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Integrative experimental/computational approach establishes active cellular protrusion as the primary driving force of phagocytic spreading by immune cells

Short Title: Computational analysis of immune cell spreading

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Abstract

The dynamic interplay between cell adhesion and protrusion is a critical determinant of many forms of cell motility. When modeling cell spreading on adhesive surfaces, traditional mathematical treatments often consider passive cell adhesion as the primary, if not exclusive, mechanistic driving force of this cellular motion. To better assess the contribution of active cytoskeletal protrusion to immune-cell spreading during phagocytosis, we here develop a computational framework that allows us to optionally investigate both purely adhesive spreading ("Brownian zipper hypothesis") as well as protrusion-dominated spreading ("protrusive zipper hypothesis"). We model the cell as an axisymmetric body of highly viscous fluid surrounded by a cortex with uniform surface tension and incorporate as potential driving forces of cell spreading an attractive stress due to receptor-ligand binding and an outward normal stress representing cytoskeletal protrusion, both acting on the cell boundary. We leverage various model predictions against the results of a directly related experimental companion study of human neutrophil phagocytic spreading on substrates coated with different densities of antibodies. We find that the concept of adhesion-driven spreading is incompatible with experimental results such as the independence of the cell-spreading speed on the density of immobilized antibodies. In contrast, the protrusive zipper model agrees well with experimental findings and, when adapted to simulate cell spreading on discrete adhesion sites, it also reproduces the observed positive correlation between antibody density and maximum cell-substrate contact area. Together, our integrative experimental/computational approach shows that phagocytic spreading is driven by cellular protrusion, and that the extent of spreading is limited by the density of adhesion sites.

Author Summary

To accomplish many routine biological tasks, cells must rapidly spread over different types of surfaces. Here, we examine the biophysical underpinnings of immune cell spreading during phagocytosis, the process by which white blood cells such as neutrophils engulf pathogens or other foreign objects. Our computational framework models the case in which a human neutrophil spreads over a flat surface coated with antibodies, which we also test experimentally in a companion paper. Our primary purpose is to assess whether phagocytic spreading is actively driven by protrusive forces exerted by the cell, or passively by adhesive forces acting between receptors in the cell membrane and antibodies on the surface. By directly comparing our model predictions to experimental results, we demonstrate that phagocytic spreading is primarily driven by protrusion, but the extent of spreading is still limited by the availability of binding sites. Our findings improve the fundamental understanding of phagocytosis and may also pave the way for future investigations of the balance between adhesion and protrusion in other forms of cell spreading, such as wound healing or cancer cell migration.

Introduction

The ability of cells to spread on surfaces is critical to many biological processes, including cell migration, wound healing, and tissue formation. Immune cells are especially adept at rapid spreading; for instance, neutrophils commonly travel up to an order of magnitude faster in motility assays than fibroblasts or endothelial cells [1-5]. Vital immune cell functions, such as firm arrest at the endothelium and phagocytosis of pathogens, rely on this ability. A deeper understanding of the physical mechanisms driving cell spreading is essential for informed pharmaceutical strategies and new therapies targeting immune cells, such as current efforts to enhance phagocytosis for more effective clearance of cancer cells [6, 7].

Many experimental and theoretical studies have sought to unravel the physical principles of cell spreading by analyzing the initial growth of cell contact regions on a flat, adhesive substrate [8-11]. However, it often remains unclear whether any given type of cell spreading is primarily driven by passive forces due to adhesion or by active protrusive and/or contractile forces generated by the cell. In the simplest model, cell spreading is treated as a purely passive process, similar to a viscous droplet spreading on an adhesive substrate [8, 12, 13]. Alternative models assume that cytoskeleton-driven protrusion determines the rate of cell spreading, neglecting the effective attractive force due to ligand-receptor binding [10, 14, 15].

Here, we aim to illuminate fundamental cell-spreading mechanisms by focusing on phagocytic spreading. In conventional phagocytosis, an immune cell first adheres to the surface of a target particle such as a bacterium, often by binding to opsonic ligands such as immunoglobulin G (IgG) antibodies. The cell then spreads over the target surface until its membrane closes around the particle. On the other hand, when presented with an excessively

large target, the cell is unable to fully engulf the particle and continues to spread until its target-

contact area reaches a maximum [16, 17]. Such cases, including phagocytic spreading on flat

substrates, are termed frustrated phagocytosis. The relatively simple geometry of a cell

undergoing frustrated phagocytic spreading on a flat surface is particularly amenable to

theoretical analysis, especially when the cell spreads in an axisymmetric manner.

Reflecting the above-mentioned contrasting mechanistic notions about generic cell

spreading, two hypotheses have been put forward to explain phagocytic spreading, i.e., the

"Brownian zipper" and "protrusive zipper" models [18]. Both models concur that fresh contact

between the cell membrane and target surface results in a zipper-like adhesive attachment that is

essentially irreversible. However, regarding the driving force of cellular advancement, the

Brownian zipper model postulates that strong adhesion alone is responsible for pulling the cell

membrane onto the target surface. In contrast, the protrusive zipper model assumes that the

cytoskeleton actively generates protrusive force to push the front of the cell outwards.

We seek to establish which of these hypotheses is more realistic by developing

mathematical models of the mechanics of isotropic cell spreading and comparing our theoretical

predictions with experimental observations of human neutrophils spreading on flat, IgG-coated

surfaces. As reported in detail in a companion paper, our experimental design allowed us to

examine the spreading behavior of neutrophils on surfaces coated with different densities of IgG

[19]. Because higher IgG densities correspond to stronger adhesive forces, we reasoned that the

Brownian zipper model should predict a much stronger correlation between IgG density and rate

of contact-area growth ("spreading speed") than the protrusive zipper model. Here, we use

computer simulations of phagocytic spreading to verify this common-sense expectation and

further investigate mechanisms governing immune-cell spreading. Together, our integrative

experimental/theoretical approach establishes that the Brownian zipper model is inconsistent

with experimental results, whereas the spreading dynamics predicted by the protrusive zipper

model agree well with our experiments.

