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6   Monolayer force generation and transmission is dictated by focal adhesion distribution
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28

Abstract

For tissues to develop and maintain their function, cells must orchestrate their behaviour by generating and transmitting contractile forces. These forces are transmitted to their surrounding matrix or neighbouring cells via adhesion complexes. How tissues reach a force-balance is often assumed to involve intercellular stresses counterbalancing those in the substrate. However, experimental findings indicate that dampening focal adhesions can increase intercellular stresses. As the ECM is rarely uniform in composition or mechanical properties, it is important to understand how focal adhesions alter stress transmission and the force-balance of a tissue. To address this, we confined monolayers on disk or ring adhesive patterns to alter how they were bound to the substrate. Traction force microscopy and laser ablations of cell-cell junctions were used to examine stresses across epithelial monolayers whilst modulating substrate stiffness. We show that monolayers reach different force-balance states depending on focal adhesion distribution, with intercellular stresses not correlated with overall traction stresses on rings. Using an active matter model to examine the force-balance dynamics, we reveal that tissues reach a force-balance by generating non-uniform patterns of contractility linked to adhesion patterning. This work highlights the importance of considering the position and mechanical properties of cell-ECM and cell-cell attachments to capture the mechanical landscape of living tissues.

Main

A key aspect of many developmental, physiological, and pathological processes is the

ability of cells to generate and transmit forces across a tissue. Cells mainly generate

contractile forces through their actomyosin cytoskeleton, which are then transmitted to the

environment through adhesion complexes[1]. Stress transmission is essential for orchestrating

cooperative cell processes such as morphogenesis[2], collective migration[3] and wound

healing[4]. Stresses are transmitted across adhesion complexes to either the substrate or

neighbouring cells[2]. As epithelial cells have both cell-substrate and cell-cell adhesions, they

must balance these different modes of stress transmission to drive the appropriate

behaviours. However, at present we do not have a clear understanding of the relationship

between stresses transmitted across cell-substrate or cell-cell adhesions in epithelia.

Various methodologies are available to interrogate cell-derived forces within

tissues[5]. Traction force microscopy, where the movement of microbeads embedded within a

substrate is tracked, is a proven method for examining cell-generated forces transmitted to

the substrate[6]. Examining traction forces of cell doublets[7–9], small cell clusters[10] and

epithelial sheets[11,12] revealed local stress imbalances, suggesting an internal force balance

must be reached within the cell assemblies. Following intuition based on mechanical

arguments, unbalanced cell-substrate traction forces are proposed to be transmitted across

cell-cell junctions[7,10,11,13]. Assuming even contractility across cell doublets or small cell

clusters, intercellular stresses were inferred with force balance equations based on traction

data. This yielded a positive correlation between traction forces and intercellular stress,

with increased tractions leading to greater intercellular stresses[7,10]. There is some

experimental data supporting this model, tension sensors for different cell-cell adhesion

molecules based on Förster resonance energy transfer (FRET), have shown increased

molecular tension in monolayers cultured on stiffer substrates[14,15]. However, it has also

been reported in cell doublets, that cell-cell forces inferred from traction force data do not

correlate with the FRET-efficiency of an E-Cadherin tension sensor, with the authors

suggesting a molecular tension homeostasis[9]. Furthermore, laser ablation experiments in

various biological systems are inconsistent with a simple proportional relationship between

traction and intercellular forces.

Laser ablation is a widely employed technique to quantify junctional tensions within

tissues and through rheological models infer tissue mechanical properties. This is achieved

by examining the relaxation of cells after individual or groups of junctions have been cut[16,17].

By disrupting entire cell-cell junctions, this method provides a holistic overview of cell

mechanics incorporating both cortical cytoskeleton and all cell-cell adhesion dynamics. It is

the gold-standard approach in developmental systems that are not amenable to other types

of biomechanical techniques to measure or infer tissue mechanics. Laser ablation of

amnioserosa cells during *Drosophila* embryonic dorsal closure revealed that focal adhesions

act as tethers that limit intercellular stress transmission[18]. Furthermore, work in the

Drosophila abdominal epidermis showed that degradation of the basal ECM occurring at the

pupal stage dramatically reduced cell-substrate friction without eliciting a commensurate

drop in intercellular tension[19]. These observations are not limited to developing tissues:

Madin-Darby canine kidney (MDCK) cells cultured on large micropatterned disks show

higher tension on softer hydrogels where cell-ECM attachments are weaker compared with

stiffer hydrogels[20]. However, the role of focal adhesions in this example was thought to

impact cell spreading after cell divisions[20]. Taken together, these studies suggest that cell-

substrate adhesions can limit rather than promote stress transmission across cell-cell

adhesions. It is therefore important to understand what role focal adhesion arrangement

plays in tissues acquiring a force-balance. This is especially true when considering that ECM

composition, architecture and mechanical properties are heterogeneous[21]. Furthermore,

the ECM is dynamic *in vivo*, especially during development[22] and wound healing[23], and local

remodelling can elicit changes in cell behaviour leading to diseases such as cancer[24].

Here, we combine traction force microscopy and laser ablation to examine the

generation and transmission of stresses across both the substrate and cell-cell adhesions. As

traction forces are known to be dependent on the size and geometry[25,26] of cells and tissues,

we employed micropatterning of hydrogels to standardise these factors. To examine the

role of focal adhesions in determining a tissues mechanical equilibrium we cultured

monolayers on disks or rings limiting the adhesive surface area. To alter stresses generated

by the monolayers, we modulated substrate stiffness which is known to regulate traction

forces[25]. When focal adhesions are distributed throughout the monolayer, traction force

generation and stress transmission are dependent on the substrate stiffness within our

experimentally tested range. However, when focal adhesions are restricted to the

monolayer periphery, traction forces become independent of substrate stiffness and stress

transmission occurs mainly through the monolayer. Furthermore, we observe that

intercellular stress is inversely proportional to substrate stiffness, so that intercellular stress

reduces as stiffness increases. Through theoretical modelling and experimental

observations, we show that this relationship between substrate stiffness and intercellular

stress is elicited by the emergence of non-uniform contractility across the monolayer, with

greater contractility present at regions with greater adhesions.

Results

<u>Adhesive surface area dictates focal adhesion patterns across a monolayer</u>

To examine the effect of the environment on stress transmission across a monolayer, we cultured non-tumorigenic mouse mammary epithelial cells (EpH4)[27] on methacrylated hyaluronic acid (MeHA) hydrogels[28]. 3% w/v MeHA solutions were crosslinked with a range of dithiothreitol (DTT) crosslinker concentrations to modulate the rigidity of hydrogels from 10.8 ± 2.5 kPa to 31.4 ± 2.8 kPa at intervals of ~5kPa (Extended data Fig. 1a-c). These values are higher than what has been reported for mouse mammary tissue[29] but span the reported basement membrane range[21] and a range from physiological to disease state in human breast tissue[30]. ECMs are heterogenous and dynamic[21,22], and it can be absent from tissues altogether[19]. We therefore wanted to modulate the adhesive surface area beneath monolayers to mimic states where the matrix is present or absent. For this purpose, we micropatterned MeHA hydrogels with laminin, the EpH4's preferred ECM component[31], either as a disk (Fig. 1a) or ring (Fig. 1b). The diameter of the micropatterns was 200μm (approximately 10 – 20 cells wide) with the width of rings being 20μm (approximately 1-2 cells wide). We conjugated Alexa633 fluorophore to laminin to assess if increasing levels of MeHA crosslinking increased the concentration of laminin on the surface of hydrogels for both disk (Fig. 1c) and ring (Fig. 1d) patterns. Whilst there were fluctuations in laminin intensity on different hydrogel stiffnesses (Fig. 1c,d) and radially across the disk pattern (Fig. 1c), this did not correlate with differences in focal adhesions (Fig. 1g,h). Therefore, the concentration of laminin in patterned areas did not limit the adhesions that cells can generate with the substrate.

To measure active focal adhesions on different patterns, we immunostained monolayers for phosphorylated focal adhesion kinase (pFAK) (Fig. 1e,f). Altering the adhesive surface did lead to changes in the distribution of pFAK across the monolayer. On disks, pFAK was evenly distributed across the entire monolayer with a slight peak at the periphery of the monolayer (Fig. 1g). On rings however, pFAK was mainly focused on the perimeter of the adhesive area with peaks at the boundary, with a low-level present in the non-patterned area (Fig. 1h). As no laminin is present in the middle of the ring micropatterns (Fig. 1d), there are two possible explanations that could explain the presence of adhesions in the non-patterned region. The first is that cells adhere to non-modified

hyaluronic acid present in the MeHA hydrogel[32], and the second, that EpH4 cells deposit

nascent proteins[33,34]. As our modification rate was between 76 – 79% (Extended Data Fig.

1a) far higher than the threshold for cells to bind to unmodified disaccharides, it is more

likely that cells are binding to nascent proteins. Whether these nascent peptides allow force

transmission into the substrate is not clear. On disks, most cells across the monolayer are

surrounded by pFAK (Fig. 1c), whilst on rings, cells in the centre tended to only have isolated

puncta of pFAK and at the patterned region pFAK was mainly localised at the laminin-

positive edges (Fig. 1d,h). Examining the total pFAK coverage beneath disks and rings

revealed that rings consistently had less total pFAK coverage than disks, and both patterns

showed a slight reduction as substrate stiffness increased (Extended Data Fig. 1d,e). The

regulation of focal adhesion dynamics is dependent on many factors[35], and there are

contradictory reports on how substrate rigidity alters focal adhesion coverage[36,37]. Most of

these studies examine single cells rather than monolayers, therefore it is not clear why total

pFAK coverage reduces on stiffer hydrogels. However, cells have been reported to sense

and respond to strain energy and not substrate rigidity[38], and as we are examining active

focal adhesions it is possible that strain energy is reducing in our system. In summary, we

established experimental conditions that allow us to vary adhesive surface distribution and

substrate stiffness.

We next examined if altering the adhesive pattern or substrate rigidity altered cell-

cell adhesions or cell morphology across the monolayer. We observed no obvious

differences in the localisation of E-Cadherin for both patterns on all hydrogel stiffnesses,

with strong localisation along entire cell boundaries (Fig. 1e,f). Likewise, whilst there was a

distribution in the number of cells that composed each monolayer, the distribution was the

same for all patterns and substrate rigidities (Fig. 1i,j). Examining cell morphology, we

observed that cell height does not significantly change as substrate rigidity increases (Fig.

1k,l). However, we did observe that whilst on disks height is relatively constant ($8.9 \pm$

$1.3\mu m$; Fig. 1k), on rings height increases from $8.9 \pm 1.8\mu m$ in the centre to $10.4 \pm 1.8\mu m$ on

the adhesive area (Fig. 1l). Cell area tended to be slightly higher in the centre of the

patterns, especially for disks (Extended data Fig. 1f,g) whilst there tended to be a slight

increase in elongation at the perimeter for both patterns (Extended data Fig. 1h,i). However,

there was no clear differences in cell morphology between the different patterns suggesting

that packing was not affected by limiting the adhesive surface.

Finally, we examined how stable cell-cell junctions were over our experimental

timescales, or whether there was a high degree of junctional instability. For our movies, we

imaged for one minute before performing laser ablations, so subtracted the frame prior to

laser ablation from the initial frame and calculated the percentage pixel intensity that

remained. This analysis revealed a value close to zero on both patterns and on all hydrogel

stiffnesses (Extended Data Fig. 1j,k). Furthermore, overlayed images of cell membranes for

the same duration as our ablation experiments (5 minutes apart), showed a high degree of

overlap (Extended Data Fig. 1l). We therefore assume that junctional rearrangements is not

a major contributing factor to the force balance dynamics of the monolayer.

