The Neuromusculoskeletal Modeling Pipeline: MATLAB-based Model

Personalization and Treatment Optimization Functionality for OpenSim

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Abstract

Neuromusculoskeletal injuries including osteoarthritis, stroke, spinal cord injury, and traumatic brain

injury affect roughly 19% of the U.S. adult population. Standardized interventions have produced

suboptimal functional outcomes due to the unique treatment needs of each patient. Strides have been

made to utilize computational models to develop personalized treatments, but researchers and

clinicians have yet to cross the "valley of death" between fundamental research and clinical usefulness.

This article introduces the Neuromusculoskeletal Modeling (NMSM) Pipeline, two MATLAB-based

toolsets that add Model Personalization and Treatment Optimization functionality to OpenSim. The two

toolsets facilitate computational design of individualized treatments for neuromusculoskeletal

impairments through the use of personalized neuromusculoskeletal models and predictive simulation.

The Model Personalization toolset contains four tools for personalizing 1) joint structure models, 2)

muscle-tendon models, 3) neural control models, and 4) foot-ground contact models. The Treatment

Optimization toolset contains three tools for predicting and optimizing a patient's functional outcome

for different treatment options using a patient's personalized neuromusculoskeletal model with direct

collocation optimal control methods. Support for user-defined cost functions and model modification

functions facilitate simulation of a vast number of possible treatments.

An NMSM Pipeline use case is presented for an individual post-stroke with impaired walking

function, where the goal was to predict how the subject's neural control could be changed to improve

walking speed without increasing metabolic cost. First the Model Personalization toolset was used to

develop a personalized neuromusculoskeletal model of the subject starting from a generic OpenSim full-

body model and experimental walking data (video motion capture, ground reaction, and

electromyography) collected from the subject at his self-selected speed. Next the Treatment

Optimization toolset was used with the personalized model to predict how the subject could recruit

existing muscle synergies more effectively to reduce muscle activation disparities between the paretic

and non-paretic legs. The software predicted that the subject could increase his walking speed by 60%

without increasing his metabolic cost per unit time by modifying existing muscle synergy recruitment.

This hypothetical treatment demonstrates how NMSM Pipeline tools could allow researchers working

collaboratively with clinicians to develop personalized neuromusculoskeletal models of individual

patients and to perform predictive simulations for the purpose of designing personalized treatments

that maximize a patient's post-treatment functional outcome.

Abbreviations

NMSM   Neuromusculoskeletal Modeling

JMP   Joint Model Personalization

MTP   Muscle-tendon Model Personalization

NCP   Neural Control Model Personalization

GCP   Ground Contact Model Personalization

TO   Tracking Optimization

VO   Verification Optimization

DO   Design Optimization

SynX   Synergy Extrapolation

IK   Inverse Kinematics

46	ID	Inverse Dynamics
47	EMG	Electromyography
48	DOF	Degrees of Freedom
49	RMS	Root Mean Squared
50	ADL	Activity of Daily Living
51	TKR	Total Knee Replacement
52	CP	Cerebral Palsy
53	GUI	Graphical User Interface
54	XML	Extensible Markup Language

55 1. Introduction

Approximately 19% of the U.S. adult population is afflicted by a movement impairment caused by

stroke, osteoarthritis, traumatic brain injury, limb amputation, cerebral palsy, Parkinson's disease, or

spinal cord injury.[1–3] In addition to the physical challenges caused by a movement impairment, these

individuals are more likely to experience increased health care costs, lower work productivity, a higher

risk of developing heart disease or diabetes, a reduction or loss of independence, and a decreased

quality of life.[1,4] At present, treatment of these life-altering impairments typically involves selection of a

standardized treatment based on subjective clinical assessment rather than design of a customized

treatment based on objective evidence-based methods. Consequently, existing treatments for

movement impairments do not address the unique clinical situation and needs of the individual patient

to the extent that they could, and should.

Not surprisingly, the standardized treatment paradigm is often unable to achieve the level of post-

treatment functional recovery that patients desire and expect. The percentage of patients who are

dissatisfied with their functional outcome following a standardized treatment supports this viewpoint.

For those who experience stroke, satisfaction with functional outcome is closely tied to ability to return

to a pre-stroke level of movement function.[5] However, stroke patient satisfaction with mobility

improvements generally declines after hospital discharge,[5] with only 65% of individuals post-stroke

recovering the ability to walk.[6] Even then, they tend to walk at a slow self-selected speed with an

asymmetric gait pattern that is less efficient metabolically than for healthy individuals.[6–8] Furthermore,

20% of stroke survivors remain dependent on others to perform activities of daily living (ADLs).[9] For

those with physician-diagnosed arthritis, roughly 44% have functional limitations that affect their ability

to perform ADLs.[10] For those who receive a total knee replacement (TKR), the best predictor of post-

surgery patient satisfaction is functional outcome.[11] However, 22% of TKR patients are dissatisfied with

their functional outcome one year after surgery,[12] while 16 to 30% are dissatisfied with their ability to

perform specific ADLs.[13] For those who receive a total hip replacement, 7% are dissatisfied with their

functional outcome,[14] with expectations for improved walking and stair climbing ability not being met in

over 30% of patients.[15] For those who receive opening wedge high tibial osteotomy surgery, 22% are

dissatisfied with their outcome, primarily due to unmet expectations for their post-surgery ability to

perform functional activities.[16] For those with cerebral palsy (CP), 33% do not improve walking speed as

a result of multi-level orthopedic surgery,[17] while 21% of parents of children with CP do not feel that

their child's orthopedic surgery was worth the time, effort, pain, and cost.[18] More than 50% of children

with CP who undo multi-level surgeries do not see improvements in their gait patterns[19]. For those with

lower limb amputation, between 12 and 32% cannot perform desired ADLs with their prosthesis, while

only 30% to 52% find the same ADLs very easy to perform.[20] Those with upper limb amputation use their

prosthesis primarily for cosmetic rather than functional reasons, with the percentage of individuals who

rate their upper extremity prosthesis as beneficial for performing various ADLs ranging from 5% to only

25%.[21] These statistics across a myriad of clinical conditions that impair movement highlight the need for

a better treatment design paradigm to help a larger percentage of patients recover their desired amount

of post-treatment function.