Results

Model implementation of key biophysical mechanisms of cell spreading

We consider a simple model cell that captures the basic geometrical and mechanical properties of

human neutrophils, the most abundant type of white blood cell and one of the prototypes of

professional phagocytes. This model cell consists of an axisymmetric, highly viscous fluid body

of constant volume that is surrounded by an elastic cortex with uniform tension (Fig 1). Termed

the "cortical shell, liquid core model", this theoretical concept has successfully reproduced the

passive response of human neutrophils to imposed deformations [20-22]. In the undeformed

reference state, the persistent tension of the cortex maintains a spherical cell shape with a typical

diameter of 8.5 μm. The nucleus of neutrophils is segmented into three to five lobes and appears

to play only a minor role during deformations, lending support to the approximation of the cell

interior as a homogeneous fluid. The effective viscosity (μ) of the cytoplasm has been found to

be about 200,000 times the viscosity of water at room temperature in passive neutrophils [20,

21], and another ~3-times higher in active neutrophils [23]. It is well known to increase during

phagocytosis [24-26]. We use a viscosity value of $\mu = 200$ Pa-s in our passive Brownian zipper

model and a value of $\mu = 1660$ Pa-s in our active protrusive zipper model. The original

assumption of a constant cortical tension [20, 22] was later found to be approximately true only

for small deformations. The revised relationship between tension (τ) and cell surface area (A_{cell})

was shown to be roughly biphasic [27]. Assuming an isotropic and uniform tension, and in

overall agreement with a number of quantitative experimental studies [24, 27, 28], our

simulations incorporate a smoothed version of the following biphasic constitutive relationship:

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$$\tau(A_{cell}) = \begin{cases} 0.01 + 0.16\left(\dfrac{A_{cell}}{A_{cell,0}} - 1\right)\dfrac{\text{mN}}{\text{m}} & \text{if} \quad \dfrac{A_{cell}}{A_{cell,0}} \leq 1.26 \\[3mm] 0.0516 + 0.545\left(\dfrac{A_{cell}}{A_{cell,0}} - 1.26\right)\dfrac{\text{mN}}{\text{m}} & \text{if} \quad \dfrac{A_{cell}}{A_{cell,0}} > 1.26 \end{cases} \tag{1}$$

133   Where $A_{cell,0}$ is the surface area of the resting neutrophil before spreading.

Fig 1. Illustration of our computational model of isotropic cell spreading.

(A) 3D rendering shows the geometry and defines coordinates for an axisymmetric spreading

cell on a flat surface. The enlarged inset (right) illustrates the stress balance at the free cell

boundary. (B) Adhesion stress effectively pulls the membrane onto the flat surface. The enlarged

insets conceptually depict how the adhesion stress is computed for different ligand densities ρ_l.

(C) Cortical tension and membrane curvature give rise to an effective inward normal stress. (D)

The protrusion stress acts normal to the cell membrane and is concentrated at the region of the

membrane closest to the substrate. (E) The cross-sectional snapshot of a simulation illustrates the

mesh composed of quadrilateral elements used in the calculations, with tighter element packing

closer to the flat surface. The computational domain only includes half of this mesh due to axial

symmetry. Boundary regions are labeled Γ, and the vertical dashed line is the symmetry axis (r

$= 0$) (F) This snapshot of a simulation illustrates the fluid velocity (vector field) and relative

pressure (heat map) computed for a given cell shape with known boundary stresses.

Movements of the viscous cytoplasm generally do not exceed velocities of 1 µm/s during

phagocytic cell spreading and are characterized by low Reynolds numbers. Such movements are

well described by the Stokes equations for creeping flow:

152                             $$\mu \nabla^2 \mathbf{v} = \nabla p \qquad\qquad (2)$$

153   along with the continuity equation for incompressible fluids:

154                             $$\nabla \cdot \mathbf{v} = 0 \qquad\qquad (3)$$

Here, $\mathbf{v}$ denotes the fluid velocity vector, and p is fluid pressure. Together, these equations

govern the flow behavior of our model cell.

Interactions between the cell surface and the substrate can facilitate cell spreading

directly via adhesion, and indirectly through receptor-induced signaling that leads to protrusion.

Including the respective stresses, the moving boundary condition governing the free (i.e.,

nonadherent) part of the cell surface (Γ_{free}) balances up to four types of stress vectors: fluid stress

($\boldsymbol{\sigma}_{fluid}$), adhesion stress ($\boldsymbol{\sigma}_{adh}$), protrusion stress ($\boldsymbol{\sigma}_{fluid}$), and cortical stress ($\boldsymbol{\sigma}_{cortex}$) (Fig 1A):

162                 $$\boldsymbol{\sigma}_{fluid} + \boldsymbol{\sigma}_{adh} + \boldsymbol{\sigma}_{cortex} + \boldsymbol{\sigma}_{prot} = \mathbf{0} \quad \text{on } \Gamma_{free} \qquad\qquad (4)$$

The fluid stress vector $\boldsymbol{\sigma}_{fluid}$ encompasses the pressure difference across the cell surface

as well as the stress exerted on the surface by the moving cytoplasm. It is determined by the

constitutive relation for a Newtonian fluid:

$$\boldsymbol{\sigma}_{fluid} = \boldsymbol{\sigma}_{fluid,out} - \boldsymbol{\sigma}_{fluid,in} = (p - p_{out})\mathbf{n} - \mu\left(\nabla\mathbf{v} + (\nabla\mathbf{v})^{T}\right)\cdot\mathbf{n} \qquad (5)$$

where $\mathbf{n}$ is the unit surface normal, and the dot in the last term on the right-hand side denotes

the inner product between a tensor and a vector. The extracellular medium has a much lower

viscosity than the intracellular fluid; therefore, Eq (5) neglects the medium's viscous

contribution and only accounts for its hydrostatic pressure denoted p_{out}.

Our implementation of the adhesion stress is based on the assumption that adhesion can

effectively be represented by a short-range attractive potential between the cell surface and the

ligand-coated substrate. We compute the effective adhesion stress at a given point on the cell

surface by summing over all pairwise interactions with substrate molecules that lie outside the

cell-substrate contact region at the time (Fig 1B). For a continuum of ligand molecules, the

resulting expression takes the form (derived in S6 Appendices)

$$\boldsymbol{\sigma}_{adh} = \sigma_{o}\rho_{l} \iint\limits_{substrate} \mathbf{f}_{unit} \left[\left(\frac{D_{0}}{D}\right)^{7} - \left(\frac{D_{0}}{D}\right)^{4} \right] dA \qquad (6)$$

where ρ_{l} is the ligand surface density and σ_{0} is a scaling factor representing the strength of

interaction per unit area of the cell surface. The unit vector $\mathbf{f}_{unit}$ specifies the direction of a given

interaction, D denotes the distance between the interacting points, and D_{0} is a constant setting

the overall range of the adhesion potential (set to 50 nm in our simulations).