<u>Focal adhesion patterning alters dependence of traction forces on substrate stiffness</u>

We next wanted to assess how altering the adhesive area affected traction forces. To

measure traction forces, we embedded fluorescent microbeads within the MeHA hydrogels

and measured their displacement[39]. Following recent reporting of extensile forces

generated by MDCK cell layers[20], we first confirmed that all displacement vectors indicated

contraction towards the centre of the cell layer across all substrates (Fig. 2a,b, Extended

Data Fig. 2a-d). We also observed the greatest displacements at the periphery of the

monolayer (Fig. 2a,b, Extended Data Fig. 2e,f). As expected from previous reports[20,25], we

observed a reduction in displacement magnitude as substrate rigidity increased for both

disks and rings (Fig. 2c,d, Extended Data Fig. 2g-h). We next examined the traction forces

generated by the monolayers and noticed stark differences between disk and ring patterns

(Fig. 2e-h). On disk patterns we observe a decrease in both total traction forces and the

maximum traction force as substrate stiffness increased (Fig. 2e,g). On rings, total traction

force remained almost constant (Fig. 2f), and maximum traction forces showed a weak

reduction (Fig. 2h). It has been reported in micropatterned single MDCK cells that strain

energy is not affected by substrate rigidity[25]. In the case of the monolayers considered here,

as displacement decreased for both patterns, but traction forces only decreased for disk

patterns, we were interested in examining if our adhesive patterns showed marked

differences in strain energy. We observed that for both disks and rings there is a decrease in

strain energy as substrate stiffness increases but that this difference is stronger for disks

than it is for rings (Fig. 2i,j); with a mean strain energy reduction from 10kPa to 30kPa for

disks (25,242pJ) being almost double that of rings (13,481pJ). As the traction forces

highlighted a clear difference in behaviour between disk and rings on different substrates,

we decided to examine whether this reflected a difference in the spatial distribution of

traction forces. Examining mean traction forces radially along the epithelial clusters showed

the highest traction forces at the periphery for both ring and disk patterns on all substrates

(Fig. 2k,l). Consistent to the changes in total and max traction forces, for disks we observe a

reduction in traction magnitude with increasing stiffness whilst on rings we observe virtually

no change in traction force magnitude (Fig. 2k,l). However, we noticed a slight change in the

distribution of traction forces radially between the patterns, with traction forces appearing

to be more localised at the periphery on rings than in disks especially on soft substrates (Fig.

2k,l). As our pFAK data shows on disks all cells our surrounded by focal adhesions, this

suggests that cells within the monolayer locally contribute towards deforming the substrate,

leading to a gradual radial accumulation in traction forces. However, as the hydrogel

becomes more rigid and cells are less able to deform the substrate, traction forces become

more localised to the edge, as previously theoretically predicted[40]. This is altered on ring

patterns where the cells in the central non-adhesive region do not deform the substrate

locally, so that the applied traction forces are always localised to the periphery. Taken

together our results suggest that altering the adhesive surface leads to changes in the

generation and distribution of traction forces across the epithelium.

<u>Internal stresses decrease with increasing substrate stiffness</u>

To interrogate stress transmission within the monolayer, we combined theoretical

and experimental approaches. The theoretical model developed describes the monolayer as

an active soft material in which the monolayer stresses and displacements are determined

from continuum elasticity theory, with the inclusion of an isotropic active stress in the

relationship between stress and strain that accounts for the cell-derived contractility (Fig.

3a, see Supplemental Information Table 1 for model parameters). Such active matter

models are widely adopted to describe active, contractile cells and tissues[25,40–42]. The

substrate is coupled into the model through force balance equations where an additional

resistance to contraction proportional to the displacement is included acting only where the

layer is adhered[40]. Based on our experimental observations with pFAK staining (Fig. 1i,j),

layers were either adhered uniformly to recapitulate the disk, or for the ring pattern, with

adhesions concentrated at the ring with an underlying distribution of small adhesions sites

everywhere else (Fig. 3a). A more detailed description of the model and the sensitivity

analysis can be found in supplemental information and methods section. As we observe a

reduction in total adhesion coverage as substrate stiffness increases (Extended data Fig.

1d,e), we examined with our model the sensitivity of total traction forces to different levels

of adhesion coverage (Supplemental Information). This revealed that traction forces

remained relatively constant with different levels of adhesion coverage above a 10%

coverage threshold (Supplemental Information Table 2). As the coverage of adhesions is

greater than 10% for all our conditions, we conclude that the reduction in adhesion

coverage we observe does not drastically limit the traction stresses generated by the

monolayer. As the monolayer was stable at the timescales measured (Extended Data Fig. 1k-

m), we considered the system to be in a stationary steady state and the forces balanced.

The model can be used to fit both the displacement data (Fig. 3b,c) and total traction

(Fig. 3d,e) for each substrate stiffness, with the cell-generated contractile stress as the fit

parameter. It was sufficient to assume the same uniform contractility for each cell across

the layer to reproduce the observed data, with small variations in overall contractile activity

on each stiffness. Extending this analysis, the internal stress within the layer, akin to

intercellular stress, can be determined from the force balance equations and as a reference

point, we plot the internal radial stress halfway across the radius (r=50μm; Fig. 3f,g). As

might be intuitively expected, the model predicts internal stresses that broadly follow the

same qualitative trends observed for total traction across both disks and rings. For the disks,

we predict a significant monotonic decrease as substrate stiffness increases, with the

greatest stresses being on the softer substrates (Fig. 3f). Whilst for the ring patterns, we see

that the stress remains broadly constant across the stiffnesses (Fig. 3g). We next sought to

examine experimentally whether the model's internal stress predictions were accurate by

considering both traction stresses using traction force microscopy and intercellular stresses

inferred from laser ablation.

We bisected the epithelial monolayers with an annular region of interest (ROI) (Fig.

3h)[16], and inferred bulk intercellular stresses by analysing the recoil velocity (Extended data

Fig. 3a,b). We observed that the greatest recoil was near the ablation site, and that vectors

were orientated away from the cut highlighting that the monolayers were always under

tension (Fig. 3i,j, Extended data Fig. 3c-f). Measuring the maximum recoil velocity half-life

revealed a similar relaxation time of ~20 ± 10s for both patterns and all stiffnesses. This

suggests that the viscoelastic properties of the monolayer weren't altered by focal adhesion

patterning or substrate stiffness (Extended data Fig. 3g-j), assuming that the Young's

modulus of cells is constant which has been shown to be independent of substrate

stiffness[44]. We then examined the maximum recoil velocity with respect to substrate

stiffness for both patterns. For the disk pattern, the recoil velocity showed a weak decrease

(Fig. 3k), qualitatively similar to the model predictions, but with the reduction in internal

stress being more subtle than that predicted (Fig. 3m). On ring patterns, while the model

predicts a constant recoil velocity, we observed a consistent decrease with increasing

stiffness (Fig. 3l). This reduction, which is not intuitively expected or predicted by the model,

suggests that a simple force balance with uniform mechanical activity does not describe the

system fully and that additional factors must be at play.

Comparing traction forces before and after ablation also revealed a reduction,

highlighting mechanical coupling of stresses within the monolayer to the tractions applied

to the substrate (Fig3o,p). Extending this analysis to the strain energy, we also observed a

reduction in strain energy after ablation on both patterns (Fig. 3q,r), with the exception

being for disks on the stiffest hydrogel where the was a negligible reduction (Fig. 3q). This

could be due to our imaging resolution as displacements measured for disks on 30kPa are

close to this range, and any small differences could be undetectable. As total traction and

strain energy vary for the different patterns and substrate stiffnesses, we examined the

percentage change to assess whether this reduction merely reflected the loss of cells in the

ablation region (Fig. 3o'-r'). This revealed there were differences in the percentage loss of

traction forces and strain energy (Fig. 3'-r'), which tended to be higher for rings than for

disks. Taken together, this supports the assumption that there is stress transmission from

cell-cell interactions which distributes forces into the substrate, and releasing intercellular

stress through ablation leads to a reduction in traction stresses generated by the

monolayer.

305
<u>Theoretical modelling suggests non-uniformity of contractility</u>

To illustrate the incompatibility of a model with uniform contractility , where all cells

generate equal forces across the monolayer, with the observed recoil velocities we focused

on the ring pattern which experimentally shows a constant total traction of ~53.7MPa (Fig.

2f) but a reduction in recoil velocity as substrate stiffness increased (Fig. 3l). For uniform

contractility (Fig. 4a) we examined how contractility (a) would have to be altered to

maintain a constant internal stress (represented in blue) or total traction force (represented

in red) as substrate stiffness increased. To orientate, we plotted an illustrative contour of

constant internal stress at r=0.5 (which corresponds to the ablation region, blue line) and

shaded the region below the contour which has a lower internal stress at r=0.5 (blue shaded

region, Fig. 4a). Likewise, we also plotted an illustrative contour of constant total traction

(red line) and shaded the region above the contour which has greater traction forces (red

shaded region, Fig. 4a). Note that the shaded regions do not generate a practically relevant

overlap, with uniform contractility (Fig. 4a), and a parameter sweep altering the contractility

of the layer demonstrates that this is true for all physically relevant regimes (Supplemental

information). This highlights that, as the system maintains a constant traction force (red

contour) it does not encroach into the lower internal stress regime (blue shaded region).

Likewise, to maintain a constant internal stress (blue contour) the system does not increase

traction forces (red shaded region). This would inevitably lead to a system whereby changes

in traction forces would lead to similar changes in internal stress as previously predicted

(Fig. 3g,[7,10–12]).

These phase plane plots do suggest a potential resolution by considering a non-

uniform distribution of mechanical contractility within the layer. By increasing contractility

at the edges, the system generates an overlap region where it is possible to maintain total

tractions but reduce internal stress (Fig. 4b). In the examples given, to maintain a constant

internal stress within the layer (blue line) traction forces must increase as the blue contour

now encroaches the shaded orange region, and similarly to maintain constant total traction

forces (red line) the internal stress must decrease as it now encroaches the blue shaded

region (Fig. 4b). As the latter example is similar to our experimental observations, we

explored whether parameterising the mechanical gradient could reconcile theoretical

predictions with experimental observations.

Introducing a new contractility function that generates monotonic increasing

contractility. Specifically, we take $P=a(1 + br^n)$, as this enables analytical solution in

restricted cases and simplifies the numerical solution, (see Supplemental Information). Here

increasing b indicates more concentrated contractile activity at the edge (b=0 returns the

model to uniform cell contraction). By parameterising the total contractility (P_{Total}) of the

monolayer and distribution of contractility (b), we able to fit both tractions and internal

stress across the range of stiffnesses for both disk (Fig. 4c) and ring patterns (Fig. 4h).

Namely we find that the model can reproduce a large decrease in traction and slight

decrease in internal layer stress on disk patterns with increasing stiffness (Fig. 4d-f), while

also reproducing nearly constant total tractions and large decrease in internal layer stress

on the ring pattern as stiffness increases (Fig. 4i-k). Looking beyond the cell traction and

recoil data we considered the strain energy of the system. Non uniform contractility within

the model also reproduces the trends observed in the strain energy of both adhesive

patterns (Fig. 4g,l). With the disks where adhesion is uniformly distributed, the model

successfully captures the observed reduction in strain energy with increasing stiffness (Fig.

