# 1 Hydrogels with stiffness-degradation spatial patterns control

# 2 anisotropic 3D cell response

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### 15 Abstract

In nature, tissues are patterned, but most biomaterials used in human applications are not. Patterned 16 17 biomaterials offer the opportunity to mimic spatially segregating biophysical and biochemical properties found in nature. Engineering such properties allows to study cell-matrix interactions in 18 19 anisotropic matrices in great detail. Here, we developed alginate-based hydrogels with patterns in 20 stiffness and degradation, composed of distinct areas of soft non-degradable (Soft-NoDeg) and stiff 21 degradable (Stiff-Deg) material properties. The hydrogels exhibit emerging patterns in stiffness and 22 degradability over time, taking advantage of dual Diels-Alder covalent crosslinking and UV-23 mediated peptide crosslinking. The materials were mechanically characterized using rheology for 24 single-phase and surface micro-indentation for patterned materials. 3D encapsulated mouse 25 embryonic fibroblasts (MEFs) allowed to characterize the anisotropic cell-matrix interaction in terms 26 of cell morphology by employing a novel image-based quantification tool. Live/dead staining 27 showed no differences in cell viability but distinct patterns in proliferation, with higher cell number 28 in Stiff-Deg materials at day 14. Patterns of projected cell area became visible already at day 1, with 29 larger values in Soft-NoDeg materials. This was inverted at day 14, when larger projected cell areas 30 were identified in Stiff-Deg. This shift was accompanied by a significant decrease in cell circularity 31 in Stiff-Deg. The control of anisotropic cell morphology by the material patterns was also confirmed 32 by a significant increase in filopodia number and length in Stiff-Deg materials. The novel image-33 based quantification tool was useful to spatially visualize and quantify the anisotropic cell response 34 in 3D hydrogels with stiffness-degradation spatial patterns. Our results show that patterning of 35 stiffness and degradability allows to control cell anisotropic response in 3D and can be quantified by 36 image-based strategies. This allows a deeper understanding of cell-matrix interactions in a 37 multicomponent material.

# 38 Keywords: biomaterials; stiffness; degradation; 3D cell-matrix interaction; anisotropic cell

39 response; cell morphology; image-based quantification tool

#### 40 1 Introduction

- 41 Patterns are naturally occurring in nature, macroscopically and microscopically. The constant
- 42 remodeling of the extracellular matrix (ECM) leads to emergent patterns of cells, ECM properties
- 43 and cell behavior (1)(2). Biomaterials like hydrogels are a useful tool to study cell-matrix interaction
- 44 as they can mimic various characteristics of the cell niche (3). Multiple approaches have been taken
- 45 to study cell response to specific ECM properties, for example: materials with different stiffness to
- 46 study focal adhesions (4) and mechanosensation (5), stress relaxing materials to mimic the
- 47 viscoelastic behavior of biological tissues (6), independent control of mechanical properties and
- 48 fibronectin presentation for stem cell engineering (7), modifications in the scaffold architecture and
- 49 pore distribution (8), or biomolecule presenting/releasing materials (9). Patterned materials will offer
- 50 the opportunity of imitating and guiding cell behavior with a closer relation to the natural
- 51 counterpart.
- 52 Alginate is natural, biocompatible and inert polymer. Its versatile structure allows modifications to
- 53 modulate key biophysical cues. Chemical modifications of the alginate structure, such as thiolation
- 54 (10), oxidation (11), amidation (12) and Diels-Alder addition (13)(14) can be the base to implement
- additional crosslinking, improve or control degradation behavior or enable a controlled drug release.
- 56 Alginate is capable to be crosslinked by various means such as ionic and covalent crosslinking (15).
- 57 That capability opens the possibility to mimic and control distinct ECM properties. Alginate can thus
- 58 be made such that a relatively broad range of mechanical properties can be covered or a dynamic
- 59 environment provided to cells (11)(16).
- 60 Multiple biophysical and biochemical factors contribute to the complexity of the ECM. The interplay
- 61 between these factors is a current topic of research. The mechanical properties of the ECM have been
- 62 examined in single-phase 3D hydrogels with different elastic modulus, showing that the stiffness has
- 63 an effect on cell phenotype (17)(18) and cell migration (19). The degradability of the material is
- 64 important to create dynamic 3D matrices and it can affect cell spreading, cell interactions (20) and
- morphology (21)(22). Fewer studies investigate the interaction of stiffness and degradation on cell
- 66 behavior in 3D encapsulated cells. Previous research showed that the simultaneous modulation of
- 67 stiffness and degradation can influence cell proliferation or differentiation (23) and thereby control
- 68 cell phenotypes (24).
- 69 The combination and spatial patterning of biophysical and biochemical cues can replicate complex
- 70 structures of a native ECM and allow structural properties to emerge. Previous research on
- 71 photopatterning showed the potential of tuning biophysical and biochemical cues in patterned
- 72 materials (25). To study the effect of stiffness and degradation on 3D cell behavior, we use the
- 73 combination of two different types of crosslinking. The first type of crosslinking is covalent Diels-
- Alder click chemistry, which offers an efficient and versatile reaction for hydrogel formation
- 75 (11)(13). The second type of crosslinking, UV-mediated thiol-ene peptide binding, offers tunable
- degradability by the matrix metalloprotease enzymes secreted by encapsulated cells (16). Despite the
- numerous research performed on single-phase materials, fewer investigations are looking at cell
- 78 response in multicomponent matrices such as patterned materials.
- 79 Dual crosslinked, patterned hydrogels previously described have shown an effect on cells attached to
- 80 2D substrates, such as in cell alignment (26), protein expression and differentiation (27)(26).
- 81 Previous research in 3D cell encapsulation showed that patterns in biochemical cues can influence
- 82 cell migration (28) and localized growth (29), whereas patterns in biophysical cues can influence cell
- 83 interactions (30). Research performed on patterning multiple mechanical or biochemical