The origin of the cortical stress is the cortical tension, which resists expansion of the cell

surface area and acts along the curved surface of the cell (Fig 1D). The resulting stress acts

normal to the surface and is given by the product of the tension τ and the mean curvature of the

cell surface, as dictated by Laplace's law:

$$\boldsymbol{\sigma}_{cortex} = -\tau\left(\frac{\partial\phi}{\partial s} + \frac{\sin\phi}{r}\right)\mathbf{n} \tag{7}$$

Here, the term in parentheses is the mean curvature of the axisymmetric cell surface expressed in

the coordinates defined in Fig 1A.

The protrusion stress comprises outward forces exerted on the cell surface by the actively

remodeling cytoskeleton. Purposeful reorganization of intracellular structures requires tight

coordination by biochemical signaling cues, which in turn are induced by receptor-ligand

binding. Rather than attempting to implement these highly complex mechano-chemical

mechanisms, we capture their localized character in a semiempirical manner. Our model

postulates that the protrusive stress is greatest at the perimeter of the cell-substrate contact region

and decays as a function of the distance from this leading edge measured along the arc length (s,

Fig 1A) of the contour of the unbound cell surface. We assume that this stress acts normal to the

cell boundary, and that its decay along the free cell surface is exponential (Fig 1C):

$$\boldsymbol{\sigma}_{prot} = \sigma_{prot}e^{-\frac{s_{contact}-s}{s_0}}\mathbf{n} \tag{8}$$

In this equation, $s_{contact}$ is the arc length value at which the cell-surface contour makes contact

with the substrate, and s_0 is the characteristic length that sets the spatial range of the protrusion

stress.

Bearing in mind that cytoskeletal remodeling also is responsible for the behavior of the

cortical tension, and that the tension varies during cell spreading (Eq (1)), it is reasonable to

assume that the overall strength of the protrusion stress (σ_{prot}) varies in a similar fashion. In

addition to the spatial distribution of the cortical stress governed by Eq (8), we therefore also

postulate a deformation-dependent strength of the protrusive stress. Our choice of this

dependence, and its motivation, will be explained in a later section.

Finally, for the part of the cell surface that is in contact with the substrate, we enforce a

simple no-slip boundary condition, requiring that

$$\mathbf{v} = \mathbf{0} \quad \text{on } \Gamma_{adherent} \tag{9}$$

Each simulation begins with a model cell that rests on the surface and has formed a very

small initial contact footprint (area $< 0.1 \ \mu m^2$). The shape of the upper, free part of the cell at this

time is a spherical cap. We determine the fluid velocities and pressure distribution at each time

step by solving a perturbed form of the Stokes equations using the finite element method (FEM;

Fig 1E,F) as described previously [29]. We then use the computed velocities to evolve the cell

shape over a small time step. Details of our model implementation and solution method are given

in Methods and S6 Appendices.

This generic modeling framework of cell spreading can easily be adopted to represent

different mechanistic notions by adjusting the relative contributions of the adhesion and

protrusion stresses. Disregarding the protrusion stress altogether results in a mathematical

representation of the Brownian zipper model described in the Introduction. On the other hand,

the protrusive zipper model generally includes both the protrusion stress as well as the adhesion

stress. A purely protrusion-driven mode of spreading also can be tested by setting the adhesion

stress to zero, although one needs to bear in mind that irreversible adhesion still maintains the

cell-substrate contact region in this case. In all model versions, the adhesion stress can be varied

over several orders of magnitude to predict how the spreading behavior depends on the density

of ligand displayed on the substrate.

Quantitative experimental results for the validation of model versions

The computational framework presented in the previous section can be adopted to simulate interactions by various cell types with targets of different axisymmetric geometries. Our present focus on human neutrophils spreading on flat substrates is motivated by a wealth of experimental results obtained for this particular scenario and presented in a companion paper [19]. In brief, we exposed cells to glass coverslips coated with IgG antibodies at densities (ρ_{IgG}) spanning ~3 orders of magnitude. The analysis of these highly controlled experiments included measurements of the cell-substrate contact area of spreading cells over time (Fig 2). Regardless of IgG density, we found that the area-versus-time curves typically were sigmoidal in shape (Fig 2B,C). Defining a cell's "spreading speed" as the fastest rate of contact-area growth (i.e., the slope of a sigmoidal fit to the area-versus-time curve at the inflection point), we found that all spreading cells increased their substrate-contact area at speeds of around 3 μm^2/s irrespective of the density of deposited IgG (Fig. 2D). The measured values of the maximum contact area of spreading cells, on the other hand, exhibited a moderate but significant increase at higher IgG densities (Fig 2E). These experimental results provide useful quantitative benchmarks for comparison with computer simulations and will be used in the following sections to evaluate the validity of different mechanistic notions about cell spreading.

Fig 2. Summary of experimental results.

(A) The contact region of a spreading neutrophil was imaged using reflection interference

contrast microscopy (RICM). Contact regions in this example are traced in yellow. The scale bar

in the first image denotes 10 μm. (B) Contact area is plotted as a function of time for the

spreading cell shown in (A). The spreading speed is defined as the maximum slope extracted

from a sigmoidal fit, and the maximum contact area is given by averaging the contact area at the

plateau. (C) Mean contact area is computed at discrete time values for aligned curves of cells

spreading on different densities of IgG. Mean quantified IgG densities are reported in the figure

legend as IgG molecules per μm^2. Error bars represent standard error of the mean. (D) Average

spreading speed was quantified for the different IgG densities. There is no significant difference

between mean slope values. (E) Maximum contact area increases slightly as a function of IgG

density. Statistically significant differences in maximum contact area values were verified using

ANOVA followed by a Tukey post hoc test. Error bars in both (D) and (E) indicate standard

deviation. The IgG density was quantified for each condition as described in [19].

An additional measure of interest can be inferred from the actual surface densities of IgG

used in the experiments. The most densely coated coverslips presented about 25,000 IgG

molecules per μm^2 and induced ~85% of deposited cells to spread. Remarkably, even at a low

IgG surface density of ~44 molecules per μm^2, about 30% of the deposited cells still spread in an

IgG-dependent manner. Assuming that all IgG molecules in the cell-substrate contact region

have formed bonds with the cell's Fcγ receptors, and using an average equilibrium constant of

10^{-6} M for these receptor-ligand bonds [30], conservative (upper-limit) estimates of the adhesion

energy density of cell-substrate interactions on substrates coated with the high and low numbers

of IgG yield 1,500 $\mu J/m^2$ and 2.6 $\mu J/m^2$, respectively.

