1	Larger and denser: an optimal design for surface grids of EMG
2	electrodes to identify greater and more representative samples of
3	motor units
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25 of interest.

26 Abstract

The spinal motor neurons are the only neural cells whose individual activity can be non-invasively 27 identified using grids of electromyographic (EMG) electrodes and source separation methods, i.e., EMG 28 decomposition. In this study, we combined computational and experimental approaches to assess how 29 the design parameters of grids of electrodes influence the number and characteristics of the motor units 30 31 identified. We first computed the percentage of unique motor unit action potentials that could be 32 theoretically discriminated in a pool of 200 simulated motor units when recorded with grids of various 33 sizes and interelectrode distances (IED). We then identified motor units from experimental EMG signals recorded in six participants with grids of various sizes (range: 2-36 cm²) and IED (range: 4-16 mm). 34 35 Increasing both the density and the number of electrodes, as well as the size of the grids, increased the 36 number of motor units that the EMG decomposition could theoretically discriminate, i.e., up to 82.5% 37 of the simulated pool (range: 30.5-82.5%). Experimentally, the configuration with the largest number 38 of electrodes and the shortest IED maximized the number of motor units identified (56 ± 14 ; range: 39-39 79) and the percentage of low-threshold motor units identified $(29 \pm 14\%)$. Finally, we showed with a 40 prototyped grid of 400 electrodes (IED: 2 mm) that the number of identified motor units plateaus beyond an IED of 2-4 mm. These results showed that larger and denser surface grids of electrodes help to 41 42 identify a larger and more representative pool of motor units than currently reported in experimental 43 studies.

44

45 Significance statement

Individual motor unit activities can be exactly identified by blind-source separation methods applied to 46 multi-channel EMG signals recorded by grids of electrodes. The design parameters of grids of EMG 47 electrodes have never been discussed and are usually arbitrarily fixed, often based on commercial 48 49 availability. In this study, we showed that using larger and denser grids of electrodes than conventionally 50 applied can drastically increase the number of motor units identified. These samples of motor units are 51 moreover more balanced between high- and low- threshold motor units and provide a more representative sampling of neural drive to muscles. Gathering large datasets of motor units using large 52 53 and dense grids will impact the study of motor control, neuromuscular modelling, and human-machine 54 interfacing.

55

56 Introduction

Decoding the neural control of natural behaviours relies on the identification of the discharge activity 57 of individual neural cells. Classically, arrays of electrodes are implanted close to the cells to record their 58 59 electrical activity. The application of algorithms that separate the overlapping activity of these cells has enabled researchers to study neural processes in multiple areas of the brain (Stringer et al., 2019), such 60 61 as in the motor or the sensorimotor areas (Churchland and Shenoy, 2007; Gallego et al., 2020). At the 62 periphery of the nervous system, it is also possible to record the activity of individual motor neurons 63 innervating muscle fibres (Heckman and Enoka, 2012; Farina et al., 2016; Enoka, 2019). The motor 64 unit, i.e., a motor neuron and the fibres it innervates, acts as an amplifier of the neural activity, as one 65 action potential propagating along a motor neuron's axon generates an action potential in each of the innervated muscle fibres. The activity of motor units can be identified by decomposing surface 66 67 electromyographic (EMG) signals into trains of motor unit action potentials (MUAPs) using blind-68 source separation algorithms (Holobar and Farina, 2014; Farina and Holobar, 2016). The multiple 69 observations for source separation are obtained by recording EMG signals with grids of electrodes. This 70 approach usually allows for the reliable analysis of 5 to 40 concurrently active motor units (Del Vecchio et al., 2017; Del Vecchio et al., 2020; Hug et al., 2021a). 71

While the design of intracortical (e.g., (Jun et al., 2017; Steinmetz et al., 2018)) and intramuscular (e.g., 72 73 (Muceli et al., 2015; Muceli et al., 2022)) arrays of electrodes has scaled up over the years to record 74 larger samples of neural cells, the configuration of surface EMG grids of electrodes has not 75 systematically evolved. Most researchers currently use grids with 64 electrodes arranged in 13×5 or 8 76 \times 8 montages, the interelectrode distance (IED) between adjacent electrodes (e.g., 4 mm, 8 mm, or 10 77 mm) being dictated by the size of the muscle to cover. Yet, optimizing these parameters, i.e., grid size 78 and IED, may influence the performance of EMG decomposition. Currently, there are no 79 recommendations on optimal design parameters for grids when using surface EMG for the study of 80 motor units.

81 Source separation algorithms are based on the necessary condition that identifiable motor units have 82 unique representations across the multi-channel EMG signal (Farina et al., 2008; Holobar and Farina, 83 2014; Farina and Holobar, 2016). This implies that the three-dimensional waveform of a MUAP (one 84 time dimension and two spatial dimensions) should be unique within the pool of motor units detected 85 by the surface grid. In practice, the identified motor units are those that innervate larger numbers of 86 muscle fibres, as their action potentials tend to have the largest energy. Conversely, low-threshold motor 87 units usually remain hidden since their energy is close to the baseline noise. Increasing the density of 88 electrodes would increase the spatial sampling frequencies of the EMG signals (Farina and Holobar, 89 2016). This should improve the discrimination of MUAPs, allowing the identification of a larger number 90 of motor units. Additionally, increasing the electrode density may reveal the hidden low-threshold motor

units by sampling their action potentials across a larger number of electrodes, leading to a bettercompensation of the additive noise in the mixture model of the EMG signal.

In this study, we combined computational and laboratory experiments to identify the optimal design 93 94 criteria for grids of surface electrodes with the aim of maximizing the number of identified motor units, 95 specifically increasing the relative number of identifiable low-threshold motor units. We first simulated 96 a pool of 200 motor units and the associated EMG signals recorded from grids of electrodes of various 97 sizes and densities. These simulations showed that the greater the size and the density of the grid, the higher the percentage of identifiable motor units and the relative ratio of identifiable small and deep 98 99 units. We confirmed these theoretical results with experimental signals recorded with a grid of 256 100 electrodes with a 4-mm IED that was downsampled in the space domain to obtain six grid configurations (surface range: 2-36 cm² and IED range: 4-16 mm). Finally, we prototyped a new grid of 400 electrodes 101 102 with a 2-mm IED and demonstrated that the number of identified motor units approximately plateaus 103 beyond a 2-4-mm IED.

