# Osseointegration of functionally-graded Ti6Al4V porous implants: Histology of the pore network

Joseph Deering<sup>a</sup>, Dalia Mahmoud<sup>b,c</sup>, Elyse Rier<sup>d</sup>, Yujing Lin<sup>e</sup>, Anna Cecilia do Nascimento Pereira<sup>f,g</sup>, Silvia Titotto<sup>f,g</sup>, Qiyin Fang<sup>h</sup>, Gregory R. Wohl<sup>b,d,i</sup>, Feilong Deng<sup>e</sup>, Kathryn Grandfield<sup>a,d,i\*</sup>, Mohamed A. Elbestawi<sup>b\*</sup>, Jianyu Chen<sup>e\*</sup>

<sup>a</sup> Department of Materials Science and Engineering, McMaster University, Hamilton, ON, Canada

<sup>b</sup> Department of Mechanical Engineering, McMaster University, Hamilton, ON, Canada

<sup>c</sup> Production Engineering Department, Faculty of Engineering, Alexandria University, Alexandria 21544, Egypt

<sup>d</sup> School of Biomedical Engineering, McMaster University, Hamilton, ON, Canada

<sup>e</sup> Guanghua School of Stomatology, Hospital of Stomatology, Guangdong Provincial Key Laboratory of Stomatology, Sun Yat-sen University, Guangzhou, China

<sup>f</sup> Center of Engineering, Modeling and Applied Social Sciences, Federal University of ABC (UFABC), Santo André, Brazil

<sup>g</sup> 4D Printing and Biomimetics' (4DB) Research Group, Federal University of ABC (UFABC), Santo André, Brazil

<sup>h</sup> Department of Engineering Physics, McMaster University, Hamilton, ON, Canada

<sup>i</sup> Brockhouse Institute for Materials Research, McMaster University, Hamilton, ON, Canada

\* Co-Corresponding authors:

Kathryn Grandfield Email: kgrandfield@mcmaster.ca Mohamed A Elbestawi Email: elbestaw@mcmaster.ca Jianyu Chen Email: chenjy89@mail.sysu.edu.cn

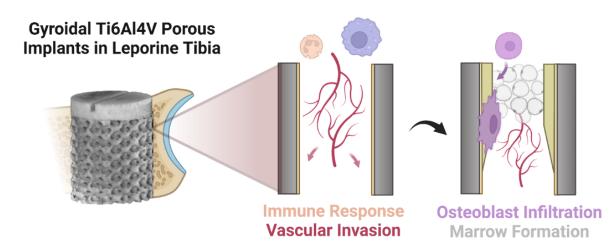
## Abstract

The additive manufacturing of titanium into porous geometries offers a means to generate lowstiffness endosseous implants with a greater surface area to improve osseointegration. In order to optimize pore size in the scaffolds, it is important to first understand the timeline of osseointegration in pre-clinical models. In this work, selective laser melting was used to produce gyroid-based scaffolds with a uniform pore size of 300  $\mu$ m or functionally-graded pore size from 600  $\mu$ m to 300  $\mu$ m before implantation in New Zealand white rabbit tibiae for 4 and 12 weeks. Initial *in vitro* assessment with Saos-2 cells showed favourable cell proliferation at pore sizes of 300 and 600  $\mu$ m. At four weeks, histological observations indicated some residual inflammation alongside neovessel infiltration into the scaffold interior and some early apposition of mineralized bone tissue. At twelve weeks, both scaffolds were filled with a mixture of adipocyte-rich marrow, micro-capillaries, and mineralized bone tissue. X-ray microcomputed tomography showed a higher bone volume fraction (BV/TV) and percentage of bone-implant contact (BIC) in the implants with 300  $\mu$ m pores than in the functionally-graded specimens, indicating that these smaller pore sizes may be favourable for osseointegration in leporine bone.

### **Keywords**

Additive manufacturing; Selective laser melting; Osseointegration; Porous implants; Histology; Bone ingrowth; Neovascularization

## **Graphical Abstract**



## Introduction

Central to the success of dental and orthopaedic implants is the development of a structural and functional connection at the bone-implant interface [1]. Careful control over material biocompatibility, surgical technique, and macroscale implant design are among the core parameters for governing the early stages of osseointegration – especially important as failure is most common within the first year of implantation [2]. These design strategies [3,4] have been developed to include elements of isotropy [5,6] and biomimetics to tune the mechanical characteristics [7,8] of tissue scaffolds, with renewed interest in optimizing scaffolds for osseointegration. In particular, the advancement in laser powder bed fusion (L-PBF) has allowed for the fabrication and geometric control of metallic lattice structures for use in bone tissue engineering applications [9–11]. These lattice structures utilize interconnected pore structures to provide additional surface area for bone ingrowth [12] and their use aims to improve the secondary stability of dental and orthopaedic prostheses. Moreover, the porosity reduces the overall stiffness of the implant and potentially helps to mitigate bone resorption associated with stress shielding phenomena as suggested by numerical simulations with a low-stiffness implant stem [13].

In general, additively manufactured lattice structures can be categorized by their repeating topology into a dichotomy of computer-aided drawings (strut-based) or triply periodic minimal surfaces (TPMS) [14,15]. Gyroid is one subset of TPMS lattice family, with the possibility to mimic the mechanical properties of bone by tuning the relative density of the scaffold [16]. The main advantage of gyroid structures is that their architecture facilitates cell migration, in part due to their infinitely smooth architecture and relatively high fluid permeability [17]. TPMS structures also demonstrate high surface area to volume ratio, high energy absorption [18], and high specific strength/stiffness [19]. Recent research has been directed to investigate the capability of functionally-graded (FG) TPMS designs in terms of pore volume fraction and morphology [20-22]. While the optimal pore size for each pre-clinical animal model is still disputed, a benchmark for adequate pore size ranges between 300-500 µm for osseointegration to occur and porosity values in the implant ranging from 50-70% appear to be most abundant for porous implants [11]. Numerous experimental and numerical studies of functionally-graded TPMS scaffolds have shown they are suitable for bone tissue engineering based on their mechanical properties [23–25], but there is a distinct research gap relating to the osseointegration of additively manufactured implants with a changing pore size throughout their interior.

Despite the design and *in vitro* characteristics of TPMS structures having been reviewed elsewhere [26], these forms of experimentation are generally limited compared to *in vivo* studies [27]. In general, the *in vivo* wound healing response in the peri-implant environment follows distinct stages of clotting and inflammatory response, sprouting of new blood vessels and extracellular matrix deposition, and formation of mineralized bone tissue around classical implants [28]. However, there is a distinct lack of in-depth histological probes describing whether these biological processes occur through the interior of porous metals during the healing timeline – especially in implants with TPMS geometries.

In this work, we assessed the *in vitro* cytocompatibility and *in vivo* osseointegration within the interior of uniform and functionally-graded Ti6Al4V gyroid structures. Using Saos-2 metabolic activity measurements, X-ray microcomputed tomography of newly formed tissue in the leporine tibia, and hematoxylin/eosin staining of histological sections, we describe common themes in bone tissue nucleation and adaptation over twelve weeks within the sheltered porous interior of metallic implant materials.

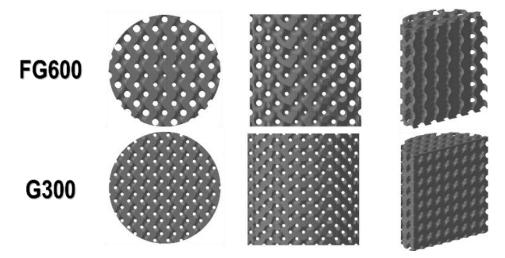
### Methods

### Scaffold Design and Fabrication

TPMS Ti6Al4V gyroid parts were fabricated by selective laser melting additive manufacturing. The Renishaw additive manufacturing machine was equipped with a 200 W pulsed laser, creating a series of overlapping exposures to assemble parts one layer at a time using an exposure time of 40 µs, point distance of 60 µm, layer thickness of 30 µm, and hatch spacing of 65 µm [29]. The surface of gyroids was modelled using Equation 1, where *a* defines the unit cell size, *t* defines the volume fraction (relative density) of the gyroids, and x/y/z represents the spatial coordinates within the scaffold interior.