Purely adhesion-driven spreading: predictions by the Brownian zipper model

275   We first tested the simplest version of our framework, the Brownian zipper model, by

276   simulating purely adhesion-driven spreading in the absence of any protrusion stress (Fig 3, S1

277   Movie). In this scenario, the model cell is passive and is pulled onto the substrate by short-range

278   attraction. This case is conceptually equivalent to a viscous droplet spreading on an adhesive

279   substrate.

Fig 3. Predictions of the Brownian zipper model.

(A) A model cell spreading on the highest tested ligand density (100%) quickly approaches a

spherical cap morphology. Time stamps are included for each snapshot. (B) Curves of contact

area vs. time show that the spreading rate decreases monotonically. The contact area ultimately

approaches steady-state values predicted by the Young-Dupre equation (dashed lines). Predicted

equilibrium shapes are included on the right. (C) Log-log plot of contact area vs. time is nearly

linear over the initial spreading phase. The slope of this line corresponds to the exponent of a

power law describing contact area growth as a function of time. The dashed line shows a slope of

0.5 for reference.

Varying the ligand density ρ_l over two orders of magnitude, we found that the model

cells generally spread fastest immediately after first contacting the substrate. Afterwards, the

growth rate of the cell-substrate contact area decreased monotonically until the contact area

reached a steady-state plateau marking equilibrium (Fig 3B). As expected, the equilibrium

shapes were spherical caps. Log-log plots of the contact-area-versus-time predictions during the

initial, fast spreading phase were approximately linear, with slopes close to 0.5 (Fig 3C). Hence,

the contact-area growth initially obeys a power law, in agreement with various laws proposed to

describe droplet wetting dynamics [31] or passive cell spreading [8, 13]. In fact, the exponent of

0.5 is an excellent match to results of a previous study that modeled cells as highly viscous

droplets [13]. In S6 Appendices, Appendix B, we show how this exponent naturally arises during

early spreading of a passive model cell driven by adhesion stresses concentrated at the contact

perimeter.

Although the predictions of the Brownian zipper model agree well with the typical

theoretical behavior expected for this kind of passive model cell, they clearly differ from the

results of our phagocytic spreading experiments (Fig 2) in several important ways. First, the

simulated contact-area-versus-time curves lack the characteristic sigmoidal shapes observed in

experiments. Second, the predicted spreading curves exhibit a very strong dependence on the

density of encountered ligands, in stark contrast to the observed spreading behavior. This

dependence is evident in both the predicted spreading speeds, which increase dramatically with

ligand density, as well as the predicted maximum contact areas, which increase several-fold as a

function of the tested adhesive strengths.

Finally, the equilibrium shapes obtained for the adhesion energy densities used in the

simulations are inconsistent with the cell deformations observed on the experimentally tested

IgG densities. At equilibrium, the adhesion energy density (γ) of the Brownian zipper model cell

is related to the cortical tension τ and the contact angle θ_c via the Young-Dupre equation (Fig

4):

$$\gamma = \tau(1 - \cos\theta_c)$$ (10)

For a given value of the maximum cell-substrate contact area A_c, the equilibrium shape of the

model cell—a spherical cap—is uniquely defined by A_c and the known, constant cell volume.

Thus, basic geometry allows us to calculate the contact angle θ_c as well as the total cell surface

area A_{cell}. Inserting the value of the latter into Eq (1) provides the cortical tension at equilibrium,

which then can be used in Eq (10) to obtain the adhesion energy density as a function of A_c (Fig

4). As expected, the relationship between maximum contact area and adhesion strength predicted

by our numerical simulations agrees well with the Young-Dupre equation (Fig 3B, Fig S2 in S6

Appendices). The quantitative comparison of this theoretical prediction to actual adhesion energy

densities—estimated from the densities of deposited IgG molecules as explained earlier—

exposes entirely different behaviors between the model and experiments, however (Fig 4).

Especially in experiments performed at lower IgG densities, the conservatively estimated

adhesion energy densities were much lower than what would be required to form the measured

maximum contact areas solely by adhesion. In summary, the results of this section rule out

adhesion as the primary driving force of frustrated phagocytic spreading.

Fig 4. Relationship between ligand density and maximum contact area, as predicted by the

Young-Dupre equation.

The adhesion energy γ, and therefore the ligand density ρ_{IgG}, can be expressed as a function of

the contact area of the final spherical cap formed by a viscous droplet. The tested adhesion

strengths are marked as red dots. Actual experimental values are shown for comparison. Error

bars indicate standard deviation.

Protrusion-dominated spreading: predictions of the protrusive

zipper model

The protrusive zipper model incorporates the protrusion stress into the basic framework

considered in the previous section, enabling us to account for active force generation by the

model cell. Our semiempirical implementation is motivated by biological plausibility, and by the

goal to reproduce experimental observations with a minimum set of rules for the spatial

distribution (Eq (8)) and the deformation-dependent evolution of the protrusion stress during cell

spreading. To capture the presumed correlation between receptor-induced signaling and

protrusive force generation by the cytoskeleton, we express the strength of the protrusion stress

as a function of the cell-substrate contact area A_c. We assume that in the initial low-tension

regime, the protrusion stress grows linearly with A_c. Once the cortical tension increases more

steeply, the protrusion stress is assumed to grow faster as well. Ultimately, the strength of the

protrusion stress levels out at a maximum value of $\sigma_{prot,max} = 3.5$ kPa, within the range of

experimentally measured stresses exerted by parallel actin filaments [32, 33]. This behavior is

implemented in our model through a smoothed version of the following rule:

$$355 \quad \sigma_{prot} = \sigma_{prot,max} \times \begin{cases} \left[0.05 + 0.3\left(\dfrac{A_c}{A_{c,trans}}\right)\right] & \text{if} & \dfrac{A_{cell}}{A_{cell,0}} \le 1.26 \\[2em] \left[0.35 + 0.65\left(\dfrac{A_c - A_{c,trans}}{120\,\mu m^2}\right)^{1/2}\right] & \text{if} & \dfrac{A_{cell}}{A_{cell,0}} > 1.26 \text{ and } A_c \le A_{c,trans} + 120\,\mu m^2 \quad (11) \\[2em] 1 & \text{if} & A_c > A_{c,trans} + 120\,\mu m^2 \end{cases}$$

where $A_{c,trans}$ is the contact area when the total cell surface area A_{cell} is equal to $1.26A_{cell,0}$, the

transitional moment when the cortical tension starts rising more rapidly (Eq (1)).