104 Methods

105 Computational study

A pool of 200 motor units was simulated to test whether increasing the density and the size of surface 106 107 grids of electrodes would impact the number of identifiable motor units. The simulations were based 108 on an anatomical model of a cylindrical muscle volume with parallel fibres (Farina et al., 2008; 109 Konstantin et al., 2020), where subcutaneous and skin layers separate the muscle from the surface 110 electrodes. Specifically, we set the radius of the muscle to 25.4 mm and the thicknesses of the 111 subcutaneous and skin layers to 5 mm and 1 mm, respectively. The centres of the motor units were distributed within the cross section of the muscle using a farthest point sampling. The farthest point 112 sampling filled the cross-section by iteratively adding centres points that were maximally distant from 113 114 all the previously generated motor unit centres, resulting in a random and even distribution of the motor 115 unit territories within the muscle. The number of fibres innervated by each motor neuron followed an exponential distribution, ranging from 15 to 1500. The fibres of the same motor unit were positioned 116 around the centre of the motor unit within a radius of 0.0082 to 0.8 mm, and a density of 20 fibres/mm². 117 118 Because motor unit territories were intermingled, the density of fibres in the muscle reached 200 fibres/mm². The MUAPs were detected by circular surface electrodes with a diameter of 1 mm. The 119 simulated grids were centred over the muscle in the transverse direction, with a size ranging from 14.4 120 to 36 cm^2 , and an IED ranging from 2 to 36 mm. 121

122

123 Laboratory study

124 Participants

Six healthy participants (all males; age: 26 ± 4 yr; height: 174 ± 7 cm; body weight: 66 ± 15 kg) volunteered to participate in the first experimental session of the study. They had no history of lower limb injury or pain during the months preceding the experiments. One of these individuals (age: 26 yr; height: 168 cm; bodyweight: 51 kg) participated in a second experimental session to test the prototyped grid with an IED of 2 mm. The Ethics Committee at Imperial College London reviewed and approved all procedures and protocols (no. 18IC4685). All participants provided their written informed consent before the beginning of the experiment.

132

133 Experimental tasks

The two experimental sessions consisted of a series of isometric ankle dorsiflexions performed at 30% and 50% of the maximal voluntary torque (MVC) during which we recorded high density electromyographical (HD-EMG) signals over the Tibialis Anterior muscle (TA). The participants sat on

137 a massage table with the hips flexed at 30° , 0° being the hip neutral position, and their knees fully

extended. We fixed the foot of the dominant (right in all participants) leg onto the pedal of a commercial 138 dynamometer (OT Bioelettronica, Turin, Italy) positioned at 30° in the plantarflexion direction, 0° being 139 140 the foot perpendicular to the shank. The thigh was fixed to the massage table with an inextensible 3-cm-141 wide Velcro strap. The foot was fixed to the pedal with inextensible straps positioned around the 142 proximal phalanx, metatarsal and cuneiform. Force signals were recorded with a load cell (CCT 143 Transducer s.a.s, Turin, Italy) connected in-series to the pedal using the same acquisition system as for 144 the HD-EMG recordings (EMG-Quattrocento; OT Bioelettronica). The dynamometer was positioned 145 accordingly to the participant's lower limb length and secured to the massage table to avoid any motion 146 during the contractions.

147 All experiments began with a warm-up, consisting of brief and sustained ankle dorsiflexion performed at 50% to 80% of the subjective MVC. During the warm-up, all participants learnt to produce isometric 148 ankle dorsiflexion without co-contracting the other muscles crossing the hip and knee joints. At the same 149 time, we iteratively adjusted the tightening and the position of the straps to maximize the comfort of the 150 participant. Then, each participant performed two 3-to-5 s MVC with 120 s of rest in between. The peak 151 152 force value was calculated using a 250-ms moving average window, and then used to set the target level 153 during the submaximal contractions. After 120 s of rest, each participant performed two trapezoidal 154 contractions at 30% and 50% MVC with 120 s of rest in between, consisting of linear ramps up and 155 down performed at 5%/s and a plateau maintained for 20 s and 15 s at 30% and 50% MVC, respectively. 156 The order of the contractions was randomized. One participant (S2) did not perform the contractions at

- 157 50% MVC.
- 158

159 <u>High-density electromyography</u>

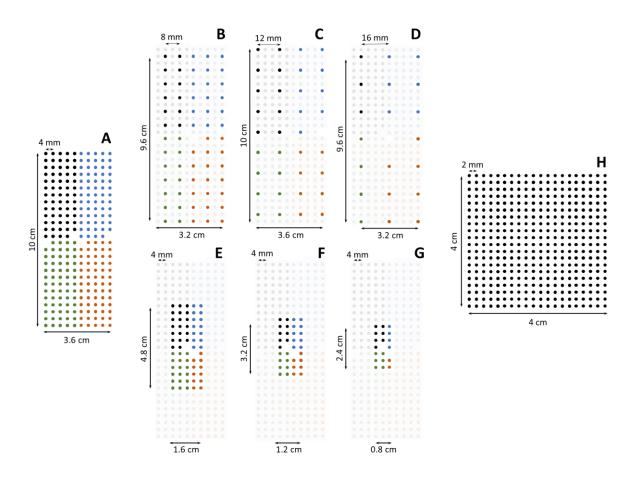
160 In the first experimental session, four adhesive grids of 64 electrodes (13 x 5; gold coated; 1 mm 161 diameter; 4 mm IED; OT Bioelettronica) were placed over the belly of the TA. The grids were carefully positioned side-to-side with a 4-mm-distance between the electrodes at the edges of adjacent grids 162 163 (Figure 1A). The 256 electrodes were centred to the muscle belly and laid within the muscle perimeter identified through palpation. The skin was shaved, abrased and cleansed with 70% ethyl alcohol. 164 165 Electrode-to-skin contact was maintained with a bi-adhesive perforated foam layer filled with 166 conductive paste. The grids were wrapped with tape and elastic bands to secure the contact with the skin. The four 64-pre-amplifiers were connected in-series with stackable cables to a wet reference band 167 placed above the medial malleolus of the same leg. HD-EMG signals were recorded in monopolar 168 169 derivation with a sampling frequency of 2,048 Hz, amplified (x150), band-pass filtered (10–500 Hz), and digitised using a 400 channels acquisition system with a 16-bit resolution (EMG-Quattrocento; OT 170 171 Bioelettronica).

172 In the second experimental session, one ultra-dense custom-made grid of 400 dry electrodes (20 x 20;

- 173gold coated; 0.5 mm diameter; 2 mm IED) was placed over the belly of the TA. The skin was first shaved
- and cleansed with abrasive paste. Then, the electrode was directly placed on the skin after the skin was
- 175 wetted to decrease the impedance between the skin and the dry electrodes. The HD-EMG signals were
- then recorded in monopolar mode with a sampling frequency of 2,048 Hz, following the same procedure
- as before with eight 64-pre-amplifiers connected in-series with stackable cables to a wet reference band
- 178 placed above the medial malleolus of the same leg.