(Eqn. 1) G: 
$$\sin\left(\frac{2\pi x}{a}\right)\cos\left(\frac{2\pi y}{a}\right) + \sin\left(\frac{2\pi y}{a}\right)\cos\left(\frac{2\pi z}{a}\right) + \sin\left(\frac{2\pi z}{a}\right)\cos\left(\frac{2\pi x}{a}\right) - t = 0$$

A MATLAB® code was used to generate the surface of the gyroids, both with functional grading and without (i.e., uniformity) in the pore structure. Uniform gyroid structures with an approximate pore size of 300  $\mu$ m (herein denoted as G300), uniform pore size of 600  $\mu$ m (G600), or functionally-graded gyroid structures (FG600) were fabricated as illustrated in Figure 1. FG600 implants were created with a radially-varying pore size using a linear distribution of unit cell size to create a pore size distribution between 600  $\mu$ m at the scaffold exterior and 300  $\mu$ m at the scaffold midpoint. The porous fraction of all implants was designed with a height of 6 mm and Boolean merged to a slotted crown with a height of 1 mm prior to PBF, with a total implant diameter of 6 mm. The relative porosity of the G300 scaffold was estimated at 50% while the net porosity of the FG600 was estimated at 60%.



*Figure 1: Overview of porous regions within the gyroid implants.* The FG600 implant contained pores that decreased in size from 600  $\mu$ m to 300  $\mu$ m as a function of implant radius in the gyroid. The G300 implant contained a uniform array of 300  $\mu$ m pores through the gyroid. The G600 implant (not shown) contained a uniform array of 600  $\mu$ m pores through the gyroid.

### In Vitro Saos-2 Culture

Saos-2 cells (ATCC HTB-85) were seeded on uniform titanium gyroids to mimic osteoblast proliferation in vitro as described elsewhere [30]. Briefly, cells were seeded onto six replicates of G300 and G600 scaffolds using a seeding density of 10,000 cells/cm<sup>2</sup> in a 24-well plate (approximately 17,700 cells per specimen). Culture was conducted in McCoy's modified 5A media (Life Technologies Inc.) using incubation at 37°C and 5% CO<sub>2</sub>. After one, three, and seven days of culture, cell metabolism was measured by incubating samples with a mixture of 5% alamarBlue dye (Life Technologies Inc.) in culture media for 60 min and extracting the dye for fluorescence readings at excitation-emission wavelengths of 540/580 nm. A two-way analysis of variance (ANOVA) was conducted to determine statistical significance for each test group using R 3.6.1 ( $\alpha = 0.05$ ). Following metabolic measurement at seven days, cells on a gyroid specimen were fixed by immersion in 0.25% glutaraldehyde in cacodylate buffer for 2 hr and stained with osmium tetroxide. Samples were dehydrated in a graded ethanol series (50%, 70%, 70%, 95%, 95%, 100%, 100%) in approximately 1 hr intervals before critical point drying in ethanol. Scanning electron microscopy (SEM) was conducted on the gyroid specimen following the application of a 5 nm platinum coating using a TESCAN VP microscope at an accelerating voltage of 10 kV to examine cellular interaction with the titanium.

### Surgical Implantation

20 adult male New Zealand white rabbits, weighing about 3 kg, were used in this study under the approval of the Animal Care Committee of Sun Yat-sen University (Approval No. SYSU-IACUC-2020-000198). Under general anesthesia and routine disinfection, a FG600 and a G300 implant were alternately and bilaterally placed in the left and right anteromedial, proximal tibial epiphyses of each rabbit to avoid bias from strong and weak responders [31]. The surface of the implant was set level with the cortical bone surface before suturing the surgical sites. Antibiotics were

administered for three consecutive days after surgery. In order to trace and quantify new bone growth, calcein (C0875 Sigma-Aldrich) and alizarin red (A3882 Sigma-Aldrich) fluorochrome labels were injected into all rabbits in the 2<sup>nd</sup> and 6<sup>th</sup> week of implantation respectively. The doses of calcein and alizarin red were 5 mg/kg and 30 mg/kg respectively.

At each end-point (4 and 12 weeks after surgery), 10 rabbits were sacrificed, and the tibia-implant blocks were retrieved and fixed in 10% neutral buffered formalin solution. Five of the blocks were taken for X-ray microcomputed tomography (micro-CT) and the remaining five were used for the histological evaluation at each time point.

### X-ray Microcomputed Tomography

Following tissue fixation, tibia-implant samples were subjected to an ethanol dehydration series (70%, 80%, 90%, 95%, 95%, 100%, 100%) in 48 hr intervals and gradually infiltrated with Embed812 resin (Electron Microscopy Sciences) in sequential ratios of 1:3, 1:1, and 3:1 with either acetone or propylene oxide. Resin was cured for 48 hr at 65°C. Micro-CT (Bruker Skyscan 1172) was conducted using a 100 kV beam and 100  $\mu$ A current with a 0.5 mm Al filter. Voxel size during acquisition was set to 3.55  $\mu$ m with a 0.25° rotation step. NRecon software (Bruker) was used to create an image stack from the projections using misalignment compensation, moderate ring-artifact reduction, and beam-hardening correction of 67%.

Image processing was conducted in Dragonfly 2022.1 (Object Research Systems) where all micro-CT datasets were subjected to a Gaussian smoothing operation with a kernel size of 9 and  $\sigma = 3.0$ . A 5-layered convolutional neural network (CNN) was created to semantically segment four classes within the micro-CT datasets (Figure S1), designated as implant material, bone residing within the implant, bone residing outside the implant, and resin/void space. The CNN was trained using augmented training data from 19 periodically sampled images across two separate datasets, where 80% of the training data was used for training and 20% of the training data was used for validation. Training was conducted using a patch size of 64, stride ratio of 0.5, batch size of 32, learning rate of 0.30, and was stopped early after 10 consecutive epochs without decrease in the validation loss to avoid overfitting.

Scaffold pore size validation and strut size variation was found by fitting a cylindrical sub-volume to the porous interior of the scaffold and masking regions attributed to implant and non-implant. Island removal was conducted to remove connected components with a voxel count of 1,000,000 or fewer and each region was assigned to a thickness mesh using a downsampling factor of three for three-dimensional measurement of pore and strut size. Bone volume fraction (BV/TV), measured here as the percent of available pore space in the implant filled with tissue, was measured by applying a cylindrical mask to the segmentation at the boundaries of the porous midsection and calculating the number of bone-classified voxels divided by the sum of total voxels (pore and bone). Percentage of bone-implant contact (BIC) was measured by performing a 3D cubic dilation with a kernel size of 15 on the region of interest (ROI) labelled as implant within the previously defined cylinder to create a zone within 25  $\mu$ m of implant struts. The Boolean difference between the dilated ROI and original implant ROI was taken. BIC was then calculated as the ratio of the number of bone-labelled voxels within the Boolean subtraction divided by the total volume of the

Boolean subtraction. BIC and BV/TV measurements were compared using a two-way ANOVA and Tukey's HSD test using a significance value of  $\alpha = 0.05$ .

### Scanning Electron Microscopy

Select bone-implant blocks were subjected to serial dehydration in acetone using 48 hr intervals and infiltrated with Embed812 resin in ratios of 1:3, 1:1, and 3:1 before transfer to 100% resin for curing at 60°C. Bone-implant samples were bisected using a low-speed diamond saw (Bueler Isomet) for backscattered (BSE) scanning electron microscopy. Specimens were polished (400-1200 SiC paper), mounted on an aluminum stub, and sputtered with 10 nm of carbon. Backscattered electron images were acquired using a JEOL 6610 LV microscope (JEOL, Peabody, USA) at an acceleration voltage of 10 kV.

To reveal the underlying osteocyte network of samples, approximately 5 ml of 37% phosphoric acid was placed on the top surface of the embedded samples for 10 seconds. The samples were then rinsed with excess deionized water for 20 seconds, immersed in a bath of 5% sodium hypochlorite for 5 minutes, thoroughly rinsed again for 30 seconds, and air-dried overnight. The samples were prepared for SEM imaging with a 10 nm gold coating and imaged using secondary electron imaging in a JEOL 6610LV microscope (JEOL, Peabody, USA) at 7 kV.