We started examining the behavior of this model by first disregarding the adhesion stress

altogether. In this scenario, cell spreading is driven solely by protrusion, and the only role of

adhesion is to render cell-substrate contacts irreversible. We found that in this case, the model

cell begins spreading slowly while a distinctive leading edge gradually develops (Fig 5A, S2

Movie), resulting in a morphology that clearly differs from the spherical caps predicted by the

Brownian zipper model (Fig 3). Spreading slows noticeably at about 90 s, around the time the

protrusion stress reaches its maximum value. The resulting contact-area-versus-time curve has a

sigmoidal shape (Figure 5B,C). Plots of the protrusion stress and the cortical tension as a

function of time illustrate the qualitatively similar evolution of these two quantities, with the rise

of the tension lagging due to the initial "slack" of the cell surface in the low-tension regime (Eq

(1)).

Fig 5. Predictions of the protrusive zipper model.

(A) For purely protrusion-driven spreading, lamellar pseudopods form as the protrusion stress

increases over time. Time stamps are shown for the sample images. (B) Contact area increases

sigmoidally over time for the protrusive zipper model. The slope of the sigmoidal fit here is 3.0

μm^2/s at the inflection point, which matches the average spreading speed observed

experimentally. (C) Protrusion stress (governed by Eq (11)) and cortical tension (governed by Eq

(1)) increase during cell spreading. (D) Varying the parameter s_0 determines the thickness of the

pseudopods, with skinny protrusions for $s_0 = 0.4$ μm (top) and coordinated global cell

deformation at $s_0 = 2.0$ μm (bottom); all sample profiles are shown at t = 120 s. For the

protrusive zipper simulations shown in all other cases, we used $s_0 = 0.8$ μm.

We chose the value $s_0 = 0.8$ μm for the characteristic length that defines the spatial range

of the protrusion stress (Eq (8)) in the simulations shown in Fig 5A-C. Because s_0 does not

appear to be a directly measurable quantity, it is instructive to inspect how its value affects the

spreading model cell. Snapshots from simulations using different values of s_0 demonstrate how

the cell morphology (here: at 120 s) depends on the spatial range over which the protrusion stress

acts (Fig 5D, S3 Movie). Unsurprisingly, the leading edge of the cell assumes the shape of a thin

lamella for small values of s_0 and becomes increasingly thicker at larger s_0-values. We note

though that aside from this varying thickness of cellular protrusions, the overall spreading

behavior is similar across different values of s_0.

We next repeated the simulation with the same settings as used for Fig 5 but now also

included the adhesion stress. We again examined the same set of adhesion strengths as used in

our tests of the Brownian zipper model (Fig 3). The simulations expose how, in this scenario,

cell-substrate adhesion promotes spreading, affecting the overall spreading behavior in a

quantitative manner but without altering it qualitatively. The model cells spread somewhat faster

and farther on substrates coated with higher ligand densities (Fig 6A), with slightly larger contact

angles between their leading edge and the substrate (Fig 6B, S4 Movie). However, the sigmoidal

character of the contact-area-versus-time curves is conserved through most of the tested adhesion

strengths, and both the spreading speeds as well as the maximum contact areas vary much less

than in the predictions of the Brownian zipper model (Fig 3).

Fig 6. Predictions of the protrusive zipper model with varying adhesion stress.

(A) Contact area increases faster and reaches higher values for higher ligand densities. The

protrusion-only curve is shown for reference as a dashed line. (B) The leading edge of model

cells spreading on $\rho_l = 0\%$ and $\rho_l = 100\%$ differ visibly at the sampled time points. On higher

ligand density, both the extent of spreading and the dynamic contact angle increase.

Clearly, the predictions of the protrusive zipper model are in much better agreement with

experimental observations than those of the Brownian zipper. A spreading cell morphology that

is characterized by a forward-bulging leading lamella (Figs. 5-6) matches the cross-sectional

profile of phagocytes engulfing large particles well [24, 34], in contrast to model cell shapes

whose leading edge coincides with the perimeter of contact between the cell and substrate (Fig

3). The timing of spreading and sigmoidal shapes of the contact-area-versus-time curves

predicted by the protrusive zipper model (Fig 5-6) agree with experiments as well, and the time-

dependent increase in protrusion stress is consistent with a biphasic signaling response measured

during FcγR-mediated phagocytosis [35]. Furthermore, both the predicted spreading speeds as

well as the maximum contact areas are comparable to the respective values measured in

experiments, and the slight increase of the maximum contact area at higher adhesion strengths is

consistent with our measurements (Fig 6A). On the other hand, the predicted increase of the

spreading speeds on higher ligand densities (Fig 6A) differs from our experimental data (Fig 2).

Therefore, this model still somewhat overestimates the contribution of the adhesion stress to the

dynamics of phagocytic spreading. Nevertheless, of the two considered models only the

protrusive zipper model succeeds in capturing the essential dynamics of experimentally observed

phagocytic spreading, establishing that active cellular protrusion rather than passive cell-

substrate adhesion is the dominating driving force of this type of cellular motion.

Protrusive zipper model with discrete adhesion sites: best match

between experiments and theory

The previous sections presented continuum models of cell spreading, resulting in

predictions that overestimated the role of cell-substrate adhesion even in the case where short-

range adhesion plays only a secondary role. In reality, however, adhesive ligands encountered by

a spreading cell reside at discrete substrate locations rather than presenting a contiguous adhesive

film. A pioneering study that considered discrete adhesion sites not only predicted dramatic

qualitative differences compared to continuum models of adhesion but even concluded that,

depending on the lateral spacing of discrete cell-substrate cross-bridges, "there is little or no

tendency for the contact to spread unless the surfaces are forced together" [36]. These

considerations prompted us to design and examine a version of the protrusive zipper model in

which the model cell can only form new attachments to the substrate at prescribed locations (Fig

7, S5 Movie).

Fig 7. Predictions of the protrusive zipper model with discrete adhesion sites.

(A) Two time series (times shown at the left) of simulation snapshots illustrate how the

progression of the model cell's leading edge is affected by the spacing of discrete adhesion sites.

Unoccupied binding sites are depicted by empty circles, whereas filled circles indicate that the

cell membrane is locally attached. (B) Contact area vs. time curves share similar slopes over

three orders of magnitude of ligand density, but plateau at different maximum contact areas. (C)

The ligand-density-dependent increase in maximum contact area agrees well with experimental

results obtained in frustrated phagocytosis experiments. Error bars indicate standard deviation.

