Erroneous compensation for long-latency feedback delays as origin of Essential Tremor

Running title: Erroneous delay compensation as origin of ET

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Abstract

Essential tremor (ET), a movement disorder characterized by involuntary oscillations of the limbs

during movement, remains to date not well understood. It has been recently suggested that the

tremor originates from impaired delay compensation, affecting movement representation and online

control. Here we tested this hypothesis directly with ET patients (N=24) and neurologically intact (NI)

volunteers (N=28) in an upper limb postural perturbation task. After maintaining their hand in a

visual target, participants experienced perturbations of unpredictable direction and magnitude, and

were instructed to counter the perturbation and steer their hand back to the starting position. In

comparison with NI volunteers, ET patients early muscular responses (Short and Long Latency

Responses, 20-50 ms and 50-100 ms respectively) were preserved or even slightly increased.

However, they exhibited perturbation-dependent deficits when stopping and stabilizing their hand in

the final target supporting the hypothesis that the tremor was generated by the feedback controller.

We show in a computational model that errors in delay compensation accumulating over time

produced the same small increase in initial feedback response followed by oscillations that scaled

with the perturbation magnitude as observed in ET population. Our experimental results therefore

validate the computational hypothesis that inaccurate delay compensation in long-latency pathways

could be the origin of the tremor.

Significance Statement: Essential Tremor origin remains poorly understood. In the present study, we

focused on motor impairments associated with feedback control. Following a mechanical

perturbation applied to their arm, patients' short and initial long latency stretch responses were

preserved. However, we observed clear impairments during the stabilization phase that scaled with

the perturbation magnitude. These results were reproduced in a computational model where delay

compensation was inaccurate, suggesting that the origin of the tremor may lie in an underestimation

of the delays impacting the internal monitoring of the motor commands.

Introduction

Essential Tremor (ET) is one of the most frequent movement disorders (Clark & Louis, 2018;

Louis & Ferreira, 2010). It usually affects patients with involuntary oscillations of the upper limbs and

less frequently head, legs and trunk, mainly during movement (Bhatia et al., 2018; Shanker, 2019).

The tremor properties have been described extensively such as its frequency and the impact of

loading, yet the pathophysiology of this disorder remains poorly understood (Clark & Louis, 2018;

Elble, 2003; Ibrahim et al., 2021). Several clinical, postmortem and neuroimaging studies pointed out

that ET could originate from the cerebello-thalamo-cortical loop (Ibrahim et al., 2021), without

characterizing how the movement deficits arise from a functional perspective. Identifying the

cerebellar functions preserved and impaired in ET would therefore help to better understand the

mechanisms at the origin of the tremor (Butler et al., 2023; Louis & Faust, 2020b; Trillenberg et al.,

2006).

From a computational perspective, it is well known that the presence of delays in a feedback

control system can lead to oscillations if the impact of the delay is not taken into account (Miall et al.,

1993; Stein & Oĝuztöreli, 1976). A parallel can be drawn with the way we control our limbs. Indeed,

the sensory feedback, used in motor control, is delayed due to the conduction time of sensory signals

and motor commands through the nerves. The delay depends on the feedback loop: in the upper-

limb, short latency delays associated with spinal stretch reflex are in the range of 20 to 30 ms, and

long-latency delays involving a transcortical loop are in the range of 50 to 60 ms (Scott, 2016).

Importantly, it has been also suggested that state estimation, and therefore compensation for

temporal delays, is performed in the long-latency feedback pathway (Crevecoeur & Scott, 2013).

Assuming erroneous delay compensation in this sensorimotor system, previous simulations

reproduced oscillations in the frequency range observed in ET (Crevecoeur & Gervers, 2019),

allowing us to formulate the hypothesis that ET originates from errors in the long latency feedback

loop.

Indeed, LLRs are not only elicited for large perturbations but that they are also present for very

small perturbations, with a magnitude close to the magnitude of errors observed during voluntary

control (Crevecoeur et al., 2012). This result indicates that LLRs could therefore also be present

constantly in movements to compensate for the undesirable effects of motor variability. The

modulation of LLRs parallels some features of unperturbed behavior around a variety of tasks (De

Comite et al., 2021). If the LLRs continuously play a role in the control of movements, errors in this

pathway could lead general movement deficits affecting both voluntary movements and feedback

responses to perturbations. This hypothesis is further supported by our previous study showing that

ET could learn to anticipate the effect of a perturbation but exhibited adaptation impairments linked

to online control (Blondiaux et al., 2023). Together, there is strong evidence that movement

execution is impaired in ET, and errors in the long-latency feedback loop is a candidate model for

their deficits.

