower than the relative-speed  
4 match.

5 Overall, the humans had smaller moments, work and power at matched dimensional  
6 speed than at matched dimensionless speed. As such, the interspecific differences in  
7 dimensional positive mechanical work and power output were consistently larger, with  
8 the exception of the second double-support period positive work and power (SOM Figs.  
9 S2–S8; SOM Tables S2–S5). In this case, the positive mechanical work and power output  
10 were more similar between species than at the relative-speed match (SOM Fig S5). The  
11 human 3-D joint moments and powers had similar profiles at  $1.08 \text{ ms}^{-1}$  and  $1.66 \text{ ms}^{-1}$ .  
12 However, the magnitude of the interspecific difference in total mechanical work and  
13 power were much larger (H = 83.6% vs. C = 77.8%; SOM Fig. S7) than at matched  
14 dimensionless speeds, even without accounting for elastic power output. Indeed, the  
15 interspecific difference in total ‘muscle fiber’ work and power are larger still (H =  
16 106.9% vs. C = 111.9%; SOM Fig S7). This reinforces the importance of careful, speed-  
17 controlled comparisons for testing the effects of musculoskeletal structure on locomotor  
18 capabilities.

19

## 20 **4. Discussion**

### 21 *4.1. Ground reaction forces, stride-to-stride and intraspecific variation*

22 Our results are broadly consistent with previous descriptions of the 3-D ground force  
23 components in bipedal chimpanzee walking (Kimura et al., 1977; Pontzer et al., 2009).  
24 As expected, all three animals exhibited monophasic vertical force patterns, with small  
25 magnitude anterior-posterior force peaks compared to a human walking step at similar  
26 dimensionless speeds, especially in the second double-support period (i.e., push-off). The  
27 species difference in peak vertical force magnitude (H = 1.27, C = 1.13; Fig. 2) supports  
28 the inference that facultative bipeds walk with lower peak vertical force (Schmitt, 2003),  
29 albeit by a small amount at matched dimensionless speeds. However, this difference is  
30 not present at matched dimensional speeds (SOM Fig. S2). Overall, the ground reaction  
31 forces in bipedal chimpanzees appear quite similar to the 3-D forces of ‘highly-trained’



1 bipedal macaques (Kimura et al., 1977; Ogihara et al., 2007), as well as some other  
2 facultative bipeds (Kimura, 1977). A qualitative comparison of our chimpanzee dataset to  
3 similar data from ‘highly-trained’ bipedal macaques (Ogihara et al., 2007) suggests that  
4 bipedal chimpanzees and macaques are much more similar to each other than either are to  
5 humans.

6 The data herein indicate that bipedal chimpanzees exceed humans in the variation of  
7 their ground reaction forces from stride to stride. Among individuals, chimpanzees are  
8 more variable than humans in their anterior-posterior and medio-lateral ground forces,  
9 but similar in their vertical component. These results are consistent with CMC results for  
10 the pelvis and lower/hind limb 3-D kinematics reported in O’Neill et al. (2015). The  
11 similarities in the vertical force CMC values suggest that the monophasic pattern is quite  
12 consistent across our three subjects, as suggested by average patterns from chimpanzees  
13 in earlier studies from a range of ages and body masses (Kimura et al., 1977; Pontzer et  
14 al., 2009).

15

#### 16 *4.2. Joint moments*

17 Our results are consistent with earlier 2-D data on the sagittal plane moments of  
18 humans and bipedal chimpanzees throughout stance (Yamazaki et al., 1981; Sockol et al.,  
19 2007). In particular, bipedal chimpanzees—like all facultative bipeds studied to date  
20 (Yamazaki et al., 1981; Yamazaki, 1985)—have a substantial hip extension moment for  
21 nearly the full duration of stance.

22 However, these 3-D data also provide insight into bipedal chimpanzee mechanics in  
23 the non-sagittal planes, and over a full walking stride. Hip abduction-adduction moments  
24 are different in magnitude and opposite in direction for human and bipedal chimpanzee  
25 walking. The absence of an abductor moment in the stance phase in bipedal chimpanzee  
26 walking, and throughout the single-support period in particular, provides quantitative  
27 support to the longstanding view that the human ‘lateral balance mechanism’ is a derived  
28 aspect of hominin walking (e.g., Stern and Susman, 1981; Lovejoy, 1988). The marked  
29 contrast in hip abduction-adduction moments between humans and bipedal chimpanzees  
30 demonstrates that the single-support period of a bipedal walking stride need not follow  
31 the simple ‘mechanical model’ of hip loading, which assumes a large abduction moment

1 during single-support (e.g., Lovejoy et al., 1973; Ruff, 1995; see also Warrener, 2017).  
2 This is an important consideration in general, but especially when extending this human-  
3 based approach to the earliest hominins (e.g., Richmond and Jungers, 2008).

4 The single-support period of bipedal chimpanzees is characterized by a larger internal  
5 (i.e., medial) rotation moment than in human walking. This supports the inference of  
6 Stern and Susman (1981:164) that for chimpanzees, "... the problem posed during the  
7 single support phase of bipedality is to prevent collapse into lateral rotation at the stance  
8 side hip." Our results confirm and extend this inference, indicating that there is also a  
9 substantial hip adduction moment in bipedal chimpanzee walking, which reaches a  
10 similar magnitude to the internal rotation moment near the end of the single-support  
11 period. Taken together, the moment data herein confirm that the distinction between the  
12 3-D mechanics of the single-support period in bipedal chimpanzee and human walking is  
13 a reliance on 'rotation-based' or 'rotation-adduction-based' hip mechanics in  
14 chimpanzees, and 'abduction-based' hip mechanics in humans for 'maintaining lateral  
15 balance'. How individual hind-limb muscle-tendon units contribute to balancing these  
16 moments in bipedal chimpanzees requires additional quantitative analyses, since an  
17 individual muscle-tendon unit will, in general, have non-zero moment arms about all  
18 three hip joint axes that can change in magnitude and sign during movement (e.g.,  
19 O'Neill et al., 2013).

20 The joint moment data also extend our earlier findings (O'Neill et al., 2015, 2018)  
21 that the use of a 'heel strike' during walking in humans is distinct, not just in its  
22 consistency (Elftman and Manter, 1938; Webber and Raichlen, 2016), but in both its  
23 associated ankle kinematics and mechanics, despite some qualitative similarities with  
24 other African apes overall (Schmitt and Larson, 1993). At the human ankle, there is a  
25 consistent, net dorsiflexion moment from 'heel strike' through the first double-support  
26 period, which contrasts with the net plantar flexor moment in bipedal chimpanzees. How  
27 these different foot strike patterns impact ankle muscle-tendon mechanics and energetics  
28 in walking is still unclear, but some limited metabolic data indicate that evolution of the  
29 hominin 'heel strike' is of much greater consequence for walking than running (e.g.,  
30 Cunningham et al., 2010; Gruber et al., 2013). When human-like 'heel strike' walking  
31 first appeared in hominin evolution is still unclear, although a robust calcaneal tuber and

1 lateral plantar process has been used to infer its presence as early as *Australopithecus*  
2 *afarensis* (e.g., Latimer and Lovejoy, 1989; Prang, 2015; DeSilva et al., 2019). Still, this  
3 is difficult to establish even from fossil footprints such as the Laetoli site tracks (e.g.,  
4 Leakey and Hay, 1979; Masao et al., 2016), since both human and bipedal chimpanzee  
5 foot strikes induce relatively deep heel impressions (Hatala et al., 2016a).