4g). For the ring pattern the model predicts a reduction in strain energy that qualitatively

fits the trend, however, with a more subtle level of reduction (Fig. 4l). This deviation in

strain energy at lower adhesion percentages is expected given the linear model of substrate

resistance to deformation (see Supplementary Information).

Significantly, we find a qualitative difference in behaviour between disk and ring

patterns for resolving experimental observations. For disk patterns the contractility must

become more uniformly distributed, with more cells sharing the work as stiffness increases

(Fig. 5a). However, on the ring pattern the opposite trend is required with the cells at the

edge of the layer being required to be more contractile compared with the rest of the layer

as stiffness increases, so that these edge cells then do the majority of the work (Fig. 5a).

<u>Active myosin and F-actin are not uniformly distributed across monolayers</u>

As our model suggested that non-uniformity of contractility could reconcile our

experimental observations, we decided to examine contractility within the monolayers. We

measured phosphorylated myosin light chain II (pMyoII) intensity across the monolayers as

a proxy for contractility, but also examined actin architecture which plays an essential role

in generating stresses[45]. As traction and intercellular stresses are dependent on myosin

activity[42,46], we initially wanted to examine if the total intensity of pMyoII altered depending

on the pattern and substrate stiffness. To minimise experimental variation, we processed all

independent samples in parallel to allow direct comparison in intensity using widefield

imaging for speed (Extended data Fig. 4a.b). Measuring the intensity of DAPI (Fig. 5b,c), we

observed consistent results with our cell count data (Fig. 1i,j). Examining F-actin revealed

that on disks there is a consistent level of F-actin, that appears to be linked to cell number

(Fig. 5d). However, on rings we observe a slight decrease in total F-actin intensity as

substrate stiffness increases (Fig. 5e). Next, we examined total intensity of pMyoII which

revealed a decrease as substrate stiffness increases, for both patterns but more pronounced

for rings (Fig. 3f,g). This is in agreement with our fitted model parameters which predicted

that there needed to be a reduction in contractility as substrate stiffness increased (Fig.

4c,h).

We did observe spatial variation in pMyoII to varying degrees on our monolayers

(Fig. 5h,i, Extended data Fig. 4a,b). As we observed minor radial differences in height on

rings (Fig. 1l) we wanted to examine pMyoII localisation within the monolayers for our

various conditions with optical sectioning, so employed confocal microscopy. pMyoII was

predominantly localised basally for both disks and rings (Extended data Fig. 4c-e), so we

focused our further analysis to this region (Fig. 5h-s). However, examining the whole

monolayer thickness shows similar but weaker trends (Extended data Fig. 4f,g).

Quantification of pMyoII intensity, normalised to the mean intensity in our ablation ROI (40-

50μm), revealed that no condition had a uniform localisation, with radial variation always

present (Fig. 5j,k). However, depending on the pattern and substrate stiffness there were

differences in the extent of non-uniformity across the monolayers. On disks, pMyoII

intensity was up to 10% greater at the periphery of the monolayers compared to the ROI on

the softest hydrogels but became more uniform as substrate stiffness increased (Fig. 5j). On

rings, there was a greater accumulation of pMyoII at the inner boundary of the adhesive

area in all conditions which became more pronounced as substrate stiffness increased (Fig.

5k). We next quantified the ratio in pMyoII radial intensity between the centre (<40μm) and

edge (>50μm) of the monolayer (Fig. 5l). For pMyoII, on disks the softest substrate showed

the greatest ratio (more concentrated to the edge) which plateaus to a more uniform

distribution on stiffer substrates (Fig. 5l). However, on rings, we see a reversal of this trend

with the stiffer substrates showing the greatest radial distribution (Fig. 5l). Taken together,

we observe radial variation in pMyoII localisation and actin architecture, in accordance with

our conclusions from the model that contractility must have a radial distribution to

reconcile our experimentally observed traction and intercellular stresses. Furthermore, the

parameterisation predictions that on disks radial contractility must become more uniform

on stiffer substrates whilst on rings the opposite must occur also holds true in experimental

observations (Fig. 4c-h and 5l).

Overall, reconciling the model and experimental observations suggests that across

the monolayer, the transmission of forces between cells generates internal stress such that

the cell-substrate adhesion and traction forces do not follow simple counterbalancing

relationships. Instead, the distribution of contractility adapts to generate a whole tissue

mechanical force balance, which is dependent on the distribution of focal adhesions across

the tissue.

Discussion

Discussion

The control of a tissue's mechanical equilibrium is essential for the regulation of a

wide array of physiological processes such as morphogenesis[2], wound healing[4], and when

disturbed can lead to disease progression[47]. Here we describe for epithelial monolayers, the

role of focal adhesion distribution in reaching a mechanical equilibrium. Through

experimental observations, we found on ring patterns where focal adhesion distribution is

non-uniform, that epithelial monolayer stresses do not conform to intuitions on force-

balance, namely that traction and intercellular stresses are proportionally counterbalanced

(Fig. 3m,n). To reconcile experimental observations with monolayers being at force-balance,

we proposed and confirmed that spatial patterns in contractility emerge. Whilst spatial

distribution of contractility has been observed in single cells[48,49] linked to focal adhesion

signalling[48], to our knowledge this has not been reported for monolayers. Furthermore,

often active matter models assume that contractility is uniform across a tissue. Whilst

spatial variation in myosin have been observed in tissues, these are generally localised to

cell-population boundaries[50] or in specific populations for morphogenesis[51,52]. However, we

recently observed in *Drosophila* histoblasts that a tissue-wide spatial pattern of myosin

develops during the pupal stages[19] but whether this is important for the tissue's mechanical

equilibrium is not known.

What mechanisms lead to these spatial patterns of contractility? Whilst not directly

examined here, we can speculate based on mechanobiology arguments. Cells sense their

environment and tissue stresses through mechanotransduction mechanisms and modulate

their contractility to achieve a mechanical equilibrium[47]. Each cell generates contractile

forces through the actomyosin cytoskeleton, which when linked to adhesions transfers this

force to the local environment[2]. Forces can be transferred through cell-cell or cell-ECM

junctions but whether they are transmitted across a tissue is dependent on the mechanical

properties of neighbouring cells and the ECM. For example, blocking stress transmission

through cells by disrupting cell-cell junctions leads to a redistribution of traction stresses,

from localised at the periphery of cell clusters to locally around each cell[53,54]. Likewise,

induction of E-Cadherin expression leads to traction forces becoming radially organised and

larger, as cells globally increase pMyoII[55]. Therefore, cell-cell junctions enable long-range

stress transmission through a tissue. Likewise, the physical properties of the ECM can alter

stress transmission through a tissue. Avian fibroblasts remodel the ECM through

contractility, and diminishing tissue-scale stress transmission by cross-linking the ECM

blocks the emergence of supracellular ordered behaviours[56]. Therefore, when considering

how mechanotransduction might affect cellular processes across a tissue, it is important to

understand how forces are both locally transferred to the surroundings and transmitted

across a tissue.

In comparison with single cell studies, in large clusters of cells a range of possibilities

for how stress can be transmitted within the tissue and to the substrate open-up. Here, we

observe that monolayers alter their contractility spatially as cells respond to their

mechanical environment, and this deviates between ring and disk patterns as substrate

stiffness increases. We can reason why this is the case, assuming that on our disk patterns

cell-generated forces are dominated by focal adhesions and not cell-cell junctions. This

seems a reasonable assumption given the flat morphology of our cells (Fig. 5c),

accumulation of pFAK near cell-cell junctions (Fig. 1e), and that actin architecture appears

connected to focal adhesions (Extended data Fig. 4h) which has been reported to determine

stress transmission[42,5718–20]. On soft hydrogels, where we observe the greatest radial

distribution in pMyoII on disks, cells can locally deform the substrate (Extended data Fig. 2),

allowing forces to be transmitted across the monolayer through both the hydrogel substrate

and cell-cell adhesions (Fig 3). We speculate that in soft conditions, a high proportion of cell-

generated forces are transmitted across the monolayer, leading to higher contractility (Fig.

5f) and the radial increase in contractility towards the periphery as cells sense the

accumulation of stresses transmitted. However, on stiff substrates cells are no longer able

to locally deform the substrate (Extended data Fig. 2), limiting stress transmission through

the substrate. We speculate that in this situation, cells locally transfer forces to both the

substrate and neighbouring cells. However, this can only be transmitted across the

monolayer through cells, with this transmission dampened by restrictions of local ECM

attachment, leading to a more uniform contractility. For our ring micropatterns, only the

most peripheral substrate adhered cells can transfer forces to the substrate as well as cell-

cell junctions, with the bulk of the monolayer transferring solely through cell-cell adhesions.

This is emphasised by the fact the loss in traction forces and strain energy tends to be higher

on rings than disks (Fig. 3o-r) highlighting that the central cells are contributing more to

these variables. This leads to a scenario where focal adhesions do not dominate the transfer

of forces to the local surroundings, and non-local effects emerge through long-range stress

transmission leading to an integrated tissue. On soft hydrogels, we speculate that peripheral

cells transmit forces transferred to the substrate to neighbouring cell-cell junctions due to

its compliance. This then leads to global substrate sensing and an increase in contractility

globally (Fig. 5l). However, on stiffer substrates this global substrate sensing is lost, as the

rigidity of the substrate limits peripheral cells transmitting their generated forces to their

neighbours, and cells reduce their contractility. However, the peripheral cells are still

sensing the forces transmitted by the central cells across cell-cell junctions, as well as the

substrate, and therefore increase their contractility.

The emergence of spatial patterns of contractility in our monolayers has important

implications on the application of force inference techniques. To examine intercellular

stresses of a monolayer, inference methods such as monolayer force microscopy (MSM)[11–13]

or Bayesian inversion stress microscopy (BISM)[58] have been developed. These techniques

infer intercellular stresses based on traction forces measured and can estimate spatial

variation in intercellular stresses in a non-destructive manner, unlike laser ablation, allowing

long-term analysis to be made. Often the implementation of these techniques assumes a

counterbalance between traction and intercellular stresses[10,12,13,42,59]. For MDCK cell-

doublets, where focal adhesions have been shown to disassemble along cell-cell contacts[60],

the direct balance of traction forces with cell-cell adhesions potentially holds[7]. However,

even in these simple cell-doublet systems the distribution of focal adhesions can drastically

alter the propagation of forces. For instance, cardiomyocyte doublets seeded or cultured on

90kPa substrates generated focal adhesions at the site of cell-cell junctions, impairing

mechanical coupling and force propagation[8]. This highlights the importance of examining

the distribution of focal adhesions when inferring stress transmission. Moreover, on our

200μm diameter disk micropatterns, we observed spatial variation in pFAK with some

regions having higher intensity than others (see Fig 1c). Considering a larger tissue, the

distribution of focal adhesions could vary drastically even on a uniform substrate, altering

the local mechanical equilibrium in that region of a tissue. This would impact on whether

local intercellular stresses were positively correlated with traction stress or not. Indeed,

analysis of epithelial monolayers showed a "rugged landscape" of traction forces[12], and

spatial patterns of ECM composition and properties have been observed in developmental

and pathological situations[21]. Therefore, when employing techniques such as MSM and

BISM it is important to examine the variation in local distribution of focal adhesions to

confidently infer intercellular stresses.