## Histology

Tibia-implant specimens for histology were dehydrated using increasing concentrations of alcohol (70%, 80%, 90%, 95%, 95%, 100%, 100%) and then embedded in methylmethacrylate for sectioning. Cutting of 100-µm-thick sections, parallel to the long axis of the implants, was performed by using an EXAKT E300CP (EXAKT, Germany) to extract a single slide section from the midpoint of the implant. The sections were then ground by EXAKT 400CS (EXAKT, Germany) and stained with hematoxylin and eosin (H&E).

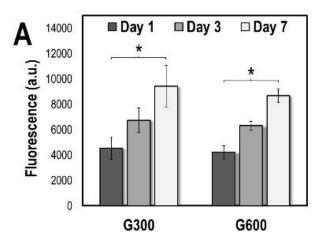
H&E-stained histological sections were observed using an EVOS inverted microscope (Life Technologies Inc.) to view cell and bone matrix deposition at ROIs defined on the interior and exterior of the scaffolds. Four slides for each implant type at 4 wk and 12 wk of implantation were imaged using bright-field imaging, and fluorescent signals from calcein and alizarin red on the same sections were observed using an A1R HD25 inverted confocal microscope (Nikon) to assess locations of calcification in the new tissue after 2 weeks and 6 weeks. Fluorescent images were overlaid in Dragonfly 2022.1 with gamma correction and implant boundaries were found using a grayscale-derived segmentation of the implant volume.

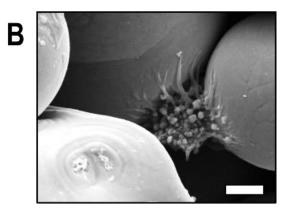
## **Results and Discussion**

### In Vitro Scaffold Characterization

*In vitro* characterization of the gyroid scaffolds (G300 and G600) was conducted using the Saos-2 cell line as a rapidly proliferating approximation of the behaviour of osteoblasts on the scaffolds

[32]. By measuring the metabolic activity of Saos-2 cells on the scaffolds at one, three, and seven days of culture (Figure 2A), statistically significant growth was observed between each time point regardless of scaffold geometry. At each unique time point in the seven-day study, gyroid scaffolds in the G300 and G600 groups showed similar potential for osteoblast proliferation and *in vitro* bone growth via metabolic measurement. SEM of cellular interactions with the additively manufactured titanium showed that Saos-2 cells adhere to the Ti6Al4V substrates and can co-locate to bridge gaps between partially-fused titanium powder particles on the surface (Figure 2B).





*Figure 2: In vitro assessment of uniform gyroid Ti6Al4V scaffolds.* (*A*) Saos-2 metabolic activity increases for each type of scaffold at three and seven days of culture (p < 0.05). Scaffolds showed comparable behaviour with pore sizes of 300  $\mu$ m and 600  $\mu$ m at each time point. (*B*) Adherent Saos-2 cell on the surface of an additively manufactured Ti6Al4V gyroid specimen, showing interaction with the cleft between two sintered powder particles on the surface. Scale bar: 5  $\mu$ m.

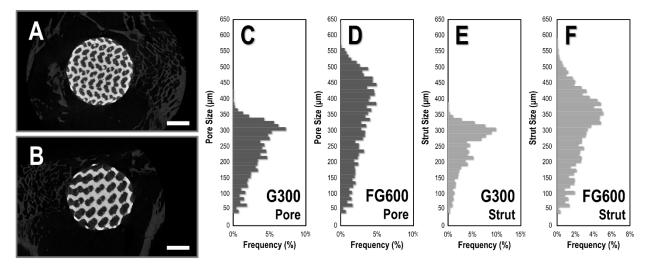
For laser powder-bed fusion additive manufacturing, in the absence of post-processing surface modification strategies such as acid-etching [33,34] or grit-blasting [35,36], the packing behaviour of surface-bound metallic particles is governed by characteristics of the feedstock powder and processing parameters defined during selective laser melting [37]. Where similar observations of *in vitro* cell-surface interaction have been observed on stainless steel powder particles [38], it seems as though the pore design of the scaffold may have less of a role than physical or chemical modification of the surface for *in vitro* proliferative effects. Similar fluorescence readings were obtained for the G300 scaffolds and G600 scaffolds, despite the increase in internal surface area in the G300 group. It appears the bulk of the early cellular activity can therefore be attributed to near-surface cells in the scaffold. Similar behaviour has been observed with 3D cell culture in porous microcarriers for other cell types, including chondrocytes [39] and adipose-derived stem cells [40], where cell proliferation to internal surfaces only starts to become evident around five or seven days of culture.

### X-ray Microcomputed Tomography

### Scaffold Feature Size Validation

To assess the deviation in pore and strut size in each *in vivo* scaffold type (G300 and FG600) from the design, measurements were extracted from micro-CT scans of the implants (Figure 3).

Representative slices from the porous midsection (Figure 3A-B) show a distinguishable difference between the two scaffolds (3A: G300 uniform, and 3B: FG600 functionally-graded) at a glance based on their relative pore size. Mapping the pore and strut size distributions for the G300 implant (Figure 3C and 3E) showed a similar distribution in each. The highest frequency of pore size for the G300 implant was measured to be between 300-310  $\mu$ m, indicating that the build parameters utilized during additive manufacturing result in parts with a relatively high tolerance. The median pore size for the G300 implants lies in the range of 250-260  $\mu$ m, however, the lower bound of the distribution is subject to image processing artifacts as pores at the edge of the scaffold can be partially truncated when performing the Boolean intersection with the bounding cylinder or some marginal pore occlusion by partially-fused powder particles. Similarly, the most frequent strut size in the G300 scaffold also ranges between 300-310  $\mu$ m with a median between 250-260  $\mu$ m. For uniform pore sizing, the gyroid topology appears to offer a consistent interconnected pore structure throughout the scaffold interior and avoids sharp self-intersections as is typical of TPMS geometries.



*Figure 3: Micro-CT and gyroid topology validation.* (*A*) *Micro-CT* slice showing cross-section of G300 scaffold after 12 wk of implantation in leporine tibia. (*B*) *Micro-CT* slice showing cross-section of FG600 scaffold after 12 wk of implantation in leporine tibia. (*C*) *Pore size distribution (n = 10) within the G300 scaffold interior.* (*D*) *Pore size distribution (n = 10) within the FG600 scaffold interior.* (*E*) *Titanium strut size distribution (n = 10) in the G300 scaffolds.* (*F*) *Titanium strut size distribution (n = 10) in the FG600 scaffolds. FG600 scaffolds. FG600 scaffolds appear to have a wider distribution of both pore diameter and strut diameter as a result of the functionally-graded pore design. Scale bars: (A-B) 2 mm.* 

In contrast, it is clear from the pore and strut size distributions in the FG600 implant that the addition of functional grading widens the overall pore and strut size distribution in the implant. Here, larger pore sizes are more commonplace, with the highest frequency between 440-450  $\mu$ m although the median lies between 350-360  $\mu$ m. Due to the relative size of the implants, the functional grading from 600  $\mu$ m to 300  $\mu$ m occurs over a short radius of 3 mm in the scaffold. As a result, only the outermost surface of the scaffold is anticipated to have pores of 600  $\mu$ m diameter before shrinking with radius and this is the portion that is most prone to edge effects during image processing. The titanium strut diameter has a slight shift towards smaller values in the FG600 scaffold, with a mode between 350-360  $\mu$ m. The mismatch between pore size and strut size distributions in the FG600 implant can be attributed to the overall scaffold design. Since functional

grading of the scaffold is with respect to the entire unit cell, it is possible to tune topology without one-to-one inverse proportionality in the strut-pore relationship.

#### **Bone Apposition**

Bone apposition occurred within the pores and surrounding the exterior of both scaffolds at 4 and 12 weeks in the tibia, as demonstrated in the micro-CT reconstructions in Figure 4. The BV/TV for the G300 implants at 4 and 12 wk was measured at  $0.68 \pm 0.10$  and  $0.74 \pm 0.04$ , respectively. For the FG600 implants, BV/TV was measured at  $0.58 \pm 0.12$  after 4 weeks and  $0.47 \pm 0.04$  after 12 weeks. As illustrated in Figure 5, a significant difference (p < 0.05) was found between the two types of scaffolds after retrieval, with the functionally-graded scaffold (FG600) containing a lower bone volume fraction than the scaffold with uniformly-sized pores (G300).