6 Human and bipedal chimpanzee joint moments are broadly similar in direction and  
7 magnitude throughout limb swing, except in hip internal-external rotation. This is  
8 consistent with greater circumduction of the hind limb in bipedal chimpanzee walking  
9 (O'Neill et al., 2015). The limb-swing rotational moments also provide some indirect  
10 support to the inference of Stern and Larson (1993:425) that m. obturator externus is  
11 activated “to counteract [a] medial rotatory effect” in the first half of limb swing, as there  
12 is a net internal (i.e., medial) rotation moment at this time in bipedal chimpanzees.

#### 13 14 *4.3. Mechanical work and power in stance*

15 Our results provide some support for the first hypothesis that human walking involves  
16 lower work and power output in stance phase than bipedal chimpanzees. This is due, in  
17 large part, to significantly less positive mechanical work and power output in the first  
18 double-support and single-support periods of a human walking stride. While both humans  
19 and chimpanzees absorb mechanical energy at the hip in the first double-support period,  
20 there is greater net positive mechanical work at the knee (Figs. 3A, B) in bipedal  
21 chimpanzee walking.

22 The greater positive mechanical work in the single-support period in chimpanzees is  
23 due primarily to greater positive power at the hip, with small contributions from the knee  
24 and ankle. This is consistent with previous assessments of sagittal plane hip moments,  
25 which had indicated a substantial force-requirement at the hip during stance phase in  
26 bipedal chimpanzees (Sockol et al., 2007; Pontzer et al., 2009). In middle single-support,  
27 the lower back, pelvis and lower limbs of humans facilitate near-zero lower limb joint  
28 power, followed by a short period in which mechanical energy is absorbed at the hip and  
29 ankle (i.e., ‘preload’: Kuo et al., 2005; Zelik et al., 2015).

#### 30 31 *4.4. Elastic work and power*

1 In contrast to the first double-support and single-support periods, humans markedly  
2 exceed bipedal chimpanzees in total positive mechanical work and power during the  
3 second double-support period due to substantial mechanical energy generation at the  
4 ankle for push-off. Muscle-tendon models (e.g., Hof et al., 1983) and direct imaging of  
5 muscle fiber dynamics (e.g., Fukunaga et al., 2001; Ishikawa et al., 2005; Farris and  
6 Sawicki, 2012b) indicate that much of the positive power for human push-off is due to  
7 the elastic recoil of the Achilles tendon, stretched during the single-support period. Based  
8 on the mechanical energy absorbed at the ankle during the single-support period at this  
9 speed, we estimated that  $39 \pm 13\%$  of the positive power for ankle push-off is from  
10 elastic storage, on average (Fig 5). The upper error margin of our indirect, inverse  
11 dynamics-based approximation overlaps direct imaging of muscle fiber behavior in  
12 humans walking between  $1.25$  and  $1.75 \text{ ms}^{-1}$ , which indicates a significant contribution  
13 from elastic power (i.e., 50 to 55%), at least for m. gastrocnemius (Farris and Sawicki,  
14 2012b). It has been reported that the typical procedures used in direct imaging studies can  
15 overestimate the elastic energy returned from tendons (Zelik and Franz, 2017), which  
16 may account for some of the difference in mean values. Of course, both these indirect and  
17 direct estimates are subject to the limitations of the inverse-dynamics approach and  
18 would benefit from continued refinement using detailed musculoskeletal models that  
19 account for individual muscle-tendon unit behavior (e.g., Horner and Zelik, 2016).

20 The contribution of elastic positive hip work to the second double-support period and  
21 limb swing is less well understood but has been estimated to be 10–58% across a range of  
22 walking speeds (Yoon and Mansour, 1982; Varhas et al., 1990; Whittington et al. 2008).  
23 Herein, we estimated that the human hip stored and released  $25.5 \pm 10.7\%$  of the positive  
24 work to the second double-support period and limb swing, which is in the middle of this  
25 published range. Hip joint capsular ligaments and associated tissues have long been  
26 identified as a source of hip elastic work (e.g., Neptune et al., 2008; Whittington et al.,  
27 2008), since the anterior tissues (e.g., iliofemoral ligament) will be strained during hip  
28 extension. The iliotibial tract, which has a hip flexion moment arm, appears to contribute  
29 as well (Eng et al., 2015). Direct imaging of hip flexor muscle fiber behavior (e.g., rectus  
30 femoris) would help elucidate the role of muscle and tendon to positive power output in  
31 the second double-support and limb swing periods of a human walking stride.

1 Over a full stride, our estimated total elastic work contributions (i.e., ankle and hip:  
2  $24.2 \pm 3.1\%$  at  $1.66 \text{ ms}^{-1}$ ;  $31.1 \pm 7.2\%$  at  $1.08 \text{ ms}^{-1}$ ) is similar to the series elastic element  
3 contributions to the total lower limb work from individual muscle tendon dynamics (e.g.,  
4  $29.4\%$  tendon elastic work to muscle fiber work at  $1.2 \text{ ms}^{-1}$ : Sasaki et al. 2009). This  
5 suggests that our estimates are reasonable initial approximations. It is well known that net  
6 joint-level measures do not equate to total muscle-tendon unit work and power, owing to  
7 bi-articular muscle recruitment and muscle co-contraction (Sasaki et al. 2009), which  
8 may differ between human and bipedal chimpanzee walking.

9 The hind limb joint mechanics and muscle-tendon structure of bipedal chimpanzees  
10 suggest a limited capacity for elastic work and power output in a walking stride. First, the  
11 joint mechanics data herein demonstrate that, unlike human walking, the second half of  
12 the single-support period of chimpanzee bipedal walking involves no net negative hip or  
13 ankle work (see Fig. 4 and SOM Fig. S4) for elastic energy storage and is instead a  
14 continuous period of positive work. The absence of this negative work suggests that there  
15 is no significant elastic contribution from the hip and ankle to ‘push-off’ in bipedal  
16 chimpanzees. This is also implied by the hip flexion-extension range of motion, which is  
17 about half that of humans (O’Neill et al., 2015: C:  $27^\circ$ ; H:  $48^\circ$ ), indicating less capacity  
18 for hip tissue strain and elastic energy storage overall. Indeed, the passive tissue strain  
19 and elastic work of the iliotibial tract of bipedal chimpanzees has been estimated to be  
20 only a small fraction of human values (Eng et al., 2015), due in large part to this  
21 kinematic difference. Second, chimpanzee pelvis and hind limb muscles are also  
22 characterized by relatively longer muscle fibers than human lower limb muscles, and the  
23 near absence of a free Achilles tendon (e.g., Thorpe et al., 1999; O’Neill et al., 2013,  
24 2017). Chimpanzee pelvis and hind limb relative muscle fiber lengths (i.e., ratio of  
25 muscle fiber length to total muscle-tendon unit length) are about 15% longer than humans  
26 overall (C =  $0.59 \pm 0.21$ , H =  $0.44 \pm 0.25$ ), and about twice as long for the leg/shank  
27 muscles in particular (C =  $0.33 \pm 0.14$ , H =  $0.15 \pm 0.04$ ; Arnold et al., 2010; O’Neill et  
28 al., 2013; see also Thorpe et al., 1999). This architectural design requires the muscle  
29 fibers to more closely track the muscle-tendon length changes due to the joint motions,  
30 implying a limited capacity for tendon strain and thus storage and release of elastic  
31 energy. Still, short, stiff tendons, long, thin internal tendons and sarcomeric proteins may

1 permit some degree of elastic work and power output (e.g., Alexander, 1988; Roberts,  
2 2016). Decomposition of joint-level 3-D mechanics among individual muscles and series  
3 elastic elements via optimization can provide a more detailed accounting of the muscle-  
4 tendon mechanical work and power (e.g., Anderson and Pandy, 1993, 2001), and more  
5 precise estimates of the elastic contribution to human and bipedal chimpanzee walking.