We tested this hypothesis directly by investigating feedback control in a population of patients

with ET and in a neurologically intact (NI) control group using a postural perturbation task. We

observed similar initial perturbation-related limb displacement and intact short and initial long

latency responses, suggesting preserved peripheral system and initial stretch responses. However,

perturbation-dependent deficits arose during the later phase of the feedback correction and during

stabilization, which followed an enhanced stretch response in the late long latency response epoch

dependent on the load magnitude. We reproduced both movement kinematics and transient

perturbation related increase in the stretch response in a computational model considering an error

in the delay parameter. Together our analyses suggest that Essential Tremor could arise from partial

or inaccurate compensation of long-latency delays, leading to oscillations in movements caused by

accumulation of error over time.

Methods

Participants

A total of 24 ET patients (14 females, mean age: 61.1 +-13.1) and 28 NI volunteers (17

females, mean age: 62.7 +-12.6) were recruited for this study. The ethics committee at the host

institution (*Comité d'Éthique Hospitalo Facultaire*, UCLouvain, Belgium) approved the experimental

protocol and all participants provided written informed consent following standard procedures. All

participants were evaluated using the Fahn-Tolosa-Marin Tremor Rating Scale (FTM-TRS) and

participants with other neurological disorders were excluded. The FTM-TRS scale was divided into 3

sections. Part A quantified the tremor amplitude of the limbs at rest, during postural control, and

during action. Part B assessed writing, drawing and pouring liquids. Finally, Part C evaluated the

impact of the tremor in daily life activities (eating, drinking, getting dressed, working, ...) (Fahn et al.,

1993). The latter part was filled by the participant and was not considered during this study due to its

inherent subjectivity. ET patients did not interrupt their medication prior to the evaluation. The FTM

TRS Score for part A and B was 2.3 ± 0.38 (mean ± SEM) for the NI group and 21.6 ± 1.98 for the ET

group.

Task

Participants sat on a height-adjustable chair and grabbed the robotic handle of an End-Point

KINARM device (KINARM, Kingston, Ontario). Direct vision of volunteers' hands was blocked and a

semitransparent mirror that reflected the virtual reality screen (VPixx, 120 Hz), allowing them to

interact with virtual targets (Figure 1a). A hand-aligned cursor was always represented (white dot,

radius 0.6 cm). The experiment was composed of 2 trial types: voluntary movements and

perturbation trials.

Figure 1: *Schematic representation of the protocol design and theoretical model.* **A,** Prior perturbation, participants maintained the hand-aligned cursor in the home target. Direct view of the limb was blocked by an occluder but participants had continuous visual feedback about the hand-aligned cursor. **B,** Perturbation trials started in the home target, participants received one of three perturbation magnitudes (4, 6.5, 9N) in one of four directions (+x,-x,+y,-y). Visual feedback about movement timing was provided via target color (see methods). **C,** Model pathway adapted from Crevecoeur and Gevers (2019). Model compensating for the delay in sensorimotor control. The dotted pathway corresponds to the sensory feedback, the dashed pathway corresponds to the internal prior and the orange pathway correspond to the delay compensation that is suspected to be faulty in ET.   and   define the dynamics of the model, dt is the time step,   the system delay and K are the Kalman gains. For clarity, we omitted the explicit dependencies of M on   and K on t, see methods for variable and matrices definitions.

Participants started with a block of 60 voluntary movements. A home target of radius 1 cm was presented approximately 30 cm ahead of the participant's torso, aligned with the right hand. They had to maintain the hand in the home target (coordinates: [x, y] = [0, 0]), after a random time uniformly distributed between 1 and 2 sec, an external target was lit and used as a go signal. Participants were instructed to pass through the external target (radius 2.5 cm) and to finish their movements inside the home target. The goal target was randomly selected within 4 targets with coordinates [10,0], [-10,0], [0,7.5], and [0,-7.5]. Each target was presented 15 times during the block. Participants were encouraged to finish their movements in less than 2 s. This initial block with

voluntary movements was performed to collect information about movement kinematics without

perturbations, but the results were consistent with the main experiment and with previous reports

on reaching movements in this population (Blondiaux et al., 2023). Because these results did not

provide specific additional information, we do not show the corresponding dataset here.