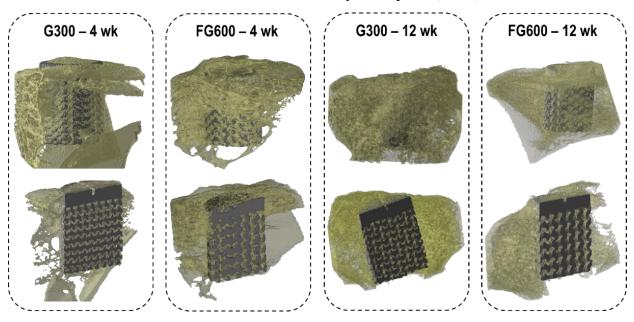
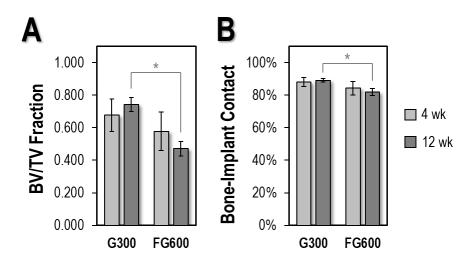


Figure 4: 3D Micro-CT reconstructions at 4 wk and 12 wk. Formation of bone inside the tibial defect area has occurred after four weeks and twelve weeks, resulting in implant fixation. The porous region of the implants is situated within the trabecular fraction of the epiphysis in the leporine tibia, while the full-density titanium in the crown lies in the cortex. Longitudinal crosssections for all implants show evidence of bone apposition at both four weeks and twelve weeks.

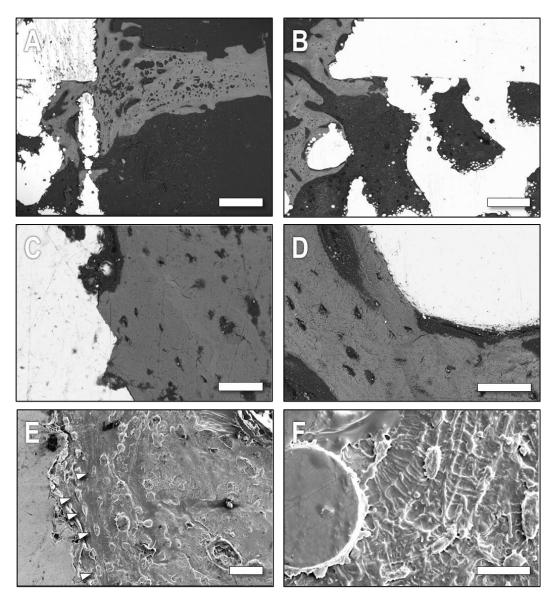
The measured BIC values for the G300 implants at the 4-week time point were  $87.9\% \pm 2.7\%$ , with a similar value after 12 weeks ( $89.1\% \pm 1.1\%$ ). Ranges in the FG600 implants were approximately the same amount, with  $84.2\% \pm 4.1\%$  BIC at four weeks and  $82.0\% \pm 2.2\%$  at twelve weeks. The G300 implant had significantly greater BIC at the twelve-week endpoint compared to the FG600 implant (p < 0.05). BIC measurements in these porous scaffolds appear greater than what has been reported for pore sizes of 800 and 1200 µm after 3 and 8 weeks in leporine femora using scanning electron microscopy (SEM) [41], but it is also important to note that differences between the studies could also be associated with differences in resolution and measurements by 2D SEM and 3D micro-CT. Micro-CT of porous titanium with a pore size range of 500-700 µm placed into ovine femora yield BIC measurements of approximately 60% at 26 weeks [42]. Imaging artifacts can occur at the implant interface due to attenuation from the titanium [43]; using a threshold of 25 µm from the implant surface for BIC assessment may help

reduce noise in these interfacial calculations, but the number of transitions from bone to implant along the path of a single X-ray is still expected to be greater in implants with more pores in the cross-section. Correlation to histological observation is important to confirm trends observed through micro-CT at the bone-implant interface.



*Figure 5: Histomorphometry of G300 and FG600 scaffolds at 4 wk and 12 wk.* (A) Bone volume fractions for each scaffold. The uniform 300 μm pore size retains a greater bone volume fraction at 12 wk than the implant with functionally-graded pore size. (B) Percentage of bone-implant contact for each scaffold. BIC is greater at 12 wk in the implant with a uniform 300 μm pore size.

Backscatter electron imaging in the SEM was also performed on cross-sections of the implant to assess the degree to which bone interacts with both types of implant. Based on a perspective from a lower magnification (Figure 6A-B), bone formation is most apparent at the crown of the implant and among the outermost implant struts. Examination by SEM into the interior of the implants suggests an overestimation of BIC and BV/TV measurements in the micro-CT due to beam hardening, but close bonding between bone and implant is still visible towards exterior scaffold sites at both 4 and 12 weeks (Figure 6C-D). Resin cast etching reveals underlying osteocytes and cell processes in the newly formed peri-implant bone (Figure 6E-F). Roughly 20 µm from the interface of a FG600 implant, the osteocytes are co-aligned with their major axis parallel to the titanium surface. An intervening layer of mineralized matrix separates the osteocytes from the titanium. As secretion of extracellular matrix from osteoblasts is a polar phenomenon, it is likely that these osteocytes were once adherent to the outermost surface of the implant and deposited osteoid as a template for early bone formation at the scaffold exterior. Osteocytes further from the implant have a rounded appearance, and potentially a higher surface area to volume ratio. Among the near-implant osteocytes (Figure 6F), cell processes appear majorly oriented into circumferential arrays with connecting branches oriented tangentially.



**Figure 6: Scanning electron microscopy of the bone-implant interface.** Bone formation at the exterior of (A) G300 and (B) FG600 scaffolds after 12 wk of implantation. Higher magnification view showing close bone-implant contact after both (C) 4 wk in a G300 scaffold and (D) 12 wk in a FG600 scaffold. (E-F) Following resin cast etching, osteocytes at the interface of a G300 implant after 12 wk have an oblong morphology (arrowheads) but become rounded with increasing distance. Propagation of the lacunocanalicular network appears in both radial and tangential patterns around the near-implant osteocytes. Scale bars: (A-B) 500 μm; (C-E) 50 μm; (E) 20 μm.

### Histology of Scaffolds in Leporine Tibiae

#### H&E Staining

Representative histological sections detailing interior and exterior sites of FG600 and G300 implants retrieved at 4 wk are shown in Figure 7. Additional H&E sections can be found in Figure S2 and S3.

At the outermost layer of the FG600 scaffold (Fig. 7B), there is evidence of an inflammatory response occurring in close proximity to the apex of the titanium scaffold. The inflammatory tissue that has formed varies widely in its composition across distances of 500 µm or less. In the inset shown in Figure 7C, dense clusters of dark-coloured basophilic cells or white blood cells tend to aggregate around dispersed lipids in the tissue. Due to their lack of eosinophilic cytoplasm in most cases and large nuclear fraction, these cells are consistent with lymphocytes [44]. At the FG600 apex, the white blood cells (black/purple) and erythrocyte-rich microvasculature (red) both infiltrate the space between lipids (white) in the region. This region has direct line-of-sight access to the scaffold exterior, with no titanium struts obfuscating osteoblasts or other biological response. In the first interior layer of pores (Figure 7D), there is a much lower density of white blood cells present in the inflammatory tissue, with similar volumes of red blood cells in the titanium-bound microcapillaries and a comparable dispersion of lipids near the titanium surface. The immune cells here appear to have a higher cytoplasmic fraction than in the high-density region and are more consistent with granulocytes [44]. Figure 7E shows a neighbouring region, with a finer capillary structure in the tissue and a slightly higher granulocyte density compared to what is seen in Fig. 7D. With respect to the apposition of bone tissue at the implant surface, nearby regions have an 'interlocking' effect where new bone has formed to fully encapsulate an exterior scaffold strut (Figure 7F). Osteocyte lacunae are visible within the bone matrix as close as 20 µm from the implant surface, with an approximate concentric alignment around the contours of the strut surface. The extent of bone regeneration at this site and maturity of the tissue seems to indicate that bone at exterior sites is further along in the modelling cascade than bone nucleating at interior sites. This distinction is often made in porous implant materials, where quantitative histomorphometry can be subcategorized into interior and exterior moieties depending on whether near-surface pores are sampled [42].