#### 6 7 *4.5. Mechanical work and power in limb swing*

8 Our results also provide some limited support for our second hypothesis that human  
9 limb structure reduces limb swing positive work and power. The greater positive work  
10 and, to a lesser extent, power in bipedal chimpanzee limb swing is consistent with the  
11 hypothesized differences in limb structure. However, it is difficult to isolate the  
12 contribution of the limb-mass distribution per se. This is because bipedal chimpanzees  
13 engage in more hip rotation about abducted, flexed hind limbs throughout limb swing  
14 (O'Neill et al. 2015), for reasons likely independent of limb-mass distribution. Increasing  
15 limb flexion (Wu and Kuo, 2016) and circumduction (Shorter et al., 2017) in limb swing  
16 increases limb joint work and positive power over a stride in human perturbation studies,  
17 regardless of limb-mass distribution.

18 Elastic work and power from the hip likely contribute to both the second double-  
19 support period and the first half of limb swing in human walking. Given the sinusoidal  
20 shape of the positive power burst at the hip that peaks at the stance-swing transition (Fig.  
21 5A), we can estimate that about half of the hip elastic work and power is output for limb  
22 swing, which would further increase the human-chimpanzee limb swing differential. In  
23 contrast, in the second double-support period of bipedal chimpanzee walking, the hip is  
24 insufficiently extended (i.e., 25° of hip flexion, on average; O'Neill et al., 2015) to strain  
25 the associated elastic tissues and permit a positive elastic power contribution to the first  
26 half of limb swing. This suggests a distinct contribution of human hip mechanics during  
27 the single and second double-support periods to reducing limb swing work and power,  
28 independent of limb-mass distribution.

#### 29 30 *4.6. Total mechanical work and power*

1 On average, human walking involves 23.3% and 12.0% less positive mechanical  
2 work and power than bipedal chimpanzees, respectively. These differentials are enhanced  
3 by human capacities for elastic work and power output over a stride, which are assumed  
4 to be zero in bipedal chimpanzees herein. Together, these results support our third  
5 hypothesis, as the total ‘muscle fiber’ work and power output of the human lower limb is  
6 46.9% and 35.8% lower than the hind limbs of bipedal chimpanzees walking at matched  
7 dimensionless speeds. This is consistent with the broad-sense expectation that our mobile  
8 lower back, pelvis and long lower limbs with short feet of humans reduce the total  
9 mechanical work and power output of our walking stride when compared to bipedal  
10 chimpanzees; however, decomposing the individual contributions of specific traits to  
11 these joint-level differences is complex, and requires additional investigation.

12 Our total mechanical power differential accounts for some, but not all, of the  
13 differential in the metabolic cost of walking between humans and bipedal chimpanzees  
14 (i.e., 50 to 75%: Sockol et al., 2007; Pontzer et al., 2014). Of course, joint-level metrics  
15 do not account for differences in muscle co-contraction, muscle contractile behavior (i.e.,  
16 force-length-velocity dynamics), muscle architecture and myosin heavy chain content  
17 between species (e.g., O’Neill et al., 2013, 2017), all of which can further increase the  
18 human-chimpanzee differential. For example, the relatively small, mobile limb joints of  
19 chimpanzees (e.g., Jungers, 1988) may require higher levels of muscle co-contraction for  
20 joint stabilization over a bipedal walking stride. In our view, model-based approaches  
21 that permit optimization of individual muscle mechanics and metabolic costs can improve  
22 upon previous joint-level ‘force-based approximations’ of muscle energy use (e.g.,  
23 Roberts et al., 1998; Sockol et al., 2007; Pontzer et al., 2009), since they parameterize  
24 individual-muscle excitation patterns as well as the metabolic costs of activation, cross-  
25 bridge cycling, shortening-lengthening and associated contractile element dynamics (e.g.,  
26 Umberger and Rubenson, 2011).

27

#### 28 *4.7. Distribution of work and power across the limb joints*

29 In humans, positive mechanical work and power output has been shifted to the distal  
30 joints, with 47% of the work performed at the ankle throughout stance phase. Notably,  
31 this facilitates the use of shorter muscle fibers (Thorpe et al., 1999; Arnold et al., 2010;



1 O'Neill et al., 2013, 2017) and a greater reliance on elastic energy storage and release at  
2 the ankle. Both humans and chimpanzees have relative muscle fiber lengths (i.e., ratio of  
3 muscle fiber length to total muscle-tendon unit length) that are more than twice as long  
4 for pelvis and thigh muscles ( $H = 0.55 \pm 0.15$ ,  $C = 0.67 \pm 0.20$ ) as for leg muscles ( $H =$   
5  $0.15 \pm 0.04$ ,  $C = 0.33 \pm 0.14$ ; Arnold et al., 2010; O'Neill et al., 2013; see also Thorpe et  
6 al., 1999). Our enlarged m. soleus and long Achilles tendon (e.g., O'Neill et al., 2013), in  
7 particular, are likely derived traits within the hominin lineage that enhance our positive  
8 push-off mechanics as well as elastic energy storage and release. Bipedal chimpanzees  
9 have a more proximal distribution of limb work, with 49% performed at the hip during  
10 stance. A reliance on proximal joints for positive work and power necessitates the  
11 activation of longer, parallel-fibered muscles (e.g., Thorpe et al., 1999; O'Neill et al.,  
12 2013), whose shortening-lengthening behavior is expected to more faithfully track 3-D  
13 joint motion, with less capacity for decoupling of muscle fiber and tendon strain. In limb  
14 swing, both humans and bipedal chimpanzees primarily use the hip. To the extent that the  
15 longer, heavier feet of chimpanzees affect their limb swing mechanics, this may account  
16 for some of the relatively larger contribution of hip ( $H = 83\%$ ,  $C = 89\%$ ) work (Fig. 8) in  
17 bipedal chimpanzees than humans.

18 Over a steady, level walking stride, no net mechanical work is performed on the  
19 environment, and the total whole-body positive and negative work must sum to zero. In  
20 humans, muscle-tendon units of the lower limb provide most of the positive work through  
21 rotations of the joints; however, soft tissues such as the heel pad, intervertebral discs or  
22 articular cartilages likely compress and perform significant negative work on the body  
23 without rotating the lower limb joints (Zelik and Kuo, 2013; Zelik et al., 2015). Our  
24 results indicate that humans exhibit an imbalance of limb joint work, with average  
25 negative-to-positive ratios of  $67 \pm 9\%$  per step (i.e., excluding limb swing). This is nearly  
26 identical to ratio of 68% per step in level walking in DeVita et al. (2007). At matched  
27 dimensionless speeds, bipedal chimpanzee negative-to-positive work is more balanced,  
28 with a ratio of  $88 \pm 8\%$  per step. This is due to greater negative work—and more active  
29 muscle-tendon unit lengthening—in bipedal chimpanzee than human walking. Although  
30 the metabolic cost of performing negative muscle fiber work is low (Woledge et al.,  
31 1985), energy dissipation through soft tissue deformations has no cost at all. As an



1 example, a human-like heel strike permits mechanical energy dissipation *via* the heel pad  
2 (e.g., Baines et al., 2018; Honert and Zelik, 2019), rather than muscle-tendon  
3 lengthening. The shift from facultative to habitual bipedal walking in hominin evolution  
4 may have increased our reliance on soft (non-muscular) tissues for mechanical energy  
5 dissipation, which may have some metabolic and fatigue-resistance benefits in walking  
6 overall.