One possible way to improve treatment design and thus functional outcomes for individuals with

movement impairments is to employ engineering design optimization methods that utilize physics-

based computational models. Physics-based computational models have an advantage over "black box"

machine learning models since they extrapolate better to situations outside the boundaries of the

training data, which is where optimal solutions often lie. Engineering design optimization methods have

dramatically improved function and reliability of commercial products in numerous industries including

automotive, aerospace, farming, construction, and structural engineering, among others.[22–27] Using

these virtual prototyping methods, engineers can evaluate countless designs – including highly novel

ones – in a time- and cost-efficient manner to determine an optimal design for a given problem, thereby

reducing or eliminating trial-and-error design iterations performed on physical prototypes. Researchers

have already demonstrated the benefits of combining engineering design optimization with

personalized models to develop effective personalized interventions for a small number of clinical

problems.[28–33]

While a similar computational approach holds promise for designing personalized treatments for

movement impairments, at least three significant challenges must first be overcome for such an

approach to become a reality. First, researchers must be able to personalize the neuromusculoskeletal

computer models used in the computational treatment design process.[34] Published musculoskeletal

modeling studies have typically used scaled generic models rather than models whose relevant

characteristics have been personalized to a subject's movement data.[34] This decision is understandable

given the challenges of collecting the experimental movement (and possibly imaging) data needed for

the model personalization process coupled with the challenges of performing the personalization

process itself for any aspect of a model (e.g., joint functional axes). However, differences between

patients with the same clinical condition are precisely what make the clinical treatment design process

so challenging. Second, researchers must be able to perform the treatment design optimization process

using a patient's personalized neuromusculoskeletal model. Such a process requires performing

repeated predictive simulations of patient function following different implementations of a planned

intervention. To date, the majority of such simulations have been performed using "home brew"

computational software,[35–47] making it difficult for the broader research community to engage in the

process, to repeat studies performed by others, and to transfer knowledge about the process to others.

Third, researchers must have access to computational software that makes the model personalization

and treatment optimization processes easy, repeatable, and transferable. While recent software

advances such as OpenSim Moco[48] have made it possible to perform predictive simulations more easily,

neither OpenSim[49,50] nor Moco[48] provide means to personalize relevant aspects of a patient's

neuromusculoskeletal computer model or to use a personalized model to perform the treatment design

optimization process.

Several existing musculoskeletal modeling software tools have sought to address these challenges to

various degrees.[51–58] These tools primarily focus on personalizing the musculoskeletal model creation

process, including personalizing bone geometry from medical imaging data, personalizing muscle

attachment points on bones, and generating scaled generic musculoskeletal models using automated

methods. The SimCP simulation platform, designed to predict post-surgery walking function for

individuals with cerebral palsy, goes beyond other tools in several important ways.[51] It supports

personalization of Hill-type muscle-tendon model properties, personalization of neural control

properties using a muscle synergy structure, and prediction of the joint moment "capability gap" that

would remain following implementation of a proposed surgical plan. Nonetheless, none of these tools

can personalize multiple aspects of a patient's neuromusculoskeletal computer model and then use the

personalized model within a predictive simulation framework to design clinical interventions.

This article introduces the Neuromusculoskeletal Modeling (NMSM) Pipeline, a MATLAB-based

software package that provides researchers and clinicians working together with state-of-the-art

computational tools for designing effective personalized treatments for movement disorders. The

software package is built on the foundation of the OpenSim musculoskeletal modeling software and

adds two toolsets to OpenSim[49,50]. The Model Personalization toolset uses patient movement data and

gradient-based optimization to personalize four subcomponents of a patient's neuromusculoskeletal

computer model: 1) joint structure models, 2) muscle-tendon models, 3) neural control models, and 4)

foot-ground contact models. The Treatment Optimization toolset uses a patient's personalized model

with direct collocation optimal control methods[35,41,48,59–62] to predict how the patient's neural control

and/or anatomy should be changed, or how an external device (e.g., an exoskeleton) or implant should

be designed and/or controlled, to maximize improvement in the patient's post-treatment movement

function. By emphasizing functionality, ease of use, flexibility, and computational speed, the NMSM

Pipeline will hopefully accelerate involvement of the neuromusculoskeletal modeling research

community in the computational design of clinically implementable personalized neurorehabilitation

and surgical interventions.

The remainder of this article is outlined as follows. First, a design overview of the NMSM Pipeline is

presented, including an overview of the philosophy and goals of the software and an introduction to the

two included toolsets. Second, implementation details, design decisions, and important information for

each tool are presented. Third, an example treatment design use case is provided including specifics

about the use of each tool and final results. Fourth, a discussion section is included to provide

information about future work, limitations, and access to the software.

2. Design Overview

2.1 Philosophy and Goals

The goal of the NMSM Pipeline software is to help neuromusculoskeletal modeling researchers engage in clinical research - and cross the valley of death,[63] thereby moving neuromusculoskeletal modeling a significant step closer to becoming a clinically useful tool. To achieve this goal, the NMSM Pipeline uses a personalized medicine approach, where physics- and physiology-based personalized neuromusculoskeletal computer models constructed from patient movement data are used to design personalized treatments for movement impairments.[64] Such impairments arise from clinical conditions like osteoarthritis, stroke, cerebral palsy, spinal cord injury, Parkinson's disease, limb amputation, and even cancer. Because the open-source OpenSim[49,50] and commercial Anybody[65] software commonly used for musculoskeletal modeling research lack the ability to personalize neuromusculoskeletal computer models to patient movement data, these software tools cannot currently be used to optimize treatments for individual patients. To overcome this critical limitation, the open-source NMSM Pipeline software uses MATLAB (The MathWorks, Natick MA) to build on the OpenSim foundation and provides two new toolsets - a Model Personalization toolset that facilitates the creation of personalized neuromusculoskeletal computer models, and a Treatment Optimization toolset that uses the personalized models to design personalized treatments that maximize a patient's post-treatment movement function.