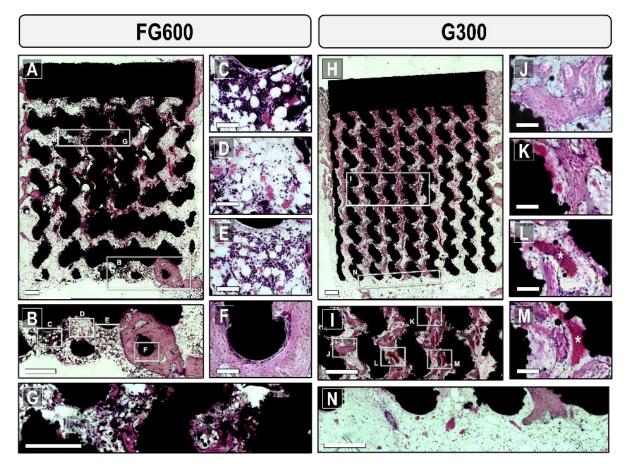


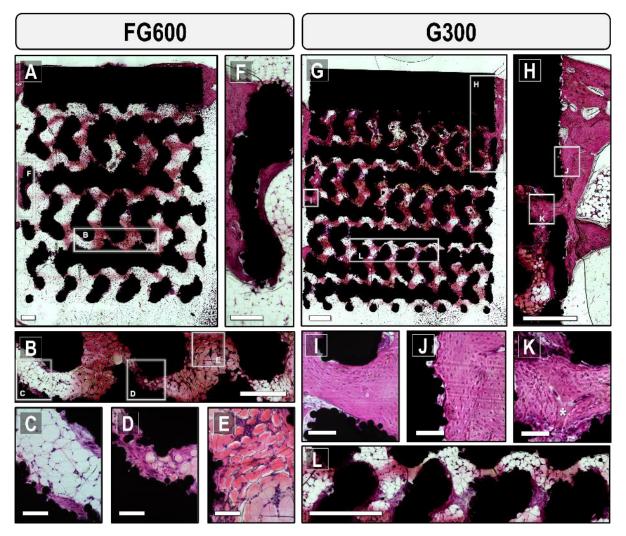
Figure 7: Histology of interior and exterior implant sites after four weeks for an FG600 (A-G) and G300 (H-N) implant. (A) Hallmarks of bone formation throughout the FG600 scaffold with H&E staining after four weeks of implantation. (B) Inflammatory interactions occur at the FG600 exterior with a trabecular and marrow-like appearance around the initial clot. including the formation of: (C) Dark-appearing cells, likely lymphocytes, apparent among clusters of adipocytes and erythrocytes; (D) Erythrocyte-rich regions in the granulation tissue with fewer white blood cells present; (E) Inflammatory tissue without formation of a mineralized matrix at the implant interface and an intermediate fraction of white blood cells; (F) More extensive bone regeneration to create intimate bone-implant contact at the scaffold exterior. (G) Formation of bone matrix along with inflammatory tissue occurs within the FG600 interior. (H) Patterns in early osseointegration of the G300 implant. (I) Thin regions of appositional bone tend to span the implant interior with less inflammation than in the FG600 implants. (J) Bridging of the scaffold struts occurs with the formation of new trabecular bone. Bone appears to integrate closely at the strut surface and partially contour around titanium particles. (K) Competition occurs at the strut surface between microvascular entities and osteocyte-rich bone. The orientation of new bone seems to be mostly in parallel with the pore wall. (L-M) Vascular structures, denoted by asterisks, are able to permeate deep into the scaffold interior with bone forming around the vasculature. Microvasculature propagates through both the void volume in the scaffold and along the titanium surface. (N) G300 exterior with high content of adipocytes, a network of microvasculature, and low relative counts of white blood cells. Scale bars (A-B, G-I, N) 500 μm; (C-F, J-M) 100 μm.

While the *in vitro* results at early timepoints showed a biological response that was predominantly occurring on the exterior of the scaffolds or within the first layer of pores, the *in vivo* results showed formation of bone in the scaffold interior after only four weeks of implantation. Figure 7G and 7I illustrate bone regeneration at interior sites within the scaffolds at this time point, where lower-magnification images show a disperse network of thin bone that populated the scaffold interior in the G300 implant (Figure 7H-I) and residual inflammatory tissue mixed with bone

matrix in the FG600 implant (Figure 7I). The apical portion of the G300 implant (Figure 7N) after four weeks had a characteristic appearance of bone marrow and is mostly filled with adipocytes and microcapillaries rather than white blood cells. At the crown of the G300 and FG600 implants, osteoconduction from cortical regrowth was beginning to occur, providing inward growth into the pores nearest the cortex.

Looking at pores at increasing radial depth into the G300 scaffold (Figure 7I) tends to illustrate a lack of depth-dependency for bone growth, with pores at the midpoint of the G300 scaffold containing similar amounts of bone to shallow pores near the implant surface in this instance. The location of the scaffold in the medullary canal also appeared to affect bone tissue apposition, as osteogenesis appeared more dominant in the leftmost and central regions of Figure 7G for the G300 implant. However, at sites within the scaffold interior, appositional bone tissue appeared to bridge adjacent scaffold struts at the four-week endpoint with an appearance that is consistent with trabecular bone (Figure 7J-K). Osteocytes in these regions of new bone formation appeared mostly disorganized, with high density and no clear direction of co-alignment as is typically seen in mature bone tissue [45], e.g., the apical regrowth in the FG600 implant. Tissue regeneration in the scaffold was not always unidirectional with respect to the scaffold struts, where bone formation occurred in a predominantly transverse direction (as in Figure 7J), or with longitudinal components (Figure 7K). There were also fewer lipids and granulocytes in and around the G300 scaffold compared to the FG600 implant in Figure 7, suggesting that bone repair and the fracture healing cascade may be slightly more advanced in the G300 implant compared to the FG600 implant.

In terms of biological interaction, a fine network of vasculature permeated throughout the entirety of the implant to aid in both tissue formation and homeostasis. These microcapillaries contained an abundance of erythrocytes, denoted by asterisks in Figure 7L and 7M, and appear to be sectioned obliquely based on their aspect ratio. The ability of this provisional capillary network to maintain carrying capacity is important for osseointegration as it mediates the delivery of oxygen, growth factors, and the removal of waste by-products at these interior scaffold sites during bone modelling and remodelling [46]. With respect to osseointegration, neovascularization has been documented to occur on the surface of solid titanium implants long before the formation of new bone tissue [47] with local expression of factors such as Runt-related transcription factor 2 [48] that control the pre-osteoblast to osteoblast transition. Here, we note that this newly formed vasculature was able to infiltrate a porous metallic scaffold in leporine tibial defects in a similar manner to what has been seen for murine cranial defect interfaces with solid titanium [47]. The newly formed vasculature has a tendency to interface and propagate along the porous titanium (as in Figure 7K and 7M) but also spans scaffold struts in a freeform manner (as in Figure 7L). At early timepoints, the capillary network is observed to periodically interact with the titanium as a self-supporting mechanism during trabecular modelling.