7

#### 8 *4.8. Limitations of this study*

9 Studies of the development of human walking mechanics indicate that children over  
10 the age of 5 years have adult-like gait mechanics and metabolic costs, once differences in  
11 size are accounted for (Sutherland, 1997; Stansfield et al., 2003; Weyand et al., 2010).  
12 Chimpanzees grow into adults at a faster rate than humans (Zihlman et al., 2004), but are  
13 still sub-adult between the ages of 5 and 6 years old. Ontogenetic studies of chimpanzee  
14 bipedal walking ground reaction forces indicated that by the age of 5, chimpanzees  
15 exhibit adult-like mechanics, independent of speed (Kimura, 1996). Sagittal plane hip,  
16 knee and ankle joint moments of bipedal chimpanzees that range in age from 6 to 33  
17 years old were all quite similar to each other (Pontzer et al., 2014). A qualitative  
18 comparison of our ground reaction forces and sagittal plane moments during stance phase  
19 to these data indicates that our results are similar to chimpanzees across a broad age and  
20 size range and, given the commonalities in the between-subject CMCs for both the force  
21 and kinematic results (Table 2; O'Neill et al., 2015) as well, should therefore be  
22 representative of bipedal chimpanzee walking in general.

23 Our analyses did not quantify intrinsic foot motion. Bipedal chimpanzees walk with  
24 less 3-D midfoot (Holowka et al. 2017) and forefoot (Fernandez et al., 2016) motion than  
25 humans. These new data indicating greater intrinsic foot motion in humans than bipedal  
26 chimpanzees were unexpected given long-standing dichotomies of human feet as ‘stiff’  
27 and chimpanzees as ‘mobile’ in bipedal walking (e.g., Elftman and Manter, 1935;  
28 Susman, 1983). However, the ‘stiff’ and ‘mobile’ dichotomy may be more reflective of  
29 passive ranges of motion as well as an overemphasis on the ‘midtarsal break’ in the  
30 single-support period of bipedal chimpanzee walking. Indeed, most of human 3-D  
31 midfoot and forefoot motion actually occurs in the second double-support period, not in

1 the single-support period (e.g., Lundgren et al. 2003; Holowka et al. 2015). Our inverse  
2 kinematics weighted markers located on the calcaneus more heavily than other foot  
3 markers for calculating ankle joint kinematics, which keeps intrinsic foot deformation  
4 from contaminating ankle joint angular velocities, and therefore ankle joint power. This  
5 approach helps prevent overestimation of ‘push-off’ power, which is important for proper  
6 calculation of plantar flexor muscle function (e.g., Zelik and Horner, 2018). Still, we did  
7 not take into account the possible intrinsic foot power generation in late stance. Greater  
8 human intrinsic foot motion may have some adaptive value in contributing positive  
9 power to push-off (e.g., Takahashi et al., 2017; Farris et al., 2019; but also see Zelik et  
10 al., 2015). The limited midfoot and forefoot motion, together with small peak forces in  
11 the second double-support period of bipedal chimpanzee walking (see Fig. 2) suggest  
12 little foot positive power in push-off, by comparison. Thus, the inclusion of intrinsic foot  
13 mechanics in comparisons of human and bipedal chimpanzee walking may affect the total  
14 limb power output and is an important area of future study for understanding hominin  
15 foot evolution.

16

#### 17 *4.9. Implications for fossil hominin bipedal biomechanics*

18 The single-support period of a walking stride has particular relevance for hominin  
19 evolution since a number of skeletal traits have been tied to ‘maintaining lateral balance’  
20 in hominins, such as ilia orientation (e.g., Stern and Susman, 1981; Lovejoy, 1988).  
21 Humans are well known to use an ‘abductor-based hip mechanism’ in the single-support  
22 period, an assumption that has been extended to a wide range of fossil hominins (e.g.,  
23 Lovejoy et al., 1973; Ruff, 1995), including the earliest hominins (e.g., Richmond and  
24 Jungers, 2008). Our results demonstrate that bipedal chimpanzees use an alternate  
25 mechanism, in which there are large internal rotation and adduction moments in the  
26 single-support period. This ‘rotation-based’ or ‘rotation-adduction-based’ mechanism for  
27 ‘maintaining lateral balance’ confirms and extends the inferences of Stern and Susman  
28 (1981), who proposed these single-support period mechanics for bipedal chimpanzees  
29 and other apes (i.e., gibbons, orangutans). This represents an alternative means of  
30 maintaining whole-body stability during bipedal walking; one that likely preceded the  
31 ‘abductor-based’ mechanism in the hominin lineage. Indeed, the likelihood that the

1 kinematics and mechanics of bipedal walking at the origins of hominin lineage were quite  
2 distinct from humans and much more similar to bipedal walking in facultative bipeds (cf.  
3 O'Neill et al., 2018) is an important consideration when searching for skeletal adaptations  
4 for 'terrestrial bipedal travel' in the earliest putative hominins (e.g., Macchiarelli et al.,  
5 2020). More experimental and modeling-simulation studies are needed to evaluate how  
6 musculoskeletal trait evolution in the pelvis and hind/lower limbs, including shifts in ilia  
7 length and orientation (e.g., Stern and Susman, 1981; Lovejoy, 1988) facilitate the use of  
8 an 'adduction-based mechanism' for 'maintaining lateral balance'.

9 An important difference in musculoskeletal structure between humans and  
10 chimpanzees is that chimpanzees possess a longer ischium than humans (e.g., Stern and  
11 Susman, 1983; Lovejoy, 1988). A long ischium is evident in *Ar. ramidus* at 4.4 million  
12 years ago (Lovejoy et al. 2009), as well as all Miocene apes with associated pelvis  
13 remains (Hammond et al., 2013, 2020; Morgan et al., 2015; Ward, 1993; Ward et al.,  
14 2019). Komza et al. (2018:4136) has recently proposed that shortening the ischium in  
15 hominin evolution facilitated 'hamstrings-powered hip extension'. However, our results  
16 demonstrate that the second-double support period in a human walking stride is  
17 associated with a net flexion moment at the hip, not a net extension moment (cf. Fig. 3  
18 and SOM Fig. S3). As such, the net mechanical energy generated during the second-  
19 double support period at the human hip is not due to 'hamstrings power', but instead to  
20 substantial hip flexor muscle (e.g., m. iliopsoas; Capellini et al., 2006) and elastic power.  
21 Indeed, in both human and bipedal chimpanzee walking, the hamstring muscles (i.e., mm.  
22 semimembranosus, semitendinosus and biceps femoris, long head) are quiescent in late  
23 stance (e.g., Winter and Yak, 1987; Capellini et al., 2006; Schmitz et al., 2009; Larson  
24 and Stern, unpublished data). Instead, our results indicate that a shorter ischium in  
25 humans is associated with greater hip extension than bipedal chimpanzees in the second  
26 half of the single-support and double-support periods, which permits a passive elastic  
27 contribution at the hip, thereby contributing positive power through push-off into limb  
28 swing.