Perturbation trials started with the same home target (Figure 1B): participants maintained

the hand in the home target, after a random time between 1 and 2 s, the robot applied a step force

(rise time: 5 ms) in one of 4 directions [+x,-x,+y,-y], with a magnitude of 4, 6.5, or 9 N. The

perturbation magnitude and direction were randomly selected. The participants performed a total of

300 trials composed of 25 trials per combination of perturbation direction and magnitude. The trials

were divided into 5 blocks of 60. Participants were instructed to return and stabilize in the home

target, and they received a positive mark indicating good performance (target turned green) if they

completed their movement in less than 3 s. The total score was projected on the screen for their

motivation. When movements were too slow, the target remained red. Trial timed out after 3 s if the

participant was not able to stop their hand. The criterion on movement time was applied to

encourage consistent speeds, but all movements that returned to the target were kept for analyses.

The step force turned off at the end of the trial and the inter-trial time was 1 s. Participants were

encouraged to take short breaks between the blocks to reduce fatigue (15 s to 2 min).

For the perturbations along the y-axis, we did not observe any significant scaling of the EMGs

with perturbation magnitude both in the NI and ET group. This was likely due to participants' limb

configuration (the arm and forearm were approximately vertical and horizontal, respectively) and of

the action of gravity, which in this direction passively brought the hand back to the initial position.

Thus, although all perturbations were applied during data collection to reduce anticipation, the

following analyses focus on the positive and negative perturbations along the x-axis, for which we

collected a clear EMG response that scaled with the perturbation magnitude.

 Data collection and analysis

Kinematics data was filtered using a dual pass 4th order low pass Butterworth filter with a cut-

off frequency of 20 Hz. Movement velocity was extracted using KINARM's data extraction scripts

(version 3.1) and movement path lengths were defined as the integral of the velocity vector norm.

Movement onset and end were defined using a speed threshold of 3 cm/s for at least 200 ms.

Movements were included in the dataset if the participant returned to the target after perturbation.

Movements oscillating around the target at the end were also included in the analysis when possible.

Based on these criteria, we kept all trials for ET participants and removed 1 trial for two NI volunteers

who did not return to the target. NI volunteers managed to stop all their trials at the end of the trial

time, while on average, ET participants managed to stop for a fraction of trials corresponding to

89.42%+-4.36% of the total number of trials. The return time was defined as the duration between

perturbation onset and the moment when the hand re-entered the target. The stabilization phase

was defined as the remaining duration of the trial.

Surface EMG electrodes (Bagnoli surface EMG sensor, Delsys INC. Natick, MA, USA) were

used to record the muscular activity during movement. The 6 electrodes were located on the

Pectoralis Major (PM), Posterior Deltoid (PD), Biceps, Brachialis, and Long and Lateral heads of the

Triceps. The electrodes were attached after light abrasion of the skin with cotton and ether. A

conductive gel was used to improve data quality. The EMG data was sampled at a frequency of 1000

Hz. The reference electrode was located on the right ankle. Raw EMGs were filtered using a dual pass

6th order Butterworth filter with a passband frequency range of 20 Hz to 250 Hz, rectified and aligned

on the perturbation onset for analyses. To normalize EMG data, participants had to apply a force of

15 +-1 N during 3 s on the handle which was locked by the robot for this calibration procedure. A

force gauge was displayed on the screen to help applying the target force. Calibration blocks of 12

trials (3 trials in each direction: $\pm x$, $\pm y$ (unused)), were used at the beginning, middle and end of the

experiment (3 blocks in total). We normalized the EMG of each muscle by dividing the signals by the

mean value across the calibration trials.

Statistical Analysis

Comparisons across ET and NI populations were performed based on linear mixed models

(LME). The fixed predictors were the perturbation *Direction* (2 level categorical factor, -x or +x) and

Force (numerical) as well as the *Diagnosis* (2 level categorical factor, NI or ET), plus a random

intercept to capture inter-individual variability. We use Y_{ij} to designate the dependent variable of

interest, with index i corresponding to the trial number and j to the participant. We used a

significance threshold of 0.05 given the higher variability inherent with clinical population, as well as

with the between-participants design. LME were used for the kinematics analyses with Y_{ij}

representing respectively for the movement phase the pre-perturbation average speed,

displacement at 100 ms, maximum displacement, path length and return time and for the

stabilization phase, the stop time, maximum displacement, and path length. LME were also used in

the EMGs analyses for the average EMG activity prior the perturbation (-50-0 ms), short latency

(R1:25-45 ms), and long latency bins (R2:45-75 ms and R3:75-105 ms). Effects of the direction and

the force (p-value smaller than 10^{-3} in all tests) will not be reported. The statistical model can be

written as follow:

$Y_{ij} = \beta_0 + \beta_1 * Direction + \beta_2 * Force + \beta_3 \, Diagnosis + \beta_4 * Diagnosis * Force + b_j + \epsilon_{i,j}$.