Methods
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Cell culture

EpH4 cells with Cas9 inserted into the Rosa26 locus (kind gift from high throughput

screening STP, Francis Crick Institute) were cultured in 4.5g l^{-1} Dulbecco's modified Eagle

medium (Gibco, Thermo Fisher Scientific) containing 10% foetal bovine serum (Sigma-

Aldrich, Merck) and 1% penicillin-streptavidin (Gibco, Thermo Fisher Scientific). For seeding

on hydrogels, 180,000 cells in 2ml of culture medium were centrifuged at 80 r.c.f for 5

minutes. Cells were cultured for 2 hours and then extensively washed in PBS to remove non-

adherent cells and 2ml of fresh media was added. Cells were incubated for 48 hours, to

proliferate and cover the micropatterns. For live-imaging experiments, cells were washed in

PBS and then labelled for 15 minutes with 1.5μl CellMask Green (Thermo Fisher Scientific),

diluted and vortexed in 1.5ml FluoroBrite DMEM (Gibco, Thermo Fisher Scientific)

containing 1% penicillin-streptavidin but no FBS. Media was then replaced with 1.5ml

FluoroBrite DMEM media as described, ready for imaging.

Micropatterning of methacrylated hyaluronic acid hydrogels

3g of methacrylated hyaluronic acid (MeHA) was synthesised as previously described[28], with

a methacrylate modification of hyaluronic acid monomer between 76 – 79% as

characterised through ^{1}H NMR (Extended Data Fig. 1a). MeHA hydrogels were formed at a

concentration of 3 wt% and crosslinked with increasing amounts of dithiothreitol (DTT) to

modulate substrate rigidity. Specifically, hydrogels were formed within a 250μm high silicon

gasket with a 16mm inner diameter and outer diameter of 18mm, sandwiched between a

19mm micropatterned coverslip and a silanized glass surface. Hydrogels were incubated

with 5% BSA (Tocris Bioscience) in PBS for 2 hours before seeding cells.

Micropatterned coverslips were generated by plasma-activating 18mm coverslips and

coating in 0.1mg ml^{-1} poly-L-lysine poly(ethylene glycol) (PLL(20) – g[3.5]-PEG(2), SuSoS)

suspended in 10mM HEPES buffer at pH7.4. To pattern the coverslips, a quartz photomask

(Compugraphics) and UVO-cleaner (Jelight) were used to remove PLL-g-PEG from the

surface of the coverslip. Patterned coverslips were then incubated for 30 minutes with

laminin diluted in 100mM sodium bicarbonate buffer at pH7.4. Laminin consisted of either

20μg ml^{-1} laminin (Sigma-Aldrich, Merck) solution or 20μg ml^{-1} 2:1 mix of laminin and

laminin-labelled with alexa633 for live-imaging and immunostaining, respectively. To label

laminin, 500μl of 1mg ml^{-1} laminin solution was injected into a Slide-A-Lyzer (Thermo Fisher

Scientific) and dialysed two times in 1L of PBS at 4°C and stirred at a low shear rate for 24

hours. The dialysed laminin was then labelled with Alexa633 following the manufacturers

protocol (Thermo Fisher Scientific). Micropatterns were either repeating patterns of disks

with a diameter of 200μm, or rings with an outer diameter of 200μm and inner diameter of

160μm.

For silanized glass surfaces, either No. 1.5 glass bottom 35mm μ-dishes high (Ibidi) or 20mm

diameter uncoated 6-well plates (Mattek) were employed for live-imaging or

immunostainings, respectively. Glass surfaces were plasma-activated and silanized with (3-

aminopropyl) trimethoxysilane (VWR) and 5% glutaraldehyde (VWR).

Atomic force microscopy

Gels were generated as described but using non-patterned, passivated coverslips and No.

1.5 50mm dish with 30mm uncoated glass diameter (Mattek). Force curves were measured

on a JPK Nanowizard 4 using a CP-qp-CONT-Au-B-5 cantilever probe (sQube, NanoAndMore

GMBH). Measurements were taken in four regions per hydrogel (two at the periphery and

two central) with 50 indentations over a 100μm x 100μm grid. The number of hydrogels

quantified for each DTT concentration was 7 for 6.30 to 15.75mM and 6 for 18.9mM. Force

curves were made with an extend speed of 2μm s^{-1} and a setpoint (8 – 25nN, depending on

substrate stiffness) set to achieve a maximum indentation depth of ~500nm. The young's

modulus was calculated by fitting a Hertz model using the AFM_Youngs_modulus_fit

programme developed by Dr Stefania Marcotti (available on GitHub), at different

indentation depths (Extended data Fig. 1b). A standard indentation depth of 250nm across

all hydrogel conditions was used to calculate the Young's modulus, as it is within the linear

phase of the modulus versus indentation depth for all hydrogel conditions and is 1/1000 of

the hydrogel thickness (Extended data Fig. 1c).

Traction force microscopy

Crimson labelled 0.2μm carboxylate modified FluoSpheres (Thermo Fisher Scientific) were

mixed with MeHA hydrogel precursor solution with a 1:40 ratio prior to crosslinking with

DTT. Images were acquired as detailed below. After live-imaging, cells were treated with 10x

trypsin-EDTA, no-phenol red (Gibco) until cells detach from the hydrogels and a final

reference frame acquired.

Laser ablation

Images were acquired on a Zeiss LSM 780 system with an LD C-Apochromat 40x NA 1.1

water objective and 0.8 zoom, so that micropatterns could be acquired in a single 512 x 512

pixel tile. Z-stacks were acquired by measuring excitation by 480nm and 633nm lasers

simultaneously for z-slices every 1μm, spaced between 5 - 6μm below the hydrogel surface

and 10 - 12μm above. Z-stacks were acquired every 10 seconds for one minute before a

laser ablation and five minutes afterwards. An annulus ROI was generated using the

freehand tool and had an internal diameter of 80μm (154 pixels) – approximately 4 – 6 cells

in diameter – and external diameter of 100μm (193 pixels) – leaving 3 – 4 cells at the

periphery. Ablations were made in a z-plane positioned in the middle of the epithelial layer

(3 - 6μm from the hydrogel surface) with a Coherent Chameleon NIR tuneable laser set at

780nm and 40% - 60% power output and lasted ~6.7ms.

Immunostaining

Samples were fixed in 4%-paraformaldehyde (TAAB) for 15 minutes and permeabilised with

0.3% Triton X-100 for 5 minutes, covered from light. Samples were then blocked with 10%

neonatal goat serum (Generon) for an hour at room temperature and incubated with

primary antibodies diluted in 10% neonatal goat serum at 4°C overnight. Samples were then

incubated in secondary antibodies, Phalloidin-Alexa568 (Thermo Fisher Scientific, #A12380:

dilution 1:400) and DAPI (1000x stock solution; Sigma) for 1 hour at room temperature.

Samples were washed and stored in 0.1% Triton X-100. For batch processing of all samples

to examine total pMyoII levels, images were acquired on a Zeiss Celldiscoverer 7 widefield

system with a Zeiss Plan-Apochromat 20x NA 0.7 Autocorr objective with 1x zoom and 2240

x 2254 pixels and a x-y resolution 0.1747602 for a single plane. To examine spatial

localisation of proteins of interest, samples were imaged on a Nikon CSU-W1 spinning disk

with an Apo LWD 40x WI λS DIC N2 NA 1.15 objective with 1200 x 1200 pixels and a x-y

resolution of 0.2731993μm. Z-slices were acquired 0.4μm apart for each channel

sequentially. The following antibodies were used, mouse anti-phospho-Myosin Light Chain 2

(Ser19) (Cell Signalling Technology, #3675: dilution 1:200), rabbit anti-phospho-FAK (Tyr397)

(Thermo Fisher Scientific, 44-624G: dilution 1:400), mouse anti-E-Cadherin (BD Transduction

#610182: dilution 1:400), Goat anti-mouse IgG H&L Alexa 405 (Abcam, #175660: dilution

1:400), and Goat anti-rabbit IgG H&L Alexa 488 (Thermo Fisher Scientific, #A-11008: dilution

1:400). F-actin was stained with Alexa Fluor 568 Phalloidin (Thermo Fisher Scientific, #A-

12380) along with the secondary antibodies.

Data analysis

All images were processed and analysed in Fiji, Matlab and Wolfram Mathematica.

Traction force microscopy pipeline

Images were acquired as detailed above. After adding trypsin to detach cells, there is slight

stage movement in the in x, y and z directions. Therefore, all movies were registered with

the trypsin frame as a reference. For z registration, the surface of the hydrogel was

calculated by examining the total intensity across the image in 24x24 pixel blocks for each z-

slice, with the surface for each block set by the last frame with a signal. To project on a

pixel-by-pixel basis, a Gaussian Filter was employed across all blocks and then rounded, to

minimise any jumps in z-plane. A maximum projection of the beads was then calculated for

both the movie and trypsin reference frame from the surface to the same number of z-slices

below the surface set by the least number of frames available, normally 3 - 4 slices. Once z-

registration is complete the trypsin frame was added as the final frame of the movie and

registered in Fiji with the StackReg macro, using the last frame as the reference. Bead

displacement, traction forces and strain energy were calculated using the TFM package

developed by Gaudenz Danuser's group[39], using a 31x31 pixel template size and L-

parameterisation of 0.00000001.

Laser ablation analysis

Initially a projection of the cell mask was generated by identifying the ablation plane and

calculating a maximum projection between two slices above and below this frame. The

ablation plane was identified by measuring the loss of intensity within the ablation ROI for

each frame after the ablation and selecting the frame with the biggest loss. To measure the

recoil velocity, the Mathematica ImageFeatureTrack function was employed with specifying

features in every pixel and filtering pixels where no motion was detected. To measure

maximum recoil velocity for each movie, the recoil velocity value for the 95th percentile

across the entire field of view was taken (see Extended Data Fig. 3).

Cell morphology quantification

To measure cell elongation and area, projections generated for analysing the recoil velocity

were segmented through Skeletor[19] and manually corrected in Fiji. Using a watershed

algorithm in Mathematica, cell area and elongation (1-width/length) were measured. To

measure cell height, all immunostaining experiments were combined, and an orthogonal

projection made using the Fiji macro with a box ROI 20 x 850 pixels centred on the

monolayer centroid in both the x and y direction. In Mathematica, cell height was measured

by combining F-actin intensity with either pMyoII or E-Cad intensity for the orthogonal

projections, depending on the experiments, and binarizing based on pixels whose intensity

was greater than the mean plus four standard deviations of the entire projected image. A

FillingTransform and DeleteSmallComponents function were applied to clean up the

binarization so only the monolayer remained.

Membrane intensity changes

To measure the movement of the epithelium in our movies before the ablation to

determine their dynamics, the frame immediately before the ablation was subtracted from

the initial frame and the remaining pixel values summed and normalised to the original

summed pixel values. A value close to zero highlights very little movement within the

epithelium.

Basal projection algorithm

To quantify just the basal layer of the monolayers we used Laminin labelling to identify the

surface of the hydrogel. We selected a z-slice for each pixel that corresponded to the

highest laminin intensity, after noise-filtering the z-intensity profile with a LowpassFilter. We

then generated a contour map by smoothening the pixel values with a GaussianFilter,

before rounding to a whole number to correspond to a z-slice. Based on this contour map,

we then did a maximum projection over three z-slices, one above and one below our

contour map value.

