Auxin-mediated stress relaxation in pericycle and endoderm remodelling drive lateral root initiation

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Plant development relies on the precise coordination of cell growth, which is influenced by the mechanical constraints imposed by rigid cell walls. The hormone auxin plays a crucial role in regulating this growth by altering the mechanical properties of cell walls. During the post-embryonic formation of lateral roots, pericycle cells deep within the main root are triggered by auxin to resume growth and divide to form a new root. This growth involves a complex interplay between auxin, growth, and the resolution of mechanical conflicts with the overlying endodermis. However, the exact mechanisms by which this coordination is achieved are still unknown. Here, we propose a model that integrates tissue mechanics and auxin transport, revealing a connection between the auxin-induced relaxation of mechanical stress in the pericycle and auxin signalling in the endodermis. We show that the endodermis initially limits the growth of pericycle cells, resulting in a modest initial expansion. However, the associated stress relaxation is sufficient to redirect auxin to the overlying endodermis, which then actively accommodates the growth, allowing for the subsequent development of the lateral root. Our model uncovers that increased pericycle turgor and decreased endodermal resistance licence expansion of the pericycle and how the topology of the endodermis influences the formation of the new root. These findings highlight the interconnected relationship between mechanics and auxin flow during lateral root initiation, emphasizing the vital role of the endodermis in shaping root development through mechanotransduction and auxin signalling.

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Introduction

The rigidity of plant cell walls imposes precise coordination of growth among cells, where spatial variations in growth generate mechanical stresses serving as instructive cues. This feedback mechanism links tissue geometry to gene expression (1, 2). Auxin, a pivotal plant hormone involved in cell growth and differentiation (3–9), plays a central role in growth regulation by modifying cell wall properties (10, 11). Its distribution relies on polar transport regulated by influx and efflux carriers (12–14). Efflux carrier polarization, particularly the PIN protein family, directs auxin flow, regulating plant growth and development (15–17). In the shoot meristem, PIN proteins have also been found to possess mechanical-sensing properties (18, 19), contributing to the complex interplay between auxin-mediated cell wall soft-ening, tissue mechanics, and PIN-mediated auxin transport, ultimately shaping developmental auxin patterns (18, 20). Specifically, efflux carrier distribution correlates with the microtubule orientation and both are affected by stress orientation.

A prime example of coordinated cell and tissue growth is the formation of lateral roots (LRs) (21–23). In *Arabidopsis thaliana*, LRs originate from pericycle cells beneath the endodermis (24, 25). These Xylem pole pericycle (XPP) cells, typically in pairs, become activated through auxin accumulation, driven by local synthesis (26), lateral auxin diversion (27–29), and endodermal-to-pericycle auxin reflux (30) (Fig. 1 A). Activated XPP cells expand radially, pressing against the overlying endodermis (31). Nuclei migrate, triggering asymmetric cell division and lateral root primordium formation (21, 23, 32). Notably, this radial expansion is more pronounced at shared cell walls (31, 33), necessitating cortical microtubule (CMT) rearrangements in founder cells (33). Reciprocal auxin flows between the endodermis and the pericycle, accompanying lateral root initiation. Just before the founder cell radial expansion, active auxin transport via PIN3 from the endodermis to the pericycle aids accumulation in the founder cells (30). Upon radial expansion, the change in endodermis shape depends on auxin signalling in the endodermis, which implies auxin accumulation in the endodermis (31, 34). It is unknown whether this auxin originates from the pericycle and is part of the signal instructing the endodermis of the growth of the pericycle. It is also unknown which modification(s) of the mechanical properties of the pericycle and/or endodermis, such as turgor difference, licences the radial expansion.

Here, building on the conceptual framework established in the shoot apical meristem, we model the interplay between growth mechanics and auxin flow during LR initiation (Fig. 1 B). Our model combines a vertex model for tissue mechanics and a compartment model for auxin transport (20). The growth of the shared anticlinal wall between adjacent XPP cells is constrained, allowing only modest radial swelling. However, auxin-induced stress relaxation in this wall relocates auxin efflux carriers to the periclinal walls, redirecting auxin flow to the endodermis and triggering an auxin-dependent response. Empirical observations support this prediction. Furthermore, we demonstrate that endodermal wall properties and arrangement limit the radial expansion of ac-