29 Our results demonstrate significant differences between humans and bipedal  
30 chimpanzees over a full walking stride but place new emphasis on the second half of the  
31 single support period (i.e., for elastic tissues strain) and the second-double support period

1 (i.e., for push-off) for the evolution of hominin walking. An abducted hallux in *Ar.*  
2 *ramidus* (Lovejoy et al., 2009b; Simpson et al., 2019; see also Haile-Selassie et al., 2012)  
3 suggests that the earliest hominins still utilized a relatively weak push-off in the double-  
4 support period at 4.4 Mya, quite distinct from human walking. Lovejoy et al. (2009b) has  
5 proposed that, in the absence of an adducted hallux, the center of pressure was directed  
6 along the full length of the foot and through the more lateral phalanges in *Ar. ramidus*. In  
7 bipedal chimpanzees, the center of pressure remains proximal to the phalanges over a  
8 walking step, including during the second double-support period (see Fig 1; see also  
9 Vereecke et al. 2003). Skeletal correlates of an enhanced capacity for  
10 metatarsophalangeal flexion in digits 2–4 in *Ar. ramidus* compared to African apes  
11 (Lovejoy et al., 2009b; Fernández et al., 2018; Simpson et al., 2019), raise the possibility  
12 of a more distal progression of the center of pressure than in bipedal chimpanzees;  
13 however, the lateral digits still lack the structural integrity of a large hallux for applying a  
14 substantial push-off impulse via the ankle plantar flexors (and, to a lesser extent, the  
15 intrinsic foot tissues: Takahashi et al., 2017). Nevertheless, this may represent some  
16 improvement over the limited capabilities of bipedal chimpanzees or a *Pan-Homo* last  
17 common ancestor with an African ape-like foot (e.g., Pilbeam and Lieberman, 2017;  
18 Prang, 2019). A more adducted hallux is evident in *Au. afarensis* (e.g., Susman et al.,  
19 1984; DeSilva et al., 2019) as well as the associated Lateoli site G and site S footprints  
20 (Leakey and Hay, 1979; Masao et al., 2016), although the substantial positive power at  
21 the ankle via a human-like push-off may not appear until *Homo* (e.g., Fernández et al.,  
22 2016, 2018). Indeed, the differences between the ca. 3.7 Mya Laetoli footprints and the  
23 1.5 Mya Ileret footprints may reflect this (Bennett et al., 2009; Hatala et al., 2016b; but  
24 see Raichlen and Gordon, 2017). More experimental-modeling studies of the effects of  
25 foot musculoskeletal structure on push-off mechanics in walking are needed to clarify  
26 these issues.

27

## 28 **5. Conclusions**

29 The analyses presented herein provide the first description of the 3-D hip, knee and  
30 ankle moments, work, and power of bipedal chimpanzees, and direct comparisons to  
31 humans walking at matched dimensionless and dimensional speeds over a full walking

1 stride. They provide partial or full support for our three main hypotheses relating  
2 musculoskeletal structure to mechanics across a full walking stride.

3 Still, it is difficult to decompose the individual contributions of musculoskeletal traits  
4 such as a mobile lower back, a short pelvis, and long lower limbs and short feet via joint-  
5 level analyses alone. Additional contributions from differences in upper body size and  
6 shape or neural control may also be relevant. Yet, this is a necessary step for linking the  
7 hominin fossil record to shifts in hominin walking capabilities. As such, future research  
8 should use the results herein to investigate the effects of isolated traits, both skeletal (e.g.,  
9 ilia orientation, hallux adduction) and soft tissue (e.g., m. soleus, Achilles tendon), on the  
10 mechanics of human walking (e.g., single support, ‘push-off’, etc.) and across lower limb  
11 joints over a stride. While studies of isolated traits in hominin evolution have historically  
12 been approached using either comparative morphology or, to a much lesser extent,  
13 experimentation in living taxa (e.g., Ross et al., 2002), there is an increasingly viable and  
14 important role for computer simulation and optimization methods to establish direct  
15 cause-and-effect relationships based on high-fidelity models of the neuromusculoskeletal  
16 systems (e.g., Falisse et al., 2019). This approach may be especially useful for testing the  
17 adaptive nature of trait combinations not present in living species or along a single  
18 lineage, such as hominins. High-quality, controlled experimental data, such as the force,  
19 moment, work, and power measurements of humans and bipedal chimpanzees herein,  
20 provide the experimental basis for these studies.

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1 **Figure legends**

2

3 **Figure 1.** A full bipedal walking stride. A full stride includes both stance and swing  
4 phases. The stance phase is divided among the first double support (double support 1),  
5 single support, and the second double-support (double support 2) periods. In the first  
6 double-support period the right hind limb is the leading limb, while in the second double-  
7 support period the right hind limb is the trailing limb. The green arrow shows the  
8 direction and relative magnitude of the resultant ground reaction force under each foot  
9 over a full stride.

10

11 **Figure 2.** The vertical (A–B), anterior-posterior (C–D) and medio-lateral (E–F) ground  
12 reaction forces over a walking step (mean  $\pm$  s.d.) for the three chimpanzees (column 1) as  
13 well as chimpanzees (solid blue line) and humans (dashed black line) as groups (column  
14 2). Each step begins at heel strike (i.e., foot touchdown) and ends at toe off of the same  
15 foot. Broken vertical lines show the average step event times for the chimpanzees,  
16 representing contralateral limb toe off (H = 21%, C = 23%) and the contralateral limb  
17 heel strike (H = 81%, C = 77%), which define the double-support and single support  
18 periods of a step.

19

20 **Figure 3.** The hip flexion-extension moment (A), abduction-adduction moment (B),  
21 internal-external rotation (C), knee flexion-extension moment (D) and ankle plantar  
22 flexion-dorsiflexion moment (E) over a walking stride (mean  $\pm$  s.d.) for chimpanzees  
23 (solid blue line) and humans (dashed black line). Moments are in dimensionless units.  
24 Each stride begins and ends at ipsilateral ‘heel strike’ (i.e., foot touchdown). All vertical  
25 lines show the average stride event times for the chimpanzees, which were similar among  
26 the species. The broken vertical lines represent contralateral limb toe-off (H = 13%, C =  
27 14%) and contralateral limb ‘heel strike’ (H = 51%, C = 48%), which define the double-  
28 support and single support periods of a stride; the solid vertical line represents ipsilateral  
29 toe off (H = 63%, C = 62%), which defines the start of the swing phase.

30

31 **Figure 4.** The 3-D hip power (A), knee power (B), and ankle power output (C) over a  
32 walking stride (mean  $\pm$  s.d.) for humans (dashed black line) and chimpanzees (solid blue



1 line). All vertical lines show the average stride event times for the chimpanzees, which  
2 were similar among the species. The broken vertical lines represent contralateral limb  
3 toe-off ( $H = 13\%$ ,  $C = 14\%$ ) and contralateral limb ‘heel strike’ ( $H = 51\%$ ,  $C = 48\%$ ),  
4 which define the double-support and single support periods of a stride; the solid vertical  
5 line represents ipsilateral toe off ( $H = 63\%$ ,  $C = 62\%$ ), which defines the start of the  
6 swing phase. Powers are in dimensionless units.

7

8 **Figure 5.** The stance phase positive joint work (A) and power (B) output in the first  
9 double support (DS1), single support (SS) and second double-support (DS2) period of a  
10 walking stride for humans (black) and chimpanzees (red) (mean  $\pm$  s.d.). The relative  
11 contributions of the ankle elastic work and power (‘ankle elastic’) and muscle fiber work  
12 and power (‘muscle fiber’) to the total limb work and power output in the human DS2  
13 period is shown.