<u>pFAK segmentation</u>

To quantify adhesion coverage and size, pFAK images were binarized based on pixel

intensity value in Mathematica. Due to variable background intensity across the field of

view, a MedianFilter was applied with a 61 pixel-by-pixel sliding window and subtracted

from the original image. A background threshold value was then calculated by measuring

the mean intensity plus two standard deviations of pixels outside the micropatterned region

which was determined based on the laminin micropattern channel. Any pixel which had a

higher intensity value than the background threshold was binarized. To de-noise the binary

image, isolated binarized pixels were removed using the DeleteSmallComponents function

with a value set to 1.

<u>Statistical analysis</u>

All statistics were performed in Mathematica using the LocationEquivalenceTest function

which tests the null hypothesis that populations are equal choosing the most powerful test

that applies to the data. The most common test applied was the Kruskal Wallis test as often

one condition would fail normality tests. If the LocationEquivalenceTest was significant a

post-test Mann-Whitney was performed comparing the value on the softest substrate to all

other substrate stiffnesses. For trend fitting, the LinearModelFit function was used on the

mean values for each population with a confidence interval of 95%. The model with the

greatest R^2-value was selected.

For all statistical values used in the analysis, see Extended data tables.

Theoretical modelling

We describe the theoretical and computational modelling briefly here, for a more detailed

description see the additional supplementary information.

<u>Active matter model for the cell layer</u>

An active matter model was used to predict the deformations and stresses in the cell layer.

This widely adopted approach incorporates an active cell-generated stress additively into

the constitutive relation of the cell material, see[40,61–63]. As such we assumed a constitutive

relation such that the stress $\sigma = \sigma_{\text{passive elastic}} + \sigma_{\text{active}}$, as Fig. 3a specifically in tensor notation this

gives:

708
$$\sigma_{ij} = \frac{hE}{1+\nu}\left(\epsilon_{ij} + \frac{\nu}{1-\nu}\epsilon_{kk}\delta_{ij}\right) + \frac{hE}{2(1-\nu)}P(\mathbf{x})\delta_{ij},$$

709 Where we use the summation convention and introduce the kronecker delta. The active contractility

710 is assumed to act isotropically. The deformations are then determined from the force balance

711
$$\nabla \cdot \sigma - KT(\mathbf{x})\mathbf{u} = \mathbf{0},$$

Where K quantifies substrate resistance to deformation and $T(\mathrm{x})$ is an indicator function

that take the value of 1 where the cell is adhered and 0 otherwise. The contractility function

is assumed to be constant throughout the layer $P(\mathrm{x})=P_0$, for Fig. 3, with the addition of a

monotonic increasing contractility profile $P(\mathrm{x})=a(1+br^5)$ for Fig. 4. The polynomial

contractility profile is selected to enable analytical phase plane analysis. Where adhesion is

uniform analytical solutions of the force balance equation may be obtained by standard

techniques as the resulting equations are of Bessel type and solutions may be obtained by

variation of parameters. Where non-uniform adhesion is observed numerical solutions of

the force balance equation are obtained using finite element methods within the MATLAB

PDE Toolbox.

<u>Adhesion geometry</u>

For uniform adhesion the indicator function is either taken as unity throughout for the disk

geometry or as unity in the ring region. Where adhesion is informed by the pFAK data (Fig.

1) and modelled as non-uniform we take the resulting adhesion geometry is as in Fig. 1h.

Specifically, we consider two thin annuli of thickness r_t=0.06 at the edges of the

micropatterned ring corresponding to the regions with highest intensity pFAK. Additionally,

we set a distribution of adhered spots in the internal region and between the two annuli as

the pFAK intensity is non-zero in these regions; spots between the two annuli have a radius

of r_s=0.0167r_0 and in the internal region have radius r_s=0.018r_0. In these adhered regions

$T(\mathrm{x})$=1 and elsewhere we set $T(\mathrm{x})$=0.

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Figure 1

Fig. 1. Modulating adhesive surface of EpH4 monolayers. a,b Example projection of laminin

micropatterns for disk (**a**) and ring (**b**). **c,d** Quantification of mean laminin intensity radially

across micropatterns. **e,f** Example projections of basal pFAK and apical E-Cadherin on disk

(**e**) and ring (**f**) micropatterns. **g,h** Quantification of mean pFAK coverage radially across

micropatterns. **i,j** Dot plot of cell number within each monolayer, bars highlight mean value

for each population. **k,l** Quantification of mean cell height radially across micropatterns.

Scale bars = 20μm. For all quantification thick line are mean values and ribbons are S.E.M,

grey shaded region represents adhesive surface. All N numbers and statistics included in

statistical Table.

Figure 2

Fig. 2. Monolayer traction stresses are altered by modulating adhesive surface. a,b Mean

displacement vector plots for monolayers on disks (**a**) and rings (**b**) on different substrate

stiffnesses. Red dashed line outlines the adhesive surface and scale bars represent 4μm. **c,d**

Quantification of maximum bead displacement by monolayers adhered to disks and rings on

different substrate stiffnesses. **e,f** Quantification of total traction forces generated by

monolayers adhered to disks and rings on different substrate stiffnesses. **g,h** Quantification

of maximum traction forces generated by monolayers adhered to disks and rings on

different substrate stiffnesses. **i,j** Quantification of strain energy transferred by monolayers

into substrate adhered to disks and rings on different substrate stiffnesses. For **c-j** black dots

highlight mean value, whiskers represent S.E.M and grey line is line of best fit. **k,l**

Quantification of mean traction forces radially across micropatterns. Thick lines are mean

values and ribbons are S.E.M, grey shaded region represents adhesive surface.

Figure 3

Fig. 3. Intercellular stress is not proportional to traction stress. a Schematic representation

of the major components that comprise the force balance model. Cells are considered as

active contractile agents (red arrows) bound together to form a monolayer continuum as

well as being bound to the substrate through adhesions (blue springs). Any stresses within

the monolayer are therefore a product of these active forces and passive elastic forces

transmitted through the monolayer (top equation). The active forces generated by the cells

are modelled as a pressure term (red equation) describing cell contractility, and for the

initial model we assumed a uniform distribution of contractility. Cell adhesions are

distributed throughout the monolayer based on experimental observations (blue

schematic), and at these points stresses within the monolayer are transmitted to the

substrate to deform it (bottom two equations). Schematic produced in part with

Biorender.com. **b,c** Total hydrogel displacement from experiments (same as Extended data

Fig. 2g,h) were used to parameterise the model. **d,e** Based on this parameterisation the

model is able to recapitulate the overall trend in experimental traction forces (same as Fig.

2e,f). **f,g** Model predictions on intercellular stresses at the radial midpoint of the layer

(r=0.5) normalised to E=10kPa show changes as substrate stiffness increases. The model

predicts intercellular forces change in a manner similar to the total traction forces as

substrate stiffness increases. **h** Example time course projections of our laser ablation

procedure for both micropatterns. A ring ROI with outer radius of 50μm and inner radius of

40μm was ablated. Merge shows overlay of 0s before and 60s after the ablation only to

highlight deformations, where white highlights regions of no deformation. Scale bar =

20μm. **i,j** Mean recoil velocity vector plots for monolayers on disks (**i**) and rings (**j**) on

different substrate stiffnesses. Red dashed line outlines the adhesive surface and scale bars

represent 3.5μm/min. **k,l** Quantification of maximum recoil velocity after ablation for

monolayers adhered to disks and rings on different substrate stiffnesses. **m,n** Recoil velocity

(same as Fig. 3k,l) and model predictions of radial midpoint intercellular stresses (same as

Fig. 3f,g) where both have been normalised to the value on the softest hydrogel (E=10kPa).

The model is not able to mimic experimental observations. **o,p** Quantification of the total

loss in traction forces once a new steady state is reached after ablations for monolayers

adhered to disks and rings on different substrate stiffnesses. Where **o',p'** represent this

value as a percentage of total traction forces (see Fig. 2e,f). **q,r** Quantification of the total

loss in strain energy once a new steady state is reached after ablations for monolayers

adhered to disks and rings on different substrate stiffnesses. Where **q',r'** represent this

value as a percentage of total strain energy (see Fig. 2i,j). For all quantification graphs,

experimental data is in black, with dots representing mean value, whiskers the S.E.M and

grey line the line of best fit. Model outputs are red circles, where included.

Figure 4

Fig. 4. Non-uniform contractility reconciles experimental observations. a,b Phase plane

plots of contractility in the centre of the monolayer against substrate stiffness for ring

monolayers only. The examples showcase situations where the spatial distribution of

contractility (b), represented with accompanying heatmaps, is either uniform (b =0, **a**) or

non-uniform (b =1, **b**). In both, solid lines represent situations where either intercellular

stress at the radial midpoint of the layer (r=0.5) is constant (blue lines) or total traction

forces generated by the monolayer is constant (red line). The shaded regions represent

either situations where the intercellular stress must be lower (blue shaded region) or total

traction forces must be greater (red shaded area). Note on uniform contractility there is no

workable overlap of shaded regions meaning no workable parameters exist that allow

constant traction forces but lower intercellular stresses as substrate stiffness increases as

occurs experimentally, however with non-uniform contractility an overlap region does exist

highlighting a large parameter space which could reconcile experimental observations. For

c-l the model was parameterised to include non-uniform contractility for both disks (**c-g**)

and rings (**h-l**). **c,h** Schematic representations of the total and spatial distribution of

contractility parameters (b = spatial distribution of contractility; P = total contractility

normalised to softest substrate) used for disk (**c**) and rings (**h**) on different substrate

stiffnesses. **d,i** Total hydrogel displacement from experiments (same as Extended data Fig.

2g,h), **e,j** total traction forces (same as Fig. 2e,f), and **f,k** normalised intercellular stress at

the radial midpoint of the layer (r=0.5) normalised to the softest substrate (same as Fig.

3m,n) were used to parameterise the model. **g,l** Normalised strain energy to the softest

substrate was used as a final check to examine the power of the model to mimic all

experimental observations. Note that for disks (**g**) the model can reproducibly mimic

experimental observations but for rings (**l**) it mimics the trend but not reproduce the actual

change. The discrepancy may be due to non-local effects from the thickness of the hydrogel

not being fully accounted for in the model. For all quantification graphs, experimental data

is in black, with dots representing mean value, whiskers the S.E.M and grey line the line of

best fit and model outputs are red triangles.

Figure 5

Fig. 5. Contractility is non-uniform across micropatterned monolayers. a Schematic

representation of predictions based on parameterisation of the model. For disks the model

suggests that there needs to be a shift from contractility focused to the edge on soft

substrates to more uniformity on stiffer substrates. On rings, the model suggests the

opposite needs to occur with contractility being more uniform on soft substrates and

becoming more localised to the edge on stiff substrates. **b-g** Dot plots of total intensity

within each monolayer for DAPI (**b,c**), F-actin (**d,e**) and pMyoII (**f,g**) adhered to disks (**b,d,f**)

and rings (**c,e,g**). Each dot represents one monolayer, and the bars represent mean value for

each population. **h,i** Example images of pMyoII and F-actin on disk (**h**) and ring (**i**)

micropatterns. Scale bar = 20μm. **j,k** Quantification of mean normalised pMyoII intensity

radially across micropatterns for a basal projection, with the normalisation to the mean

intensity at the ablation site (40-50μm). **l** Quantification of edge to centre normalised

intensity ratio for pMyoII. Dots represent mean value, whiskers S.E.M and shaded line the

line of best fit, with disks in red and rings in black. Note that the trend corroborates the

model predictions (**a**).