Fig. 1. Biological context and modelling framework (A) Activation of pericycle (p) before lateral root initiation results from the accumulation of auxin in these cells by local auxin synthesis, redirection of the rootward auxin flow in the vasculature (v) and from the endodermis (en). Upon activation, the pericycle cells with high auxin acquire a trapezoidal shape, and the endodermis accommodates this morphological change by shrinking. This accommodation of the endodermis requires the endodermis cells to perceive auxin. The diagram visualises the cellular template used in our mechanical vertex model, including the cortex (c) and epidermis (ep). (B) Diagram of an Arabidopsis seedling showing the location (arrow) we model here. (C) The interplay between auxin accumulation and cell wall mechanics: Auxin induces growth by altering the properties of the cell wall, which modifies the patterns of mechanical stress. Efflux carriers of auxin respond to mechanical stress perturbations, creating a mechanical feedback loop that affects the auxin concentration and flow pattern. (D) In our model, cell-cell interfaces in their entirety, including primary and secondary cell walls, membrane and middle lamella, are modelled as viscous rods that resist longitudinal deformations with an elastic modulus, E, and bending at the junctions with bending modulus k_b. Turgor, T, generates stresses to which the walls respond by growing according to the extensibility, φ, of the respective viscous rod. (E) Lattice used for simulations. The left-most vertices form a boundary representing the inside of the root, and the right-most vertices define the plant's boundary, which faces a container of lower pressure. The inner-most vertices can only move parallel to this boundary, whereas the vertices on the outer boundary are free to move in general (lower zoom in, red arrows). On the upper and lower boundaries, we emulate the effects of having neighbours pushing back against the tissue with the same constraints, leading only to horizontal displacements and resulting in vertical confinement (upper zoom in, red arrows). From the pericycle layer, two cells are selected as primed (lower zoom-in, grey). Auxin is reflected at the boundaries (blue arrows). (F) After a few iterations, depletion around the primed cells is visible, and auxin progressively accumulates in the two primed XPP cells. Most efflux carriers bind from one cell to the other. (G) Schematic of the order of operations during a time step of our model along with the inputs and outputs of each major section. (H, I, J) Experimental results of bound carriers during stage 0 LR initiation (arrowhead denotes the shared wall between activated XPP cells). (H) The influx carrier AUX1 is predominantly expressed in these two cells. (I, J) Efflux carriers are only detected in and around the primed XPP cells and the vasculature. Scale bar: 20 μm.

tivated XPP cells. These findings propose a biphasic radial growth model for activated XPP cells, initially constrained by the endodermis, enabling auxin redirection to the endodermis. This, in turn, triggers an auxin-dependent response, facilitating radial expansion of activated XPP cells.

Materials and Methods

We previously developed a two-dimensional vertex model that integrates a compartment model for auxin transport to explore the interaction between tissue mechanics and auxin patterns (20). This approach is similar to previous works on plant tissue mechanics using mass-spring models (35, 36), yet within a vertex model framework (37–39), and auxin transport models employed to study phyllotaxis (16, 18, 40, 41). Additionally, the viscous stress-based growth of cell walls is modelled similarly to (42, 43). Here, we describe the model used and its implementation. The symbols used are described upon their usage and in Table 1. For a more detailed and formal version, refer to the Supporting Material.

Vertex model describes tissue mechanics. Cells are subject to hydrostatic pressure, and the interfaces between them exhibit resistance to compression, extension, and resistance to bending at junctions (Fig. 1 C). We minimize the total mechanical energy of the tissue, $\mathcal{H}^{\text{mech}}$, decomposed as:

$$\mathcal{H}^{\text{mech}} = \mathcal{H}^{\text{elastic}} + \mathcal{H}^{\text{bending}} + \mathcal{H}^{\text{pressure}}, \quad (1)$$

where $\mathcal{H}^{\text{elastic}}$ represents the energy cost of longitudinal deformation (extension or compression) of the interface between cells, $\mathcal{H}^{\text{bending}}$ the energy cost of changing the internal angle of the cell at one of its junctions, and $\mathcal{H}^{\text{pressure}}$ the work done by cell turgor.

We describe the deformation of the interface by a simple elastic term of an elastic rigid one-dimensional rod as if it were a wall, similar to (35, 36). Here, the term wall refers to these rods as a proxy for the cell-cell interface, including primary and secondary cell walls, membrane and middle lamella. The total elastic energy, $\mathcal{H}^{\text{elastic}}$, is the sum over all individual cell walls, each contributing the quantity

$$\mathcal{H}^{\text{elastic}}_{\text{wall}} = \frac{hwl_0}{2} E_{\text{wall}} \left(\frac{l - l_0}{l_0} \right)^2, \quad (2)$$

where h and w denote the height and width, l_0 the rest length, l the current length, and E_{wall} the elastic modulus of the wall element in question. Note, the elastic modulus of a wall, E_{wall}, will be a function of the auxin content of the surrounding cells.

We base our approach to wall bending energy on models often employed in the field of polymer physics (44–46) and assign a cost to change the angle, θ, concerning its rest value, θ_0. Then, we account for each junction of each cell for the bending contribution to the mechanical energy,

$$\mathcal{H}^{\text{bending}}_{\text{cell, junction}} = 2k_{b\text{cell}} \frac{1 - \cos(\theta - \theta_0)}{l + l'}, \quad (3)$$

where l and l' are the lengths of the walls whose intersection forms the junction in question, and $k_{b\text{cell}}$ the bending modulus of the cell whose internal angle we are measuring. This allows us to readily assign a bending modulus following the cell's internal processes and implicitly couple the contribution of several cells surrounding a particular junction.

The final term in Eq. 1 represents the effect of cell turgor, summed over all cells T_{cell}. The work of internal hydrostatic pressure per cell of area, A, contributes

$$\mathcal{H}^{\text{pressure}}_{\text{cell}} = -AT_{\text{cell}}. \quad (4)$$

Therefore, given a set of rest lengths, rest angles, cell elastic moduli, bending moduli, and turgor pressures, we can compute the mechanical energy for a configuration of the tissue and by minimising the mechanical energy for the junction positions, we obtain the tissue configuration balancing all forces arising from the competing elastic, bending and pressure contributions.