In this model version, the spacing of adhesion sites is determined by the ligand density ρ_l

(the number of ligand molecules per μm^2), with the in-plane spacing given by $(\rho_l)^{-1/2}$.

Furthermore, we introduce two additional rules to capture realistic aspects of cell spreading on

discrete adhesion sites. First, we replace the continuous adhesion stress (Eq (6)) with the

following concept of discrete bond formation. We consider a new bond as "formed" as soon as

the distance between the next free ligand site and the closest point of the advancing cell

membrane reaches a threshold distance d_{thresh}. As a consequence of such bonding, we place the

cell surface into irreversible contact with this substrate site when carrying out computations at

the next time step. The value of the threshold distance is determined by the magnitude of thermal

membrane fluctuations. Assuming that the time scale of membrane fluctuations is generally

smaller than our time step, we define d_{thresh} to be the root mean square height $<h^2>^{1/2}$ of

membrane fluctuations at equilibrium through [37]:

$$d_{thresh} = \sqrt{\langle h^2 \rangle} = \sqrt{\frac{k_B T}{4\pi\tau} \ln\left(1 + \frac{\tau A_{cell}}{\pi^2 \kappa_b}\right)} \qquad (12)$$

where k_B is Boltzmann's constant, T is temperature, A_{cell} is the cell surface area, and κ_b is

the membrane bending modulus. According to this rule, increased cortical tension τ suppresses

membrane fluctuations, making it more difficult for the cell to form new adhesive connections at

later time points.

Second, because it seems unlikely that persistent receptor-ligand contacts induce

signaling indefinitely, we also assume that the protrusion stress can diminish over time. This

assumption is supported by experimental data showing that actin polymerization does not

continue indefinitely during phagocytosis if the cell encounters an unopsonized region of the

target particle [18, 38, 39]. We implement this behavior by postulating a transient protrusion

stress that initially is triggered by fresh cell-substrate contact (occurring at time t_{bind}) and then

decays exponentially according to the relation:

$$\tilde{\sigma}_{prot} = \sigma_{prot} e^{-\frac{t - t_{bind}}{t_0}}$$ (13)

In this version of the model, σ_{prot} in Eq (8) is replaced by $\tilde{\sigma}_{prot}$ defined in Eq (13).

To avoid possible bias due to the exact placement of discrete binding sites, we performed

each simulation multiple times, shifting all binding sites laterally by small increments without

changing their spacing. We then averaged the results of these individual simulations to predict

the cell-spreading behavior as a function of the chosen spacing—or density—of adhesion sites.

Overall, the predictions of this discrete protrusive zipper model (Fig 7) agree well with

those of the continuum model version. For instance, maximum cell-substrate contact areas

exhibit a similar dependence on the ligand density in both models. However, in this discrete

model, the sigmoidal contact-area-versus-time curves are aligned much more closely, reflecting

spreading speeds that hardly depend on the ligand density anymore (Fig 7B).

The behavior of model cells spreading on discrete adhesion sites agrees amazingly well

with that of real human neutrophils during frustrated phagocytosis. As in experiments, the

spreading speed remains remarkably consistent over a range of ligand densities spanning 3

orders of magnitude. Moreover, the moderate increase of the maximum contact area at higher

ligand densities successfully reproduces experimental observations (Fig 7C). These results

reinforce the conclusion that active cytoskeletal protrusion drives phagocytic spreading. They

also highlight that it can be important for realistic models of cell spreading on substrates coated

with specific adhesion molecules to account for the discrete distribution of these adhesion sites.

Discussion

Quantitative understanding of the behavior of motile mammalian cells—from immune

cells to metastasizing cancer cells—is a prerequisite for transformative biomedical advances in

diagnosis, treatment, and therapy of many current and future health threats. Motile cells integrate

a complex variety of physical and chemical cues to carry out specific functions. Genuine

understanding of the underlying mechano-chemical processes not only requires an

interdisciplinary strategy but also integrative experimental/theoretical approaches. Translation of

mechanistic notions into mathematical models, and comparison of theoretical predictions with

experimental observations, often provides the strongest arguments for or against the validity of

biological hypotheses. Confidence in the predictive power of computer simulations requires that

the model assumptions be realistic and biologically plausible. Guided by this perspective, we

here examined fundamental biophysical mechanisms that potentially can facilitate spreading of

biological cells on a substrate.

Unpolarized cells usually begin spreading in a symmetric fashion [8, 40]. This stage is

often viewed as a passive process that is entirely driven by adhesion energy due to receptor-

ligand binding [8, 41]. An alternative class of models considers such spreading as dependent on

cytoskeletal activity [10, 14, 15]. In this study, we have developed a mechanical modeling

framework that allows us to establish whether frustrated phagocytosis, a specific form of

isotropic cell spreading, is primarily driven by adhesion (Brownian zipper model) or by

protrusive forces generated by the cell (protrusive zipper model). Our findings likely carry over

to other types of cell spreading inasmuch as key characteristics of adhesion and protrusion are

shared [42].

The incompatibility of our Brownian zipper simulations with experimental data

invalidates models of phagocytosis that treat neutrophil spreading as an adhesion-driven wetting

phenomenon [43]. Moreover, our findings invite a careful review of mathematical models of

other types of cell spreading that consider adhesion as the main driving force [8, 13]. A first

important prerequisite for the validity of such models is the use of realistic values of basic

mechanical parameters, such as the effective viscosity of the cell interior, the cortical tension,

and the adhesion energy density. For example, if the equilibrium cell-substrate contact areas

measured in our spreading experiments on low-to-moderate ligand densities were due to

adhesion, then the involved adhesion energies would have to be several orders of magnitude

higher than those estimated from our measurements of ligand density. Even receptor

accumulation in the contact region could not make up for this difference, because the smaller

number of available ligands limits the number of possible adhesion bonds. Furthermore, the

ability to simulate not only equilibrium situations but also the dynamical cell behavior, and to

leverage time-dependent experimental observations against the predictions of such models,

considerably raises confidence in a model's evaluation. As demonstrated in this study, such

comparison greatly benefits from the availability of experimental data obtained on substrates

presenting a large range of known densities of adhesive ligands.

It appears that adhesion-driven spreading is largely limited to situations where adhesion

is unusually strong, and where the cells—like red blood cells—or surrogate objects—like lipid

vesicles—are characterized by a low-viscosity interior and very low tension of their cortex or

membrane. Indeed, a recent mechanical modeling study found that Brownian membrane

fluctuations were only sufficient to drive very small amounts of cell spreading on a surface [44].