179 <u>Grid configurations</u>

- 180 During the first experimental session, we recorded the myoelectric activity of the TA with a total of 256 181 electrodes covering 36 cm² of the muscle surface (10 cm x 3.6 cm, 4-mm IED, Figure 1A). To investigate the effect of the electrode density, we downsampled the 256-electrode grid by successively discarding 182 rows and columns of electrodes and artificially generating three new grids covering the same area with 183 184 IEDs 8 mm, 12 mm, and 16 mm, involving 256, 64, 35, and 20 electrodes, respectively (Figure 1B-D). It is noteworthy that the 8-mm and 16-mm grids covered a surface of 32 cm^2 because they included an 185 odd number of rows and columns. To investigate the effect of the size of the grid, we discarded the 186 187 peripherical electrodes to generate grids of 63, 34 and 19 electrodes with a 4-mm IED, covering 7.7, 3.8 188 and 2 cm^2 of the muscle (Figure 1E-G). Note that we chose these grid sizes to match the number of 189 electrodes used in the density analysis, thus comparing grids with similar number of electrodes, but 190 different densities and sizes (in Figure 1, B versus E, and C versus F). 191 During the second experimental session, we recorded the myoelectric activity of the TA with the ultra-
- dense grid of 400 dry electrodes covering 16 cm² of the muscle (4 cm x 4 cm, 2-mm IED). Using the
- 193 same procedure as above, we generated two artificial grids with an IED of 4 mm and 8 mm, and 100
- and 25 electrodes, respectively.



195

Figure 1: The eight grid configurations considered in this study. From the grid of 256 electrodes (A, grid
size: 36 cm², IED: 4 mm), six shallower and smaller grids (B-G) were artificially obtained by discarding
the relevant electrodes and used in the first experimental session. (B,C,D) Density analysis: 8, 12, and
16mm IED. (E,F,G) Size analysis: 7.7, 3.6, and 2 cm² surface area. (H) The ultra-dense grid of 400 dry
electrodes (grid size: 16 cm², IED: 2 mm) used in the second experimental session.

201

202 <u>HD-EMG decomposition</u>

203 We decomposed the signals recorded in all the conditions using the same parameters and procedure. First, the monopolar EMG signals were bandpass filtered between 20-500 Hz with a second-order 204 205 Butterworth filter. After visual inspection, channels with low signal-to-noise ratio or artifacts were 206 discarded. The HD-EMG signals were then decomposed into motor unit spike trains using convolutive 207 blind-source separation, as previously described (Negro et al., 2016). In short, the EMG signals were 208 first extended to reach 1000 channels and spatially whitened. Thereafter, a fixed-point algorithm that 209 maximized the sparsity was applied to identify the sources embedded in the EMG signals, i.e., the series 210 of delta functions centred at the motor unit discharge times. These sources are sparse, with most samples being 0 (i.e., absence of discharge) and a small number of samples being 1 (i.e., discharge times). In this 211 212 algorithm, a contrast function was iteratively applied to the EMG signals to estimate the level of sparsity

of the identified sources, and the convergence was reached once the level of sparsity did not vary when 213 compared to the previous iteration, with a tolerance fixed at 10⁻⁴ (see Negro et al., 2016, for the definition 214 215 of the detailed contrast functions). At this stage, the estimated source contained high peaks (i.e., the 216 delta functions from the identified motor unit) and low peaks from other motor units and noise. High 217 peaks were separated from low peaks and noise using peak detection and K-mean classification with 218 two classes. The peaks from the class with the highest centroid were considered as the spikes of the 219 identified motor unit. A second algorithm refined the estimation of the discharge times by iteratively 220 recalculating the motor unit filter and repeating the steps with peak detection and K-mean classification 221 until the coefficient of variation of the inter-spike intervals was minimized. This decomposition 222 procedure has been previously validated using experimental and simulated signals (Negro et al., 2016). 223 After the automatic identification of the motor units, duplicates were removed, and all the motor unit 224 spike trains were visually checked for false positives and false negatives (Del Vecchio et al., 2020). This 225 manual step is highly reliable across operators (Hug et al., 2021b). Only the motor units which exhibited 226 a pulse-to-noise ratio (PNR) > 28 dB were retained for further analysis.

227

228 We further tested whether decomposing subsets of electrodes within a highly populated grid of 256 229 electrodes increased the number of identified motor units. Indeed, the lower ratio of large motor units 230 sampled by each independent subset of 64 electrodes could allow the algorithm to converge to smaller 231 motor units that contribute to the signal. For a similar number of iterations, it is likely that these motor 232 units would have otherwise contributed to the noise component of the mixture model of the EMG signal 233 (Farina and Holobar, 2016). Thus, we decomposed the four separated grids of 64 electrodes before removing the motor units duplicated between grids. Similarly, the grid with 400 electrodes was 234 235 decomposed as eight separated partially overlapping subsets of 64 electrodes.

236

237 Analysis

238 <u>Computational study</u>

239 We first estimated the theoretical percentage of identifiable motor units for each of the simulated 240 conditions. To do so, the simulated MUAPs detected over the entire set of electrodes were compared 241 with each other. The comparisons were done pairwise by first aligning the MUAPs in time using the 242 cross-correlation function, and then computing the normalised mean square difference between the 243 aligned action potentials. Pairs of action potentials with a mean square difference below 5% were considered not discriminable. The 5% criterion was based on the variability of motor unit action 244 245 potential shapes observed experimentally for individual motor units (Farina et al., 2008). After 246 computing all pair-wise comparisons, we then computed the proportion of action potentials that could

be discriminated from all others, i.e., the proportion of unique action potentials. This metrics is independent from the algorithm used for decomposition and establishes an upper bound in the number of motor units that can be identified by any decomposition algorithm. For each unique action potential, we also computed the distance between the centre of the territory of the corresponding muscle fibres and the skin surface.

252

253 <u>Laboratory study – number of identified motor units</u>

We reported the absolute number of motor units (PNR > 28 dB) identified with all the experimental grid 254 255 configurations. For each participant, the number of identified motor units was then normalized to the 256 maximal number of motor units found across all conditions, yielding normalized numbers of identified 257 motor units \overline{N} then expressed in percentage. For each condition, we calculated the mean and standard 258 deviation of the \overline{N} values across participants. To investigate the effects of density and size of the grid, we fitted logarithmic trendlines to the relationships between the averaged \overline{N} values and IED and grid 259 size. We also fitted a logarithmic trendline to the average \overline{N} values and their corresponding number of 260 electrodes, in which case the conditions involving the same number of electrodes, but different grid size 261 and density, were given a weight of 0.5 in the minimization function. We reported the r^2 and p-value for 262 263 each regression trendline. To maintain consistency with the computational study on the investigation of 264 the maximum number of identifiable motor units depending on grid design, the trendlines were fitted on the results obtained when the complete grids of 256 electrodes were decomposed as independent subsets 265 of 64 electrodes, which systematically returned the highest number of identified motor units. The 266 267 trendlines fitted on the results obtained when all available signals were simultaneously decomposed are 268 reported in Supplementary Material A.