Growth as a viscous wall response. Cell walls grow when under positive strain/stress (47, 48). To model this behaviour, we describe the cell wall as a Maxwell material similar to (42, 47), by taking irreversible deformation into account. Because of how we discretize the system, we opt for the approach of Corson et al. (42). We incorporate cell wall growth into our model by defining the rate of change of the rest length, l_0, of a particular wall with length l, elastic modulus E_{wall}, and extensibility φ_{wall} (here defined as the reciprocal of viscosity) as

$$\frac{1}{l_0} \frac{dl_0}{dt} = \varphi_{\text{wall}} \sigma_{\text{wall}} = \varphi_{\text{wall}} E_{\text{wall}} \frac{l - l_0}{l_0}, \sigma_{\text{wall}} > 0 \quad (5)$$

Table 1. List of Symbols

Symbol		Meaning
$\mathcal{H}^{\text{mech}}$	-	Total mechanical energy
$\mathcal{H}^{\text{elastic}}$	-	Total elastic energy
$\mathcal{H}^{\text{bending}}$	-	Total bending energy
$\mathcal{H}^{\text{pressure}}$	-	Total work exerted by turgor
$\mathcal{H}^{\text{elastic}}_{\text{wall}}$		Elastic energy of a single *wall*
l, l'	-	Current wall length
l_0	-	Wall target length
E_{wall}	-	*Wall* elastic modulus
h	-	Wall height
w	-	Wall width
$\mathcal{H}^{\text{bending}}_{\text{cell, junction}}$	-	Bending energy of *junction* of *cell*
θ	-	Current junction angle
θ_0	-	Target junction angle
$k_{b\,\text{cell}}$	-	Bending modulus of *cell*
A	-	Area of a cell
T_{cell}	-	*Cell* turgor
φ_{wall}	-	*Wall* extensibility
σ_{wall}	-	*Wall* stress
E_{cell}	-	Elastic modulus of *cell*
φ_{cell}	-	Extensibility of *cell*
a_{cell}	-	Auxin concentration of *cell*
$\Omega_{\text{cell}\vert\text{other}}$	-	$l_{\text{cell}\vert\text{other}}/A_{\text{cell}}$
D	-	Diffusion strength
P	-	Efflux carrier strength
Q	-	Influx carrier strength
$p_{\text{cell}\vert\text{other}}$	-	Density of efflux carriers bound to membrane of *cell* facing *other*
$q_{\text{cell}\vert\text{other}}$	-	Density of influx carriers bound to membrane of *cell* facing *other*
K_{efflux}	-	Saturation constant of efflux carriers
K_{influx}	-	Saturation constant of influx carriers
$\sigma_{\text{cell}\vert\text{other}}$	-	Stress of wall separating *cell* and *other* as perceived by *cell*
L_{cell}	-	Perimeter of *cell*
η	-	Mechanical feedback coupling constant
E_0	-	Base elastic modulus
r	-	Ratio of highest and lowest possible elastic moduli

where σ_{wall} represents the longitudinal stress acting on the wall (Fig. S1 A). As mentioned before, the properties of each wall are a function of the processes taking place inside the surrounding cells. Therefore, we want to link the quantities E_{wall} and φ_{wall} to cell-specific counterparts, E_{cell} and φ_{cell}. In a similar approach to (35), we associate elastic elements in parallel, resulting in E_{wall} being the average of E_{cell} of the two surrounding cells (Fig. S1 B). We also associate the viscous elements in parallel, assuming each viscous element is affected by the same stress as the corresponding elastic element (Fig. S1 B). If wall A|B separates cells A and B,

then we obtain

$$\varphi_{\text{A}\vert\text{B}} = \frac{2\varphi_{\text{A}}\varphi_{\text{B}}}{\varphi_{\text{A}} + \varphi_{\text{B}}}. \tag{6}$$

Interestingly, this coupling implies that extensibility, and, therefore, growth rate, is limited by the least extensible wall. This result can be obtained by inspecting the limit $\varphi_A \gg \varphi_B$. If the extensibilities are the same between the two cells, then so is the extensibility of the wall. Also, keeping a Maxwell material's overall constitutive relation allows us to keep a single value of rest length, l_0.

Auxin transport as a compartment model. At the same time as we integrate wall growth, we also integrate auxin transport, which is described by a set of ordinary differential equations relating the quantity of auxin of a cell to the auxin quantity of the same cell and its neighbours in the previous time step. We assume auxin, being a small molecule, diffuses quickly within the cell and, therefore, we approximate auxin concentration as a constant value inside the cell. The auxin concentration within each cell is regulated by synthesis, influx, and efflux carriers, with efflux carriers responding to membrane stress. Higher cell membrane stress increases efflux carrier accumulation (19), facilitating auxin transport up a concentration gradient (18, 20, 35). Our approach here differs to from (20) in considering influx carriers and efflux carriers. Auxin concentration of a cell, a_{cell}, evolves over time according to

$$\frac{da_{\text{cell}}}{dt} = 1 - a_{\text{cell}} + D \sum_{\substack{n \in \\ \text{neighbourhood}}} \Omega_{\text{cell}\vert\text{n}}\left(a_{\text{n}} - a_{\text{cell}}\right)$$