If there are cases in which motile mammalian cells spread predominantly due to adhesion, then

such spreading will likely occur on much longer timescales than considered here. Finally, it may

be possible that adhesion plays a more relevant role in the engulfment of very small particles

whose uptake does not require a significant expansion of the cell surface area. Irrespective of the

relevance of Brownian-zipper-type models in a particular practical situation, we note that the

excellent agreement of our theoretical treatment of purely adhesion-driven spreading with other

studies focusing on this form of motion [8, 13] strengthens confidence in our modeling approach

and its numerical implementation.

The only alternative mechanism by which cells can expand their region of contact with a

suitable substrate appears to be active, protrusion-dominated spreading. Many imaging studies

indeed have documented an increased density of F-actin at the protruding front of motile immune

cells [16, 45, 46], supporting the biological plausibility of the protrusive zipper concept.

Moreover, inhibition of actin polymerization with cytochalasin B or latrunculin A eliminates the

rapid phase of fibroblast spreading [10, 14, 47]. Similarly, chemical disruption of the actin

cytoskeleton generally inhibits phagocytosis by immune cells [28, 38]. We have previously

shown that extremely small concentrations of actin inhibitors actually can increase the size of

transient, chemotactic-like protrusions [28, 48]. However, the cortical tension was reduced in

such cases, and phagocytic spreading was not enhanced, highlighting the multiplicity of—likely

dichotomous—mechanical roles of F-actin during cell deformations.

Our simulations based on the protrusive zipper model not only reproduce the main

features of neutrophil spreading on IgG-coated substrates but, in the case of discrete adhesion

sites, they also agree very well with experimental data. We note that this agreement neither is

surprising, nor does it constitute solid proof of the validity of this model. The scarcity of

quantitative insights into the underlying mechanisms simply does not place sufficient constraints

on the design of computational models. Instead, our goal here was to explore what set of

minimalistic rules would need to be postulated to achieve a good match between theory and

experiment. The successful implementation of this approach allows us to propose likely

mechanistic details that can then provide guidance for future studies. Still, we are confident that

the protrusive zipper model paints a reasonably accurate picture of phagocytic spreading, not

only because of the elimination of the only alternative hypothesis, but also because our

semiempirical model is plausible, i.e., it does not contradict pertinent biophysical and biological

insights. For example, our implementation of the relationship between receptor-induced

signaling and the generation of protrusive force is consistent with the hitherto most successful

model of phagocytosis [24], as well as with previous measurements of the biphasic signaling

response from a macrophage-like cell line during Fcγ receptor-mediated phagocytosis [35].

Importantly, this implementation is independent of the exact mechanism by which intracellular

processes are translated into protrusive force; instead, it encompasses different mechanistic

notions such as the Brownian ratchet [49] and end-tracking motors [50].

An important outcome of our simulations of the protrusive zipper model is the difference

in predictions depending on whether we considered continuous or discrete cell-substrate

adhesion, in agreement with a previous theoretical study [36]. We are unaware of physiological

situations in which cell adhesion is not predominantly supported by specific receptor-ligand

bonds. Thus, the model version that is based on discrete binding sites is the more realistic version

of the protrusive zipper. Remarkably, it is also the version that yielded the best match between

theory and experimental observations. To achieve this agreement, we postulated that the

formation of new receptor-ligand bonds is coupled to the protrusion stress in a time-dependent

manner (Eq (13)), based on the assumption that receptor-induced signaling and subsequential

actin polymerization are not sustained indefinitely after a ligand activates the receptor. There are

multiple factors that could lead to this effective decay, such as the depletion of precursor

molecules needed for the production of signaling messengers (e.g. release of IP_3 will cease once

PIP_2 has been locally depleted [51]).

Perhaps the most important insight from the comparison of model versions based on

continuous versus discrete adhesion is that models based on continuous adhesion are likely to

misrepresent key aspects of the cell behavior, especially on lower ligand densities. For example,

such models cannot capture the possibility that too large ligand spacing may prevent the next

unbound receptor-ligand pair from approaching one another to within the distance at which they

are likely to form a bond. In our protrusive zipper model with discrete adhesion, variation of

substrate adhesivity by changing the density of adhesion sites primarily affects the maximum

cell-substrate contact area. This prediction agrees well with our experiments, unlike the

predictions by model versions that treat the ligand layer as a continuum.

The mechanisms governing isotropic cell spreading studied here are likely to also play a

crucial role in the directional motion of migrating cells. Many immune cells, for example, are

capable of executing both types of motion, as required during phagocytic spreading versus

chemotactic and other forms of migration. As revealed by our experiments and reproduced by

our discrete adhesion model, the rate of isotropic cell spreading is largely conserved on

substrates presenting a broad range of densities of adhesion sites. This finding exposes an

interesting difference to the prediction by models of migrating cells, i.e., that the crawling speed

of such cells has a maximum on substrates with intermediate adhesion strengths [52-54]. This

difference is a reminder that directional migration generally is a more complex type of motion

that involves, in addition to protrusion and adhesion, important mechanisms regulating

contraction and detachment of the rear of the migrating cell from the substrate. The positive

correlation between low-to-moderate ligand densities and the speed of motion predicted by

models of migrating cells can be attributed to either a direct scaling of protrusion with the

amount of adhesion [53], or a postulated increased actin retrograde flow at lower adhesion

strengths [52]. The predicted slowing of migrating cells at higher ligand densities is caused by an

effective frictional force due to the need to break stronger adhesive attachments at the cell's rear

[55, 56]. A noteworthy recent model of cell migration that decoupled friction from adhesive

attraction actually predicted faster movement for higher adhesion energies [41]. The excellent

agreement between our experiments and the protrusive zipper model suggests that the above

additional mechanisms included in models of migrating cells play at most a minor role in

isotropic phagocytic spreading. On the other hand, we believe that the main insights exposed by

our study provide important suggestions on how to treat the interplay between protrusion and

adhesion in models of migrating cells.

Methods

The perturbed Stokes equations

Assuming the cell interior can be approximated by a single, highly viscous, slow-moving Newtonian fluid, its motion obeys the Stokes equations for creeping flow with no body force, as given by Eq (2). Furthermore, for an incompressible fluid, the equation of continuity simplifies to the incompressibility condition (Eq (3)). Due to axial symmetry, there are three unknowns: v_r, v_z, and p, where r and z are cylindrical polar coordinates.