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Extended data Fig. 1. Characterisation of micropatterned MeHA on EpH4 cells. a ^{1}H NMR spectra of methacrylated hyaluronic acid (MeHA). **b** Young's moduli at different indentation depths on 3%(w/v) MeHA hydrogels cross-linked with different DTT concentrations. Dashed line is at 250nm which was used to define the young's moduli for each DTT concentration. **c** Dot plot of Young's moduli for each concentration of DTT. Each dot is the average value from 50 force-curves taken for a 100μm x 100μm region. **d,e** Dot plot of total pFAK coverage within each monolayer, bars highlight mean value for each population. **f,g** Quantification of mean cell area radially across micropatterns. **h,i** Quantification of mean cell elongation radially across micropatterns. For **f-i** thick line are mean values and ribbons are S.E.M, grey shaded region represents adhesive surface. **j,k** Dot plot of % intensity change after subtracting the cell outline projection from the frame before an annular ablation from the initial frame 1 minute before. Lines represent mean value for each population. **l** Cell outline projections five minutes apart overlayed with the initial frame in green and last frame in Magenta. White represents pixels where there is no change in intensity. Scale bar = 20μm.

Extended Data Figure 2

Extended data Fig. 2. Displacements of microbeads embedded within MeHA hydrogels by

EpH4 monolayers. a-d Quantification of mean displacement along the x-axis (**a,b**) and y-axis

(**c,d**). Grey region represents adhesive surface. **e,f** Quantification of mean displacement

radially across micropatterns, where thick lines are mean values, ribbons are S.E.M, and

grey shaded region represents adhesive surface. **g,h** Quantification of total bead

displacements generated by monolayers adhered to disks and rings on different substrate

stiffnesses. Dots represent mean values, whiskers are S.E.M, and grey line is line of best fit.

i,j Quantification of the mean bead displacement around the perimeter of monolayers, with

0° along the horizontal axis, where thick lines are mean values, ribbons are S.E.M, and grey

shaded region represents adhesive surface.

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Extended Data Figure 3

Extended data Fig. 3. Recoil velocity dynamics and correlations after laser ablation. a,b

Cumulative plots of all recoil velocity values for each movie on both micropatterns. To

calculate the maximum recoil value the 95th percentile (grey dashed line) value was used,

which was always located near the edge of the ablation site. **c-f** Quantification of mean

recoil velocity along the x-axis (**c,d**) and y-axis (**e,f**). Grey region represents adhesive surface.

g,h Quantification of the mean maximum recoil velocity over the time course of our movies

for both micropatterns. **i,j** Dot plot of recoil half-life calculated from Extended data Fig. 3g,h.

Each dot represents a movie, and the line represents population mean value.

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Extended Data Figure 4

Extended data Fig. 4. pMyoII localisation within monolayers. a,b Example images of

pMyoII, DAPI and F-actin on disk (**a**) and ring (**b**) micropatterns. Scale bar = 20μm. **c** Example

orthogonal projections through the middle of a monolayer of pMyoII, F-actin and Laminin

on disk (left) and ring (right) micropatterns. **d,e** Quantification of mean orthogonal intensity

of laminin, pMyoII and F-actin normalised to the maximum value for the entire orthogonal

projection (see **c**). Note that pMyoII maximum intensity is always near the laminin intensity

highlighting basal accumulation of pMyoII. **f,g** Quantification of mean normalised pMyoII

intensity radially across micropatterns for a whole z-projection of the monolayer, with the

normalisation to the mean intensity at the ablation site (40-50μm). Thick line are mean

values, ribbons are S.E.M, and grey shaded region represents adhesive surface. **h** Example

basal projection of pFAK, F-Actin and E-Cadherin on disk micropattern with expanded insert

(**h'**) to highlight F-actin fibres that span epithelial cells, mainly between pFAK labelled

adhesions. Scale bar = 20μm.

Supplementary Information: Monolayer force generation and transmission is dictated by focal adhesion distribution

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Active stress model for confluent cell layers

The active stress model for the cell layer is based on a continuum description with active stress incorporated into the constitutive relations. This is a widely adopted approach, for a detailed treatment see e.g. [1, 2]. Here, due to the relative thinness of the cell layer compared with its extent, and the lack of cell rearrangements (see Extended Data Fig. 1(l)), we assume plane stress and a (linear) elastic response. We additionally assume that the within layer contractility has no preferred direction (isotropic contraction), to give the constitutive relations

$$\sigma_{ij} = \frac{hE}{1+\nu}\left(\epsilon_{ij} + \frac{\nu}{1-\nu}\epsilon_{kk}\delta_{ij}\right) + \frac{hE}{2(1-\nu)}P(\mathbf{x})\delta_{ij}, \tag{1}$$

where E is the Young's modulus of the cells, ν the Poisson's ratio of the cells, and h the thickness of the layer. The function $P(\mathbf{x})$ describes the contractility throughout the cell layer and we initially assume a uniform contractility throughout so that $P(\mathbf{x}) = P_0$. Later where we consider non-uniform contractility, we require a contractility function P such that being closer to the edge of the layer means greater contractile activity. In this case, we follow [3, 4] and use the functional form $P(r) = a(1 + br^5)$. Although any monotonic increasing function would be sufficient [3], a polynomial form has the added benefit that in circular geometries (as considered here) explicit analytical solutions may be obtained. The degree $n = 5$ is chosen to ensure a sufficiently sharp transition from the edge region into centre where there is a more uniform contractile activity. The parameter a is a scaling parameter for the total contractility of the layer. The parameter b represents the extent of the localisation of that contractility to the edge of the layer. See Fig. 1 for some example radial profiles of differential contractility for different parameters a and b.

The model is completed through a force balance equation. Here, we follow [1], and take

$$\nabla \cdot \sigma - KT(\mathbf{x})\mathbf{u} = \mathbf{0}, \tag{2}$$

where $T(\mathbf{x})$ is an indicator function that denotes discrete regions of adhesion so that $T(\mathbf{x}) = 1$ where the layer is adhered and $T(\mathbf{x}) = 0$ where there is no adhesion. The boundary conditions are zero stress on the outer boundary and continuity of both stress and deformation at all internal boundaries. The substrate resistance to deformation has been approximated as linear in the deformations (as if it were comprised of a dense network of linear springs). This approximation becomes exact for thin or stiff gels where deformations become localised, see e.g. the papers [2, 5]. The parameter K thus quantifies the stiffness of the substrate and its resistance to deformation.

Figure 1: Sketch of differential contractility $P(r) = a(1 + br^5)$. Underlying contractility a is taken as 1 (solid lines) or 2 (dashed lines) each illustrating the effect of varying localisation factors b.

Fixing model parameters

In the constitutive relation (1) we take the parameters as per Table 1. The key control parameter determining model solutions is the non-dimensional parameter $\gamma^2 = K(1 - \nu^2)r_0^2/hE$, [1, 4], which quantifies the relative stiffness of substrate and cell layer. The other key element is the contractility function P. K describes the stiffness of the substrate and for very thin substrates it can be shown analytically that this parameter is proportional to Young's modulus of the gel E_s, i.e. $K = \kappa E_s$ [2]. We make this approximation for the substrates used here, validating the approximation from the traction force data. Specifically, for complete adhesion we see that integrating the force balance over the domain A and applying the boundary conditions gives $K = \int_A \nabla \cdot \sigma dA / \int_A \mathbf{u}dA$. In Fig. 2, we plot the data from the disc traction force measurements $K = \Sigma T/\Sigma u$ against the gel stiffness E_s. We observe an approximately linear relationship validating the approximation. Taking the mean ratio of K/E_s from all the traction force data gave κ as per Table 1. Finally where the contractility is constant so that $P = P_0$, P_0 may be fitted to either the strain energy or traction data collected from the traction force measurements, and we select traction throughout, see below.

Computational domains

The experiments are performed on two adhesion patterns: a completely functionalised disk (radius 100μm) and a functionalised annular ring with inner and outer radii, 80μm and 100μm, respectively. For the disk we assume complete adhesion so that $T(\mathbf{x}) \equiv 1$ across the whole domain $|\mathbf{r}|/r_0 < 1$. For the ring of outer radius 100μm and inner radius 80μm we consider two patterns of adhesion. For the phase plane analysis, see the main paper Figures 4(a) and 4(b), we consider the ideal arrangement of $T(\mathbf{x}) \equiv 1$ in $0.8 < |\mathbf{r}|/r_0 < 1$, taking advantage of the analytical solutions this symmetry affords (see below). For all other simulations we consider a pattern of adhesion informed by the experimental pFAK imaging data (see e.g. main paper Fig. 1(h)). Specifically, we consider two thin annuli of thickness $r_t = 0.06$ with $T(\mathbf{x}) \equiv 1$ in $0.8 < |\mathbf{r}|/r_0 < 0.8 + r_t$ and $1 - r_t < |\mathbf{r}|/r_0 < 1$, corresponding to the regions with highest intensity pFAK. Additionally, we set a distribution of adhered spots in

Figure 2: Traction to deformation ratio scales linearly with gel stiffness. Plot shows the ratio of the sum of tractions over the sum of displacements as derived from the experimental data plotted against Young's modulus (E). The dashed line has slope κ, as per Table 1, the mean ratio from all experimental data.

Figure 3: Computational adhesion pattern for simulations of adhesive rings.

Parameter	Value	Source
Young's modulus: cell E	1kPa	literature see e.g. [6]
Layer thickness h	9μm	measured (Fig. 1 k and l in the main paper)
Poisson's ratio: cell ν	0.45	within literature range: 0.38–0.5 [7, 8]
Domain size: radius r_0	100μm	adhesive pattern size
Substrate parameter: κ	29000m^{-1}	estimated from traction data

Table 1: Constitutive parameter values used to calculate dimensionless parameter $\gamma^2 = K(1 - \nu^2)r_0^2/hE$ which is used to quantify the relative stiffness of the substrate to the monolayer throughout the study.

the internal region and between the two annuli as the pFAK intensity is non-zero in these regions; spots between the two annuli have a radius of $r_s = 0.0167$ and in the internal region have radius $r_s = 0.018$. The pattern of spot placement used throughout is shown in Fig. 3.

Sensitivity analysis of adhesion patterning

To explore how sensitive the results are to the precise patterning of adhesion, and the possible role of imperfect adhesion in functionalised patches, we simulated different adhesive patterns and looked at their effect on the reported quantities of total traction and internal radial stress at ablation point. For the disk we compared the completely adhered disk used in the study to a simulation with discrete adhesions randomly distributed across the disk, as per Fig. 4A. Specifically, a square grid was generated across the disk such that there were 50 grid squares across the diameter. Adhesions with radius $0.0179r_0$ were then placed in randomly selected grid squares such that the total covered area is approximately 30% the total area of the disk. On this domain, solving on the random domain for the deformations with $\gamma = 15$ and uniform contractility, we calculate the total traction to be $\approx 93\%$ of the total traction calculated with complete adhesion across the entire interface. With the same parameters, we observed similarly small changes in the radial stress at ablation ($\sigma_{rr}(r = 0.5r_0)$): we calculate the $\sigma_{rr}(r = 0.5r_0)$ on the random domain to be $\approx 97\%$ of $\sigma_{rr}(r = 0.5r_0)$ of a disk with complete adhesion.