$$+ P \sum_{\substack{n \in \\ \text{neighbourhood}}} \Omega_{\text{cell}\vert\text{n}}\left[p_{n\vert\text{cell}}\,g_{\text{e}}(a_n) - p_{\text{cell}\vert n}\,g_{\text{e}}(a_{\text{cell}})\right]$$

$$+ Q \sum_{\substack{n \in \\ \text{neighbourhood}}} \Omega_{\text{cell}\vert\text{n}}\left[q_{\text{cell}\vert n}\,g_{\text{i}}(a_n) - q_{n\vert\text{cell}}\,g_{\text{i}}(a_{\text{cell}})\right], \tag{7}$$

where D, P, and Q determine the strength of diffusion, active efflux, and active influx respectively, $p_{\text{A}\vert\text{B}}$ means the density of efflux carriers bound to the membrane of cell A pumping auxin in the direction of cell B, $q_{\text{A}\vert\text{B}}$ is the density of influx carriers bound to the membrane of cell A taking auxin from cell B, $\Omega_{\text{A}\vert\text{B}} = l_{\text{A}\vert\text{B}}/A_{\text{A}}$, i.e., the length of wall separating cells A and B divided by the area of cell A, and, finally,

$$g_e(a) = \frac{a}{K_{\text{efflux}} + a} \qquad g_i(a) = \frac{a}{K_{\text{influx}} + a}, \tag{8}$$

where K_{efflux} and K_{influx} define how quickly the activity of the respective carriers saturates with auxin concentration. The first and second terms in the right-hand-side of Eq. 7 stand for auxin synthesis and decay, the third for passive transport and the last two for active auxin efflux and influx, respectively. Note that the auxin transport equation has adimensional units of time and auxin concentration such that $a = 1$ is the base value cells would acquire by synthesis and decay alone and a decay rate equal to 1.

Although influx carrier density will be set according to experimental observations (Fig. 1 H), we model efflux carriers as being regulated by stress. The pattern formation mechanism proposed by (18) relies on having a differing value of membrane stress on each side of a single wall (18, 20), therefore we write down the stress perceived by cell A in contact with wall A|B, of length l and rest length l_0 as $\sigma_{A|B} = E_A (l - l_0)/l_0 \neq \sigma_{B|A}$. Taking into account competition for the same pool of efflux carriers within a cell and modelling binding rate as a power law of stress, we obtain

$$p_{\text{cell}|n} = \frac{f(\sigma_{\text{cell}|n})}{1+\sum_m \frac{l_{\text{cell}|m}}{L_{\text{cell}}} f(\sigma_{\text{cell}|m})}, \quad f(\sigma) = \begin{cases} (\eta\sigma)^3, & \sigma > 0 \\ 0, & \sigma \leq 0 \end{cases},$$
$$\tag{9}$$

where n and m are cells in the corresponding neighbourhood, L_{cell} is the perimeter of the cell, and η is a coupling constant. Note that efflux carrier distribution is not dynamic but the steady-state result of a parsimonious carrier binding model (20).

Auxin modulates cell wall mechanics. The effect of auxin on mechanical properties (10, 11) allows efflux carriers to sense auxin content and gives rise to a modulation of wall elastic modulus by auxin concentration written as(18, 20),

$$E_{\text{cell}}(a) = E_0 \left(1 + r\frac{1-a^2}{1+a^2}\right), \tag{10}$$

where E_0 is the value of the elastic modulus at base auxin concentration, which we will call base elastic modulus for short, and r is the ratio between the maximum and minimum elastic modulus the tissue can exhibit in response to auxin. A change in auxin concentration leads to a change in efflux carrier distribution, resulting in up-the-gradient auxin flows. The bending modulus ought to be related to the elastic modulus in some way; however, due to the composition of the cell wall, it is difficult to tell what that relationship might look like, and thus, we vary them independently.

Parametrization. Values for the different parameters were either obtained from the literature or imputed to ensure stable tissue behaviour. Details are provided in supplemental material.

Implementation. Given an initial lattice of cells and the initial auxin concentration of each cell, as well as the initial rest length for each wall, along with the mechanical parameters E_{cell}, $k_{b\text{cell}}$, T_{cell}, and target angles, θ_0, we minimize mechanical energy, arriving at a new geometry. We do so while conserving auxin content before and after geometrical changes. With new wall lengths, l, we compute strain and stress. We then advance the state of rest lengths and auxin concentrations with Eq. 5 and Eq. 7. We, thus, arrive at a new set of values of auxin, and hence of E_{cell}, and rest lengths for which our geometrical configuration is no longer at minimum energy. We iteratively repeat the above process until we reach

the desired simulation time (Fig. 1 G). The simulation program was written in C++, using the Quad-Edge implementation by Paul Heckbert (49), and wrapped up in Python as a library with SWIG. The optimization routine used is a low-storage-BFGS from the NLopt package (50). As the lattice deforms at each time step, we use a simple explicit forward Euler method for ODE integration. The NumPy (51) and Matplotlib (52) packages were used to read data and generate graphics.