269

270 <u>Laboratory study – characteristics of identified motor units</u>

To investigate the effects of electrode density and grid size on the characteristics of the motor unit identified, we used a typical frequency distribution of the motor unit force recruitment thresholds in the human TA (Caillet et al., 2022a), where $F^{th}(j)$ is the force recruitment threshold of the jth motor unit in the normalized motor unit pool ranked in ascending order of F^{th} .

275
$$F^{th}(j) = 0.50 \cdot (58.12 \cdot j + 120^{j^{1.83}}), j \in [0; 1]$$

Based on their measured force recruitment threshold, the identified motor units were classified with this
relationship to the first ('low-threshold' or 'small') or second ('high-threshold' or 'large') half of the
active pool, consistent with the Henneman's size principle (Henneman and Mendell, 1981; Caillet et al.,
2022b). For each condition, we reported the percentage of identified motor units classified as 'small'.

We did not report this metric when five or fewer motor units were identified in one condition for threeor more participants.

282

283 <u>Laboratory study – correlation between observations</u>

We assessed how the density of electrodes impacted the information redundancy in the EMG signals 284 recorded by adjacent electrodes. To this end, MUAP shapes were identified over the 256 electrodes with 285 286 the spike-triggered averaging technique. To do so, the discharge times were used as a trigger to segment 287 and average the HD-EMG signals over a window of 50 ms. For each motor unit, we identified the 288 electrode with the highest MUAP peak-to-peak amplitude and calculated the average correlation coefficient ρ with the MUAPs recorded by the four adjacent electrodes using an IED of 4 mm, 8 mm, 289 290 12 mm, and 16 mm. We also repeated this correlation analysis for the ultra-dense grid of 400 electrodes 291 using an IED of 2 mm, 4 mm, and 8 mm.

292 **Results**

293 Computational study

We simulated the firing activity of 200 motor units recorded by 84 configurations of grids of electrodes 294 295 (Figure 2; surface range: 14.4 to 36 cm², IED range: 2 to 36 mm). The number of identifiable motor 296 units increased with the surface size of the grid, from $49.9 \pm 6.5\%$ of the motor units identifiable with a grid of 14.4 cm² to 78.7 \pm 2.6% of the motor units identifiable with a grid of 36 cm². The number of 297 298 identifiable motor units also increased with a decrease in interelectrode distance. For example, with a 299 grid of 36 cm², the number of identifiable motor units increased from 72% to 82.5% of the motor units with an IED of 36 and 2 mm, respectively (Figure 2B). Increasing the surface size and the density of the 300 grid of electrodes revealed smaller and deeper motor units, with averaged territories radius of 0.165 and 301 0.149 mm with grids of 14.4 and 36 cm², respectively, and an IED of 2 mm (Figure 2C). The average 302 303 distance of identifiable motor units from the skin increased with the surface size of the grid (Figure 2D; 15.7 ± 0.1 mm vs. 17.3 ± 0.1 mm with grids of 14.4 and 36 mm², respectively), but not with the IED of 304 the grids (Figure 2D; 16.4 ± 0.6 mm vs. 16.3 ± 0.8 mm with an IED of 36 and 2 mm, respectively). 305

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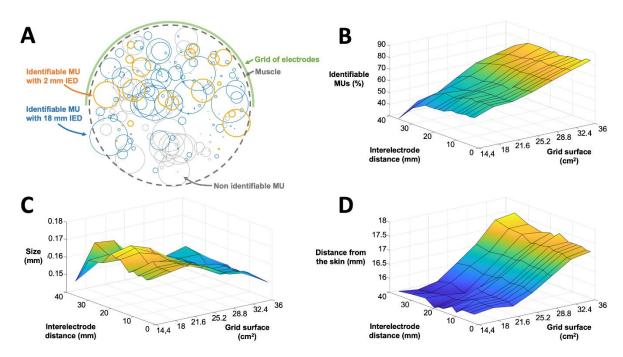




Figure 2: Results from the 200 simulated motor units with 84 configurations of grids of electrodes. (A)
Each circle represents a motor unit territory, the dash line being the muscle boundary. Blues circles are the
identifiable motor units with a grid of 21.6 cm² and an interelectrode distance (IED) of 18 mm, while the
orange circles are the motor units revealed with a grid of 21.6 cm² and an IED of 2mm. Grey circles
represent the non-identifiable motor units. The percentage of identifiable motor units (B), the size of their
territory (C) and their distance from the skin (D) are reported for the 84 configurations.

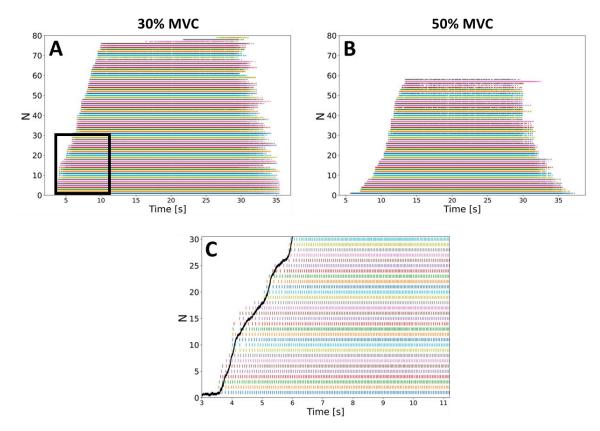
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316 Laboratory study - grids of 256 electrodes

317 <u>Number of identified motor units</u>

The motor unit spike trains identified across all conditions, intensities, and participants were visually 318 319 checked and carefully edited when a missing spike or an identified artifact were observed. The highest number of identified motor units was systematically reached with the separate decomposition of the four 320 321 grids of 64 electrodes with an IED of 4 mm, resulting in 56 ± 14 motor units (PNR = 34.2 ± 1.1) and 45 \pm 10 motor units (PNR = 34.0 \pm 0.9) for 30% and 50% MVC, respectively (Figure 3). At least 82% of 322 the motor units identified in one condition were also identified in the conditions involving a higher 323 324 number of electrodes. Similarly, 91% to 100% of the motor units identified in one condition were also 325 identified with the 256-electrode configuration (4-mm IED, 36-cm² size, Figure 1A) when the four grids 326 were decomposed separately.



327

Figure 3: Maximum numbers of motor unit spike trains identified in one participant (S1) at 30% (A) and 50% MVC (B), 79 and 58 motor units (PNR > 28 dB) respectively, obtained when the four grids of 64 electrodes (4 mm IED) were decomposed separately. (C) The pulse trains of the 30 motor units of lowest recruitment threshold identified at 30% MVC (black box in A) are reproduced during the ascending ramp of force (black curve).