- 84 characteristics has shown promising results on guiding cell behavior (31). Our research contributes
- 85 on evaluating the cell response in patterned hydrogels with spatially discrete patterns in degradation
- 86 and stiffness. Furthermore, the evaluation of the cell response in patterned materials has been limited
- to the independent evaluation of each phase; no method has been proposed to quantitatively assess
- 88 patterned cell response in a multicomponent matrix. To achieve this, an image-based analysis tool is
- 89 required.
- 90 Here we present an alginate-based hydrogels with anisotropic stiffness-degradation spatial patterns
- and compatible with 3D cell encapsulation. The hydrogels exhibit emerging patterns in stiffness and
- 92 degradability over time, taking advantage of dual covalent Diels-Alder click crosslinking and UV-
- 93 mediated peptide crosslinking. Further, we develop a novel quantitative, image-based analysis tool to
- 94 evaluate the emerging anisotropic cell behavior in 3D and over time. We characterize cell
- 95 morphology and proliferation in photopatterned materials and compare the results with equivalent
- single-phase materials. Such patterned materials allowing the emergence of 3D anisotropic cell
- 97 response, together with the image-based analysis method, are valuable tools to understand cell-matrix
   98 interactions in multicomponent materials.

### 99 2 Materials and Methods

### 100 2.1 Alginate modification

- 101 To form the click-crosslinking, norbornene and tetrazine must be added in the alginate backbone. The
- alginate used was low molecular weight, high guluronic acid sodium alginate (MW 75kDa Pronova
- 103 UP VLVG; NovaMatrix). The coupling of norbornene (N, TCI Chemicals, #N0907) and tetrazine (T,
- 104 conju-probe, #CP-6021) to the alginate molecule was performed as previously described (27).
- 105 Alginate modification with norbornene was performed with a theoretical degree of substitution
- 106  $(DS_{theo})$  of  $DS_{theo}$  200 for norbornene. Tetrazine modification was performed with a  $DS_{theo}$  50 for
- 107 tetrazine. To determine the reaction efficiency and the actual DS  $(DS_{actual})$  required to ensure
- appropriate norbornene to tetrazine (N:T) ratios for crosslinking, NMR measurements were
- 109 performed, using a 1.5% w/v alginate solution in deuterium oxide (64 scans; Agilent 400 MHz
- 110 Premium COMPACT equipped with Agilent OneNMR Probe) and analyzed using MestrNova
- 111 Software (14.6) (Supplementary Figure S1; Supplementary Table S1).

# 112 **2.2** Mouse Embryonic Fibroblast (MEF) cell culture

- 113 Mouse embryonic fibroblasts (SCRC-1040; ATCC) were cultured in Dulbecco's Modified Eagle's
- 114 Medium (Sigma, #D5546) supplemented with 3.5 g/l glucose (VWR, # 0188), 15% v/v fetal bovine
- serum (Biochrom, #S0615), and 1% penicillin/streptomycin (Gibco, #15140-122). Cells were
- maintained in a 5% CO<sub>2</sub> environment at 37°C and passaged every 3–5 days. For 3D encapsulation,
- 117 cells were used at passage 16.

# 118 2.3 Hydrogel formation

- 119 The hydrogel formation was performed based on previously established protocols (27) with
- 120 modifications in N:T ratios and alginate concentration, as described below.

# 121 2.3.1 Non-degradable matrix: Click-crosslinked hydrogels

- 122 The precursors for the hydrogel were dissolved in phosphate-buffered saline (PBS, without  $Ca^{2+}$ ,
- 123  $Mg^{2+}$  and phenol red; Biozym) and distributed into 2 tubes. The first tube contained norbornene-
- 124 modified alginate (N-alg); MMP-sensitive (MMPsens) peptide (GCRD-VPMS  $\downarrow$  MRGG-DRCG,