To develop these two new MATLAB-based toolsets, we defined a high-level software design philosophy. First, the NMSM Pipeline was designed to be both accessible for basic users and extensible for advanced users so that neuromusculoskeletal modeling researchers of all levels can benefit from it. Second, modeling and simulation methods were based on laws of physics and principles of physiology and neuroscience rather than on machine learning, since no training data exist for post-treatment

movement conditions, and machine learning methods do not, in general, extrapolate well outside the

boundaries of the training data. Third, existing OpenSim functionality and model entities were utilized to

the fullest extent possible to avoid duplication. Fourth, NMSM Pipeline functionality was designed to

have the "look and feel" of OpenSim so that those with experience using OpenSim can quickly become

proficient using the Pipeline. Fifth, the NMSM Pipeline was designed to work with any OpenSim model,

providing complete flexibility in the musculoskeletal anatomy and movement situations that can be

modeled and simulated.

To achieve the goal of accessibility for basic users and extensibility for advanced users, we designed

NMSM Pipeline tools to work using Extensible Markup Language (XML) settings files, similar to OpenSim.

This approach allows users to run each NMSM Pipeline tool with only a single line of code. For basic

users, we developed two OpenSim GUI plugins - one for the Model Personalization toolset with its four

tools, and one for the Treatment Optimization toolset with its three tools, where each toolset appears

under the OpenSim "Tools" menu. The GUI plugin window for each tool allows users to set up tool runs

by configuring the most common settings for each tool (Figure 1), with default values being used

automatically for advanced tool settings. Tool settings selected in the GUI plugin, along with default

advanced tool settings, can be exported by

Figure 1: Screenshot of the JMP GUI tool sub-window for adding a JMP task. The GUI tools allow for

modifying common settings and creating XML settings files. Advanced settings can be modified directly

in the XML file after creation.

the user to an XML settings file that can be read back into the GUI and modified as desired, just as with

OpenSim tools. For advanced users, advanced tool settings are exposed in each tool's XML settings file,

again similar to OpenSim. Advanced users can create an initial XML settings file using the GUI plugin, or

they can start from a pre-existing XML settings file and edit the values of basic and advanced tool

settings using any text editor. For both basic and advanced users, each tool is run from the MATLAB

command line using a tool-specific function that takes a tool-specific XML settings file as an input. Thus,

no "Run" button is provided in any of the GUI plugin tool windows. Tool outputs can be plotted in

MATLAB using included utility or custom functions.

Software engineering principles were used for NMSM Pipeline development to facilitate

extensibility. Namely, atomic functions - functions that complete only a single operation - were used

extensively. All code was written using clear, English-language variable and function names and

organized into logical groupings. GitHub's source control, automated testing framework, and continuous

integration tools were used to maintain this extensive project and its documentation throughout the

development process. These choices make NMSM Pipeline code easy to understand and easy to modify.

Because NMSM Pipeline tools are based on laws of physics and principles of physiology and

neuroscience, we selected computational methods that best facilitate the intended personalized

medicine approach. Gradient-based optimization was used for all tools within the NMSM Pipeline

primarily for computational speed reasons but also for the ability of gradient-based optimizers to find

better solutions than the initial guess, even if the final solution is not the global optimum. For the Model

Personalization toolset, built-in MATLAB optimization algorithms (primarily lsqnonlin and fmincon) were

used exclusively, while for the Treatment Optimization toolset, the open-source IPOPT optimizer[66] was

used within the commercial GPOPS-II direct collocation optimal control software.[60] This approach

eliminates GPOPS-II and direct collocation optimal control from the Model Personalization process,

making model personalization a more reliable and less complex process than it would be if direct

collocation optimal control were required.[41,67,68] The Model Personalization toolset automatically uses

MATLAB's built-in parallel processing capabilities for calculating finite difference derivatives needed by

MATLAB optimization algorithms, while the Treatment Optimization toolset automatically uses parallel

processing only for repeated OpenSim analyses performed through MATLAB via C++ Mex files.

Through the utilization of OpenSim's native models and entities, we included a number of

convenient facilities in the NMSM Pipeline. OpenSim native file types were used for all data interactions

including OpenSim model files (.osim), marker data files (.trc), kinematic motion and ground reaction

data (.mot), time series data (.sto), and XML settings files (.xml). Only one new file type was developed--

the NMSM Pipeline model file type (.osimx) to store personalized model properties that are not included

in native OpenSim models. Similarly, easy-to-use OpenSim GUI tools such as the Scale tool, Inverse

Kinematics (IK) tool, Inverse Dynamics (ID) tool, and Muscle Analysis tool were leveraged as part of the

typical pipeline run-through using experimental movement data. For some NMSM Pipeline tools, groups

of muscles must be identified, and the muscle groups functionality available in OpenSim models was

used for this purpose to avoid the need to store this group information elsewhere.

2.2 NMSM Pipeline Toolsets

The NMSM Pipeline is composed of two toolsets-- a Model Personalization toolset and a Treatment

Optimization toolset. The Model Personalization toolset personalizes four aspects of a scaled generic

OpenSim model using experimental movement data and gradient-based optimization (Figure 2). Those

Figure 2: Overview of the Model Personalization toolset. This toolset creates neuromusculoskeletal

models with personalized joint, muscle-tendon, neural control, and ground contact parameters through

the use of gradient-based optimization.

four aspects are 1) joint models, 2) muscle-tendon models, 3) neural control models, and 4) ground

contact models. The personalization process is important since personalized rather than generic models

are needed to support model-based treatment design for clinical conditions where patients exhibit

significant heterogeneity (e.g., stroke).[69,70] Furthermore, without a personalization process,

neuromusculoskeletal models do not reliably predict internal muscle and joint contact forces, body

motion, or metabolic cost.[41,71–78] Each stage in the NMSM Pipeline Model Personalization process has

been shown to play an important role in predicting these quantities reliably.[41,71–73,78,79]

The Treatment Optimization toolset uses the subject's personalized neuromusculoskeletal model to

predict their post-treatment movement function using direct collocation optimal control (Figure 3). Over

Figure 3: Overview of the Treatment Optimization toolset. This toolset generates a tracking

simulation and two subsequent predictive simulations through the use of direct collocation optimal

control.

the past 10 years, musculoskeletal modeling researchers have converged on direct collocation optimal

control as the best method for generating predictive simulations of human movement.[35–

37,37,40,41,48,59,67,80–88] The Treatment Optimization Toolset uses the MATLAB-based GPOPS-II direct

collocation optimal control software[60] to perform predictive simulations of movement for novel

conditions where no experimental data exist. Similar to MATLAB, GPOPS-II is inexpensive for academic

use. The optimal control solver can adjust neural and/or torque control signals along with neural

control, anatomical, internal implant, and/or external device parameters in a patient's personalized

neuromusculoskeletal model to achieve a specified treatment goal (e.g., achieve a desired reduction in

metabolic cost). For any patient, this approach can potentially provide the best treatment prescription,

the best dosage, and an estimate of the patient's capacity for improvement.