333

When considering the effect of electrode density (grid size fixed at 32-36 cm², Figure 1A-D), we found the lowest number *N* of motor units with the 16-mm IED, identifying 3 ± 1 motor units and 2 ± 1 motor units at 30% and 50% MVC, respectively (Figure 4A, C). Additional motor units were then gradually identified with greater electrode densities. The highest number of motor units was observed with the highest density (4-mm IED), respectively identifying 56 ± 14 or 43 ± 11 motor units and 45 ± 10 or 25 ± 6 motor units at 30% and 50% MVC, and this with the 4×64 or 256-electrode decomposition procedure (Figure 4A, C). Finally, we found a decreasing logarithmic relationship between the average normalized

- number \overline{N} of motor units for each participant and the IED, with $r^2 = 1.0$ (p = 2.5 $\cdot 10^{-5}$) and $r^2 = 0.99$ (p =
- 342 0.001) at 30% and 50% MVC, respectively (Figure 4B, D).
- When considering the effect of the size of the grid (IED fixed at 4 mm, Figure 1A, E-G), we found the 343 lowest number N of motor units with a grid of 2 cm^2 , identifying 4 ± 2 motor units and 4 ± 2 motor units 344 at 30% and 50% MVC, respectively (Figure 5A, C). Additional motor units were then gradually 345 identified with larger grid sizes. The highest number of motor units was observed with a grid of 36 cm², 346 347 respectively identifying 56 ± 14 or 43 ± 11 motor units and 45 ± 10 or 25 ± 6 motor units at 30% and 50% MVC, depending on the decomposition procedure (Figure 5A, C). We also found an increasing 348 logarithmic relationship between the average normalized number \overline{N} of motor units for each participant 349 and the size of the grid, with $r^2 = 0.99$ (p = 3.0·10⁻⁴) and $r^2 = 0.98$ (p = 0.001) at 30% and 50% MVC, 350 351 respectively (Figure 5B, D). It is noteworthy that, in both density and size cases, the parameters of the
- 352 fits were very similar for 30% and 50% MVC.
- As both the density and the size of the grids determine the number of electrodes, we finally fitted the
- relationship between the normalized number of motor units \overline{N} and the number of electrodes. As observed
- previously, more motor units were identified with a larger number of electrodes, following a logarithmic
- tendency with $r^2 = 0.98$ (p = 0.018) and $r^2 = 0.95$ (p = 0.016) at 30% and 50% MVC, respectively (Figure
- 357 6). A plateau should theoretically be reached with highly populated grids of 1024 and 4096 electrodes
- (36-cm² grids with 2-mm and 1-mm IED, respectively), with a prediction of 50% and 90% of additional
- 359 motor units identified.
- 360 For a fixed number of electrodes, it is noteworthy that grid size and density, although linked, may have
- different impact on the number of identified motor units (black crosses in Figure 6). For example, 1.25
- times more motor units were obtained with the 64-electrode condition (32 cm^2 , 8-mm IED, Figure 1B)
- than with the 63-electrode condition (7.7 cm^2 , 4-mm IED, Figure 1E) for the group of participants at
- 364 30% MVC.

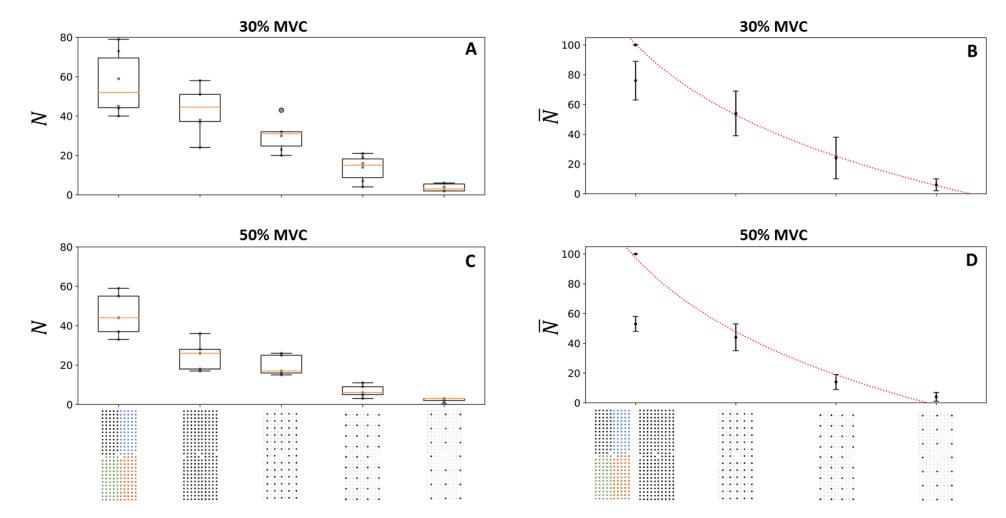


Figure 4: Effect of the electrode density on the number *N* of identified motor units at 30% (A, B) and 50% MVC (C, D). The boxplots in the left column report the absolute number *N* of identified motor units per participant (grey dots) and the median (orange line), quartiles, and 95%-range across participants. In the right column, the normalized number of motor units \overline{N} logarithmically decreases with interelectrode distance *d* (4, 8, 12, and 16mm in abscissa) as $\overline{N} = 195 - 68 \log(d)$ ($r^2 = 1.0, p = 2.5 \cdot 10^{-5}$) at 30% MVC (B) and $\overline{N} = 196 - 71 \log(d)$ ($r^2 = 0.99, p = 0.001$) at 50% MVC (D). The standard deviation of \overline{N} across subjects is displayed with vertical bars. Two decomposition procedures were considered for the 256-electrode condition; the grid of 256 black electrodes indicates that the 256 signals were simultaneously decomposed and systematically returned lower \overline{N} results than when the grid was decomposed as four subsets of 64 electrodes. To maintain consistency with the computational study, the trendlines were here fitted with the 4*64 condition that returned the higher number of identified motor units (see Supplementary Material A for the other fitting condition).

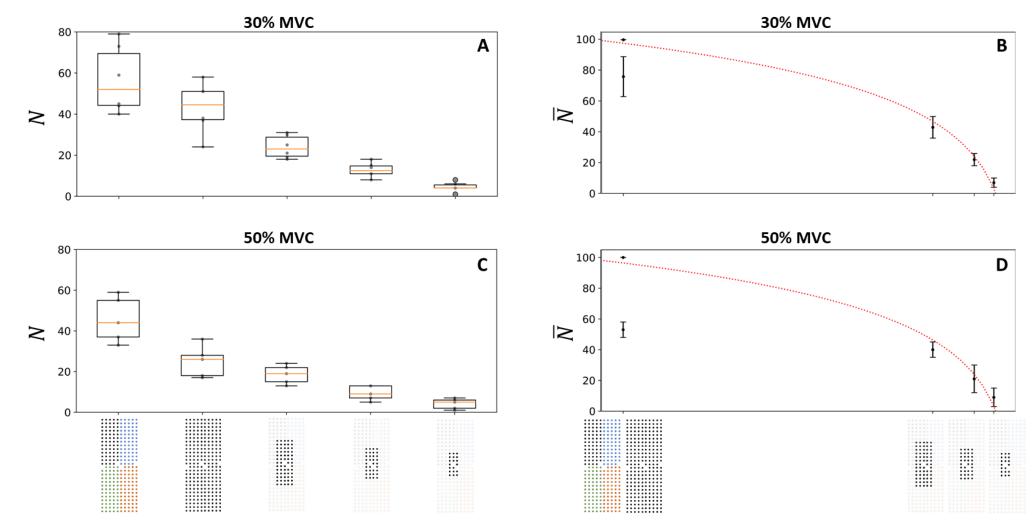
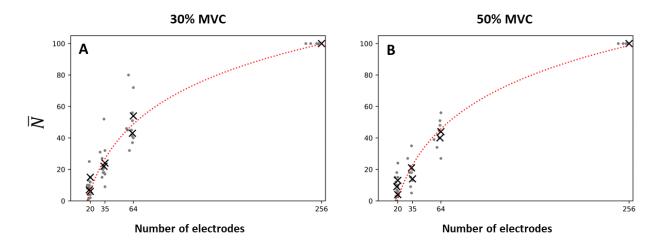