- 125 98% purity; WatsonBio) at a final concentration of 10 mg/ml of hydrogel, thiolated RGD-peptide
- 126 (CGGGGGRGDSP; Peptide2.0) at a concentration of 5 molecules of RGD per alginate chain (DS 5),
- 127 and the cell suspension at final concentration of  $5 \times 10^6$  cells/mL of hydrogel. The second tube
- 128 contained tetrazine-modified alginate (T-alg) and the photoinitiator (Irgacure 2959; Sigma-Aldrich,
- 129 #410896) at a final concentration of 3 mg/mL of hydrogel. The total final concentration of alginate
- 130 was 2% w/v at an N:T ratio of 1.5.
- 131 The two solutions were mixed by pipetting and cast onto a bottom glass plate, with the casting area
- being restricted on three sides by glass spacers, and immediately covered with a glass slide
- 133 previously treated with SigmaCoat (≥99.5%; Sigma-Aldrich, #SL2) to prevent adhesion. The gel
- height was constrained to 2 mm by the thickness of the glass spacers. Spontaneous click-crosslinking
- for 50 min at room temperature (RT) and in the dark allowed the N:T covalent bonds to form.
- 136 Despite MMPsens and the photoinitiator being present, these were not activated due to the lack of
- 137 UV exposure. Nevertheless, the MMPsens and photoinitiator need to be present to allow for
- 138 patterned materials (see section 2.3.3).
- 139 In order to ensure a homogeneous binding of the RGD-peptide, crosslinked gels were exposed to
- 140 2 min UV light (365 nm) at 10 mW/cm<sup>2</sup> (Omnicure S2000) in a custom-built exposure chamber. The
- 141 cylindrical hydrogels were punched from the cast gel sheet using 5 mm biopsy punches (Integra
- 142 Miltex) and placed in growth media at  $37^{\circ}$ C and 5% CO<sub>2</sub>.

# 143 2.3.2 Degradable matrix: MMPsens peptide crosslinked hydrogels

- 144 The production of degradable materials followed the same procedure as described in section 2.3.1,
- 145 with an additional step for the MMPsens peptide crosslinking. After casting the hydrogel solution
- between the glass plates, the material was exposed to UV light at 10 mW/cm<sup>2</sup> for 10 min to initiate
- the coupling of the degradable MMPsens peptide to the norbornene-modified alginate via thiol-ene
- 148 crosslinking. After the UV exposure, the materials were placed for an additional 50 min at RT in the
- dark to allow for the N:T covalent bonds to be formed. To ensure a homogenous binding of RGD, the
- 150 hydrogels were exposed again to UV for 2 min. Hydrogels were punched out and incubated in 151 growth modia at 27% and 5% CO
- 151 growth media at  $37^{\circ}$ C and 5% CO<sub>2</sub>.
- 152 As negative control materials, hydrogels were fabricated with peptide crosslinkers not susceptible to
- degradation, MMP-scramble (VpMSmRGG). In this case, the peptide contained the same sequence
- 154 as the degradable isoform but with some amino acids in the D-form (indicated in lower case letters),
- 155 rendering them unrecognizable to matrix metalloprotease enzymes.

# 156 2.3.3 Patterned: Dual crosslinked hydrogels

- 157 The creation of patterned materials followed the same procedure as described in section 2.3.2, with
- 158 the addition of a photomask placed on top of the cover glass during the UV mediated thiol-ene
- 159 coupling of the MMPsens peptide. The photomask had a pattern of straight lines with 500 μm
- 160 thickness (UV light blocking sections, non-degradable matrix equivalent to 2.3.1) placed 250 μm
- apart (UV light permitting sections, degradable matrix equivalent to 2.3.2).

# 162 2.4 Mechanical characterization

- 163 Mechanical characterization was performed on day 1 and day 14. All mechanical characterization
- 164 was performed with cell-loaded materials to quantify the enzymatic degradation of the hydrogels in
- stiff and degradable (Stiff-Deg) materials. This was also true for soft and non-degradable (Soft-
- 166 NoDeg) materials to keep comparable conditions. The material degradation was evaluated via three

167 different methods: unconfined compression testing for measuring bulk elastic modulus of single-

- phase materials, rheology to quantify loss and storage modulus of single-phase materials and 168
- microindentation to estimate the surface elastic modulus of single-phase and patterned materials. 169

#### 170 2.5 **Unconfined compression testing**

- Single-phase materials were subjected to uniaxial unconfined compression testing (BOSE Test Bench 171
- LM1 system) with a 250 g load cell (Model 31 Low, Honeywell) at 0.016 mm/s without preload. The 172
- 173 elastic modulus E was calculated as the slope of the linear region of the generated stress vs. strain
- curve, in the 2-10% strain range, using a MATLAB (R2019b) script (n = 6). The required MATLAB 174 175 inputs of hydrogel height and diameter were determined by lowering down the BOSE system top
- 176 plate until contact with the gel surface was established and by using calipers, respectively.

#### Rheology 177 2.6

185

- 178 Storage and loss modulus of single-phase hydrogels were determined with a rheometer (Anton Paar
- 179 MCR301) via frequency sweeps with a parallel plate geometry of 8 mm (PP08, Anton Paar). The
- frequency sweep was performed from 0.01 to 10 Hz and at 0.1% shear strain at RT (n = 6). Once 180
- contact with the gel surface was established, a pre-compression of 10% of the height of the hydrogel 181

182 was applied prior to the measurement. No additional hydration was needed as the experiment lasted less than 10 min. To obtain the elastic modulus, first the shear modulus (G) was derived from the

- 183
- 184 storage (G') and loss (G") modulus using Rubber's elasticity theory (Eq. 1).

$$G = \sqrt{G'^2 + G''^2}$$
(1)

186 The elastic modulus (E) was calculated using the values of the shear modulus obtained from Eq.1 (32) and the approximation of Poisson's ratio ( $\vartheta$ ) equal to 0.5 (33) (Eq. 2). 187

$$E = 2G (1 + \vartheta)$$

189	The mesh size ( $\xi$ ) was approximated by Eq. 3, proposed for alginate hydrogels, in which the storage
190	modulus G' in low frequencies (0.1-1Hz) was used (34), with $N_{av}$ being avogadro's number (6.022)
191	$10^{23}$ 1/mol), R being the ideal gas constant (8,314 m <sup>3</sup> Pa/K° mol) and T being the room temperature
192	(293°K).