**Figure 8: Histology of interior and exterior implant sites after twelve weeks.** (A) Bone formation throughout the FG600 scaffold with H&E staining after twelve weeks of implantation. Appositional bone has coarsened compared to the four-week endpoint and fully occupies the pore diameter in some instances. (B) Inset in the FG600 interior shows high lipid content, with: (C) Circular adipocytes in the centre of the pore, flanked by regions of bone matrix along the titanium; (D) Predominantly bone matrix where pores narrow; (E) Elliptically-shaped adipocytes in an eosinophilic matrix, with marginally higher white blood cell clustering compared to other myeloid regions. (F) Bone integration at the scaffold exterior, with bone fully encapsulating an outer strut. (G) Bone formation throughout the G300 scaffold with H&E staining after twelve weeks of implantation, with a seemingly higher bone area fraction than the FG600. (H) Inset at the crown of the implant shows cortical osteoconduction beyond to the first layer of pores within the scaffold. (I) Newly formed tissue in the trabecular region enters the implant, with mature osteocytes that concentrically align with the upper scaffold strut. (J) The tissue formation front at the crown tends to only interact with a single tangential region on each sintered powder particle. (K) New bone tissue completely surrounds a branching microcapillary, denoted by an asterisk, where the capillary is roughly located at the midplane of the two scaffold struts. Scale bars (A-B, G-H, L) 500 μm; (F) 250 μm; (C-E, I-K) 100 μm.

Examination of the FG600 (Figure 8A-F) and G300 (Figure 8G-L) scaffold geometries after twelve weeks shows evidence of sustained osteogenesis between the four and twelve-week endpoints. The interior pores of scaffolds retrieved after 12 wk tended to have much higher adiposity than those retrieved at 4 wk, where the bulk of the tissue inside the scaffold was consistent with that of myeloid tissue (Figure 8B and 8L) with radially-oriented eosinophilic regions characteristic of the

bone matrix that bridge neighbouring struts in the gyroid topology. The consistent patterns in bone apposition within the scaffold interior mirrored what was seen in the micro-CT reconstructions, confirming that the unit cell topology can, at least in part, govern the directionality of nascent tissue in the scaffold interior. At 12 wk, adaptation of the tissue is noted to maintain this pattern and preserve the functional connection of bone and implant throughout the scaffold interior. It is possible that the increase in adipocyte-rich myeloid tissue within the scaffold (Fig. 8C-E) can be attributed to a shift in stem cell differentiation, where osteoblast progenitors can ostensibly commit to an adipogenic pathway [49,50]. As bone marrow is formed inside the scaffold interior, hematopoiesis can occur to sustain red and white blood cell production. Figure S4 shows an interior pore channel, with a myeloid structure, including the presence of a suspected megakaryocyte along with white blood cells, red blood cells, connective tissue, and adipocytes – indicating that residual platelet production and clotting [51] was still occurring in the scaffold after 12 wk. Comparing the two types of scaffolds, bone matrix appeared more densely distributed throughout the interior of the G300 implant due to the smaller pore size helping to facilitate bone formation that spanned multiple scaffold struts.

There was generally less inflammatory tissue present near the implant exterior at twelve weeks for both scaffold types, although some persisted near the apex of the implant and there were fewer white blood cells present. Similar to trabecular integration at four weeks, there were regions (Figure 8F) where mature bone wrapped around the entirety of the outermost scaffold struts. At twelve weeks, newly formed bone in the trabecular and cortical regions tended to be coarser. Bone within the trabecular region was able to branch into the porous interior, spanning the entire diameter of the pore in some instances. Osteocytes within these inwardly-directed trabeculae had a mature phenotype according to their shape [52], with a flat lacunar morphology (Figure 8I). These osteocytes tended to align more closely with the upper scaffold strut in this pore, perhaps due to the higher number of sintered powder particles and therefore rougher nature of the lower strut. Tissue integration in this trabecular region followed the contours of surface-bound titanium particles but this was not ubiquitous on the implant surface. Cortical regeneration along the implant crown showed that the bone formation front can instead form tangential to the surface particles, with no tissue penetrating the crevices between powder particles (Figure 8J). Osteocyte lacunae in this region of the crown were also consistent with a mature morphology, with their flatter edge parallel to the implant surface. In some instances, at four and twelve weeks, a clear path of osteoconduction can be observed where bone developed at the existing cortex and grew along the crown of the implant to merge with other regions of newly formed bone. This bone then breached the porous layers adjacent to the cortex to enter the scaffold interior – a phenomenon observed in both the FG600 and the G300 scaffolds.

After twelve weeks, microvascular capillaries no longer appeared to be interfacing with the titanium scaffold. Capillaries instead appeared with typical appearance in mature bone tissue, propagating through continuous vascular canals in the mineralized bone tissue, with one such example shown in Figure 8K. The vascular structure seemed to follow the gyroid scaffold topology, bifurcating at a site where the pore network branches. The vascular entities also appeared to be roughly centred at the midplane between neighbouring scaffold struts. Preservation of these capillaries throughout the scaffold is essential to allow for survival of bone at the innermost

scaffold locations by acting as a transport system for biological macromolecules and regulating tissue metabolism.

It may indeed be worthwhile in the future to assess the spatial distribution of factors such as Runtrelated transcription factor 2 (RUNX2) or peroxisome proliferator-activated receptor- $\gamma$  (PPAR $\gamma$ ) [53] to validate the decline in osteogenic commitment inside the scaffolds and corresponding increase in adipocyte formation. This would provide information about the differentiation of mesenchymal stem cells over time inside the pore network of a scaffold and provide a basis for developing temporally-relevant physical and chemical surface modification strategies.

#### Fluorochrome Labels

To compare sites of calcification throughout the interior of the implant, fluorochrome signals were compared using calcein injection at two weeks and alizarin red at six weeks post-implantation. By comparing fluorochrome-labelled regions in these implants with H&E-stained sections (sampled at four weeks and twelve weeks), it is possible to localize regions of matrix mineralization within the tissue. For all implants in Figure 9, a fluorescent signal from calcein was evident within the scaffold interior after only two weeks, indicating that a framework for mineral transport into the scaffold was present in a very early period following implantation. The co-localization of calcein signal at two weeks and tissue present at four weeks (Figure 9E-H) indicates that similar quantities of mineralized tissue were present in the scaffold interior at early timepoints, despite the more extensive network of bone matrix in the G300 implant. The same trends persisted for the implants retrieved at twelve weeks, where the bulk of the fluorescent signal was co-localized with stained regions in the H&E sections. These early mineral loci did not appear ubiquitously through the matrix material and did not yet span the full pore diameter in regions where they appeared, instead nucleating as smaller clusters.

In both the H&E and fluorochrome images, periodicity was evident with respect to where new tissue formed. At similar radii through the implant, there were consistent patterns in appositional bone formation inside the implant. Bone that spans two neighbouring struts of titanium had a consistent and somewhat unidirectional appearance in all pores on the same azimuth (i.e. along the same 'rows' of pores in Figures 8 and 9). For the FG600 implants, this appositional bone had a tendency to orient itself in the radial direction of the implant, while the G300 implants tended to have a more oblique direction in the tissue. Pobloth et al. described a similar ability for bone to grow through axial, perpendicular, and oblique pore directions along the interior struts of titanium scaffolds, using collagen directionality to assess this form of tissue patterning [54]. Although the unidirectionality may be an artifact of sectioning orientation, commonalities in appositional bone orientation in the fluorochrome and H&E deserve further investigation. Where unit cell topology was shown to have only a minor role for *in vitro* scaffold assessment, the *in vivo* results suggest that topology can indeed play a larger role with respect to the directionality of osteogenesis in the scaffold interior.

The evolution of mineralization from two weeks to six weeks was more evident in the FG600 implants, where calcified regions appeared to propagate outward from the original loci present at two weeks (Figure 9C). This was consistent with the use of fluorochrome labelling in other studies, where early endpoints tended to have smaller fluorochrome-labelled areas near the interface of a

titanium implant [55]. Alizarin red fluorescence showed that mineralized tissue can span across entire pores, effectively linking two titanium struts. The G300 group of implants showed a similar trend where existing mineralized tissue coarsens, but there were also regions where new mineral apposition seemed to occur at six weeks, connecting scaffold struts with no prior mineral adjacent to them.