(1)

Model

We reimplemented the model described in Crevecoeur and Gevers, and refer the reader to

this reference for a fuller description (Crevecoeur & Gervers, 2019). The simulations describe

feedback control of a single joint system (Figure 1C). We considered three torque loads acting on the

system: a dissipative torque opposite and proportional to the velocity with a constant G = 0.14

Nm/rad/s (Crevecoeur & Scott, 2014) , a controlled torque T and an external torque T_{ext}. We

considered a first-order filter as linear model of the muscle, transforming the command $u(t)$ into the

control torque with a time constant $\tau = 60\ ms$. The system dynamics is captured by the following

system of continuous differential equations:

$$I\ddot{\theta} = -G\dot{\theta} + T + T_{ext}, \qquad (2)$$

$$\tau\dot{T} = u - T, \qquad (3)$$

$$\dot{T}_{ext} = 0, \qquad (4)$$

with the inertia set to I = 0.15 Kgm², the joint angle θ, and dots represent time derivatives. We

defined the state vector $x(t) = [\theta \quad \dot{\theta} \quad T \quad T_{ext}]^T$ and rewrote the three equations as follows:

$$dx(t) = (Ax(t) + Bu(t))dt + \alpha(t)dW, (5)$$

with:

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & -G/I & 1/I & 1/I \\ 0 & 0 & -1/\tau & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, B = \begin{bmatrix} 0 \\ 0 \\ 1/\tau \\ 0 \end{bmatrix}, \qquad (6)$$

The sensory feedback was defined as follows:

$$y(t) = x(t - \delta t) + \sigma(t), \qquad (7)$$

In Equation 5 and 7, $\alpha(t)dW$ represented signal-dependent and additive sources of noise, $y(t)$ was

the current sensory feedback signal, $x(t - \delta t)$ the delayed state with $\delta t = 55\ ms$, and the sensory

noise $\sigma(t) \sim N(0, \Sigma_\omega)$. We augmented the state with the target coordinates $x^*(t)$. We then

discretized the system using a discretization step of $dt = 5\ ms$. The system became:

$$x_{t+dt} = A_d x_t + B_d u_t + \xi_t \qquad (8)$$

$$y_t = x_{t-h} + \omega_t \qquad (9)$$

Where $A_d := M(dt)$, $B_d := \left(\int_0^{dt} M(s)ds \right) B$, $M(t) = e^{tA}$, $\xi_t = \alpha(t)dW$ and $h = \delta t/dt$.

Because of delayed and noisy sensory feedback, we needed to compute an estimate of the state

vector:

$$\hat{x}_{t+dt} = A_d \hat{x}_t + B_d u_t + K_t \left[\hat{x}_{t|y} - \hat{x}_t \right] \qquad (10)$$

Where K_t were the Kalman gains computed using a forward recursion.

This formulation differs from the standard definition of predictive Kalman filter, by

incorporating an explicit extrapolation of the system state given present sensory feedback. Indeed,

the standard form of Kalman filters uses an *innovation sequence* for the non-delayed case equal to

$y_t - \hat{x}_t$. Here, because y_t is a delayed state measurement, it is possible to extrapolate this

information and compute the current expected state given y_t, the knowledge of limb dynamics and

the motor commands during the delay interval. This extrapolation is either performed recursively

based on system augmentation, or explicitly in the formulation that we have chosen here which

corresponds to finite spectrum assignment (Mondie & Michiels, 2003). With the discrete time system

equations, the extrapolation of delayed sensory signals to the present state takes the following form:

$$\hat{x}_{t|y} = M(\delta t)y_t + \sum_{k=1}^{h} M(t - kdt)Bu_{kdt}dt \qquad (11)$$

In the sequel, we assume that this operation is performed with a value of the delay δt that

underestimated the correct value. Recall that, in addition to the explicit dependency of δt on M, the

motor commands were integrated over a smaller delay interval, h being the delay in discretized time

steps. Observe this filter is equivalent to a standard Kalman filter when the delay $\delta t = 0$ as

$\hat{x}_{t|y} = y_t$. It is also similar to system augmentation (Crevecoeur & Scott, 2013; Fridman, 2014),

where the estimation of the system state during the delay interval results from the augmented

structure of the state vector.