193 
$$\xi = \sqrt[3]{\frac{6 RT}{G' \pi N_{av}}}$$

#### 194 Microindentation 2.7

#### 195 2.7.1 Depth-Sensing Indentation/Air-Indent Method

196 Depth-sensing microindentation measurements were done using a Triboindenter TI-950 (Hysitron-Bruker, MN, USA) equipped with an XZ-500 extended displacement stage, allowing a vertical 197 198 displacement of up to 500 µm (35). After the first contact to detect the surface, the tip was retracted 199 for ~300 µm. Next, the measurements were conducted using the "air-indent" mode, allowing a 200 reliable indentation curve without any additional sample pre-contact. The measurements were done 201 using a cono-spherical tip of 50 µm radius and in automated mode to map an area of 6x6 matrix, 202 indentation spacing of 300 µm in single-phase materials and 18x11 matrix with an indentation spacing of 150 µm in patterned materials. The measurements were done in displacement control 203

(2)

(3)

204 mode, using a displacement function of 250  $\mu$ m retraction and 300  $\mu$ m approach, with a strain rate of 205  $\sim$ 30  $\mu$ m/s.

#### 206 2.7.2 Analysis of load-displacement curves

- 207 To meet the Hertzian contact model requirement, the first 30  $\mu$ m of contact depth after initial contact,
- in which the tip geometry stays spherical, was used for curve fitting and calculation of the independent state and the curve fitting and calculation of the curve fitting and calculation of the curve shares are stated as  $(E_{\rm ent})$ .
- indentation elastic modulus (Eq. 4). This model was chosen as it describes the contact mechanics of 210 and 20 solids and correlates the elastic modulus (E) with the contact surface radius (P. 50 um) load (a)
- 210 3D solids and correlates the elastic modulus (*E*) with the contact surface radius (*R*, 50  $\mu$ m), load (*y*) 211 and contact depth (*x*)
- 212  $y = \frac{4}{3} * E * R^{0.5} * x^{1.5}$  (4)

213 Considering the high number of indents, the analysis of the load-displacement curves was automated

by a custom-made Python3 script. The depth of the gel and the load of the indenter (both ordered by

time) are the main data vectors used for the analysis. This automation is divided into four main parts:

216 (1) identifying the point of interest (POI), (2) extracting the curve segment, (3) fitting the Hertzian

- 217 model on the extracted segment and (4) obtaining the indentation E value per indentation point,
- collected in a matrix and depicted in a heat map. Further information can be found in Supplementary
- Example 219 Figure S2.

#### 220 2.8 Cell viability by Live/Dead staining

221 Cell viability was assessed after 1 and 14 days using Live/Dead staining. The hydrogels were taken

out from the incubation media and washed with PBS. Then the cells were stained with a solution of 4

mM calcein AM (TRC, #C125400) and 4 mM ethidium homodimer-1 (Thermo Fisher, #L3224)

dissolved in PBS to identify live and dead cells, respectively. The staining solution volume was 400

- $\mu$  per hydrogel, stained for 12 min in a cell culture incubator at 37°C, 5% CO<sub>2</sub> in the darkness. A
- final washing step was performed with 400  $\mu$ l of PBS per hydrogel at RT for 5min and protected
- 227 from light.

228 Imaging was performed on a confocal microscope (Leica SP5, Germany). Quantification of cell

number and viability at each time point was performed using ImageJ software (ImageJ 1.53s) (36).

230 Three independent positions per gel were acquired at the gel center at 25x magnification, from 2

231 independent samples, resulting in n=6 fields of view containing multiple single cells (n>100). To

assess cell proliferation (cell number per unit volume), differential swelling of soft and stiff

hydrogels was taken into account, as explained in Supplementary Information S3.

#### 234 2.9 Cell morphology by DAPI/Phalloidin staining

235 To evaluate cell morphology, DAPI/Phalloidin staining was performed after 1 and 14 days,

visualizing nuclei and actin, respectively. All steps were performed under orbital shaking, in a 24

well plate and using a volume of 400 uL per gel. Encapsulated cells were fixed in 4%

paraformaldehyde solution (Sigma Aldrich, Sigma, #158127) for 45 min at RT, then permeabilized

with 0.3% Triton X-100 (Sigma Aldrich, #11488696) for 15 min, washed twice with 3% bovine

serum albumin (BSA, Sigma, #A2153) in PBS for 5 min and stained in the dark with 4, 6-diamidino-

241 2- phenylindole (DAPI; Sigma, #MBD0015) and TRITC-conjugated Phalloidin (Cell Signaling,

242 #8878S) for 3h. A final wash was performed with 3% BSA in PBS for 5 min at RT.