14

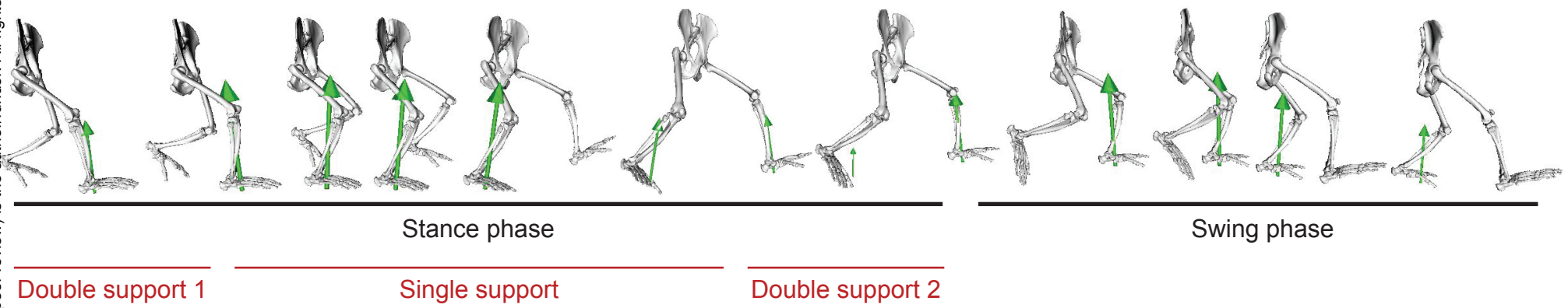
15 **Figure 6.** Total positive limb work (A) and average positive limb power (B) used to  
16 swing the limb during walking in humans (black) and chimpanzees (red; mean  $\pm$  s.d.).

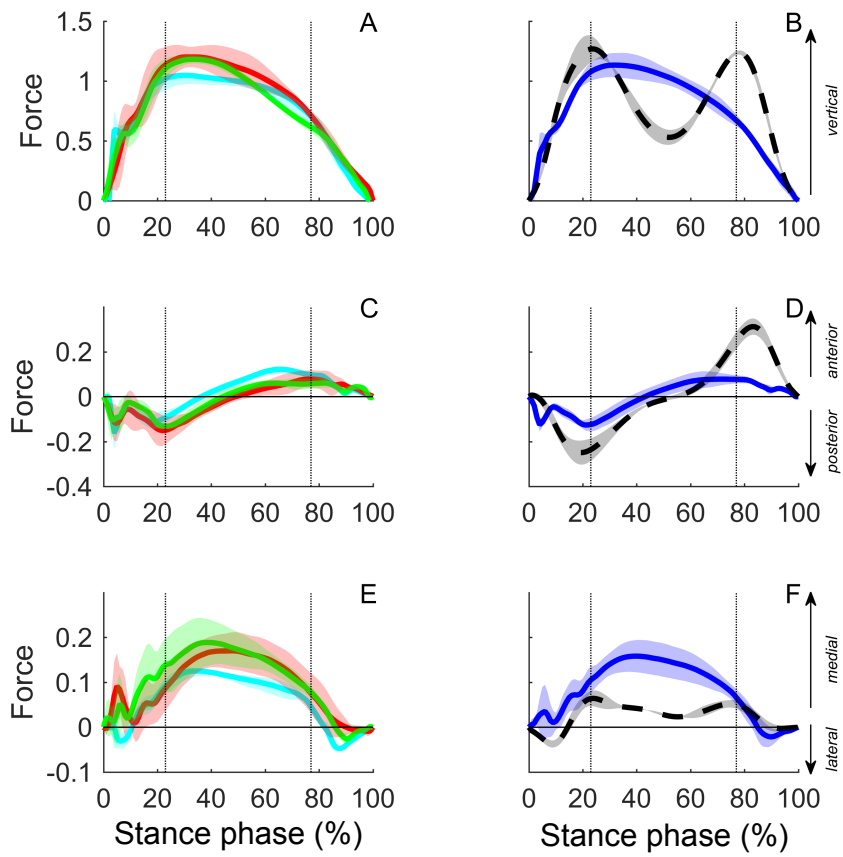
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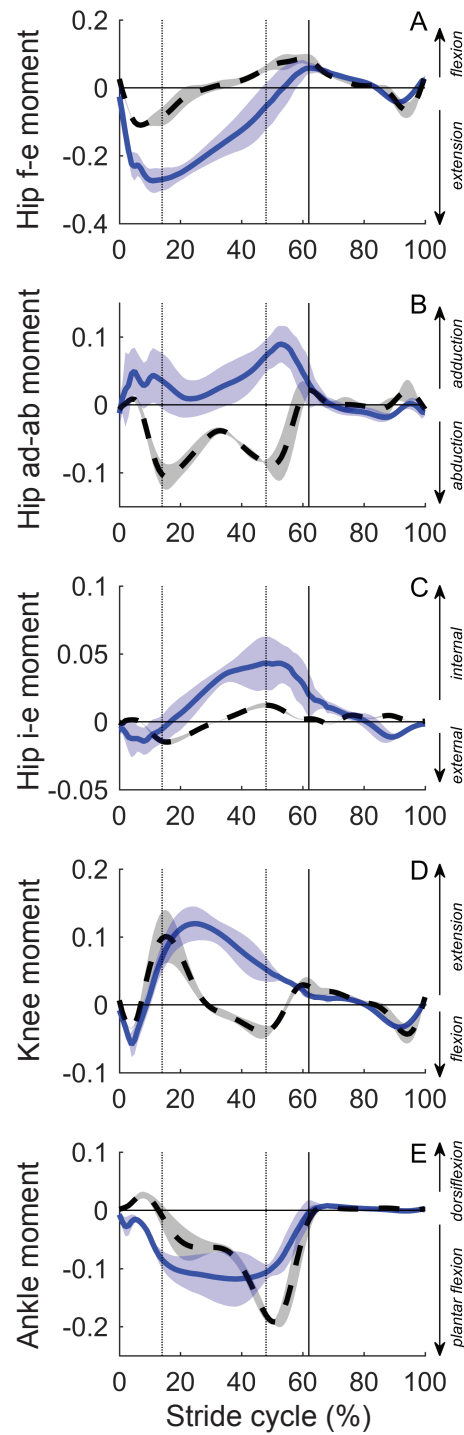
18 **Figure 7.** Total positive limb work (A) and average positive limb power (B) over a full  
19 walking stride in humans (black) and chimpanzees (red; mean  $\pm$  s.d.). The human total  
20 lower limb work and power is due to contributions from both elastic mechanisms at the  
21 hip and ankle (‘elastic’) as well as muscle fibers (‘muscle fiber’).