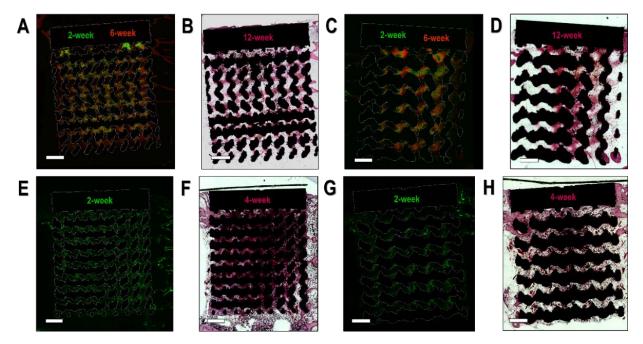


Figure 9: Fluorochrome labelling of calcification loci. (A-D) Fluorochrome images of calcein injected two weeks postimplantation, alizarin red injected six weeks post-implantation, and correlative H&E-stained section after twelve weeks in the (A-B) G300 and (C-D) FG600 implants. Calcified regions expand between the two-week and six-week endpoints, correlating closely with tissue in the H&E section at twelve weeks. (E-H) Calcein fluorochrome and H&E stain showing correlative bone apposition at two and four weeks in (E-F) G300 and (G-H) FG600 implants. Fluorescent signals are bright throughout the implant interior where bone matrix is present, indicating that mineral transport is consistently occurring within the scaffold interior within the first two weeks and corresponds with regions of connective tissue in the H&E micrographs. Scale bars 1 mm.

## Conclusions

Additive manufacturing of titanium enables the production of complex scaffolds with an interconnected pore geometry to influence early osseointegration and short-term implant stability. Ti6Al4V gyroid structures displayed *in vitro* cytocompatibility with respect to Saos-2 metabolism. *In vivo* assessment of the uniform and functionally-graded gyroid structures in leporine tibiae both show potential for improving early implant outcomes by encouraging osteogenesis to occur on the scaffold exterior and interior. In general, newly formed bone spans internal scaffold struts with a common directionality relative to neighbouring regions of bone apposition, governed at least in part by the strut orientation of the scaffold itself. BV/TV and BIC measurements from micro-CT reconstructions demonstrated that values were greater for G300 implants compared to FG600 implants at 12 wk, suggesting that the G300 implants have an increased ability to facilitate bone formation. A progression in the osteogenic cascade for implants spanning the medullary canal took place with residual inflammatory response, neovessel development along titanium struts, and some

early formation of bone occurring inside and outside of scaffold pores after four weeks. By twelve weeks of implantation, bone formed in a somewhat unidirectional manner to span scaffold struts and infiltration of bone marrow occurred into the scaffold interior. Overall, the additively manufactured scaffolds both provide additional surface area for bone growth to occur inside the pores, a means to maintain the tissue through the vascular network, and a promising means for encouraging osseointegration at the implant interface.

## Acknowledgements

Work was performed at the McMaster Center for Advanced Light Microscopy, and McMaster's Biointerfaces Institute. The authors would like to acknowledge funding from the Foshan Science and Technology Innovation Project (No. 2018IT100212), Natural Sciences and Engineering Research Council of Canada (RGPIN-2020-05722), and Canada Research Chairs Program. Funding support is also acknowledged from the Research Internship Abroad (BEPE) grant program #2022/04536-1 from the São Paulo Research Foundation (FAPESP). The authors would also like to acknowledge the scientific efforts of Bryan E.J. Lee and Chiara Micheletti toward the publication of this work. The graphical abstract was created using BioRender.com.

## References

1. Branemark PI. Osseointegration and its experimental background. J Prosthet Dent. 1983;50(3):399–410.

2. Albrektsson T, Albrektsson B. Osseointegration of bone implants: A review of an alternative mode of fixation. Acta Orthop Scand. 1987;58(5):567–77.

3. Gómez S, Vlad MD, López J, Fernández E. Design and properties of 3D scaffolds for bone tissue engineering. Acta Biomater. 2016;42:341–50.

4. Dias MR, Guedes JM, Flanagan CL, Hollister SJ, Fernandes PR. Optimization of scaffold design for bone tissue engineering: A computational and experimental study. Med Eng Phys. 2014;36(4):448–57.

5. Scaglione S, Giannoni P, Bianchini P, Sandri M, Marotta R, Firpo G, Valbusa U, Tampieri A, Diaspro A, Bianco P, Quarto R. Order versus Disorder: in vivo bone formation within osteoconductive scaffolds. Sci Rep-uk. 2012;2(1):274.

6. Deering J, Dowling KI, DiCecco LA, McLean GD, Yu B, Grandfield K. Selective Voronoi tessellation as a method to design anisotropic and biomimetic implants. J Mech Behav Biomed. 2021;116:104361.

7. Arabnejad S, Johnston RB, Pura JA, Singh B, Tanzer M, Pasini D. High-strength porous biomaterials for bone replacement: A strategy to assess the interplay between cell morphology, mechanical properties, bone ingrowth and manufacturing constraints. Acta Biomater. 2016;30:345–56.

8. Melancon D, Bagheri ZS, Johnston RB, Liu L, Tanzer M, Pasini D. Mechanical characterization of structurally porous biomaterials built via additive manufacturing: experiments, predictive models, and design maps for load-bearing bone replacement implants. Acta Biomater. 2017;63:350–68.

9. Wang Z, Wang C, Li C, Qin Y, Zhong L, Chen B, Li Z, Liu H, Chang F, Wang J. Analysis of factors influencing bone ingrowth into three-dimensional printed porous metal scaffolds: A review. J Alloy Compd. 2017;717:271–85.

10. Wang X, Xu S, Zhou S, Xu W, Leary M, Choong P, Qian M, Brandt M, Xie YM. Topological design and additive manufacturing of porous metals for bone scaffolds and orthopaedic implants: A review. Biomaterials. 2016;83:127–41.

11. Deering J, Grandfield K. Current interpretations on the in vivo response of bone to additively manufactured metallic porous scaffolds: A review. Biomaterials Biosyst. 2021;2:100013.

12. Van der Stok J, Van der Jagt OP, Yavari SA, de Haas MFP, Waarsing JH, Jahr H, Van Lieshout EMM, Patka P, Verhaar JAN, Zadpoor AA, Weinans H. Selective laser melting-

produced porous titanium scaffolds regenerate bone in critical size cortical bone defects. J Orthopaed Res. 2013;31(5):792–9.

13. Huiskes R, Weinans H, Rietbergen B van. The relationship between stress shielding and bone resorption around total hip stems and the effects of flexible materials. Clin Orthop Relat R. 1992;274(NA;):124–34.

14. Mahmoud D, Elbestawi MA. Lattice structures and functionally graded materials applications in additive manufacturing of orthopedic implants: A review. J Manuf Mater Process. 2017;1(2):13.

15. Al-Ketan O, Rowshan R, Al-Rub RKA. Topology-mechanical property relationship of 3D printed strut, skeletal, and sheet based periodic metallic cellular materials. Addit Manuf. 2018;19(Acta Biomater. 4 2008):167–83.

16. Abueidda DW, Elhebeary M, Shiang CS (Andrew), Pang S, Al-Rub RKA, Jasiuk IM. Mechanical properties of 3D printed polymeric Gyroid cellular structures: Experimental and finite element study. Mater Design. 2019;165:107597.

17. Kapfer SC, Hyde ST, Mecke K, Arns CH, Schröder-Turk GE. Minimal surface scaffold designs for tissue engineering. Biomaterials. 2011;32(29):6875–82.

18. Zhang L, Feih S, Daynes S, Chang S, Wang MY, Wei J, Lu WF. Energy absorption characteristics of metallic triply periodic minimal surface sheet structures under compressive loading. Addit Manuf. 2018;23:505–15.

19. du Plessis A, Razavi SMJ, Benedetti M, Murchio S, Leary M, Watson M, Bhate D, Berto F. Properties and applications of additively manufactured metallic cellular materials: a review. Prog Mater Sci. 2021;125:100918.

20. Yu S, Sun J, Bai J. Investigation of functionally graded TPMS structures fabricated by additive manufacturing. Mater Design. 2019;182:108021.

21. Zhou H, Zhao M, Ma Z, Zhang DZ, Fu G. Sheet and network based functionally graded lattice structures manufactured by selective laser melting: Design, mechanical properties, and simulation. Int J Mech Sci. 2020;175:105480.