243 Three independent positions per gel were acquired at the gel center using a confocal microscope

- 244 (Leica SP5, Germany). For a general quantification of cell morphology, 25x magnification was used
- and n=6 fields of view (3 different images from 2 independent samples) were taken, containing
- 246 multiple single cells (n>50). In addition, ten single cell images per gel (5 cells from 2 different
- hydrogels) were analyzed for quantification of filopodia number and length. Images were obtained
- from the center of the gel using 64x magnification.

#### 249 2.10 Image-based analysis tool to study anisotropic multicomponent materials

A custom-made image-based analysis tool in the form of a macro written in ImageJ (ImageJ 1.53s)

- 251 (36) has been created to analyze cellular readouts obtained from Z-stack projections from anisotropic
- 252 patterned materials. The macro offers the possibility to freely divide an image into rectangular units,
- which leads to a heat map in which the results are later depicted. The background is separated from
- the cells via a threshold. To compensate for pixel noise from the raw data, a denoise function (median
- filter) is built in, which can be used with different strengths depending on the image. In this way, a binary mask is created, which is used for most of the calculations. For details on the binning size
- 257 optimization, refer to Supplementary Figure S4.
- 258 Three readouts are calculated for every tile within the heat map: Cell Projected Area, Cell Circularity
- and Cell Number. Cell Projected Area is calculated for each cell as number of pixels and converted

260 into  $\mu$ m<sup>2</sup> or mm<sup>2</sup>. Cell Circularity is calculated for each cell as  $4\pi$ \*area/perimeter^2, where 1

261 indicates a perfect circle and values towards 0 indicate elongated cells. Cell Number is calculated as

- number of DAPI nuclei within each tile. Every cell in a tile will be individually calculated and the
- 263 mean of all cells in a tile is used. Cells touching the tile border are excluded. For further details, refer
- to Supplementary Figure S5.

# 265 2.11 Statistical analysis

Results are depicted as bar graphs with mean and standard deviation, or box plots with median, 1<sup>st</sup>

and 3<sup>rd</sup> quartile, using OriginLab (Pro 2022b). Comparison of hydrogel mechanical properties were

268 performed using Student t-test (p < 0.05). Comparison of cellular read-outs were performed using 269 Student t-test (p < 0.05) for normally distributed data and Wilcoxon Signed Rank test (p < 0.05) for

270 not normally distributed data.

#### 272 **2** Results

#### 273 **2.10** Mechanical characterization

274 Single-phase Stiff-Deg and Soft-NoDeg materials were characterized for their bulk elastic and

- viscoelastic properties at day 1 and day 14, as well as changes over time, using rheology and
- 276 unconfined compression testing. The storage modulus (G') of Stiff-Deg is higher than Soft-NoDeg
- 277 materials with average values of  $3353 \pm 36$  Pa and  $530 \pm 10$  Pa, respectively, at day 1 (Fig. 1A) and
- 278  $1848 \pm 41$  kPa and 776  $\pm 26$  kPa at day 14 (Fig. 1B). The values of G' showed a decrease at day 14
- 279 (Fig. 1B) compared to day 1 (Fig. 1A) for Stiff-Deg materials, whereas G" modulus presented a
- similar behavior at day 1 and day 14 for both materials.



#### 281

Figure 1: Mechanical characterization of single-phase materials: Soft-NoDeg (black) and Stiff-Deg (red). (A) Day 1 and (B) day 14 of storage (G',  $\Box$ ) and loss (G'',  $\Delta$ ) modulus in Pa obtained by rheology, n=6 gels. (C) Elastic modulus determined by unconfined compression testing in kPa, n=6 gels. (D) Mesh size estimated from the storage modulus in nm, n=6 gels. Statistical significance with Student t-test for differences between groups is indicated with \* and differences between time points with # (\*/# = p<0.05, \*\*/## = p<0.01).

Bulk elastic modulus was characterized by unconfined compression testing (Fig. 1C). At day 1, there is a significant difference between the Soft-NoDeg  $(2 \pm 0.3 \text{ kPa})$  and Stiff-Deg  $(10 \pm 0.6 \text{ kPa})$ 

- materials. At day 14, there is a significant decrease of elastic modulus in Stiff-Deg materials ( $6 \pm 0.6$
- kPa) with respect to day 1. The Soft-NoDeg materials showed a constant elastic modulus at day 14 (2)
- 291 KPa) with respect to day 1. The Soft-NoDeg materials showed a constant elastic modulus at day 14 (2
- 292  $\pm 0.2$  kPa).

- 293 The dynamic behavior of degradable materials is also evident in the change of the mesh size (Fig.
- 1D). The mesh size increases significantly in degradable materials from  $13.0 \pm 0.1$  nm on day 1 to 34
- $\pm 3$  nm on day 14. In contrast, Soft-NoDeg materials maintain the mesh size over 14 days, as the
- values of day 1 ( $24 \pm 0.3$  nm) and day 14 ( $26 \pm 2$  nm) are not significantly different.