Optimization cost function terms for both toolsets were designed to minimize squared errors and/or

cost term values and utilize a common formulation with physically meaningful cost function parameters.

Specifically, cost function terms utilize a maximum allowable error and, in some cases, a user-provided

error center (Figure 4). For example, if a cost function term seeks to minimize errors between model and

$$cost = \frac{1}{npts} \sum_{i=1}^{npts} \left(\frac{x_i - error\_center}{max\_allowable\_error} \right)^2$$

Figure 4: The generic cost function term formulation used throughout the Model Personalization

and Treatment Optimization toolsets. The formulation utilizes a maximum allowable error and error

center to make the calculated cost physically meaningful. If the difference between the current value

and the error center is greater than the maximum allowable error, then the quantity in parentheses will

be greater than 1, and squaring this quantity will amplify the cost (e.g., 1.1^2 = 1.21). In contrast, if the

difference between the current value and the error center is less than the maximum allowable errors,

then the quantity in parentheses will be less than 1, and squaring this quantity will attenuate the cost

(e.g., 0.9^2 = 0.81). Some cost function terms track experimental time-varying data, these have an

implicit error center of the experimental data value. Some cost function terms minimize errors relative

to a static reference value. The type of the cost function term is included in the name for Treatment

Optimization cost function terms.

experimental joint moments, and matching to within 2 Nm is acceptable, then the user would set their

cost term error center to 0 and the associated maximum allowable error to 2. Each cost function term

has equal weight with all other cost function terms included in the optimal control problem formulation,

where continuous cost function terms involving time series data (e.g., joint angles, joint moments) are

normalized by final time so that they do not contribute to the total cost more heavily than do terminal

cost function terms involving only a single quantity (e.g., metabolic cost). This method for formulating all

cost function terms allows for contextualized decision-making when determining weights for different

cost function terms.

Neural control models for both toolsets are described using muscle synergies. Muscle synergies

provide a physiologically-relevant low dimensional representation of a large number muscle activations

and can be personalized to represent a specific patient's neural control strategy.[89–97] Each muscle

synergy is composed of a time-varying synergy activation and an associated time-invariant synergy

vector. Each synergy vector contains a weight for each muscle in the model that defines how the

associated synergy activation contributes to the total activation of the muscle. Muscle synergies are

commonly calculated using non-negative matrix factorization,[89,90] and typically between three and six

muscle synergies are required to account for over 95% of the signal variability for common tasks such as

walking, running, and reaching.[98]

3. Implementation Details

3.1 Model Personalization

The Model Personalization toolset calibrates parameter values in an OpenSim neuromusculoskeletal model so that the model closely reproduces a wide range of experimental movement data. The toolset consists of four tools and was designed so that the tools can be used largely independently from one another, though a preferred tool workflow exists. Personalization is likely to be necessary if the musculoskeletal model is to be used for clinical treatment design purposes.[34] It also improves models for use in predictive simulations by maximizing the self-consistency of collected experimental data and easing the task of finding a realistic, dynamically consistent motion.

The four tools of the Model Personalization toolset personalize different anatomical, physiological, and neurological aspects of a patient's OpenSim model. Joint Model Personalization (JMP) calibrates the properties of OpenSim constraint-based joint models, Muscle-tendon Model Personalization (MTP) calibrates the properties of Hill-type muscle-tendon models, Neural Control Model Personalization (NCP) calibrates the properties of muscle synergy control models, and Ground Contact Model Personalization (GCP) calibrates the properties of elastic foundation foot-ground contact models. OpenSim models personalized using the Model Personalization toolset can be used in both the NMSM Pipeline's Treatment Optimization Toolset and, in the near future, OpenSim Moco. For use with OpenSim Moco, an NMSM Pipeline .osimx model file must be converted to an OpenSim .osim model file using an provided MATLAB model conversion utility program.

The Model Personalization toolset requires input data generated using standard OpenSim tools. First, a generic musculoskeletal model is scaled using the OpenSim Scale Model tool. To facilitate modeling and simulation of full-body walking motions, we recommend starting with the RCNL2023 OpenSim model (distributed with the NMSM Pipeline software), which is a modified version of the

Rajagopal full-body OpenSim model[99] where the ankle joint kinematic model has been changed to match

van den Bogert et al. (1994)[100] and the knee joint kinematic model changed to eliminate all rotational

offsets while producing the same motion. A scaled generic model is one of the required inputs for the

JMP tool. After the joints of the model are personalized to the individual's functional joint axes using the

JMP tool, the user must calculate IK motions and ID loads using the OpenSim Inverse Kinematics and

Inverse Dynamics tools, respectively. The user must then run the Muscle Analysis tool to calculate

muscle-tendon lengths and velocities as well as muscle moment arms if the NMSM Pipeline MTP and

NCP tools are to be used. For the JMP tool, marker files can be manually concatenated to personalize

joint parameters, values that characterise the transformation of the parent and child bodies of a joint,

using multiple motion trials (e.g., marker data from isolated ankle, knee, and hip motion trials can be

concatenated with marker data from a walking motion trial to calibrate the functional axes and joint

centers of all lower body joints simultaneously). The MTP and NCP tools accept data from one or more

motion trials, and the GCP tool accepts data from only a single motion trial, ideally the same trial to be

used for Treatment Optimization. If multiple motion trials are used with either the MTP or NCP tools, IK

motions, ID loads, muscle-tendon lengths and velocities, and muscle moment arms need to be

calculated for each motion trial.

3.1.1 Joint Model Personalization

The Joint Model Personalization tool optimizes joint parameters, body scaling, and marker

placement to minimize IK marker distance errors.[100–106]. Reducing inverse kinematics marker distance

errors reduces downstream errors in calculated inverse dynamic joint moments[72], muscle-tendon

lengths and velocities, muscle moment arms, and ultimately muscle activations and forces. These

quantities are used by subsequent Model Personalization tools.