Plant material and growth. Seedlings of sC111 (*pUBQ10::GFP:PIP1*; *pGATA23::H2B :mcherry*; *pDR5v2::YFP:nls*) (33) and *pSHY2::nls:mVenus*; *pLBD16::mCherry:SYP122* (31) were used to monitor DR5v2 and SHY2/IAA3, respectively. Seeds were surface-sterilized with Ethanol 70% and SDS 0.05% for 5 min, rinsed once with Ethanol 99% and air-dried. After stratification at 4°C for 48 h, seedlings were grown vertically on square Petri dishes plates containing Murashige and Skoog 0.5× medium with a pH of 5.7, 0.8% agar and 1% sucrose, at 22°C with a photoperiod of 8/16 h light/dark condition. Four days after germination, lateral root primordium (LRP) induction through 5 h of gravistimulation (turned plates vertically, 180°) to detect early events of LRP formation was applied and to proceed with live imaging.

Live Imaging and Microscopy. For imaging, the seedlings were transferred to a chambered cover glass as described in (53). Propidium Iodide (2 μg/mL) was added when required. Confocal Laser-Scanning Microscopy (CLSM) was performed on a Leica SP8 confocal microscope with a 63×, NA = 1.2 water immersion objective. GFP, YFP and mVenus fluorescence were detected using the 488 nm and 514 nm excitation laser line and a detection range of 495-560 nm and 524-550 nm, respectively. mCherry and Propidium Iodide fluorescence was detected using the 568 nm excitation laser line and a detection range of 590-750 nm. Images were taken every 30 min after LRP induction for ∼ 12 h with a resolution of 1024 × 1024 pixels, 400 Hz speed and a line average of 4. Z stacks were performed using a z-step size of 0.5mm. Post-processing of images (LUT, Bright, contrast and maximum intensity projections of 3-7 z-sections was performed in Fiji (http://fiji.sc/Fiji)).

Results and disccussion

To simulate the interplay between tissue mechanics and auxin flow during lateral root initiation, we used a cellular lattice obtained from optical longitudinal sections of *Arabidopsis thaliana* roots, matching the *in vivo* aspect ratios. Our lattice has six cell layers representing vasculature, pericycle cells, endodermis, cortex, and epidermis (Fig.1 A, E). Although the model is run on an extended longitudinal section of the root (Fig. 1 B, E), we are mostly interested in a pair of activated XPP cells and their surroundings, and only this area is depicted.

Accumulation of auxin in root pericycle cells specifies them as lateral root founder cells (24). To ensure this auxin maxi-

mum is stable, we set auxin influx carrier density to be high, in agreement with experimental data (Fig. 1 H). In addition, we assign a higher elastic modulus to the vasculature to mimic the rigid behaviour of the xylem. This also aids auxin accumulation by biasing efflux carrier polarity from the vasculature to the pericycle. We initialise two neighbouring activated pericycle cells with double the amount of basal auxin concentration, reflecting the initiation process (32). To give these two pericycle cells the best chance to expand radially, we also set their bending modulus to $k_b = 100\,\mathrm{MPa}$.

The vertices facing the boundary towards the inside of the root are only allowed to move on the root-shoot axis. In contrast, vertices facing the outside of the root can move in any direction and tend to move outwards due to the lower pressure outside the plant, resulting in the sustained stress of anticlinal walls. We choose this pressure to be $0.1\,\mathrm{MPa}$, which is approximately the value of atmospheric pressure. The simulated tissue is confined within a section of the root-shoot axis with a similar boundary condition to the vertices facing the boundary towards the inside of the root (Fig. 1 E). This means stress on periclinal walls is a free parameter we can control by setting appropriate initial wall rest lengths. Lastly, auxin is exclusively produced in cells and reflected at the lattice boundary. This is necessary since we do not consider the canalization mode of auxin transport and cannot sustain steady shoot-root flows. Setting auxin inflows and outflows at the boundary would result in artificial depletion and accumulation of auxin at that particular boundary.

In brief, auxin accumulation in the founder cells is aided by an up-the-gradient endodermal auxin flows (Fig. 1 F). This is similar behaviour to that found by (30), where PIN3 transports auxin from the overlying endodermis back to the specified pericycle cells. Because of our model's high auxin influx carrier density in activated XPP cells, this auxin maximum is stable and persists throughout growth. Auxin flow patterns before and after radial expansion of the activated XPP cells remain stable (Fig. S2).

Since auxin controls growth, we propose cell extensibility, φ_{cell}, to vary as a function of auxin. The coupling of cell extensibilities (Eq. 6 is rate-limiting, which implies that most growth occurs on the shared interface between activated XPP cells. Yet, there is a challenge with assigning nonzero extensibility to all walls of the simulated tissue. The stress on periclinal walls would artificially decay as growth occurs due to the tissue being confined according to the boundary conditions. To avoid this, we opted for simply having the two activated XPP cells with the same nonzero extensibility (φ) and zero everywhere else.

Auxin accumulation in activated XPP cells leads to modest radial growth and redirects auxin flows towards endodermis. We first examined how an increase in auxin concentration alone contributes to the radial expansion of a pair of founder cells during lateral root initiation. To quantify this expansion, we tracked changes in the length of the shared interface between the two activated XPP cells and their overall morphology. Our simulations showed that growth occurs but saturates around a 13% increase (Fig. 2 A).