Figure 2: Microindentation of single-phase and patterned materials. (A, D) Patterned materials, (B,
E) Soft-NoDeg single-phase materials and (C, F) Stiff-Deg single-phase materials, on day 1 and day
14, respectively. Each matrix is the visual representation of the indentation elastic modulus (kPa) at
the material surface. Single-phase materials (6x6 matrix, indentation spacing of 300 µm), patterned
materials (18x11 matrix, indentation spacing of 150 µm).

To characterize the anisotropic mechanical properties of patterned hydrogels we used the method of microindentation. Patterned materials show a clear difference in the elastic modulus between the 2 phases, on day 1 (Fig. 2A) and day 14 (Fig. 2D). The corresponding single-phase materials showed similar values of elastic modulus. The surface elastic modulus of Soft-NoDeg materials was comparable between day 1 (Fig. 1B) and day 14 (Fig. 1E) and the elastic modulus of the Stiff-Deg

308 materials decreased visibly between day 1 (Fig. 1C) and day 14 (Fig. 1F).

#### 309 3.2 Cell viability and proliferation in 3D single-phase and patterned materials

- 310 Mouse embryonic fibroblasts were encapsulated in 3D single-phase and patterned hydrogels. Cell
- 311 viability was evaluated at day 1 and day 14 by staining live cells with calcein (green) and dead cells
- 312 with ethidium homodimer-1 (red).







- 1 and day 14, 25x magnification, 250 μm z-stack, and corresponding (B) cell viability in % (viable
- 317 cells/total cells) and (C) cell number (cells per mL of hydrogel). (D) Live/Dead staining of patterned
- materials at day 1 and day 14, with 2 x 2 tile merging of 10x magnification, 250 µm z-stack. The
- macro function "cell number" was used to quantify and plot the heat maps corresponding to cell
- viability in patterned materials at (E) day 1 and (G) day 14, as well as total cell number at (F) day 1 and (H) day 14. The bars in B and C represent the mean and standard deviation of n = 6 fields of
- 321 and (H) day 14. The bars in B and C represent the mean and standard deviation of n = 6 fields of 322 view containing multiple single cells (n>100). Statistical significance with Student t-test for
- differences between groups is indicated with \* and differences between time points with #(\*/# =
- p<0.05, \*\*/## = p<0.01). Scale bar: 500 µm (A), 1 mm (D).
- 325 Single-phase materials showed high viability (Fig. 3A), as the fraction of viable cells remained above
- 326 90% for all materials and time points. The cell number corrected to the swelling factor (Fig. 3B)
- 327 shows that the cell proliferation was higher in Stiff-Deg materials compared to Soft-NoDeg, with
- 328 significantly higher cell number at day 14 compared to day 1 and compared to the Soft-NoDeg
- 329 counterpart at day 14. In contrast, no significant differences over time were seen in the cell number
- 330 for Soft-NoDeg materials.
- 331 The macro function "cell number" allowed the quantification and visualization of cell viability and
- 332 proliferation in patterned materials. Comparable to single-phase materials, patterned materials also
- 333 showed high viability in both phases and over time (Fig. 3D). No visible patterns or changes were
- shown in viability, neither at day 1 (Fig. 3E) or day 14 (Fig. 3G).
- 335 Encapsulated cell number showed an initial homogeneous distribution of cells, as on day 1 there are
- no visible patterns (Fig. 3F). However, patterns in cell proliferation are evident at day 14, which
- 337 show higher cell number in the Stiff-Deg areas compared to the Soft-NoDeg zones (Fig. 3H).
- 338

#### 340 **3.3** Cell morphology in 3D single-phase materials

343

341 Staining of the nuclei (DAPI, cyan) and the actin cytoskeleton (phalloidin, green) in single-phase 342 materials was used to analyze the effect of material properties on cell morphology.