JMP tool inputs are a scaled generic OpenSim model and marker data from one or more motion

trials, where the tool settings file allows the user to specify one or more tasks (Figure 5). The design

Figure 5: Flowchart showing the inputs to and outputs from the JMP tool. The diagram key also

applies to Figs. 6 through 9.

variables available in a JMP settings file include joint locations and orientations in parent and child

bodies, body scale factors applied uniformly, and marker location offsets for each direction

independently. The only cost function term is the sum of the squared marker distance errors normalized

by the motion trial duration and number of markers. No constraints are included in this optimization

problem. The output of JMP is a new OpenSim model with optimized joint parameters, body scale

factors, and/or marker placements.

Several important considerations should be kept in mind when using the JMP tool. A JMP run can be

split into multiple tasks, each with its own set of design variables and an associated marker file. Careful

JMP setup is required to avoid obtaining non-anatomical results. Such a result could be found by

personalizing a joint parameter for a coordinate that does not move through sufficient range of motion

(> ~25 degrees) during the motion trial[107]. This issue can be rectified by personalizing the associated

joint parameters with separate tasks using isolated joint motion trials, or by concatenating data from an

isolated joint trial with data from the desired functional trial (e.g., walking). Another cause of non-

anatomic results is selection of joint parameters that produce relative bone motions that are

inconsistent with joint function. For example, the parent frame of the hip joint is often defined to be at

the center of the acetabulum, while the child frame is often defined to be at the center of the femoral

head. Allowing joint parameters to modify the location of the hip joint in either the parent or the child

frame could move the center of the femoral head out of the center of the acetabulum, breaking that

anatomical relationship. In addition, muscle paths and/or relative body sizes may also become non-

anatomical due to inclusion of inappropriate design variables. JMP tool results should be visualized in

the OpenSim GUI and problem formulations modified to achieve an anatomically realistic post-JMP

model.

3.1.2 Muscle-tendon Model Personalization

The Muscle-tendon Model Personalization tool finds an optimal set of subject-specific muscle-

tendon properties and muscle activations from EMG, joint kinematic, and joint moment data by

balancing optimization cost function terms related to muscle properties, similarity of properties among

grouped muscles, and matching of EMG-driven and experimental inverse dynamics joint

moments.[75,76,108,109] Muscle activation and force predictions are sensitive to optimal muscle fiber length

and tendon slack length.[71,110–112] Therefore, reliable personalization of these parameters is essential for

generating reliable predictions of muscle activations and forces during predictive simulations of

movement.

The inputs to the MTP tool are a post-JMP OpenSim model as well as IK motion, ID load, muscle-

tendon length and velocity, and muscle moment arm data from one or more motion trials of interest

(Figure 6). The design variables that can be optimized include activation dynamics and muscle-tendon

length parameters for each muscle.[41,75,113] Cost function terms used by the MTP tool

Figure 6: Flowchart showing the inputs to and outputs from the MTP tool. The diagram key is

included in Fig. 5.

minimize muscle-tendon model parameter deviations from initial values, ID joint moment tracking

errors, passive muscle forces, inconsistencies among grouped normalized muscle fiber lengths,

inconsistencies among grouped muscle excitation scale factors, and inconsistencies among grouped

electromechanical delays. No constraints are applied in this optimization problem. The outputs of the

MTP tool are a .osimx model file containing optimized muscle-tendon properties and estimated muscle

activations, both for use by other tools in the NMSM Pipeline.

Several important considerations should be kept in mind when using the MTP tool. Muscle Tendon

Length Initialization is included as an option within the MTP tool and is typically used to find initial

values for muscle-tendon length parameters that act as reasonable reference values for cost function

deviation terms involving muscle-tendon length parameters. Muscle Tendon Length Initialization also

estimates the maximum isometric force of each muscle based on published regression relationships.[114]

Since scaling maximum isometric force and muscle excitation at the same time produces a non-unique

muscle force solution, and since muscle excitations are scaled using EMG scale factor design variables,

maximum isometric force is held constant during an MTP tool run.[71] Synergy Extrapolation (SynX)[115,116] is

also included in the MTP tool to estimate the activations of muscles without experimental EMG data.

SynX uses muscle synergy concepts to estimate missing activations and is more accurate than

traditionally used static optimization at predicting missing EMG signals[117]. A typical use case for SynX is

estimating the activations of deep muscles from which EMG data cannot be easily collected. SynX can

use either principal component analysis or non-negative matrix factorization to calculate the muscle

synergies needed to predict muscle activations associated with missing EMG data. The MTP tool uses a

Hill-type muscle-tendon model with a rigid tendon and assumes that muscles function primarily on the

ascending region of their normalized active force-length curves.[118] Users can modify cost terms to

specify the region of the normalized force-length curve over which muscles are assumed to operate.

Some MTP cost function terms, such as inconsistencies among grouped normalized muscle fiber lengths,

calculate the difference between the grouped values relative to their mean. These cost terms are

intended to promote similarity in muscle properties within a group under the assumption that similar

muscles, such as the three uniarticular vastus muscles, should have similar properties. These muscle

groups must be defined within the OpenSim model. Similar cost function terms are also present in NCP.

3.1.3 Neural Control Model Personalization

The Neural Control Model Personalization tool finds muscle synergies that are as consistent as

possible with ID joint moments and, when available, MTP-estimated muscle activations. The NCP tool

fits muscle synergies at the level of muscle activations (i.e., after electromechanical delay and activation

dynamics) for regions of the body where either all muscle activations are available from the MTP tool

(e.g., the right lower extremity) or no muscle activations are available.[119,120] The tool can also be used to

find muscle synergies in multiple regions of the body simultaneously - some with and some without

previously calculated muscle activations. During the NCP optimization process, grouped muscle

properties are maintained and activation-related cost function terms are minimized. Muscle synergies

are typically calculated from muscle activations alone using non-negative matrix factorization, and thus

the muscle activations reconstructed from the resulting synergies will not closely reproduce ID joint

moments when input into a subject's musculoskeletal model. NCP rectifies this issue by optimizing

synergy activations and synergy vectors to be consistent with both ID joint moments and available

muscle activations simultaneously.