We further compare different adhesion patterns for the annular micropatterns. The annular micropattern is engineered to cover a region 80μm$< r < 100\mu$m such that rings have a width of 20μm; this could be idealised to an adhesion arrangement with $T(\mathbf{x}) \equiv 1$ in $0.8 < |\mathbf{r}|/r_0 < 1$ (Fig. 4B). In table 2 we show that for such ideal arrangements a $\pm10\mu$m change in internal radius of the disk makes at most a 3% difference to the total traction measured across the layer and similarly small (4%) differences to the radial stress at the point of ablation. Indeed, even with a reduction in adhered area to $r_1 = 0.95$ we see a $\leq 10\%$ change in the total traction and radial stress. For smaller adhered areas we begin to see a sharper drop in the model predicted total traction and radial stress (see e.g. $r_1 = 0.975$ in table 2). As the arrangement of adhesion throughout the cell layer is non-uniform, we also consider different adhesion patterns inspired by the pFAK coverage (see main

paper Fig. 1(j)). Specifically, we considered adhesion patterns with two thin annuli width r_t such that $T(\mathbf{x}) \equiv 1$ in $0.8 < |\mathbf{r}|/r_0 < 0.8 + r_t$ and $1 - r_t < |\mathbf{r}|/r_0 < 1$ (as in Fig. 4C) to represent the regions of higher intensity pFAK. Reducing the width of the two annuli resulted in a decrease in both the tractions transmitted to the gel and internal radial stress, however, even when the adhesion percentage was reduced by 61% (from 36% of the disk with $r_1 = 0.8$ to 14% with $r_t = 0.04$), the reduction in total traction and internal stress was stil only 4%. We further considered a non-uniform pattern of adhered spots distributed between the two annuli with $r_t = 0.06$ (Fig. 4D), where spots had radius $r_s = 0.0167$; the spots were selected from the same square grid that was used in Fig. 4A to fill the desired domain. This addition of adhesions between the two annuli results in traction and stress values that lie between the cases of completely adhered annulus and two annuli without spots, as expected. Finally, we include a selection of spots randomly selected from a square grid with 40 squares across the diameter of the internal region as shown in Fig. 3. This addition of internal spots makes only 1% difference to the total traction and internal stress calculated from the model simulations, despite increasing the adhered area from 26% to 37% of the whole surface area of the cell layer.

	Adhesion percentage	T_{total}	T_{total} of $T_{total}(r_1 = 0.8)$	$\sigma_{rr}(r = 0.5)$	$\sigma_{rr}(r = 0.5)$ of $\sigma_{rr}(r = 0.5; r_1 = 0.8)$
RINGS, e.g. Fig. 4B					
$r_1 = 0.7$	51%	4.39	101%	0.72	101%
$r_1 = 0.75$	44%	4.38	100%	0.72	101%
$r_1 = 0.8$	36%	4.37	100%	0.72	100%
$r_1 = 0.85$	28%	4.33	99%	0.71	99%
$r_1 = 0.9$	19%	4.25	97%	0.69	96%
$r_1 = 0.95$	10%	4.01	92%	0.65	90%
$r_1 = 0.975$	5%	3.60	83%	0.58	81%
TWO THIN RINGS, e.g. Fig. 4C					
$r_t = 0.04$	14%	4.18	96%	0.69	96%
$r_t = 0.06$	22%	4.29	98%	0.70	98%
$r_t = 0.08$	29%	4.34	99%	0.71	99%
TWO THIN RINGS WITH SPOTS					
Fig. 4D	26%	4.31	99%	0.71	99%
Fig. 3	37%	4.35	100%	0.72	100%
Fig. 4E	62%	4.36	100%	0.72	101%

Table 2: Sensitivity analysis of different adhesion simulations of annular adhesion patterned gel with contractility maintained at $P_0 = 1$. Total traction, T_{total}, and radial stress at point of ablation, $\sigma_{rr}(r = 0.5)$, are computed for different adhesion patterns (shown in Fig. 4) on a gel with stiffness $\gamma = 15$. The values are also given relative to an annulus with internal radius $r_1 = 0.8$ simulating perfect adhesion across the micropattern. Adhesion percentage denotes the proportion of the circular geometry that is 'adhered'.

Figure 4: Computational adhesive patterns used for sensitivity analysis: (A) shows a distribution of 935 adhesive spots randomly selected from a uniform grid across a circular geometry for an adhesion coverage of 30%; (B) shows adhesion across an annular region. The internal radius of the annulus is $r_1 \times r_0$, where r_0 is the external radius; here $r_1 = 0.8$ is depicted; (C) shows adhesion across two annuli for a circular geometry. Both annuli have width $r_t \times r_0$, here the inner-most radius is $r_1 = 0.8$ and $r_t = 0.06$; (D) shows adhesion across the same geometry as (C) with additional adhesive spots between the two annuli. These spots have radius $r_s = 0.017$; (E) shows adhesion across the same geometry as (D) with additional adhesive spots in a square grid with 40 grid squares across the diameter of the internal region. These spots have radius $r_s = 0.018$.

Solving for deformations

Analytical solutions for complete adhesion on disk and ring

For an adhered disk, $T(\mathbf{x}) \equiv 1$ across $|\mathbf{r}| < r_0$ analytical solutions of (2) can be obtained with both $P = P_0$ and $P(r) = a(1 + br^5)$, see [4]. In both cases, symmetry implies the deformations will be purely radial so that $\mathbf{u} = u(r)\mathbf{e_r}$. For $P = P_0$,

$$\frac{u}{r_0} = \frac{-P_0(1 + \nu)}{2\left(\gamma I_0(\gamma) - (1 - \nu)I_1(\gamma)\right)} I_1\left(\frac{\gamma r}{r_0}\right), \tag{3}$$

where I_1 is the modified Bessel function and $\gamma^2 = K(1 - \nu^2)r_0^2/hE$. For the radially varying profile we obtain

$$\frac{u(r/r_0)}{r_0} = \frac{(1 + \nu)}{2\gamma}\left(cI_1\left(\frac{\gamma r}{r_0}\right) + \frac{5ab}{\gamma^5}\left[\gamma^4 r^4 + 15\gamma^2 r^2 - \frac{45\pi}{2}L_1\left(\frac{\gamma r}{r_0}\right)\right]\right), \tag{4}$$

where we have defined

$$c := \frac{-a(1 + b)}{F(\gamma)} + \frac{5ab}{\gamma^5 F(\gamma)}\left[(1 - \nu)\left(\gamma^3 + 15\gamma - \frac{45\pi}{2\gamma}L_1(\gamma)\right)\right.$$
$$\left. - \left(5\gamma^3 + 45\gamma - \frac{45\pi}{2}L_0(\gamma)\right)\right],$$

given in terms of the modified Struve functions $L_0(z)$ and $L_1(z)$ [9]. Note we use non-dimensional scaled spatial variables here (i.e. introducing r/r_0) to enable solutions to be domain size independent, in this formulation b is now also scaled to be non-dimensional so that $b = b^*/r_0^5$ (where $b^* \equiv b$ in dimensional variables). Function $F(\gamma)$ is defined by

$$F(z) := I_0(z) + \frac{(\nu - 1)}{z}I_1(z).$$

Similarly analytical solutions for both contractility profiles ($P = P_0$ and $P(r) = a(1 + br^5)$) can be obtained for the adhered ring pattern, provided symmetry is maintained and no distributed adhesions spots are assumed. However, in this case the solutions are more mathematically complicated involving additional special functions. See [4] for the full details of these solutions and their derivations. We note that the parameter $\gamma^2 = K(1 - \nu^2)r_0^2/hE$ continues to be the control parameter in the analytical solutions.

Numerical solutions for pFAK informed adhesion patterns

When considering adhesions distributed in discrete regions, such as the adhesion geometry shown in Fig. 3, numerical solutions must be obtained using finite element methods. We again work on the non-dimensional domain scaled to have maximum radius 1, as such we continue to interpret parameter b in the non-dimensional sense as for the analytic solutions. For each defined geometry, a mesh was generated automatically using the generateMesh command within the MATLAB PDE Toolbox (with `Hmax`, maximum edge length, set at 0.005). The force balance equation may be expressed as a general elliptic PDE in two dimensions

$$-\nabla \cdot (c_{11}\nabla u_1) - \nabla \cdot (c_{12}\nabla u_2) + a_{11}u_1 + a_{12}u_2 = f_1$$
$$-\nabla \cdot (c_{21}\nabla u_1) - \nabla \cdot (c_{22}\nabla u_2) + a_{21}u_1 + a_{22}u_2 = f_2.$$

As in the radially symmetric cases of a complete adhesion or an adhered ring, we have normalised length scales by the cell radius r_0. Thus, specifically the coefficient matrices are

$$c_{11} = \begin{pmatrix} 1 & 0 \\ 0 & \frac{(1-\nu)}{2} \end{pmatrix}, \quad c_{12} = \begin{pmatrix} 0 & \nu \\ \frac{(1-\nu)}{2} & 0 \end{pmatrix}, \quad c_{21} = \begin{pmatrix} 0 & \frac{(1-\nu)}{2} \\ \nu & 0 \end{pmatrix}, \quad c_{22} = \begin{pmatrix} \frac{(1-\nu)}{2} & 0 \\ 0 & 1 \end{pmatrix},$$

$(a_{11}, a_{22}) = T(\mathbf{x})\gamma^2$, and $a_{12} = a_{21} = 0$. With differential contractility given by $P(r) = a(1 + br^5)$, the coefficients on the right-hand-side are given by $f_1 = 5((1 + \nu)/2)abx \left(x^2 + y^2\right)^{3/2}$ and $f_2 = 5((1 + \nu)/2)aby \left(x^2 + y^2\right)^{3/2}$, where we have used $r = \left(x^2 + y^2\right)^{1/2}$ to convert between Cartesian and polar coordinates. The no stress boundary condition is input as generalised Neumann boundary conditions

$$\mathbf{n} \cdot (c_{11}\nabla u_1) + \mathbf{n} \cdot (c_{12}\nabla u_2) + q_{11}u_1 + q_{12}u_2 = g_1$$
$$\mathbf{n} \cdot (c_{21}\nabla u_1) + \mathbf{n} \cdot (c_{22}\nabla u_2) + q_{21}u_1 + q_{22}u_2 = g_2,$$

with $\mathbf{n}$ the normal vector to the boundary; $q_{11} = q_{12} = q_{21} = q_{22} = 0$ and $(g_1, g_2) = -((1 + \nu)/2)a \left(1 + b(x^2 + y^2)^{5/2}\right)\mathbf{n}$. To obtain solutions for a uniform contractility throughout the epithelium, we set $a = P_0$ and $b = 0$.

Parameter fitting to experimental total traction data

From the previous section, we can see that for a given adhesion geometry the model is completely parameterised by γ and ν with either P_0 defined (uniform contractility) or a and b defined (radially varying contractility). The parameters γ and ν are determined from the mechanical properties of the gel and epithelium as described above. The Poisson's ratio for all cells is expected to be close to 0.5 (the value for an incompressible material) and little variation is expected, the specific value 0.45 is taken within the range commonly reported for cells (see table 1).

We used the measured total traction data from the traction force microscopy to set the contractility parameter P_0 or a (for a given choice of b) for each gel stiffness. Specifically for each contractility model (uniform or varying) the model deformations $\mathbf{u}$ are derived as described above and from these deformations the total applied tractions T_{tot} are calculated

$$T_{tot}(P(\mathbf{x})) = \int_A KT(\mathbf{x})\mathbf{u}dA. \tag{5}$$

T_{tot} is then fit to the experimental data of ΣT via $T_{tot} = \Sigma T \cdot A_{pix}$, where A_{pix} is the area of a pixel (here $0.519\mu\text{m} \times 0.519\mu\text{m}$).