In order to calculate the control signal, we minimized a quadratic cost function penalizing

position and velocity error (first term) and control (second term), which writes as follows:

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$$J(x, u) = E[x_N^T Q_N x_N + \sum_{t=1}^{N-1} x_t^T Q_t x_t + u_t^T R_t u_t] \qquad (12)$$

With $R = 10^{-2}$ and $x^T Q x = w_1(x_1 - x_1^*)^2 + w_2(x_2 - x_2^*)^2$, with $w = [100,0]$ for $k <$

N and $w = [100,10]$ for $k = N$.

Based on these assumptions, the optimal motor commands were defined as $u_t = L_t \hat{x}_t$. The optimal

feedback gains L_t were obtained via a backward recurrence following standard technique.

For the simulations, to capture errors in the delay estimation, we considered a case for which the

delay ($\delta t = 55\ ms$) was underestimated and used $\hat{\delta}t = 0.7\ \delta t$ and $h = \hat{\delta}t/dt$ in Equation 11. The

step perturbations amplitudes were 1, 2 and 3 Nm applied at 50 ms. Movement duration was of 800

ms. The figures were produced using the average across 20 simulations in each condition. The code

will be made available upon publication.

Results

We studied the ability of ET patients (n=24) and NI volunteers (n=28) to respond rapidly to step

perturbations of various directions and amplitudes. After holding the handle of a robotic arm in the

initial visual target, participants were instructed to counter the perturbations and steer their hand

back to the initial target (Figure 1). Four directions and three force magnitudes were used for this

experiment with a total of 300 randomly interleaved trials (25 repetitions per direction and

magnitude). The analyses focus on the lateral perturbations (aligned with positive and negative

values along the x-axis, 150 trials, see methods).

Figure 2 A-C provides an overview of the hand traces of an exemplar participant of each group

for each perturbation. Initially, the perturbation had a similar effect on the ET participants, however,

once participants returned to the target and tried to stop their movements, oscillations around the

target became visible. We observed a slightly larger pre-movement speed explained by oscillations

within the target in some heavily affected patients, resulting in a significant effect of the diagnosis

(Figure 2D; LME: Diagnosis: $F_{(50)}$ =2.39 , P=0.02). We decomposed movements in two phases:

movement and stabilization, with the cut-off being the first time the participant re-entered the

target. Concerning the movement phase, the perturbation initially impacted ET patients and NI

volunteers in a similar way. There were no significant differences in hand displacement at 100 ms

(Figure 2E; LME: Diagnosis: $F_{(50)}$ =0.32, P=0.75; Diagnosis x Force: $F_{(7743)}$ =1.68, P=0.09), in maximum

hand displacement (Figure 2F; LME: Diagnosis: $F_{(50)}$ =0.29, P=0.78; Diagnosis x Force: $F_{(7743)}$ =-1.79,

P=0.07), in path length (Figure 2G; LME: Diagnosis: $F_{(50)}$ =0.25, P=0.80; Diagnosis x Force: $F_{(7743)}$ =-1.05,

P=0.29) and return time (Figure 2H; LME: Diagnosis: $F_{(50)}$ =-0.46, P=0.65; Diagnosis x Force: $F_{(7743)}$

=0.11, P=0.92). However, during the stabilization phase, ET participants faced clear difficulties, with a

longer stopping time (Figure 2I; LME: Diagnosis: $F_{(50)}$ =2.83, $P<10^{-3}$; Diagnosis x Force: $F_{(7362)}$ =5.05,

$P<10^{-4}$), larger oscillations defined as maximum displacement during the stabilization phase (Figure

2J; LME: Diagnosis: $F_{(50)}$ =0.44, P=0.67; Diagnosis x Force: $F_{(7743)}$ =3.66, $P<10^{-3}$) and increased path

length during that phase (Figure 2K; LME: Diagnosis: $F_{(50)}$ =2.18, P=0.03; Diagnosis x Force: $F_{(7743)}$

=4.94, P<10^{-4}). The interaction between the diagnosis and the force magnitude indicated that

performances of the stabilization phase significantly worsened with perturbation amplitude for the

three stabilization measures.