The inputs to the NCP tool are a post-JMP OpenSim model as well as data for IK motions, ID loads,

muscle-tendon lengths and velocities, muscle moment arms, and, optionally, MTP-calculated muscle

activations from one or more motion trials of interest (Figure 7). The OpenSim model must contain

Figure 7: Flowchart showing the inputs to and outputs from the NCP tool. The diagram key is

included in Fig. 5.

muscle groups that define lists of muscles for which synergy sets are to be fitted (e.g., all right leg

muscles). The design variables for the NCP tool are a set of time-varying synergy activations and an

associated set of time-invariant synergy vectors. The cost function terms for the NCP tool minimize ID

joint moment matching error, MTP muscle activation matching errors, muscle activations,

inconsistencies among grouped normalized muscle fiber lengths, and inconsistencies among grouped

muscle activations. The NCP tool includes a constraint that the sum of the muscle weights in each

synergy vector must equal a constant times the number of muscles described by that synergy. Upon

output, the synergy vectors and synergy activations are normalized such that the largest weight in each

synergy vector is one. The NCP tool produces a set of synergy groups inside a new or pre-existing NMSM

Pipeline model file (.osimx) as well as data files (.sto) containing synergy activations and their associated

synergy vectors.

Several important considerations should be kept in mind when using the NCP tool. Synergy-driven

Tracking Optimization (TO), part of the Treatment Optimization toolset, requires that NCP tool results be

used as the initial guess. NCP results that distribute errors equally between MTP muscle activation

matching and ID joint moment matching will facilitate the process of finding good synergy-driven TO

results. In addition, to facilitate obtaining good NCP results, users should perform their own synergy

analysis on the muscle activations produced by MTP to determine the optimal number of synergies to

use. The number of synergies should be selected to achieve the desired variability accounted for (VAF),

which is often set at 90 or 95%.[41,93,121,122] The NCP tool can be run without having MTP tool results as

inputs through the use of the activation minimization cost function term. Since running the NCP tool

without MTP tool results produces a non-unique solution, the maximum allowable error of the

activation minimization cost function term can be set to achieve a unique solution that contains

activations of expected magnitude. Shared synergy vectors between synergy groups can also be

enforced by the NCP tool. This feature allows for two muscle synergy groups, such as those for right and

left leg muscles, to have nearly identical synergy vectors.

3.1.4 Ground Contact Model Personalization

The Ground Contact Model Personalization tool finds physical properties for elastic foundation foot-

ground contact models that closely reproduce experimental ground reaction forces and moments while

allowing slight changes in foot kinematics. The elastic foundation is composed of a uniform grid of linear

springs with nonlinear damping and friction placed across the bottom of the foot. The tool can

personalize ground contact models for each foot separately, where physical properties will differ

between the two feet, or both feet together, where physical properties will be the same for the two

feet. Currently, the tool works with only a two-segment foot model composed of a hindfoot segment

(including calcaneus, cuboid, navicular, cuneiform, and metatarsal bones) and a toes segment (including

phalange bones). While generic foot-ground contact models can reproduce experimental ground

contact forces accurately, they reproduce experimental ground reaction moments less accurately,

introducing errors into the lower body joint moments generated by predictive simulations of walking.[79]

Personalized foot-ground contact models can overcome this issue by reproducing experimental ground

reaction moments as well.

The inputs to the GCP tool are a post-JMP lower-body or full-body OpenSim model along with IK

motion and associated ground reaction data for a walking trial, where the IK and ground reaction data

must possess the same time increments (Figure 8). The ground reaction data must contain three forces,

Figure 8: Flowchart showing the inputs to and outputs from the GCP tool. The diagram key is

included in Fig. 5.

three moments, and a point about which the moments are calculated, which is typically either a time-

invariant point fixed in the laboratory or a time-varying center of pressure. The tool automatically strips

off both feet from the lower-body or full-body OpenSim model and creates a 6 degrees of freedom

(DOF) custom joint connecting each specified hindfoot body to ground. The design variables for the GCP

tool are stiffness coefficients unique to each spring with a nonlinear viscous damping coefficient, a

dynamic friction coefficient, a viscous friction coefficient, and a spring resting length common to all

springs. Additional design variables are B-spline nodal points defining small deviations from

experimental foot kinematics with respect to ground. The cost function terms for the GCP tool include

minimization of foot marker position errors, foot marker velocity errors, hindfoot and toes segment

rotational coordinate errors, hindfoot segment translational coordinate errors, vertical ground reaction

force errors, horizontal ground reaction force errors, ground reaction moment errors, and spring

coefficient deviations from neighboring spring coefficient values. No constraints are present in this

optimization problem. The output of the GCP tool is a new NMSM Pipeline model file (.osimx) containing

foot-ground contact model parameter values.

Several important considerations should be kept in mind when using the GCP tool. The tool can

reproduce all six components of ground reactions with good fidelity. To facilitate reproducing ground

reaction moments, we use the time-varying projection of a midfoot superior marker onto the ground as

the point about which ground reaction moments are calculated. This automatic recalculation of the

ground reaction moments helps keep the moments well-scaled during a GCP run, since the moment arm

of the ground reaction force vector never becomes excessively large. The center of pressure is not used

for joint moment matching since it becomes inaccurate at the transitions into and out of contact due to

division by small vertical ground reaction force values. At this time, the GCP tool requires the use of a

two-segment foot model with the distal toes segment connected to the hindfoot segment via an oblique

pin joint. Before personalization, the GCP tool automatically extracts two-segment OpenSim foot models

from the post-JMP lower-body or full-body OpenSim model and automatically calculates hindfoot

kinematics with respect to ground that are consistent with the input lower-body or full-body kinematics.

Since the foot-ground contact model is sensitive to foot kinematic changes below the measurement

accuracy of a markered motion capture system, the GCP tool allows for small changes to the foot

motion trajectory to facilitate ground reaction matching. Each foot model possesses seven coordinates:

six ground-to-hindfoot coordinates via a 6 DOF custom joint and one toes coordinate via a pin joint.

Coordinate deviations are parameterized with B-spline nodes to reduce the number of design variables.

The GCP tool automatically estimates the number of B-spline nodes needed based on a specified

lowpass filter cutoff frequency. Another important feature of the GCP tool is its ability to use a different

time window for calibrating each foot. This feature facilitates the use of the GCP tool with ground

reaction data obtained from labs possessing only two in-ground force plates. The GCP tool also allows

for symmetric physical properties between contact surfaces on the two feet, and users can modify the

number of springs along each dimension of the grid.