As an alternative to fitting to the traction data we could have chosen to fit to the total strain energy data. However, as the strain energy data is a derived quantity from the traction force data we chose to fit our single fit parameter to the traction directly. The model with these contractility parameters then subsequently predicts qualitatively similar trends in the strain energy as observed (see e.g. Figs. 4(g,l)), however, on rings, at a slightly higher level than observed. One contributory factor to the observed difference in strain energy is the approximation of a linear spring resistance in the force balance (2), which on finite depth gels and at low adhesion percentages may overpredict strain energy due to the contribution of non-local effects.

When fitting the model with differential contractility, the localisation of contractility to the edge of the layer, b, also needs to be assigned. In the paper, we illustrate the model predictions for a particular choice of parameter values. Namely, we set values of $b = 2.1$ and $b = 0.1$ on the softest

Figure 5: Contour plot shows lines of constant total traction (red-orange) and constant internal stress (blue-green) as a and b are varied. Black crosses mark two choices of a and b parameters such that T_{total} is the same at both points, however, the value of internal stress ($\sigma_{rr}(r = 0.5)$ is different at each point). Here substrate stiffness is kept fixed at $\gamma = 5$.

gels for disk and ring adhesion patterns, respectively. From these initial parameters, we set b values on stiffer gels such that the internal radial stress follows the same trend as the recoil velocity when normalised by their values on the softest gels. Of course, different parametrisations of b could be chosen to reproduce the same qualitative trends. We illustrate this in Fig. 5 where we plot contour lines of constant total traction: this indicates the combination of a and b parameters required to produce a particular value for the total traction for an idealised annular adhesion geometry (e.g. Fig. 4B) on a given stiffness substrate. We further include contours of constant internal stress. As the contours of internal stress and total traction intersect, different parameter choices of b can be used to both fit the experimental total traction data and reproduce the qualitative trends in internal stress. For example, we have indicated two parameter choices with black crosses which correspond to the same total traction but different values of the internal stress.

In the main paper, Figures 4a and b, we show parameter sweeps of contractility scaling parameter a for different stiffness gels with uniform contractility ($b = 0$) vs differential contractility ($b = 1$). Fig. 6 demonstrates that the contour lines of constant total traction and internal radial stress depicted in the main paper show general trends in the model, and are not the only suitable values that could have been selected.

Figure 6: Contour plot shows lines of constant total traction (red-orange) and constant internal radial stress (blue-green) as a is varied on different stiffness substrates. (A) Contractility is uniform ($b = 0$): here the traction and stress contours follow similar trajectories. (B) Contractility is localised to the edge of the layer ($b = 1$): here there is a much greater overlap in traction and stress contour lines.

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Table 1: Main figures statistical values

Figure	N numbers (gels) 10	15	20	25	30	Unit	Mean 10	15	20	25	30	Standard Deviation 10	15	20	25	30	Kruskal-Wallis	Mann-Whitney 15	20	25	30
1i	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	N	122.5	109.6	150.9	104.4	116.7	23.1	23.3	50.9	34.0	26.8	0.006	0.113	0.122	0.098	0.394
1j	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	N	126.5	109.2	122.1	129.5	137.2	31.2	20.9	34.5	33.2	42.6	0.048	0.049	0.454	0.747	0.476
2c	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	μm	4.08	2.47	1.18	1.01	0.67	1.95	2.02	0.87	0.51	0.58	1.4×10^{-18}	8.1×10^{-4}	1.3×10^{-7}	3.5×10^{-8}	2.2×10^{-7}
2d	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	μm	3.34	2.20	2.14	1.11	1.15	2.58	0.97	2.54	0.94	0.80	1.4×10^{-10}	0.123	0.003	1.9×10^{-6}	6.5×10^{-7}
2e	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	Pa	8.44×10^7	4.82×10^7	3.51×10^7	4.56×10^7	2.69×10^7	4.35×10^7	1.56×10^7	2.00×10^7	2.22×10^7	1.07×10^7	4.8×10^{-9}	0.002	2.2×10^{-5}	0.001	2.0×10^{-6}
2f	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	Pa	5.75×10^7	5.13×10^7	5.23×10^7	4.78×10^7	5.91×10^7	5.23×10^7	2.25×10^7	3.15×10^7	3.15×10^7	2.77×10^7	0.255	0.434	0.684	0.421	0.070
2g	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	Pa	1859.0	1655.1	894.1	1170.6	706.5	824.9	1171.9	645.3	853.0	541.7	3.0×10^{-8}	0.116	3.9×10^{-5}	0.001	2.7×10^{-6}
2h	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	Pa	1765.8	1630.1	1927.6	1210.7	1724.3	1491.2	1037.3	2326.7	1100.3	1694.7	0.137	0.842	0.201	0.044	0.787
2i	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	pJ	26399.7	8261.6	3126.2	3272.1	1157.6	24238.5	7927.5	3417.4	3089.4	1355.2	3.2×10^{-14}	0.004	1.6×10^{-6}	3.3×10^{-6}	3.0×10^{-7}
2j	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	pJ	19440.6	7893.4	9135.1	4291.8	5959.2	42344.8	6744.3	13299.0	5777.0	7889.4	0.001	0.660	0.057	9.6×10^{-4}	0.005
3k	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	μm/s	0.138	0.136	0.110	0.112	0.110	0.079	0.062	0.050	0.021	0.024	0.172	0.827	0.163	0.758	0.570
3l	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	μm/s	0.189	0.145	0.131	0.110	0.117	0.083	0.048	0.048	0.051	0.036	6.8×10^{-6}	0.037	0.004	5.5×10^{-5}	2.2×10^{-4}
3o	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	Pa	-1.79×10^7	-1.18×10^7	-0.67×10^7	-0.75×10^7	-0.39×10^7	1.46×10^7	0.81×10^7	0.83×10^7	0.42×10^7	0.27×10^7	1.8×10^{-5}	0.192	0.006	0.023	0.003
3p	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	Pa	-2.29×10^7	-1.27×10^7	-1.66×10^7	-0.98×10^7	-1.30×10^7	2.84×10^7	0.87×10^7	1.52×10^7	0.97×10^7	1.10×10^7	0.068	0.105	0.158	0.007	0.100
3q	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	pJ	10716.3	3348.6	1435.4	973.7	-323.8	11383.4	5373.9	2772.3	726.9	2680.0	3.4×10^{-10}	0.021	2.3×10^{-4}	5.9×10^{-4}	1.0×10^{-4}
3r	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	pJ	14753.8	3660.9	3296.1	1548.7	2969.1	29915.0	4381.3	6933.5	2206.8	5415.6	3.4×10^{-5}	0.045	0.008	4.5×10^{-5}	9.3×10^{-5}
5b	32 (3)	22 (3)	69 (3)	48 (3)	61 (3)	16-bit Grey levels	15173.1	15866.3	23751.7	10.974.1	12973.7	7123.3	9272.0	10696.3	5461.2	7753.0	7.9×10^{-15}	0.867	7.1×10^{-5}	0.005	0.059
5c	34 (4)	55 (4)	59 (3)	62 (2)	41 (2)	16-bit Grey levels	15836.4	15285.4	16551.1	15368.4	14684.5	8430.0	8312.1	6529.4	7101.4	10850	0.037	0.602	0.980	0.400	0.104
5d	32 (3)	22 (3)	69 (3)	48 (3)	61 (3)	16-bit Grey levels	11168.0	11032.1	16890.4	11593.0	8938.0	5933.1	5240.4	5279.6	5762.0	4645.5	3.4×10^{-19}	0.979	2.1×10^{-7}	0.520	0.008

5e	24 (3)	32 (3)	59 (3)	62 (2)	41 (2)	16-bit Grey levels	16196.4	12414.3	8869.2	12372.9	9840.0	10533.9	6074.4	2161.9	3565.3	4245.2	5.0×10^{-12}	0.048	1.0×10^{-6}	0.081	1.9×10^{-4}
5f	32 (3)	22 (3)	69 (3)	48 (3)	61 (3)	16-bit Grey levels	15750.0	16459.8	15743.4	10402.9	11641.1	3847.4	5954.3	3990.1	3870.0	2873.5	5.4×10^{-17}	0.965	0.899	5.1×10^{-7}	1.1×10^{-6}
5g	34 (4)	55 (4)	59 (3)	62 (2)	41 (2)	16-bit Grey levels	28160.5	35148.9	18770.7	14541.5	17514.6	16042.0	12749.0	6013.8	3282.0	5099.7	7.2×10^{-26}	0.011	0.020	3.1×10^{-6}	0.002
5l (disk)	48 (4)	79 (3)	95 (3)	51 (2)	58 (3)	ratio	1.134	1.028	1.068	1.050	1.043	0.118	0.130	0.130	0.104	0.098	0.003	0.001	0.062	0.003	0.004
5l (ring)	97 (2)	24 (3)	49 (3)	33 (2)	14 (3)	ratio	1.025	1.064	1.034	1.090	1.185	0.079	0.166	0.103	0.218	0.129	2.5×10^{-4}	0.505	0.140	8.0×10^{-4}	1.2×10^{-4}

Table 2: Extended data figures statistical values

Figure	N numbers (gels)					Unit	Mean					Standard Deviation					Kruskal-Wallis	Mann-Whitney			
	10	15	20	25	30		10	15	20	25	30	10	15	20	25	30		15	20	25	30
1c	28 (7)	28 (7)	28 (7)	28 (7)	24 (6)	Pa	10810.4	14667.5	19201.8	25494.1	31418.5	2563.2	1574.4	2696.9	3795.2	2794.8	1.2×10^{-60}	1.9×10^{-7}	2.7×10^{-10}	1.3×10^{-10}	6.5×10^{-10}
1d	87 (3)	56 (3)	33 (3)	40 (1)	17 (2)	%	24.0	23.2	21.2	19.6	20.0	3.5	2.3	2.1	2.1	3.0	3.3×10^{-23}	0.002	3.0×10^{-8}	3.4×10^{-13}	1.7×10^{-6}
1e	41 (3)	13 (3)	36 (3)	15 (2)	41 (3)	%	17.6	17.2	14.7	15.4	15.5	1.7	1.7	2.3	1.6	2.5	1.2×10^{-9}	0.342	1.3×10^{-8}	1.5×10^{-4}	7.8×10^{-5}
1j	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	%	0.32	0.22	0.11	-0.13	0.53	0.90	0.71	1.01	0.71	1.29	0.227	0.970	0.945	0.123	0.560
1k	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	%	0.47	0.16	-0.42	1.12	0.12	1.62	0.60	1.22	6.72	0.71	0.288	0.615	0.074	0.389	0.652
2g	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	pixels	542025	218209	121461	114767	61743	307498	84989	67864	46357	24890	1.3×10^{-21}	2.0×10^{4}	4.7×10^{-7}	5.3×10^{-7}	1.2×10^{-7}
2h	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	pixels	350437	215146	191101	124234	122272	324791	87074	125988	84106	55581	1.2×10^{-11}	0.031	0.003	$2.8 \times 10^{-}$	6.7×10^{-8}
3i	20 (5)	23 (6)	30 (8)	25 (5)	20 (4)	seconds	26.2	16.9	20.6	18.6	22.2	295.3	81.2	45.7	36.5	111.7	0.705	0.336	0.317	0.174	0.457
3j	28 (11)	29 (11)	23 (7)	23 (6)	28 (7)	seconds	24.2	18.9	21.6	20.1	19.2	40.7	157.5	410.8	744.7	49.4	0.961	0.955	0.656	0.932	0.550