This growth coincides with reduced stress within the common wall (Fig. 2 B). However, the overall cell shape remains distinct from the trapezoidal configuration characteristic of activated XPP cells that expand and prepare for asymmetric division (Fig. 2 C).

As stress diminishes within the shared wall connecting the two activated XPP cells, the density of auxin efflux carriers binding to this interface decreases. In our model, carriers compete for binding among different interfaces, leading to the migration of carriers to the following most stressed interface. Initially, the highest density of auxin efflux carriers is in the anticlinal wall between the adjacent activated XPP cells (Fig. 2 F). With growth and stress reduction, carrier density increases at competing cell walls, particularly binding toward the endodermis (Fig. 2 G). Notably, even though the efflux carrier density associated with the endodermis remains relatively low, the cross-sectional area through which auxin flows must be considered. We introduce a measure similar to the polarity concept in (20) to quantify auxin flow due to auxin efflux carriers, showing how the component of auxin flow directed toward the endodermis evolves (Fig. 2 D, E). This measure is directly proportional to the net outflow of auxin (Supplemental Eq. 13). With auxin-induced stress relaxation between adjacent cells, a 40-50% increase in auxin flow exiting the cell toward the endodermis is predicted.

Here, we hypothesize a mechanics-based regulation of auxin transport mechanism, akin to observations in shoot ablation experiments (18, 19, 54). Although the direct link between auxin transport and mechanical stress in roots remains unproven, our model aligns with empirical findings, indicating the importance of theoretical exploration in bridging gaps left by limited experimental data. It suggests the possibility of stress-induced PIN accumulation in roots, not just shoots. While the causal connection is not established (18), there is an observed correlation in shoots between re-orientation of cortical microtubules (CMTs), stress patterns, and auxin efflux carriers post-cell ablation. Similarly, root cell ablation prompts microtubule reorientation around the wound above primed XPP cells (?). Directly assessing the correlation between stress pattern changes and auxin efflux carrier polarization post-cell ablation in roots would be an important step to validate the assumptions proposed here.

It's important to note that our findings on auxin redirection depend on the selected periclinal stress value. Since efflux carriers prefer binding to anticlinal walls (25), we chose a lower periclinal wall stress value, approximately $\sigma = 20\,\mathrm{MPa}$. This choice was made to align the initial rest lengths of periclinal walls with the desired overall stress value of a periclinal wall. Selecting lower stress values would obstruct efflux-mediated auxin transport between different layers, whereas higher values would yield an efflux carrier density different from the one empirically observed (Fig. 1 I, J, S2). We only modelled LR initiation until the first round of cell divisions. Given the dynamics of auxin transport patterns past the first anticlinal divisions (30), it would be interesting to investigate how cell division influences growth and auxin patterns.

Fig. 2. Auxin accumulation in activated XPP cells only triggers modest growth but potentiates auxin flows towards the endodermis. (A) The relative length of the shared wall (pink arrowheads in C) between two activated XPP cells (grey cells) increases over time, reaching a saturation value of around 13%. Accompanying this growth, stress decreases over time (B). The final state of the tissue remains geometrically close to the initial one (C). (D) Computation of the auxin flow. Integrating the density of auxin efflux carriers along the length of the activated XPP cells determines the flow of auxin leaving the cell (**F**). This vector can be decomposed in one component toward the endodermis (F_{en}) and one parallel to the pericycle layer (F_p). (E) The relative intensity of auxin flow leaving the activated XPP cell toward the endodermis (F_{en}). Efflux carrier density (F) before growth takes place and (G) after growth takes place. Efflux carrier density decreases on the shared wall (pink arrowhead) between activated pericycle cells (shaded cells), and efflux carrier density on the wall facing the endodermis increases (orange arrowheads). In (A), (B) and (E), the measures are normalised to the value at $t = 0$ (initial state). $t = 1$ marks the final state. The different layers are labelled: vasculature (v), pericycle (p), endodermis (en), cortex (c).

In summary, our results indicate that increased auxin concentration within adjacent pericycle cells can induce softening of the shared anticlinal wall, resulting in a modest expansion that alone falls short of reproducing the typical cell aspect changes observed *in vivo*. Nevertheless, our model predicts that this stress-induced alteration in auxin efflux carriers subsequently triggers a redistribution, leading to a 40-50% enhancement in auxin flow from the founder cells toward the endodermis.

Auxin signaling in the endodermis predates the activation of SHY2 expression and the pronounced radial expansion of the activated pericycle. Increasing the auxin flow toward the endodermis may trigger an auxin response in this layer. If this were the case, we predict that auxin responses should first occur in activated XPP cells and then in the endodermis (31). *SHORT HYPOCOTYL 2* (*SHY2*) encodes an AUX/IAA involved in endodermal auxin perception and subsequent endodermal remodelling (31). Controlled transcriptionally by auxin (55), a *SHY2* reporter shows endodermal expression from Stage I onwards (31). To empirically verify that endodermal response to auxin, followed by acti-

vation of *SHY2*, is happening *after* redirection of auxin flow from the activated XPP cells, we live-imaged the expression of the nuclear auxin signalling output *DR5v2::Venus* (56) and the *SHY2* transcriptional reporter (31).