3.2 Treatment Optimization

The Treatment Optimization toolset generates predictive simulations of a patient's post-treatment

movement function by optimizing specified treatment design parameters. The toolset consists of three

tools designed using a "theme and variation" approach, where the tools are intended to be used in a

specific order, with each tool serving a distinct purpose. Each tool uses the GPOPS-II direct collocation

optimal control software for MATLAB[60] and maintains a consistent structure for data inputs, problem

design, cost function terms (see Table S1), constraint terms (see Table S2), and outputs, with variations

(Figure 9). The Tracking Optimization tool (TO) generates "starting point" predictive simulations of

540

Figure 9: Flowchart showing the inputs to and outputs from the tools included in the Treatment

Optimization toolset. Since these tools follow a theme and variation approach, various data

combinations can be included or excluded based on the goals of the user. The diagram key is included in

Fig. 5.

patient movement that are dynamically consistent and closely reproduce all relevant experimental

movement data available from the patient (e.g., joint motion, joint moment, ground reaction, and EMG

data). The Verification Optimization tool (VO) starts from the Tracking Optimization solution and verifies

that the controls found produce the correct motion without tracking the motion directly, which ensures

that the subsequent treatment design problem is well formulated before simulated treatments are

explored. Finally, the Design Optimization tool (DO) starts from the Verification Optimization solution,

applies and (if desired) optimizes simulated treatments, and predicts the patient's resulting post-

treatment movement along with associated controls and loads. All three tools work with torque

controlled, muscle synergy controlled, and combined torque and muscle synergy controlled problem

formulations.

Several important considerations should be kept in mind when working with the Treatment

Optimization toolset. Direct collocation optimal control problems are solved by modifying states and

controls simultaneously to minimize an objective function and fulfill constraints. For Treatment

Optimization, the states consist of joint positions and velocities for selected OpenSim model coordinates

and the controls consist of corresponding joint accelerations (due to the use of an implicit dynamics

formulation[59]), torque controls, synergy controls, or both. All Treatment Optimization tools accept both

a "tracked quantities" and an "initial guess" directory. The tracked quantities directory contains

reference data (e.g., experimental joint positions, joint moments, muscle activation, and ground

reactions) to be tracked by specified cost function terms while the initial guess directory contains data

specifying the initial guess for the problem's states and controls. Treatment Optimization XML settings

files allow for joint position, velocity, and acceleration range scale factors as well as muscle synergy and

torque controller range scale factors. These range scale factors describe the search space of the optimal

 control problem by confining the states and controls to be within a certain range relative to their initial

range (see Figure 10). After a completed run, all Treatment Optimization tools output the same files to a

Figure 10: Illustration showing how range scale factors are used to set bounds on the states and

controls within GPOPS-II. The range scale factor value is used to set the maximum and minimum

searchable spaces for the states and controls as offsets beyond the initial range. In this figure, a range

scale factor of 0.5 was used.

user-specified results directory. Specifically, the solution's states and controls, along with IK motions, ID

loads, and ground reactions calculated from the solution's states and controls, are output to the

specified directory. Saved states and controls can then be passed to the next Treatment Optimization

tool as an initial guess to pick up where the previous tool left off.

Because Treatment Optimization tools use implicit dynamics,[41,59] several constraint terms must be

included for successful use of the toolset. One constraint is that the joint acceleration controls must be

the first time derivatives of the joint velocity states, and the joint velocity states must be the first time

derivatives of the joint position states. These constraints are handled internally by GPOPS-II. Another

constraint is that the net joint loads produced by the torque and synergy controls must be consistent

with the model's inverse dynamic loads. This constraint must be handled by the user by including kinetic

consistency constraint terms for all controlled coordinates included in the problem formulation. In

addition, if users want their Treatment Optimization solutions to be dynamically consistent, then the

root segment residual load constraint must be included to ensure that the residual loads acting on the

model's root segment (i.e., the segment connecting the model to ground) are close to zero. In addition,

if the motion of interest is expected to be periodic, such as for walking, running, cycling, or stair-

climbing, joint position and velocity and ground reaction force and moment periodicity constraints can

be used to ensure that a near-periodic motion is found.

3.2.1 Tracking Optimization

The Tracking Optimization tool uses a personalized model to produce a dynamically consistent

movement simulation that closely reproduces all available experimental motion data, including joint

motions, joint moments, ground reaction forces and moments, and muscle activations. To achieve a

dynamically consistent motion, the tool spreads out matching errors between the different

experimental quantities based on user-specified maximum allowable errors. The tool accepts a post-JMP

OpenSim model (.osim file) and personalized NMSM Pipeline model (.osimx file) along with

experimental IK motions, ID loads, ground reactions, muscle-tendon lengths and velocities, muscle

moment arms, and, if using synergy controls, NCP results for the trial of interest. The following cost

function terms are commonly included to achieve a successful Tracking Optimization run: generalized

coordinate tracking, generalized speed tracking, inverse dynamic moment tracking, muscle activation

tracking, external force tracking, and external moment tracking. Common constraint terms include

kinetic consistency, state position periodicity, state velocity periodicity, and root segment residual load

bounding.

Several important considerations should be kept in mind when using the Tracking Optimization tool.

Finding a good result with the Tracking Optimization tool is the biggest challenge in the NMSM Pipeline.

The goal is to trade off errors between tracked experimental data sources by modifying the maximum

allowable error in each cost function term based on the importance of and confidence in the respective

experimental data. Higher quality Model Personalization results and highly consistent tracked

experimental quantities (e.g., tracked muscle activations should closely reproduce tracked ID moments)

make finding a good Tracking Optimization solution easier.

3.2.2 Verification Optimization

The Verification Optimization tool is used to perform a "dry run" Design Optimization without

including any "design elements", the goal being to ensure a good initial guess and to verify the

appropriateness of the optimal control problem formulation. The tool accepts the same inputs as the TO

tool, but in general, the results directory of a TO run is used for both the initial guess and tracked

quantities. The cost function terms for the VO tool include controller tracking and, for uncontrolled

joints, generalized coordinate tracking. Similar to the TO tool, the VO tool includes constraint terms for

kinetic consistency, state position periodicity, state velocity periodicity, and root segment residual load

bounding. If a VO problem is well formulated, it should converge quickly since the initial guess is already

at the optimal solution.