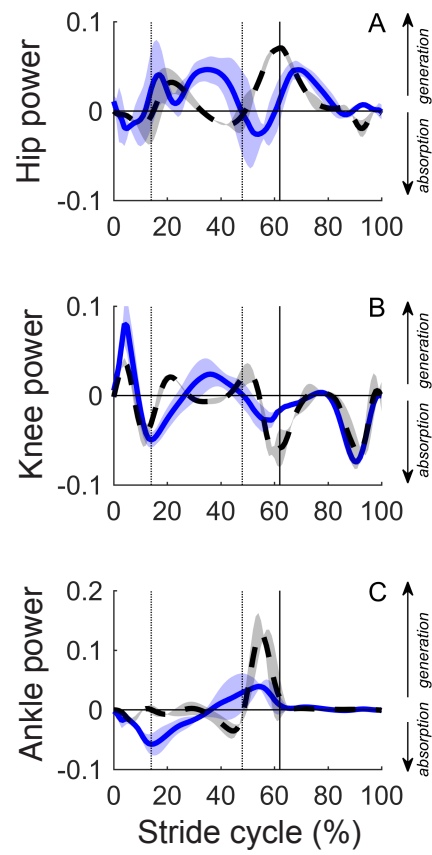
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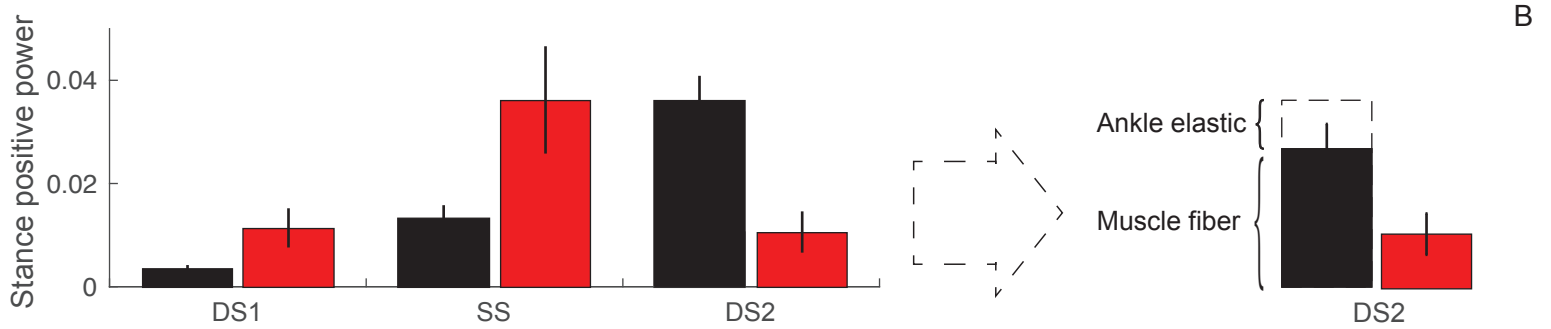
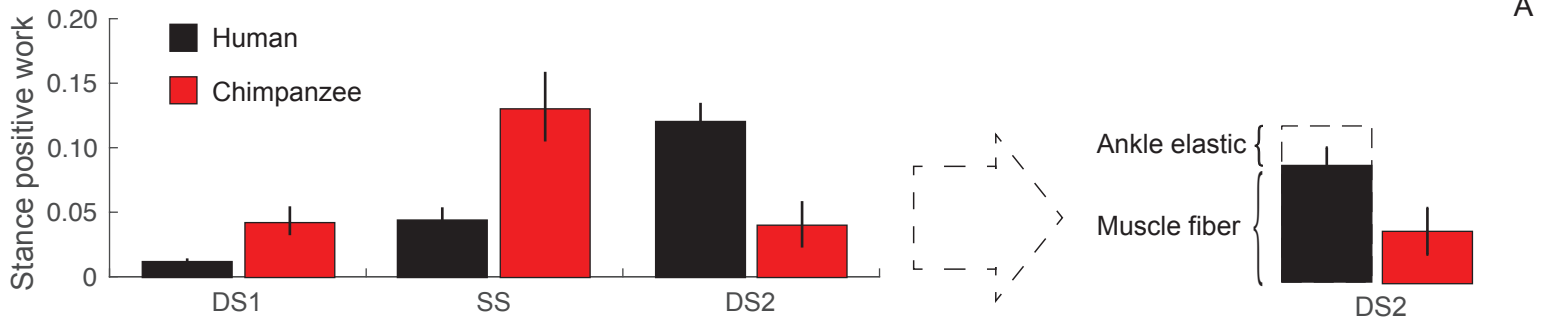
23 **Figure 8.** The distribution of positive mechanical work (A) and negative mechanical  
24 work among the limb joints (B) during stance and swing in humans (column 1) and  
25 chimpanzees (column 2).

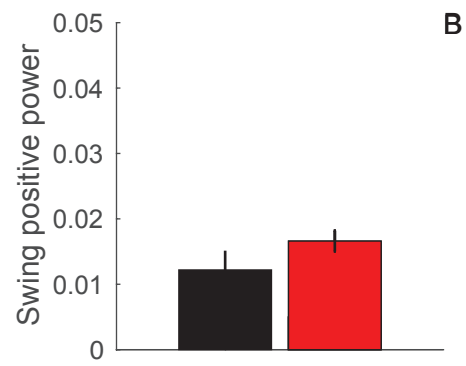
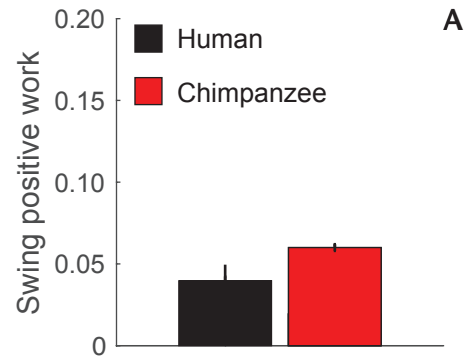




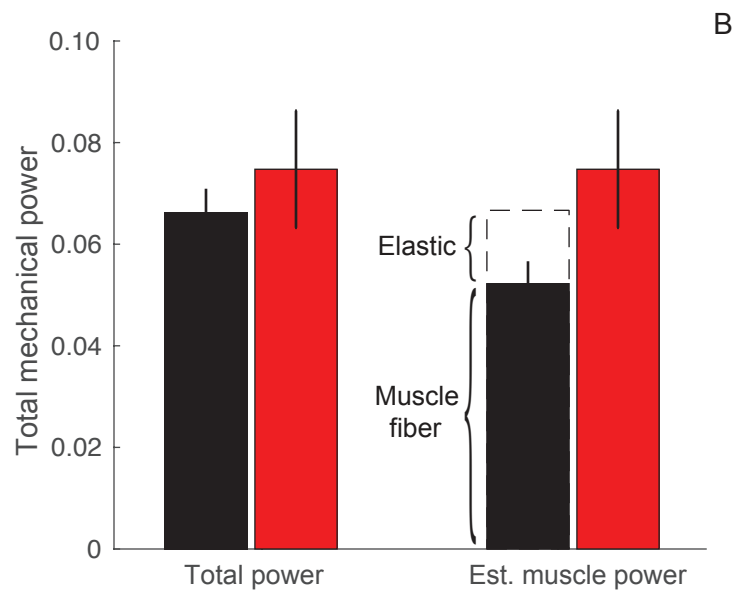
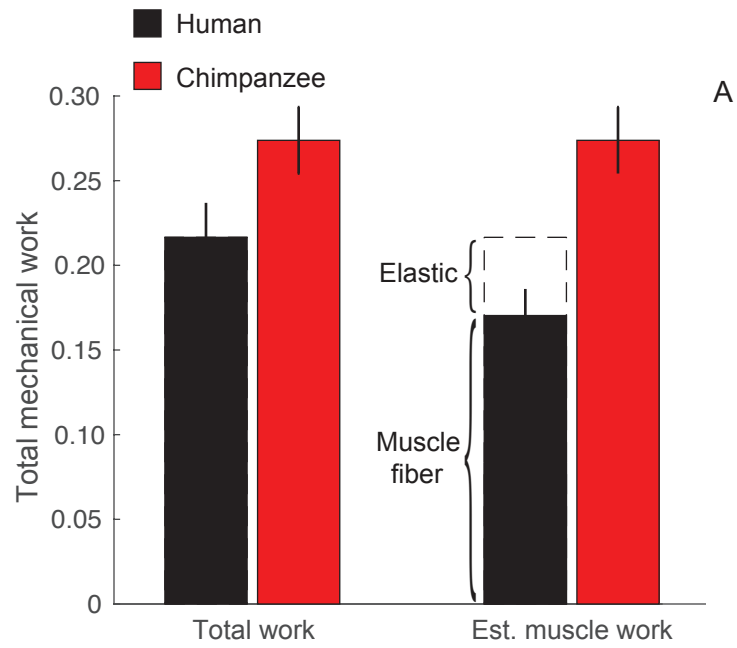