Figure 2: Perturbation *trials, ET patients' difficulties in the stabilization phase are increased with*
perturbation magnitude. **A,** Exemplar participants' hand path during the last perturbation trial, the 2
analyzed directions and 3 amplitudes are represented. **B,** Distance in the X-axis of the exemplar hand
path for the 9 N -x perturbation. **C,** X-Velocity profile of the same trials. **B, C,** Dot: time at which the
hand re-entered the target for the first time; Bar: movement stop condition met: velocity<3 cm/s for
at least 200 ms (see Methods). **D,** Pre-perturbation average speed, averaged over all perturbation
magnitudes, gray dots represent individual behavior. **E-H,** Movement phase, prior first target
crossing. **E,** Distance of the hand from the target center at 100 ms. **F,** Maximum displacement, **G,**
Path length **H,** Time elapsed between perturbation onset and first target crossing. **I-K,** Stabilization
phase. **I,** From target re-entering, time required to stop the hand in the target **J,** Maximum
displacement from target center along the X-axis. **K,** Path length. **E-K,** Metrics computed on all -x
perturbation trials for each perturbation magnitude. Error bar represents the SEM. Light lines
represent individual behavior.

In addition to the hand kinematics, we recorded surface muscular activity. We present here

recordings of the Pectoralis Major and the Deltoid, respectively the shoulder flexor and extensor

stretched by the perturbations aligned with the x −axis. No group effects were observed prior to the

perturbation (-50-0 ms; LME: Diagnosis: $F_{(50)}$ =-0.89, P=0.38). The initial reflexes elicited by the

perturbation were studied and compared between groups shortly after its onset (Figure 3). No

significant differences between groups were observed in the short latency window (R1: 25-45 ms;

LME: Diagnosis: $F_{(50)}$ =0.11, P=0.91; Force: $F_{(7743)}$ =4.02, P<10^{-4}; DiagnosisxForce: $F_{(7743)}$ =1.05, P=0.30)

and during R2, the first part of the long latency window (45-75 ms; LME: Diagnosis: $F_{(50)}$ =0.43,

P=0.74; Force: $F_{(7743)}$ =4.02, P<10^{-4}; DiagnosisxForce: $F_{(7743)}$ =-0.06, P=0.95). Note that the absence of

significant differences between NI and ET in R1 and R2 is not due to an absence of response as we

observed a strongly significant effect of the Force on the muscular activity. Differences between the

two groups are visible starting from R3, the second part of the long latency window (75-105 ms; LME:

Diagnosis: $F_{(50)}$ =0.73, P=0.47; Force: $F_{(7743)}$ =4.02, P<10^{-4}; DiagnosisxForce: $F_{(7743)}$ =-3.66, P<10^{-3}).

These results suggest similar initial response following perturbation and highlight intact

proprioception in ET. Impairments are visible in the late long latency responses (LLRs), from 75ms.

Surprisingly, this difference was associated with a slightly larger R3 response in the ET group, which

was dependent on the perturbation magnitude as indicated by the interaction term. We

demonstrate below that this effect is in fact expected in theory, assuming partial delay compensation

in ET.

Figure 3: *Short and Long Latency responses in the perturbation trials.* **A,** Early deltoid EMG responses averaged over each group for the 3 perturbation magnitudes aligned with negative direction of the -axis. Vertical lines delineate the different time windows analyzed. **B-D,** Binned data over the different time windows for the 3 perturbation magnitudes. Average baseline (-50 to 0 ms) was subtracted from the data for illustration purpose. Error bars represent the SEM. Light traces depict individual behavior. **E-H,** Pectoralis response for the perturbations aligned with the positive -direction. Same format as A-D.

Computational model of feedback control in ET

In order to describe the behavior of ET patients from a theoretical perspective, we reproduced our experimental observations with a closed loop control model featuring a state estimator that compensates for sensorimotor delays. We modeled a Linear-Quadratic-Gaussian (LQG) controller taking into account delayed sensory feedback (Fig 1C: dotted line) and internal representation of the body dynamics (Fig1C: dashed line) to produce an optimal motor command. The delay in the sensory feedback is compensated by extrapolating the sensory feedback over the delay interval (Fig1C: orange line), which is performed explicitly in this approach to study the impact of errors in this operation. Following our previous study (Crevecoeur & Gervers, 2019), we included a scenario in which the sensory feedback delay was