- Figure 4: Morphology of encapsulated cells in single-phase materials at day 1 and day 14. (A)
- 345 Phalloidin (green)/ DAPI (cyan) staining of multiple cell images with 25x magnification, 250 μm z-
- stack to determine (B) projected cell area in  $\mu$ m<sup>2</sup> and (C) circularity (-). (D) Higher 40x
- 347 magnification of single cell z-stack to determine (E) filopodia number (-) and (F) filopodia length in
- 348  $\mu$ m. Boxes represent the median and 1<sup>st</sup> and 3<sup>rd</sup> quartile of (B, C) multiple cells (>50cells) in n=6
- 349 fields of view or (E, F) n=10 cells. Statistical significance with Wilcoxon Signed Rank test for
- 350 differences between groups is indicated with \* and differences between time points with # (\*/# =
- 351 p < 0.05, \*\*/## = p < 0.01). Scale bar: 200 µm (A), 25 µm (D).
- 352 On day 1, cells in Soft-NoDeg materials displayed significantly greater projected area compared to
- 353 cells in Stiff-Deg materials (Fig. 4B). 14 days after encapsulation, when the Stiff-Deg materials
- 354 degraded and consequently softened, the cell projected area increased significantly compared to the
- initial time point and also in comparison with the Soft-NoDeg materials at day 14.
- Differences in cell circularity at day 14 are significant between the 2 materials (Fig. 4C). The cells in
- 357 Stiff-Deg materials show significantly lower circularity compared to the initial time point and to cells
- 358 in Soft-NoDeg hydrogels at day 14.
- 359 In Figure 4D, single cell images are shown, depicting detailed cell morphology and filopodia. On day
- 360 1, early filopodia formation can be seen in Stiff-Deg materials, whereas no filopodia were formed in
- 361 Soft-NoDeg hydrogels. After 14 days, the filopodia number and length increased significantly in
- 362 Stiff-Deg compared to the initial time point and to Soft-NoDeg at day 14. In Soft-NoDeg materials,
- filopodia number and length increased after 14 days of encapsulation, yet they remained lower
- 364 compared to Stiff-Deg materials.
- 365 **3.4 Cell response in 3D patterned materials**
- The photopatterning of single-phase materials created anisotropic hydrogels with spatially distinct degradation and stiffness characteristics.
- 368 Figure 5 shows the effect of patterned materials on the morphology of MEFs (Fig. 5A-F), the
- 369 evaluation and heat map representation using the novel image-based analysis tool (Fig. 5G-J) and the
- quantification of the individual material phases (Fig. 5K-N). On day 1 (Fig. 5A, C, E), there are
- patterns in projected cell area (Figure 5G) as the Soft-NoDeg phase shows cells with significantly
- larger projected cell area compared to Stiff-Deg (Fig. 5K). Initially, no significant patterns in
- circularity are visible (Fig. 5H, L) as most of the cells present a round morphology. At day 14 after
- encapsulation (Fig. 5B, D, F), there is a significant increase of the projected cell area in the Stiff-Deg
  (Fig. 5K) and even stronger significant decrease in cell circularity (Fig. 5L). This is visualized in the
- heat maps with emerging spatial patterns in cell circularity at day 14 compared to day 1 (Fig. 5J, H)
- 377 and less visible, even reverted patterns in projected cell area (Fig. 5I, G).
- 378 Regarding cell morphology, single cell images at day 1 (Fig 5E) showed that filopodia are mainly
- formed in Stiff-Deg phase, with significantly greater number (Fig. 5M) and length (Fig. 5N) of the
- 380 filopodia. This trend is amplified at day 14 (Fig 5F), with significantly increased filopodia number
- and length compared to day 1 and compared to cells in Soft-NoDeg phase.
- 382
- 383

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Figure 5: Morphology of encapsulated cells in patterned materials at day 1 and day 14. Phalloidin (green)/ DAPI (cyan) staining overview images at (A) day 1 and (B) day 14, with indicated pattern areas, 2x2 tile image, 10x magnification, 250  $\mu$ m z-stack. Zoom-in on the individual regions of the pattern at (C) day 1 and (D) day 14, 25x magnification, 250  $\mu$ m z-stack. Single cell images z-stack at (E) day 1 and (F) day 14, 40x magnification. Heat map representation of (G, I) the mean projected cell area in  $\mu$ m<sup>2</sup> and (H, J) circularity (-) in the overview images, at day 1 (G, H) and day 14 (I, J).

391 Box plots quantifying (K) projected cell area, (L) circularity, (M) filopodia number (-) and (N)

- filopodia length in  $\mu$ m, at day 1 and day 14, showing the median and 1<sup>st</sup> and 3<sup>rd</sup> quartile of n=6 fields
- of view containing multiple single cells (n>50, for K and L) or n=10 cells (for M and N) in patterned
- 394 materials. Statistical significance with Wilcoxon Signed Rank test for differences between groups is
- indicated with \* and differences between time points with #(\*/# = p < 0.05, \*\*/## = p < 0.01). Scale
- 396 bar: (A, B) 500  $\mu$ m, (C, D) 200  $\mu$ m, (E, F) 25  $\mu$ m.