To solve this system of partial differential equations, we use the finite element method (FEM). Because directly solving the Stokes equations using FEM leads to numerical instabilities [57], we follow the procedure outlined by Drury and Dembo [29] to solve a perturbed form of the Stokes equations, in which the incompressibility condition (Eq (3)) is approximated as

$$\nabla \cdot (\mathbf{v} - \epsilon \nabla p) = 0 \tag{14}$$

In this form, the fluid is nearly incompressible, which allows us to avoid the well-known problems with using FEM for incompressible problems [57]. To accurately solve the Stokes equations, the value for ϵ must be sufficiently small. Specifically, we use the condition given in [29]:

$$\epsilon \leq \frac{h_{mesh}^2}{\mu} \tag{15}$$

where h_{mesh} is the characteristic radius of a single quadrilateral element. We tested different values of ϵ in our models and found this condition to provide sufficient accuracy and convergence (Fig S5 in S6 Appendices).

Over the unbound portion of the cell, we specify Neumann boundary conditions,

corresponding to a stress balance (Eq (4)). For the adherent cell surface, we specify Dirichlet

boundary conditions, simply a no-slip condition in this case (Eq (9)). The pressure boundary

condition is given by assuming the normal component of the pressure gradient goes to zero at the

cell surface:

$$\nabla p \cdot \mathbf{n} = 0 \qquad (16)$$

648 Computational details

At each time step, we first compute values for the surface curvature of the cell. Local

values of the angle of the normal ϕ are evaluated using cubic polynomial fits. We then

calculate the boundary stresses using the relationships outlined in the main text. The integral for

the effective adhesion stress (Eq (6)) is computed numerically as described in S6 Appendices.

The values for tension and protrusion stress at each time step are evaluated using smoothed

versions of the relationships given in Eq (1) and Eq (11) (see S6 Appendices for full forms).

To find the fluid velocity and pressure fields, we must simultaneously solve Eq (2) and

Eq (14) for v_r, v_z, and p. We employ the strategy outlined in [29], which is an adaptation of the

Uzawa method. Starting with an estimate for pressure p_{est} given either by the previous time step

or as a uniform distribution prior to spreading, we solve for fluid velocities by treating the

pressure as known in Eq (2):

$$\mu \nabla^2 \mathbf{v} = \nabla p_{est} \qquad (17)$$

We then treat the fluid velocities as known ($\mathbf{v}_{est}$) and solve an altered version of equation (14):

$$\frac{1}{\mu}(p - p_{est}) = \nabla \cdot \mathbf{v}_{est} - \nabla \cdot (\epsilon \nabla p) \qquad (18)$$

The updated pressure is then inserted back into Eq (17) and the procedure is repeated until the

following condition is met:

665
$$\frac{\max\left(\left|p-p_{est}\right|\right)}{\max\left(\left|p-p_{out}\right|\right)} \leq 10^{-6}$$
(19)

666   This generally occurs in less than 50 iterations.

667   The new cell boundary is then given by

668
$$r(t+\Delta t) = r(t) + v_r \Delta t$$
$$z(t+\Delta t) = z(t) + v_z \Delta t$$
(20)

The value for Δt was set relative to the Courant number for each iteration, such that fluid flow

occurs over at most 10% of any individual element (S6 Appendices). In the continuum adhesion

case (no discrete adhesion sites), the contact line is updated at each time step by computing the

intersection between the cell boundary and the surface, then adding all points advected to $z \leq 0$

to the Dirichlet boundary condition (contact, no-slip) for the next time step. In the discrete

adhesion model, contact is determined by the distance threshold computed from Eq (12). The

contour is smoothed after each advection, and then small corrections are made to the cell contour

to compensate for any deviations from constant volume due to smoothing and numerical error.

This model was implemented in MATLAB R2020b (MathWorks) and the full code is

available at https://github.com/emmetfrancis/phagocyticSpreading. Individual simulations

generally run within 1-3 hours on a personal computer.

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Supporting Information

S1 Movie. Simulations of purely adhesive cell spreading ("Brownian zipper") on substrates

presenting different densities of adhesion sites. This sequence of animations shows side views

of model cells spreading on adhesive substrates coated with relative ligand densities (ρ_l) of 1%,

3%, 10%, 30%, and 100% for 400 s in the absence of protrusion stress.

S2 Movie. Simulation of purely protrusion-driven cell spreading. This animation shows a

side view of a model cell spreading on a flat substrate for 200 s. The cell motion is assumed to be

driven exclusively by active cytoskeletal protrusion at a maximum protrusion stress of $\sigma_{prot,max} =$

3.5 kPa. Cell-substrate contact, once established, is assumed to be permanent. All other

contributions of adhesive cell-substrate interactions to spreading are neglected.

S3 Movie. Effect of the range of action of the protrusion stress on purely protrusion-driven

cell spreading. This sequence of simulations shows side views of model cells spreading in the

absence of adhesion stress for 200 s. Increasing the range s_0 over which cytoskeletal protrusion

actively pushes the cellular pseudopod outwards (given in terms of the arc length of the free cell

contour, measured from the point of substrate contact) results in thicker pseudopods. In this

sequence, $s_0 = 0.4$ μm, 1.2 μm, and 2.0 μm, respectively. In all examples, $\sigma_{prot,max} \times s_0 = 2.8$

mN/m.

S4 Movie. Minor role of cell-substrate adhesion stress in protrusion-dominated cell

spreading ("protrusive zipper"). This sequence of simulations compares magnified views of

purely protrusion-driven spreading (adhesion stress $\rho_l = 0\%$) with protrusion-driven spreading in

the presence of moderate and strong adhesion stress ($\rho_l = 10\%$ and 100%, respectively). In all

examples, $\sigma_{prot,max} = 3.5$ kPa.

S5 Movie. Protrusive zipper simulations with discrete adhesion sites. This sequence of

simulations shows a magnified view of protrusion-driven spreading ($\sigma_{prot,max} = 3.5$ kPa) on

substrates presenting different densities of discrete adhesion sites ($\rho_l = 30$ μm^{-2}, 100 μm^{-2}, 1,000

μm^{-2}, and 10,000 μm^{-2}). Open circles denote free adhesive binding sites, and filled circles depict

sites with engaged ligand.

S6 Appendices. Derivation of important relationships and summary of numerical testing.

(A) Adhesion stress calculation. (B) Derivation of a power law for contact area growth in passive

spreading. (C) Development of C^1 versions of tension and protrusion stress relations. (D) Details

of finite element implementation. (E) Summary of numerical testing.

S7 Table. Summary of modeling parameters, with supporting references.