underestimated by the controller: the value of the delay used in the controller was 70% of the

system's delay ($\delta t = 55\ ms, \hat{\delta}t = 0.7\delta t$). This model previously showed that a mismatch in the

state estimator associated with long-latency delays can also produce oscillations. In such case,

the simulations for which the delay was underestimated produced trajectories bearing striking

similarities with those of ET participants. Initially, the arm angle and angular velocity matched

the simulations with no errors in delay estimation. We can notice a slightly smaller maximum

hand deviation in the underestimated case, a trend that was also observed in the experimental

results for the ET population (Figure 2F). An overshoot was observed when bringing the hand

back to the target and was followed by oscillations during the stabilization phase (Figure 4B and

C). Oscillations amplitude scaled with perturbation magnitude and their frequency matched the

oscillations observed with our participants; with a higher power spectral density for ET patients

in the range 0 to 15Hz (Figure 4D), and a peak frequency located around 4Hz as in the data. The

motor commands produced by the model during the LLR window showed no difference during

R2, and early differences in R3, similarly to what was observed between NI and ET participants

(Figure 4E). This effect was robust as the presence of oscillations and increased gains persisted

even when varying parameters such as delay and inertia. Simulations with parameters leading to

the most extreme changes of slopes are visible on Figure 4E. To identify the origin of these

oscillations, we separated the contribution of a delay estimation error solely in the extrapolation

of the state (first term of equation 11) with an error solely in the extrapolation of motor

commands (second term of eq. 11). We observed that the oscillations mainly arose from errors

of the latter component (simulations not shown). These results suggest that the initial pass

through the state estimator produced comparable responses, as reflected by intact R2 responses

but over time, errors due to the underestimation of the delay accumulated and resulted in

oscillations during later phases of the corrective movement.

Figure 4: *Computational model of feedback control in ET.* A, Simulations of step perturbations in a single joint system. B-E, Model underestimating the sensory delays (, orange) and model with no delay estimation error (, blue). B, Elbow joint angle following perturbation (1, 2 or 3 Nm). C, Elbow joint angular velocity following perturbation. D, Average normalized power spectral density across all perturbations for the simulated (left) and experimental (right) data. E, (Left) Average control signal for the 3 perturbation magnitudes ([1, 2, 3] Nm). Detail of the R2 (45-75 ms, middle panel) and R3 (75-105 ms, right panel) Long Latency Windows. Additional traces on the right panel represent the most extreme slope changes following changes in delay and inertia values. Lower limit: I= 0.2 Kgm², sensory feedback delay = 45 ms. Higher limit: I=0.1 Kgm², sensory feedback delay = 65 ms.

Discussion

We investigated the hypothesis that ET originates from an erroneous compensation of the

sensory delays. With a postural perturbation task, we observed feedback control impairments in the

ET population. The initial impact of the perturbation was similar for the ET and NI volunteers, in the

kinematics as well as the initial stretch responses. However, ET patients experienced perturbation

dependent deficits when stabilizing their hand in the target, and they exhibited an increased R3 long-

latency response suggesting errors in the feedback controller. We reproduced these results with a

computational model erroneously compensating for long-latency delays. The simulations were

performed with a value of the delay that was smaller than the true delay, producing an intact initial

response to the perturbation followed by an accumulation of errors over time that led to impaired

feedback control and to the emergence of oscillations that scaled with the force magnitude and

matched the frequency of oscillations measured in ET patients.

To identify which pathway is affected in ET, we can divide our computational model into 3

main processes: 1- the processing of the afferent sensory information, 2- the prior estimate of the

state of the system and of the environment (such as the external torque, estimated), 3- and finally

the delay compensation pathway requiring internal monitoring of the effect of motor commands

during the delay interval. Our results suggest that the sensory feedback is intact in ET. Indeed,

because we did not observe any difference in short-latency response, and early long-latency

responses (R2), we can conclude that the peripheral system and the early components of the stretch

responses are preserved in ET. This result is also consistent with a recent study reporting intact

proprioception in ET patients (Butler et al., 2023). In our previous study, we reported motor

adaptation impairments in ET. The anticipation of the perturbation was preserved while the metrics

related to motor control were impaired (Blondiaux et al., 2023). Their ability to anticipate an external

disturbance suggests the preservation of patients' ability to form an internal prediction of their

movement even in the presence of a perturbation.