22. Bai L, Gong C, Chen X, Sun Y, Xin L, Pu H, Peng Y, Luo J. Mechanical properties and energy absorption capabilities of functionally graded lattice structures: Experiments and simulations. Int J Mech Sci. 2020;182:105735.

23. Zhang XY, Yan XC, Fang G, Liu M. Biomechanical influence of structural variation strategies on functionally graded scaffolds constructed with triply periodic minimal surface. Addit Manuf. 2020;32:101015.

24. Zhang XY, Fang G, Xing LL, Liu W, Zhou J. Effect of porosity variation strategy on the performance of functionally graded Ti-6Al-4V scaffolds for bone tissue engineering. Mater Design. 2018;157:523–38.

25. Liu F, Mao Z, Zhang P, Zhang DZ, Jiang J, Ma Z. Functionally graded porous scaffolds in multiple patterns: New design method, physical and mechanical properties. Mater Design. 2018;160(Biomaterials 23 2002):849–60.

26. Yuan L, Ding S, Wen C. Additive manufacturing technology for porous metal implant applications and triple minimal surface structures: A review. Bioact Mater. 2019;4(1):56–70.

27. Coelho PG, Granjeiro JM, Romanos GE, Suzuki M, Silva NRF, Cardaropoli G, Thompson VP, Lemons JE. Basic research methods and current trends of dental implant surfaces. J Biomed Mater Res Part B Appl Biomaterials. 2009;88B(2):579–96.

28. Dondossola E, Friedl P. Host responses to implants revealed by intravital microscopy. Nat Rev Mater. 2022;7(1):6–22.

29. Mahmoud D, Al-Rubaie KS, Elbestawi MA. The influence of selective laser melting defects on the fatigue properties of Ti6Al4V porosity graded gyroids for bone implants. Int J Mech Sci. 2021;193:106180.

30. D'Elia A, Deering J, Clifford A, Lee BEJ, Grandfield K, Zhitomirsky I. Electrophoretic deposition of polymethylmethacrylate and composites for biomedical applications. Colloids Surfaces B Biointerfaces. 2019;188:110763.

31. Reznikov N, Boughton OR, Ghouse S, Weston AE, Collinson L, Blunn GW, Jeffers J, Cobb JP, Stevens MM. Individual response variations in scaffold-guided bone regeneration are determined by independent strain- and injury-induced mechanisms. Biomaterials. 2018;194(J. Bone Joint Surg. Am. 89 Suppl 3 2007):183–94.

32. Rodan SB, Imai Y, Thiede MA, Wesolowski G, Thompson D, Bar-Shavit Z, Shull S, Mann K, Rodan GA. Characterization of a human osteosarcoma cell line (Saos-2) with osteoblastic properties. Cancer Res. 1987;47(18):4961–6.

33. Thenard T, Catapano A, Allena R, May ME, Saintier N, Mesnard M. Topography and wettability characterization of surfaces manufactured by SLM and treated by chemical etching. Mech Adv Mater Struc. 2020;29(12):1–18.

34. Xu JY, Chen XS, Zhang CY, Liu Y, Wang J, Deng FL. Improved bioactivity of selective laser melting titanium: Surface modification with micro-/nano-textured hierarchical topography and bone regeneration performance evaluation. Mater Sci Eng C. 2016;68:229–40.

35. Rønold HJ, Lyngstadaas SP, Ellingsen JE. Analysing the optimal value for titanium implant roughness in bone attachment using a tensile test. Biomaterials. 2003;24(25):4559–64.

36. Gotfredsen K, Berglundh T, Lindhe J. Anchorage of titanium implants with different surface characteristics: An experimental study in rabbits. Clin Implant Dent R. 2000;2(3):120–8.

37. Gockel J, Sheridan L, Koerper B, Whip B. The influence of additive manufacturing processing parameters on surface roughness and fatigue life. Int J Fatigue. 2019;124:380–8.

38. Deering J, Presas A, Lee BEJ, Valentin D, Yu B, Heiss C, Grandfield K, Bosbach WA. Response of Saos-2 osteoblast-like cells to kilohertz-resonance excitation in porous metallic scaffolds. J Mech Behav Biomed. 2020;106:103726.

39. Fang J, Zhang Y, Yan S, Liu Z, He S, Cui L, Yin J. Poly(l-glutamic acid)/chitosan polyelectrolyte complex porous microspheres as cell microcarriers for cartilage regeneration. Acta Biomater. 2014;10(1):276–88.

40. Yan S, Xia P, Xu S, Zhang K, Li G, Cui L, Yin J. Nanocomposite porous microcarriers based on strontium-substituted HA-g-Poly( $\gamma$ -benzyl-l-glutamate) for bone tissue engineering. ACS Appl Mater Inter. 2018;10(19):16270–81.

41. Lopez-Heredia MA, Goyenvalle E, Aguado E, Pilet P, Leroux C, Dorget M, Weiss P, Layrolle P. Bone growth in rapid prototyped porous titanium implants. J Biomed Mater Res A. 2008;85A(3):664–73.

42. Palmquist A, Snis A, Emanuelsson L, Browne M, Thomsen P. Long-term biocompatibility and osseointegration of electron beam melted, free-form–fabricated solid and porous titanium alloy: Experimental studies in sheep. J Biomater Appl. 2013;27(8):1003–16.

43. Zhang X, Wang J, Xing L. Metal artifact reduction in x-ray computed tomography (CT) by constrained optimization. Med Phys. 2011;38(2):701–11.

44. Bolliger AP. Cytologic evaluation of bone marrow in rats: indications, methods, and normal morphology. Vet Clin Path. 2004;33(2):58–67.

45. Shah FA, Snis A, Matic A, Thomsen P, Palmquist A. 3D printed Ti6Al4V implant surface promotes bone maturation and retains a higher density of less aged osteocytes at the bone-implant interface. Acta Biomater. 2016;30(Biomaterials 27 2006):357–67.

46. Filipowska J, Tomaszewski KA, Niedźwiedzki Ł, Walocha JA, Niedźwiedzki T. The role of vasculature in bone development, regeneration and proper systemic functioning. Angiogenesis. 2017;20(3):291–302.

47. Khosravi N, Maeda A, DaCosta RS, Davies JE. Nanosurfaces modulate the mechanism of peri-implant endosseous healing by regulating neovascular morphogenesis. Commun Biology. 2018;1(1).

48. Redenski I, Guo S, Machour M, Szklanny A, Landau S, Kaplan B, Lock RI, Gabet Y, Egozi D, Vunjak-Novakovic G, Levenberg S. Engineered vascularized flaps, composed of polymeric soft tissue and live bone, repair complex tibial defects. Adv Funct Mater. 2021;31(44):2008687.

49. Augello A, Bari CD. The regulation of differentiation in mesenchymal stem cells. Hum Gene Ther. 2010;21(10):1226–38.

50. Liu TM, Martina M, Hutmacher DW, Hui JHP, Lee EH, Lim B. Identification of common pathways mediating differentiation of bone marrow- and adipose tissue-derived human mesenchymal stem cells into three mesenchymal lineages. Stem Cells. 2007;25(3):750–60.

51. Rabellino EM, Levene RB, Leung LL, Nachman RL. Human megakaryocytes. II. Expression of platelet proteins in early marrow megakaryocytes. J Exp Medicine. 1981;154(1):88–100.

52. Shah FA, Thomsen P, Palmquist A. A review of the impact of implant biomaterials on osteocytes. J Dent Res. 2018;97(9):977–86.

53. James AW. Review of signaling pathways governing MSC osteogenic and adipogenic differentiation. Sci. 2013;2013:684736.

54. Pobloth AM, Checa S, Razi H, Petersen A, Weaver JC, Schmidt-Bleek K, Windolf M, Tatai AÁ, Roth CP, Schaser KD, Duda GN, Schwabe P. Mechanobiologically optimized 3D titaniummesh scaffolds enhance bone regeneration in critical segmental defects in sheep. Sci Transl Med. 2018;10(423).

55. Koo S, König B, Allegrini S, Yoshimoto M, Carbonari MJ, Mitri-Luiz FF. Titanium implant osseointegration with calcium pyrophosphate in rabbits. J Biomed Mater Res Part B Appl Biomaterials. 2006;76B(2):373–80.