Before pericycle activation, neither *SHY2* nor *DR5v2* expression was observed in pericycle or endodermis. Upon activation, *DR5v2* signal appeared in pericycle and contiguous endodermal layers, while *SHY2* expression was solely in pericycle (Fig. 3 A). At Stage I, coinciding with noticeable pericycle swelling (Fig. 3 B), *SHY2* and *DR5v2* were observed in both pericycle and endodermis. This sequential auxin signalling in the endodermis, followed by *SHY2* activation, is in agreement with previous observations (30) and supports the model's prediction that reversed auxin flow due to modest pericycle expansion can initiate endodermal auxin responses (31).

Our model predicts that auxin accumulation within founder cells induces stress relaxation in the shared anticlinal wall, redirecting auxin flow toward the endodermis. This localized auxin accumulation triggers an auxin signalling response in the endodermis, unleashing the active accommodation of the endodermis to the outgrowing LR. Essential in this process is

Fig. 3. Auxin signaling predates expression of SHY2 in the endodermis and endodermal accommodation. (A) Confocal sections of time-lapse recording monitoring the expression of auxin signalling (*DR5v2*) and *SHY2* expression ($pSHY2 :: nls : mVenus$) before pericycle activation, in founder cells and Stage I primordia. The filled arrowheads indicate a signal in the pericycle nuclei, and the open arrowheads signal in the endodermis. Note the *DR5v2* signal in the endodermis above the founder cells before the expression of *SHY2* in this tissue. The different layers are labelled vasculature (V), pericycle (P), endodermis (En), cortex (C) and epidermis (Ep). Of note, the cell outlines are labelled by the plasma membrane marker PIP4;1-GFP (for the *DR5v2* line) and by Propidium iodide (for the *pSHY2::nls:mVenus* line). Images are representative of three biological replicates. Scale bars are 50 μm. (B) Relative pericycle and endodermis cell width (measured at the junction between the two abutting pericycle cells) before activation and at Stage I. Values are for 16 measurements from five different roots before and after pericycle activation.

the mechanical tension in the periclinal interface between the founder cells and the endodermis, which is crucial in coordinating growth and auxin distribution. Root curvature promotes the initiation of LR (57, 58). Curvature in this setting would also increase tension on the periclinal interface between founder cells and endodermis on the convex side of the root (59), which may help auxin-mediated communication between founder cells and the overlying endodermis and further promote auxin flows toward the endodermis upon stress relaxation of the founder cell shared wall.

Bending modulus of the endodermis limits the radial expansion of the pericycle. Next, we investigated the mechanical factors influencing the expansion of activated XPP cells during lateral root initiation, considering the modest radial expansion induced by initial auxin-driven stress relaxation. We systematically analyzed the impact of various parameters on cell expansion, including the base elastic modulus (E_0) of founder cells and overlying endodermis cells, bending modulus (k_b) of overlying endodermal walls (while keeping primed XPP cells at $k_b = 100$ MPa), as well as turgor pressures in the founder cells (T_p) and the overlying endodermis (T_{en}) (Fig. S3). The expansion was quantified by measuring the length of the anticlinal wall between the activated XPP cells. Notably, even though we do not explicitly consider water transport across cells, it would result in turgor differences between cells that we explicitly tested here.

We found that reducing the bending modulus (k_b) from 3600 MPa to 100 MPa led to non-linear radial expansion, from 13% to 60%, resembling the trapezoidal morphology observed *in planta* (21, 23) (Fig. 4 A, E, F, S3). An increase in pericycle turgor pressure (T_p), especially at very high values (2 MPa), amplified the expansion of the activated XPP cell (Fig. 4 D, G. S3). However, reductions in endodermal

Fig. 4. The endodermis's mechanical properties, topology, and geometry potentiate radial expansion and define LRP shape. (A-D) Relative length of the shared wall between primed XPP cells (grey) for different values of the overlying endodermis and founder cell bending modulus (k_b, A), base elastic modulus (E_0, B), overlying endodermis turgor (T_{en}, C) and founder cell turgor (T_p, D). (E-G) Morphology of the ends-state of the simulations. The grey arrows and letters in (A-D) indicate the corresponding morphologies in (E-G). (H-J) Growth simulation results with one (H), two (I), and three (J) endodermal cells overlying the activated XPP cells. The arrowheads indicate the shared wall between primed XPP cells. The labelled layers are vasculature (v), pericycle (p), endodermis (en), and cortex (c).

turgor (T_{en}) or elastic modulus (E_0) minimally affected the pericycle expansion (Fig. 4 B, C).

These findings suggest that increased pericycle turgor and decreased endodermal resistance to deformation can trigger radial expansion. One notable difference between pericycle-turgor-driven and bending-modulus-driven radial expansion lies in the final shape of the founder cells. Upon turgor-driven expansion, the founder cells expanded less toward the endodermis, resulting in a flatter emerging lateral root primordium (LRP) tip. Combining higher pericycle turgor with lower endodermal turgor might rectify this directional bias deficiency. Auxin promotes the expression and activity of pumps and channels that contribute to water influx (60), which could contribute to a local increase of turgor pressure in the pericycle. However, this aspect must be mitigated by the quick water exchange that could equilibrate the turgor pressure since the pericycle cells are still symplastically connected at this point (61). A critical difference is that this shape change is gradual when increasing pericycle turgor and more abrupt when decreasing bending modulus (Fig. 4 A, D, S4). The results suggest that this process is a tug-of-war between turgor and bending modulus, where either turgor increases enough to overcome the bending modulus or bending modulus drops, allowing the existing turgor to drive further radial expansion. Regardless, we have shown radial expansion to be possible with mechanical modulation alone.