Thus, on the one hand, it is possible that both internal priors and sensory feedback are

preserved, while, on the other hand, we observed clear deficits that could be linked to the feedback

controllers as they scaled with the perturbation magnitude. The third model component, linked to

the internal monitoring of motor commands, becomes a unique candidate pathway to account for

sensorimotor deficits in this population: it is clearly a component of the state estimator, and

therefore, of the feedback controller, and can be dissociated from both the sensory system and the

formation of internal priors. Moreover, a selective alteration of the operation performed in this

component produced all features observed experimentally, namely preserved R2 response,

increased R3 response and impaired stabilization scaling with perturbation magnitude. However, it is

important to note that, while an error in delay estimation is also affecting the pathway processing

the sensory feedback, we observed that errors solely in this pathway does not lead to the emergence

of oscillations. Consequently, we concluded that the impairment was attributable to the erroneous

integration of motor commands. A clear added value of our modeling work is to provide a

quantitative model of ET based on the simple assumption that their feedback control is not well

adjusted to the true value of long-latency delays.

Considering some quantitative differences between our results and the simulations, a note of

caution is warranted. First, an approximation of body dynamics was used in our model for the

derivation of the controller. The simulations reported in this study are a simplified version of the task

as we only modeled single-joint movements around a fixed axis. Our participants performed

movements in the 3D space using the handle of the robotic device and therefore responded to the

perturbation using more than one joint. In addition, the muscular activity collected during the

experiment and the control signal extracted from the simulations did not fully match in terms of

temporal profiles. Indeed, the model did not take the details of non-linear muscle dynamics into

account nor the effect of antagonist muscles. In spite of these differences, the range of oscillations

frequencies was similar across simulations and data, suggesting that the net effect of the muscle

responses may correspond to the simulated control signal.

Despite these simplifications, we did observe an increase of the R3 responses both in the

experimental data and the simulations, an effect that remained present even when varying

simulation parameters. While the estimation of the perturbation was intact, simulations revealed

that the velocity was overestimated starting already ~70 ms following the load onset. This might

have elicited stronger reactions to the perturbation and produced the increased gain in the response.

Based on these results, a next challenge is to identify the neural pathways behind these

operations to better identify the origin of the deficits in ET. Cerebellum is one of the main candidates

as it has been associated with state estimation (Diedrichsen & Bastian, 2014; Franklin & Wolpert,

2011; Miall et al., 1993; Wolpert et al., 1998). We also know from human and animal studies that a

suboptimal state estimation leads to incorrect movements or oscillatory behavior (Flament et al.,

1984; Miall et al., 2007; Takei et al., 2021). Interestingly, limb-imposed displacement induces changes

in cerebellar nuclei activity within 70 ms, aligning with the time range of the long-latency pathway

(Strick, 1983). In addition, severe cerebellar dysfunction induced by cerebellar ataxia or dentate

nucleus cooling in monkeys is known to reduce drastically LLRs responses (Kurtzer et al., 2013;

Meyer-Lohmann et al., 1975), making this structure a contributor to long-latency feedback pathway.

In the present study, we suggest that instead of a severe cerebellar disruption leading to response

attenuation reported above, ET could originate from partial cerebellar dysfunction such as a small

mismatch in delay estimation that is enough to produce sensorimotor deficits. This error in delay

estimation does not affect the initial pass of the sensory feedback through the state estimator as

observed with the intact initial responses, which suggests intact spinal contributions. Yet, the

accumulation of errors with the repetition of the passes through the state estimator generates

oscillations in the movement suggesting that the disorder could originate from the cortical-cerebellar

loop. Future studies should be performed to relate this functional hypothesis with the anatomical

structures behind it using for example neuroimaging. Interestingly, the link between state estimation

and cerebellum as well as its involvement in LLRs aligns with numerous indicators of a cerebellar

origin in ET as highlighted by neuroimaging studies (Holtbernd & Shah, 2021; Mavroudis et al., 2019;

Pietracupa et al., 2021; Tikoo et al., 2020) as well as postmortem studies (Louis et al., 2007; Louis &

Faust, 2020a) which report pathological cerebellar changes in ET.

Overall, this study reported intact short and initial long-latency responses in ET during a

postural perturbation task. However, perturbation-dependent deficits were observed when ET

participants stabilized their hand in the home target, confirming impairments in feedback control.

Based on computational modeling, we suggest that these deficits may stem from an erroneous

compensation for sensorimotor delays, attributed to an underestimation of the delay by the

controller.

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