Figure 5: Effect of the size of the grid on the number *N* of identified motor units at 30% (A, B) and 50% MVC (C, D). The boxplots in the left column report the absolute number *N* of identified motor units per participant (grey dots) and the median (orange line), quartiles, and 95%-range across participants. In the right column, the normalized number of motor units \overline{N} logarithmically decreases with the size of the grid s (2, 3.8, 7.7, and 36 cm² in abscissa) as $\overline{N} = -20 + 33 \log(s)$ ($r^2 = 0.99, p = 3.0 \cdot 10^{-4}$) at 30% MVC (B), and $\overline{N} = -19 + 32 \log(s)$ ($r^2 = 0.98, p = 0.001$) at 50% MVC (D). The standard deviation of \overline{N} across subjects is displayed with vertical bars. Two decomposition procedures were considered for the 256-electrode condition; the grid of 256 black electrodes indicates that the 256 signals were simultaneously decomposed and systematically returned lower \overline{N} results than when the grid was decomposed as four subsets of 64 electrodes. To maintain consistency with the computational study, the trendlines were here fitted with the 4*64 condition that returned the higher number of identified motor units (see Supplementary Material A for the other fitting condition).



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Figure 6: Effect of the number n of electrodes on the normalized number \overline{N} of identified motor units at 384 385 30% (A) and 50% MVC (B). The discrete results per participant are displayed with grey data points. The average \overline{N} values across participants per condition are displayed with black crosses. Weighted logarithmic 386 trendlines were fitted to the data and returned (A) $\overline{N} = -104 + 37 \log(n)$ ($r^2 = 0.98, p = 0.018$), and 387 (B) $\overline{N} = -113 + 38 \log(n)$ ($r^2 = 0.95$, p = 0.016). Two decomposition procedures were considered for 388 the 256-electrode condition; the grid of 256 black electrodes indicates that the 256 signals were 389 simultaneously decomposed and systematically returned lower \overline{N} results than when the grid was 390 391 decomposed as four subsets of 64 electrodes. To maintain consistency with the computational study, the 392 trendlines were here fitted with the 4*64 condition that returned the higher number of identified motor units 393 (see Supplementary Material A for the other fitting condition).

394 <u>Characteristics of identified motor units</u>

Figure 7A shows the effect of the grid density on the type (small/large) of identified motor units at 30% 395 MVC, with a percentage of identified 'small' motor units increasing from $11 \pm 9\%$, with a 12-mm IED, 396 to $29 \pm 14\%$, with a 4-mm IED. Such differences were not observed at 50% MVC, where the percentage 397 398 of 'small' motor units remained below 10% for all conditions (Figure 7C). Contrary to the density, the size of the grid did not impact the distribution of the type of identified motor units, with the percentage 399 400 of 'small' motor units ranging from 20 to 29% across all grid sizes (Figure 7B). Again, small motor units represented less than 10% of the identified motor units at 50% MVC for all the size conditions 401 402 (Figure 7D).

403 To support the above observations made at 30% MVC, grids involving the same number of electrodes 404 but of different grid density and size were directly compared. 62% of the motor units identified with the 405 64-electrode (32 cm^2 , IED 8 mm) and 63-electrode (7.7 cm^2 , IED 4 mm) conditions were identified by 406 both grids at 30%. $28 \pm 9\%$ of the remaining motor units specific to the 8-mm IED grid were 'small', 407 while $44 \pm 11\%$ of the motor units specific to the 4-mm IED condition were 'small'. Similar results were 408 obtained with the 35- (36 cm^2 , 12-mm IED) and 34-electrode conditions (3.6 cm^2 , 4-mm IED), where 409 more 'small' motor units were specifically identified with denser rather than larger grids.

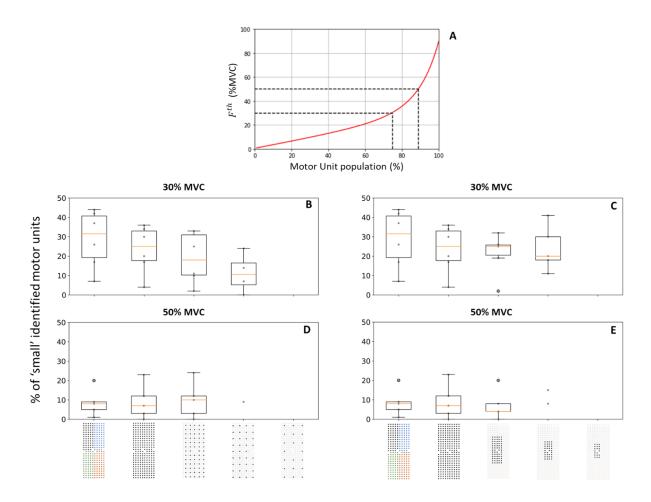


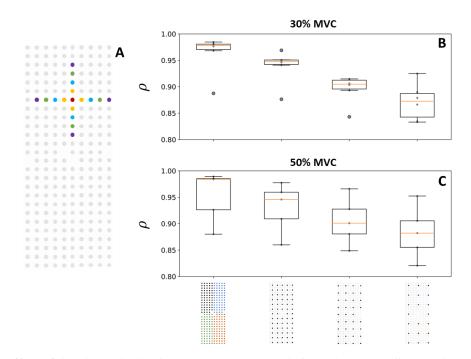
Figure 7: (A) Typical frequency distribution of motor unit force recruitment thresholds in a human TA
motor unit pool ranked in ascending order of force recruitment thresholds according to the Methods. The
black dashed lines identify the theoretical portions of the population recruited at 30% and 50% MVC.
Effect of the grid density (B, D) and grid size (C, E) on the percentage of 'small' motor units identified at
30% (B, C) and 50% MVC (D, E). The boxplots report the results per participant (grey dots) and the
median (orange line), quartiles, and 95%-range across participants.