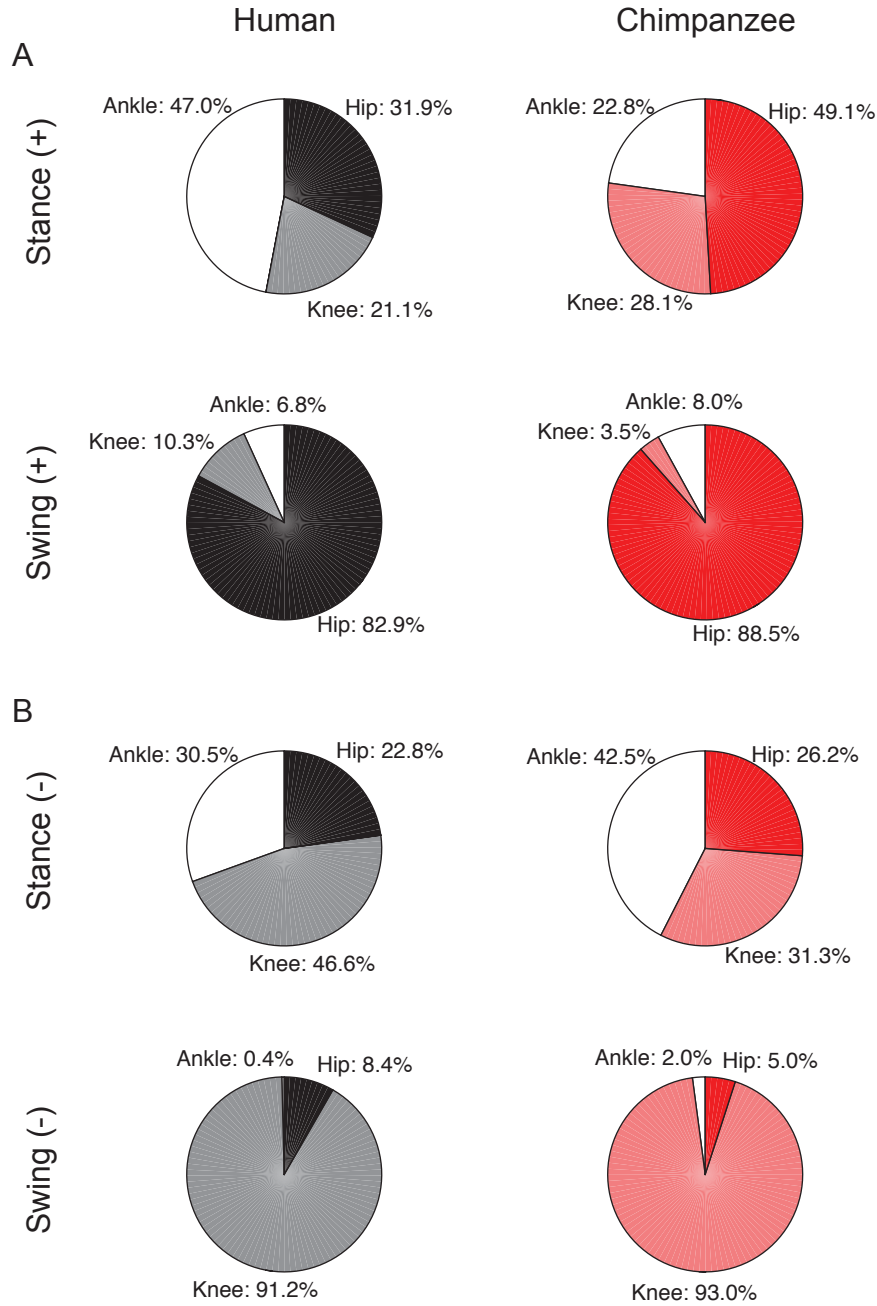












**Table 1**

Spatiotemporal gait parameters in human and chimpanzee bipedal walking. Human data are matched to the chimpanzee data in dimensionless (i.e., relative-speed match) form (mean  $\pm$  s.d.).

	$v^a$ (m s <sup>-1</sup> )	$v^b$	$Fr^c$	Stance time (s)	Swing time (s)	Stride length (m)	Stride frequency (Hz)	Duty factor
Humans	1.66 $\pm$ 0.06	0.56 $\pm$ 0.01	0.31 $\pm$ 0.02	0.64 $\pm$ 0.02	0.36 $\pm$ 0.04	1.69 $\pm$ 0.05	1.00 $\pm$ 0.05	0.64 $\pm$ 0.02
Chimpanzees	1.09 $\pm$ 0.10	0.56 $\pm$ 0.06	0.31 $\pm$ 0.06	0.45 $\pm$ 0.09	0.27 $\pm$ 0.03	0.78 $\pm$ 0.07	1.43 $\pm$ 0.23	0.62 $\pm$ 0.03

<sup>a</sup> Dimensional velocity.

<sup>b</sup> Dimensionless velocity.

<sup>c</sup> Froude number.

**Table 2**

Adjusted coefficient of multiple correlation (CMC) of ground reaction forces ( $F_y$ ,  $F_x$ ,  $F_z$ ).

	$F_y$ , vert	$F_x$ , ant-post	$F_z$ , med-lat
Humans <sup>a</sup>	$0.994 \pm 0.003$	$0.996 \pm 0.001$	$0.965 \pm 0.017$
Among humans <sup>b</sup>	$0.958 \pm 0.018$	$0.972 \pm 0.007$	$0.916 \pm 0.038$
Chimpanzees <sup>a</sup>	$0.972 \pm 0.021$	$0.911 \pm 0.054$	$0.884 \pm 0.074$
Among chimpanzees <sup>b</sup>	$0.962 \pm 0.016$	$0.883 \pm 0.031$	$0.847 \pm 0.012$

Human data are matched to the chimpanzee data in dimensionless (i.e., relative-speed match) form (mean  $\pm$  s.d.). CMC mean  $\pm$  s.d. for 4 trials per subject, 3 subjects. The y, x, z components of the ground reaction forces are vertical (vert), anterior-posterior (ant-post) and medial-lateral (med-lat).

<sup>a</sup> Correlations between strides within subjects.

<sup>b</sup> Correlations between subjects.

**Table 3**

Peak joint moments in bipedal chimpanzees and humans in dimensionless units. Human data are matched to the chimpanzee data in dimensionless (i.e., relative-speed match) form (mean  $\pm$  s.d.).

	Hip			Knee	Ankle
	Flexion-extension	Adduction-abduction	Internal-external rotation	Flexion-extension	Plantar flexion-dorsiflexion
Humans	-0.112 $\pm$ 0.006 (ext.)	-0.106 $\pm$ 0.019 (abd.)	0.025 $\pm$ 0.003 (int.)	0.102 $\pm$ 0.038 (ext.)	-0.196 $\pm$ 0.002 (plantar.)
Chimpanzees	-0.274 $\pm$ 0.036 (ext.)	0.093 $\pm$ 0.029 (add.)	-0.047 $\pm$ 0.016 (ext.)	0.122 $\pm$ 0.024 (ext.)	-0.131 $\pm$ 0.037 (plantar.)

The direction of the peak joint moment is given as flexion (flex.), extension (ext.), abduction (abd.), adduction (add.), internal rotation (int.), external rotation (ext.), plantar flexion (plantar.) or dorsiflexion (dorsi.).

**Table 4**

Peak joint power in bipedal chimpanzees and humans at matched dimensionless speeds in dimensionless units. Human data are matched to the chimpanzee data in dimensionless (i.e., relative-speed match) form (mean  $\pm$  s.d.).

	Hip power		Knee power		Ankle power	
	+	-	+	-	+	-
Humans	$0.071 \pm 0.010$	$-0.031 \pm 0.002$	$0.038 \pm 0.004$	$-0.078 \pm 0.005$	$0.145 \pm 0.037$	$-0.034 \pm 0.011$
Chimpanzees	$0.067 \pm 0.016$	$-0.050 \pm 0.016$	$0.083 \pm 0.027$	$-0.076 \pm 0.004$	$0.052 \pm 0.014$	$-0.059 \pm 0.018$