#### **Discussion**

- 398 The presented 3D hydrogels with stiffness-degradation spatial patterns allow cell encapsulation with
- high cell viability and anisotropic cell response. The hydrogel casting procedure offers the possibility
- 400 of photopatterning, combining the properties of two single-phase materials in one single,
- 401 multicomponent matrix, which allows emerging patterns in cell behavior in 3D. Evaluation of cell
- 402 behavior in multicomponent materials is crucial in order to understand how these platforms guide cell 403 response. In our case, we choose patterns in stiffness-degradation and evaluate anisotropic fibroblast
- 404 cell morphology, as an example of the application of an image-based quantification method.
- tot con morphology, as an example of the application of an image-based quantification method
- 405 All methods used for mechanical characterization led to consistent and comparable results of
- 406 mechanical properties and changes over time caused by degradation. First, the methods show a
- 407 decrease over time of the elastic modulus of Stiff-Deg materials compared Stiff-NoDeg materials.
- 408 Second, the bulk elastic modulus of the single-phase materials is comparable to the surface elastic
- 409 modulus of single-phase materials, and importantly, also consistent with the mechanical properties of
- 410 the respective phases of patterned multicomponent materials.
- 411 The decrease in the elastic modulus of the degradable material can be attributed to the degradation of
- the MMPsens peptide bonds due to the action of the enzymes secreted by the cells. A consequence of
- this degradation can be shown in the significant increase of the mesh size over time. There is no
- 414 significant change in the mesh size of Soft-NoDeg materials, as the covalent bonds of these
- 415 hydrogels are non-degradable.
- 416 Our results showed that the projected cell area of 3D encapsulated cells is dependent on the matrix
- 417 stiffness. At day 1, the significantly lower elastic modulus of Soft-NoDeg vs. Stiff-Deg results in
- 418 significantly higher projected cell area in both single-phase and patterned materials. However, at day
- 419 14, when the elastic modulus of Stiff-Deg significantly drops compared to day 1, the projected cell
- 420 area significantly increases and cell circularity decreases as degradation promotes cell spreading.
   421 These results are supported by previous results related to 3D fibroblast encapsulation (37) and in
- 421 These results are supported by previous results related to 3D fibroblast encapsulation (37)
- 422 contrast to cell behavior on 2D surfaces with patterns in stiffness (38), as expected.
- 423 Matrix remodeling and dynamic environments are crucial to stimulate cell response (39).
- 424 Degradation is essential for the formation of protrusions and we observe that Stiff-Deg materials
- 425 promote longer and higher filopodia number compared to Soft-NoDeg materials. The control
- 426 hydrogels formed with a non-degradable version of the peptide (MMP-scramble), showed that cells
- 427 do not form filopodia in non-degradable materials (Supplementary Figure 6). These results are
- supported by previous findings on the effect of matrix deformation energy in the actin cytoskeleton
- of the cell, which has been proven to have a greater effect compared to the intrinsic matrix stiffness(40). Such findings highlight the importance of matrix degradability in enabling cell protrusions to
- 430 (40). Such findings highlight the importance of matrix degradability in enabling cell protrusions 431 invade into the surrounding environment, as they regulate more advanced cell processes like
- 432 migration, motility, communication and differentiation (41).
- 433 One important feature of this work is the combination of Stiff-Deg and Soft-NoDeg phases in one
- 434 single, multicomponent matrix. Differences in cell response observed in single-phase materials are

- 435 recapitulated in patterned stiffness-degradation materials and, importantly, anisotropic cell behavior
- 436 emerges with time as the Stiff-Deg component degrades. This sets the basis for future work looking
- 437 at sharper material interfaces, or in contrast, gradients of stiffness-degradability by manipulating the
- 438 photomask. Such multicomponent materials open opportunities to investigate anisotropic 3D cell
- 439 migration, proliferation or differentiation across a cell-relevant stiffness-degradability range.

440 To evaluate anisotropic 3D cell response in patterned materials, we have developed a new image-

- based analysis tool and visual presentation of spatial anisotropies of material and cellular
- 442 characteristics using heat maps. Various research groups have evaluated patterned materials as
- independent phases, not as a single, multicomponent matrix. The developed image-based method and
- the heat map representation of cell number and morphology (projected cell area and circularity)
- 445 showed to be a valid tool to characterize and quantify anisotropic 3D cell behavior in patterned 446 materials, as it consistently represented the anisotropic cell behavior in each phase compared to
- 447 corresponding single-phase controls. This image-based analysis could be extended to other image-
- 448 based cellular read-outs.
- 449 Despite the great advantage of our novel image-based analysis tool, there are some limitations. As
- 450 input for this analysis tool, images covering the entire gel or stitched multi-tiles images are required.
- 451 However, for certain features such as filopodia formation, high magnification images are necessary.
- 452 Multi-tiles high magnification imaging covering the entire gel currently requires long acquisition
- times, which would lead to dehydration of the hydrogel.
- 454 Our research demonstrates a relevant approach to investigate emerging anisotropic 3D cell behavior
- 455 in stiffness-degradation patterned materials. The developed image-based analysis method provides
- the basis for visualizing and quantifying 3D anisotropic cell behavior with regard to cell number, cell
- 457 projected area and circularity. This anisotropic 3D cell response was confirmed with high resolution
- 458 quantification of filopodia number and length. Such stiffness-degradation patterned hydrogels
- allowing the emergence of 3D anisotropic cell response, together with the image-based analysis
- 460 method for visualization and quantification of cellular read-outs, are valuable tools to understand
- 461 cell-matrix interactions in multicomponent materials.

# 462 **3** Conflict of Interest

463 The authors declare that the research was conducted in the absence of any commercial or financial 464 relationships that could be considered as a potential conflict of interest.

# 465 **4 Data availability**

466 All raw and processed data, and the MATLAB and Python scripts are available in a publicly 467 accessible repository of the Max Planck Society https://doi.org/10.17617/3.NEHZN1.

# 468 **5** Author Contributions

- 469 A Cipitria conceived the idea. CA Garrido and DS Garske performed the experiments. S Amini
- 470 supported the microindentation experiments. S Real developed the algorithm for analysis of the
- 471 microindentation data. CA Garrido quantified and analyzed the data. M Thiele developed the image-
- based analysis macro. K Schmidt-Bleek and GN Duda evaluated the methods and results. CA
- 473 Garrido and A Cipitria drafted the manuscript. All authors discussed the results and contributed to the
- 474 final manuscript.

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