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410

418 <u>Correlation between MUAPs from adjacent electrodes</u>

Figure 8 reports the effect of electrode density on the level of MUAP correlation ρ between adjacent electrodes for the six participants. The lowest average correlation coefficient ρ calculated between the MUAP with the highest peak to peak amplitude and the MUAPs identified over adjacent electrodes was observed with an IED of 16 mm ($\rho = 0.87 \pm 0.03$ and $\rho = 0.88 \pm 0.04$ at 30% and 50% MVC, respectively). The level of correlation increased with reduced IED (Figure 8B, C), with $\rho = 0.96 \pm 0.04$ and $\rho = 0.95 \pm 0.05$ between the MUAPs from adjacent electrodes with a 4-mm IED at 30% and 50% MVC, respectively.

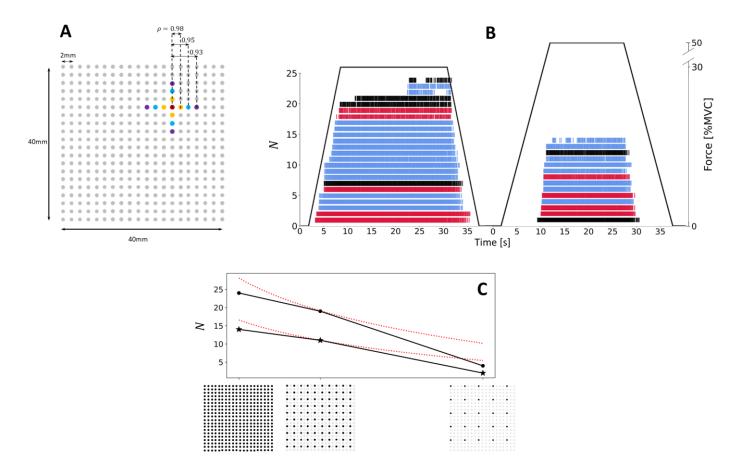


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427Figure 8: Effect of the electrode density on the MUAP correlation ρ between adjacent electrodes (A) at42830% (B) and 50% MVC (C). The MUAP shape identified over the red electrode was compared to those429identified over the four adjacent electrodes located at 4 (orange), 8 (blue), 12 (green) and 16 (purple) mm430IED (A). The boxplots report the correlation coefficient ρ per participant (grey dots) and the median431(orange line), quartiles, and 95%-range across participants.432

433 Laboratory study with an ultra-dense grid of 400 electrodes

434 Maximal N of 24 and 14 motor units (PNR > 28 dB) were identified with the ultra-dense grid of 400 electrodes for one participant at 30% and 50% MVC, respectively (Figure 9A), when 8 overlapping 435 subsets of 64 electrodes were decomposed separately. These numbers of units are consistent with the 436 437 40×40 mm size of the ultra-dense grid and the results in Figure 5, considering that dry electrodes were used in the second experimental session. Moreover, also consistent with the previous findings, fewer 438 units were identified when the electrode density decreased, with 19 and 4 motor units identified with a 439 4- and 8-mm IED at 30% MVC, respectively, and with 9 and 5 motor units identified with a 4- and 8-440 441 mm IED at 50% MVC, respectively. Although N increased between a 4- and 2-mm IED, with five and 442 four new motor units identified at 30% and 50% MVC respectively (red pulse trains in Figure 9B), the rate of increase of N with electrode density was lower than previously expected (Figure 9C). As 443 previously observed, the correlation between adjacent MUAPs increased from $\rho = 0.93$ with an 8-mm 444 IED to $\rho = 0.98$ with a 2-mm IED at 30% MVC, and from $\rho = 0.87$ with an 8-mm IED to $\rho = 0.94$ with 445 a 2-mm IED at 50% MVC (Figure 9A). All the motor units identified with the 8-mm and 4-mm IED 446 447 were also identified with the 4 mm and 2-mm IED grids, respectively. Finally, small motor units were identified when increasing the density from a 8- to 4-mm IED (blue vs black trains in Figure 9B), while 448 most of the smallest units were identified with an IED of 2 mm (red trains in Figure 9B). 449



450

451 Figure 9: Results for the ultra-dense grid (2 mm IED, 40x40 mm, 400 electrodes). (A) Description of the ultra-dense grid (electrodes represented with grey circles). In average 452 across the 24 identified MUs, the correlation between the MUAPs at a 2 mm (orange), 4 mm (blue), and 8 mm (purple) IED and the MUAP with the highest peak-to-peak amplitude (red) reached $\rho = 0.98$, 0.95, and 0.93 at 30% MVC, respectively, and 0.94, 0.91, and 0.87 at 50% MVC, respectively. (B) Identified spike trains at 30% (left) and 453 50% MVC (right). The dark spike trains were identified with an 8 mm IED, the blue trains were additionally identified with the 4 mm IED, and the red trains were identified 454 with 2 mm IED. All the spike trains identified with one grid were also identified with the denser grids. (C) Effect of electrode density on the number of identified motor units 455 456 at 30% (dots) and 50% MVC (stars). The trendlines from the density analysis in Figure 4B, D computed with the grids of 256 electrodes are also reported (red dotted lines). 457 To maintain consistency with the previous computational and laboratory results, the grid was decomposed as eight partially overlapping subsets of 64 electrodes, as explained in the Methods, to investigate the maximum number of identifiable motor units in this configuration. 458

459 **Discussion**

This study systematically investigated how the design of surface grids of EMG electrodes (grid size and 460 461 electrode density) impacts the number and the size of the motor units identified with HD-EMG 462 decomposition. Using a combination of computational and experimental approaches, we found that 463 larger and denser grids of electrodes than conventionally used reveal a larger sample of motor units. As 464 those units not identifiable with less dense and smaller grids mostly have a low recruitment threshold, 465 we conclude that denser grids allow the identification of smaller motor units. This is possible because 466 of a better spatial sampling of the MUAP distribution over the skin surface that resulted in a better 467 discrimination among action potentials of different motor units. These results clarify the directions for 468 designing new surface grids of electrodes that could span across the entire surface of the muscle of interest while keeping a high density of electrodes, with IED as low as 2-4 mm. Identifying large sets of 469 470 small and large motor units is relevant in many research areas related to motor control, such as the 471 investigation of neural synergies (Hug et al., 2022), neuromuscular modelling (Caillet et al., 2022c), or 472 human-machine interfacing (Farina et al., 2021).