The non-linear behaviour of the bending modulus helps explain sudden behaviour changes during this process, whereas the pericycle turgor-driven expansion lacks that particular property on its own. What molecular process could modulate this bending resistance in vivo? In a recent study, we highlighted the distinct organization of cortical microtubules (CMTs) in the endodermis, with an ordered longitudinally oriented array on the pericycle-facing side (34). LR initiation induces reorganization of these microtubules. As CMTs influence wall mechanical properties through cellulose fibril deposition orientation control, the organisation and/or dynamics of the CMTs arrays could thus be a modulator of the bending resistance of the endodermis. Interestingly, we showed that the auxin-dependent induction of the microtubule-associated protein MAP70-5 is necessary to remodel the CMTs (34). Thus MAP70-5 expression could alter CMTs and endodermal wall properties, enhancing founder cell expansion. Supporting this view, abolishing the bending resistance altogether (setting (k_b) to $0\,\mathrm{MPa}$) leads to a froth-like behaviour of the tissue (Fig. S5), reminiscent of the aspect of roots cells when treated with the CMT depolymerising agent oryzalin (62). The radial expansion of the shared anticlinal wall primarily occurs after the first anticlinal divisions of founder cells. As our model does not implement cell divisions, investigating how new anticlinal cell interfaces contribute to the radial expansion and how carrier density changes upon cell division could provide valuable insights.

Endodermis architecture defines LRP shape. We explored whether the arrangement of endodermis cells above the founder cells impacted pericycle growth and shape. Our simulations have mainly focused on lattices where two adjacent endodermal cells overlay the two activated XPP cells,

resulting in one endodermis-endodermis interface above the pericycle. We simulated additional cases with either no endodermis-endodermis interface or two such interfaces overlying the pericycle. Employing the same parameters as before (bending modulus of both the activated pericycle cells and overlying endodermal cells at $k_b = 100\mathrm{MPa}$), we present the outcomes (Fig. 4 H-J).

When only one endodermal cell overlays the pericycle, no radial expansion was observed, as there was no strain on the endodermis-pericycle wall (Fig. 4 H). The reduced strain and stress on the wall between the activated XPP cells corresponded to a slower growth rate (Fig. S6 A). To rule out limited degrees of freedom as a causal factor, we conducted simulations where the endodermis-endodermis junction was removed while retaining the respective vertices for displacement. This also resulted in a lack of pericycle expansion (Fig. S6 B, C).

In contrast, the configuration with three overlying endodermal cells led to distinct results (Fig. 4 J). In this scenario, the founder cells expanded to a maximum width, similar to the earlier two-cell configuration (Fig. 4 I, J, Fig. S6 A), albeit while exhibiting slower growth. However, the resulting shape showed noticeable divergence, with the three-cell arrangement producing a flatter tip than the two-cell counterpart.

These findings suggest that the spatial arrangement of endodermis cells governs the shape of the developing primordium, and not all configurations equally support the radial expansion of the primed pericycle. A prior study tracking cell lineage in lateral root primordia consistently observed that the first activated XPP cell to divide was always beneath an endodermal junction (63). Since radial expansion precedes activated XPP cell division (33), this observation is in agreement with our model predictions and underscores the critical role of endodermis topology in channelling the initiation of the lateral root. The dependence of lateral root primordium shape on endodermis topology complicates our understanding of LR initiation. The number and arrangement of overlying endodermal cells dictate the extent and direction of pericycle expansion. As additional founder cells are recruited laterally (32), the implications for LR morphogenesis and tissue morphology modulation during growth are intriguing, especially in a three-dimensional context not captured by our two-dimensional model.

Conclusion

Our study combines computational modelling and empirical observations to explore the mechanical bases governing the radial expansion of founder cells and endodermal accommodation during lateral root initiation. The central role of auxin in mediating growth and its subsequent impact on mechanical stress distribution emerge as critical components of this process. We find that the mechanical properties of the endodermis are pivotal in shaping the radial expansion of founder cells. Reducing the bending modulus of endodermal walls significantly promotes pericycle growth, highlighting the mechanical regulation of cell expansion. This complements ex-

isting knowledge about the role of turgor pressure in growth and emphasizes the importance of localized modifications in cell wall properties for cell growth

AUTHOR CONTRIBUTIONS
Conceptualization: J. Ramos, K. Alim, A. Maizel; Methodology: J. Ramos, K. Alim; Formal analysis: J. Ramos, K. Alim; Investigation: J. Ramos, B. Reyes-Hernández; Data curation: J. Ramos, B. Reyes-Hernández; Writing-original draft: J. Ramos, A. Maizel; Writing-review & editing: J. Ramos, K. Alim, A. Maizel; Visualization: J. Ramos, B. Reyes-Hernández ; Supervision: K. Alim, A. Maizel; Funding acquisition: K. Alim, A. Maizel

COMPETING FINANCIAL INTERESTS
The authors declare no competing or financial interests.

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