473

474 The number N of identified motor units increased across participants with the density of electrodes (Figure 4; Figure 8C), the size of the grid (Figure 5), and the number of electrodes (Figure 6). On 475 476 average, 30 and 19 motor units were identified with the 'conventional' 64-electrode grid (8-mm IED, 32 cm² surface area) at 30% and 50% MVC, respectively, which is consistent with several previous 477 studies using similar grid designs (Del Vecchio et al., 2020). By increasing the density of electrodes and 478 479 size of the grid to arrive to 256 electrodes separated by a 4 mm IED, we identified on average 56 and 45 480 motor units at 30% and 50% MVC, respectively. We even reached 79 and 59 motor units for one subject 481 (Figure 3), which is substantially more than the numbers of units usually reported in the HD-EMG 482 literature, and twice those obtained with grids of 64 electrodes in this study. Our computational and 483 experimental results showed that the size of the grid is a key factor contributing to the higher number of identified motor units (Figure 2B; Figure 5). According to our simulations, increasing the size of the 484 grid increases the number of identifiable motor units, i.e., the number of motor units with unique sets of 485 486 MUAPs across electrodes (Figure 2B). We concluded from the simulation that the differences between 487 MUAPs result from the anatomical and physiological differences between adjacent motor units, such as the length of their fibres, the spread of the end plates, or their conduction velocity, as well as from the 488 differences in the tissues interposed between the fibres and each recording electrode (Farina et al., 2004). 489 490 Larger grids better sample these differences across electrodes, revealing the unique shapes of each motor 491 unit (Farina et al., 2008). The density of electrodes was also found to be a critical factor contributing to increasing the number of identified motor units (Figure 4; Figure 9C). Dense grids especially contribute 492 to identifying the small motor units (Figure 7B; Figure 9B), defined in this study according to their 493

recruitment threshold (Figure 7A) (Henneman and Mendell, 1981; Caillet et al., 2022b). Classically, the 494 495 decomposition algorithms tend to converge towards the large and superficial motor units that contribute 496 to most of the energy of the EMG signals (Farina and Holobar, 2016). Conversely, action potentials of 497 the smallest motor units tend to have lower energy and are masked by the potentials of the larger units. 498 These factors explain the lowest representation of small low-threshold motor units in available HD-499 EMG datasets (Caillet et al., 2022a). Increasing the density of electrodes would therefore enable to better 500 sample the action potentials of these small motor units across multiple electrodes, enabling their 501 identification. We however observed that increasing the electrode density did not reveal small motor 502 units anymore during high-force muscle contractions (Figure 7D), potentially because of the large energy 503 of the recorded MUAPs from the large motor units recruited between 30% and 50% MVC. We also 504 showed in one subject that computationally increasing the density of electrodes by spatially resampling 505 the experimental EMG signals (Supplementary Material B) did not reveal any previously hidden motor 506 units.

507

The number of identified motor units N monotonically increased with the density of electrodes (Figure 508 4BD), the size of the grid (Figure 5BD) and the number of electrodes (Figure 6), following significant 509 510 logarithmic trendlines. Remarkably, very similar logarithmic tendencies were obtained at both 30% and 511 50% MVC in all the analyses. Altogether, these trendlines suggested that the normalized number of 512 identified motor units \overline{N} would grow with an electrode density beyond a 4-mm IED, before reaching a 513 plateau for IEDs of 1-2 mm. We experimentally tested this hypothesis by designing a new grid of 400 514 dry electrodes separated by an IED of 2 mm. While more motor units were identified at 2 mm than 4 mm IED, as expected, the rate of increase between 4-mm and 2-mm IED was lower than predicted by 515 516 the trendlines (Figure 9C). We explained this result by demonstrating that the level of correlation 517 between MUAPs identified over adjacent electrodes, which was >0.95 at both contraction levels with 4mm IED (Figure 8), tended to 1 with further increasing electrode density (Figure 9A). Therefore, the 518 519 high level of information shared between adjacent electrodes in ultra-dense grids (IED < 2 mm) limits 520 the percentage of identifiable motor units (Farina and Holobar, 2016). According to these results, we consider that optimal designs of surface grids of electrodes for identifying individual motor units would 521 522 involve a surface that cover the muscle of interest with an IED of 2 to 4 mm, depending on the size of 523 the muscle. It cannot be excluded, however, that the high correlation between adjacent electrodes with 524 a 2-mm IED was partly due to the grid design and can be improved by reducing the electric crosstalk 525 between electrodes, e.g., by reducing the electrode area.

526

Another important factor for the identification of individual motor units is the quality of the identified
pulse trains, estimated by the PNR (Holobar et al., 2014) or the silhouette value. In this study, we showed

529 that the quality of the identified motor units (i.e., decomposition accuracy) increased when increasing 530 the density of electrodes or the size of the grid, with PNR reaching on average 37-38 dB across 531 participants with the grid of 256 electrodes (Supplementary Material C). A greater average PNR implies 532 the need of less manual editing following the automatic decomposition (Hug et al., 2021b). The better 533 spike train estimate depends on the better signal to noise ratio following the inversion of the mixing 534 matrix since the pulse train of each motor unit is computed by projecting the extended, whitehed signals 535 on the separation vector (Holobar and Farina, 2014; Farina and Holobar, 2016; Negro et al., 2016). 536 Likewise, the PNR substantially increased after we computationally increased the number of electrodes 537 by spatially resampling the EMG signals. This practical result is of interest for most of the physiological 538 studies that require a lengthy processing time to visually check and manually correct the pulse trains of 539 all the motor units (Hug et al., 2021b).

540 Finally, by independently decomposing subsets of 64 electrodes, we increased both the total number and the percentage of small motor units identified from highly populated grids of 256 electrodes, compared 541 to the simultaneous decomposition of all available observations (Figure 7B, C). This was likely due to 542 543 the lower ratio of large motor units sampled by each subset of electrodes, allowing the algorithm to 544 converge to smaller motor units that contributed to the signal (Figure 7B, C). According to 545 Supplementary Material A, the plateauing behaviour previously observed in Figure 4 to Figure 6 is expected to be more pronounced when all the available signals are simultaneously decomposed. It 546 547 should however be noted that the simulation results were obtained independently of a specific 548 decomposition algorithm, as previously proposed by Farina et al (2008). On the other hand, the 549 experimental results are based on a specific algorithm. Interestingly, however, the simulation and 550 laboratory results were fully consistent and in agreement, indicating that the difference in shape of the spatially sampled MUAPs is the main factor influencing EMG decomposition. 551

552

553 <u>Conclusion</u>

554 By increasing the density and the number of electrodes, and the size of the grids, we increased the 555 number of identifiable and experimentally identified motor units. The identified motor units had pulse trains with high PNR, limiting the manual processing time. Moreover, we identified a higher percentage 556 557 of small motor units, which are classically filtered out with the current conventional grid designs. In this 558 way, a maximum of 79 motor units (PNR > 28 dB; mean: 36 dB), including 40% of small motor units, 559 were identified, which is a substantially greater sample than previously shown with smaller and less 560 dense grids. From these results, we encourage researchers to develop and apply larger and denser EMG 561 grids to cover the full muscle of interest with IEDs as small as 2 mm. This approach increases the sample 562 of motor units that can be experimentally investigated with non-invasive techniques.

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