Several important considerations should be kept in mind when using the Verification Optimization

tool. Users must decide whether each coordinate should be controlled or tracked. If controlled, the

coordinate should be assigned the same controller (synergy, torque, or both) as in the TO tool, and the

controls should be tracked by the VO tool. Conversely, if the coordinate does not have a controller or

has a non-essential controller, then the coordinate should be tracked by the VO tool. An example of a

non-essential controller is a torque controller on an upper body joint for a full body gait model with only

lower body muscles. The results of a VO run should closely match the outputs of the TO run used to

define the initial guess and tracked quantities. If the results do not match closely, then a problem

formulation issue is likely present, and users should review their TO and VO settings. Examples of

potential problem formulation issues are having a generalized coordinate that is neither controlled nor

tracked, having a generalized coordinate that is both controlled and tracked, or having a generalized

coordinate that is tracked with a different maximum allowable error than was used by TO. Each of these

situations can produce a VO solution that differs from the TO initial guess. After an adequate VO

solution is found, users can move on to the DO tool by adding a "treatment" to their VO problem

formulation.

3.2.3 Design Optimization

The Design Optimization tool predicts or optimizes how a planned treatment will affect a patient's

post-treatment movement function. The tool accepts the same inputs as the other Treatment

Optimization tools, but typically VO results are used as the initial guess. Similar to VO, DO allows for

controller tracking and generalized coordinate tracking alongside other DO-specific cost function terms.

Similar to TO and VO, DO can use kinetic consistency, state position periodicity, state velocity

periodicity, and root segment residual load constraint terms as well as other constraints to facilitate the

design of a personalized intervention.

Several important considerations should be kept in mind when using the Design Optimization tool.

Unlike the other Treatment Optimization tools, the DO tool allows for both fixed and free final time

problem formulations. For free final time problems, the time vector can be constrained to a user defined

range and tracked control quantities are stretched or compressed in time to match the current time

vector. A number of built-in cost function terms have been included in the DO tool. These terms include

minimizing braking and propulsive impulse errors from target values, metabolic cost per unit of time or

distance[123] errors from a relative target value, whole-body angular momentum error from a target

value, and joint mechanical energy generation or absorption errors from a target value. Two key

features of the DO tool are support for model modification functions and user-defined cost function

terms. By employing model modification functions alongside GPOPS-II's static parameters feature, users

can change the OpenSim musculoskeletal model, modify the neural control model, or adjust parameter

values in an assistive device. Possible model modifications include changing bone geometry (e.g.,

osteotomy parameters), changing muscle-tendon properties (e.g., strengthening muscles or adjusting

optimal muscle fiber lengths), changing neural control properties (e.g., altering synergy vector weights

or synergy activation profiles), modifying ground contact model parameters, optimizing muscle

attachment locations or muscle wrapping surface parameters, redefining joint parameters, and

modifying external device design and/or control parameters. User-defined cost function terms allow

users to write a custom MATLAB function, with a specific function signature, that is added as an

additional cost function term given the iteration's states, controls, and static parameters.

4. Example Application

4.1 Treatment Design Rationale

To demonstrate the capabilities of the NMSM Pipeline, we employed it to investigate a hypothetical

treatment to improve walking speed and function for an individual post-stroke. Published studies have

hypothesized that time-varying synergy activations originate in the brain while time-invariant synergy

vectors reside in the spinal cord.[124,125] If this hypothesis is true, then one might expect a stroke to affect

a patient's synergy activations but not synergy vectors.[125] This expectation in turn suggests that an

individual post-stroke may have similar synergy vectors between the two legs but lack the ability to

recruit one or more of them effectively on the paretic side. Furthermore, published studies have

reported that a stroke results in altered neural coordination even on the non-paretic side.[126–128] Taken

together, these observations lead to the hypothesis that a stroke may impair recruitment of one or

more synergy activations in the paretic leg, resulting in altered recruitment of one or more synergy

activations in the non-paretic leg, and that restoration of these impaired and altered synergy activations

could result in improved self-selected walking speed and metabolic cost.[128–130]

To investigate this hypothesis, we used the NMSM Pipeline to design a hypothetical treatment that

would modify paretic and non-paretic leg synergy activations for an individual post-stroke with the goal

of increasing his self-selected walking speed without increasing his metabolic cost. Previously published

experimental walking data collected from an individual post-stroke with a self-selected walking speed of

0.5 m/s were used for the investigation.[41] Research has shown that both healthy individuals and

individuals post-stroke tend to choose a self-selected walking speed to achieve a desired metabolic cost

per unit time.[131] Furthermore, to achieve successful community ambulation (as defined by the walking

speed required to cross a typical street before the light changes[132]), individuals should be able to walk at

a self-selected speed of 0.8 m/s.[132,133] Thus, the specific goal of the hypothetical treatment was to

increase the subject's self-selected walking speed to 0.8 m/s while maintaining the same metabolic cost

per unit time estimated for the subject's original self-selected walking speed of 0.5 m/s.

4.2 Experimental Data Collection

As described in Meyer et al. (2016),[41] the experimental data used for the present study were

collected from a high-functioning hemiparetic subject with chronic stroke-related walking dysfunction

(sex male, age 79 years, LE Fugl-Meyer Motor Assessment 32/34 pts, right-sided hemiparesis, height 1.7

m, mass 80.5 kg). Experimental data collection was approved by the University of Florida Health Science

Center Institutional Review Board (IRB-01) and the Malcom Randall VA Medical Center Research and

Development Committee, and the subject gave written informed consent prior to participation. Motion

capture (Vicon Corp., Oxford, UK), ground reaction (Bertec Corp., Columbus, OH, USA), and

electromyography (EMG) data (Motion Lab Systems, Baton Rouge, LA, USA) were collected

simultaneously while the subject walked on a split-belt instrumented treadmill with belts tied. The

subject walked at his self-selected speed of 0.5 m/s and fastest comfortable speed of 0.8 m/s. To

facilitate ground contact model personalization, the subject wore Adidas Samba Classic sneakers, which

possess a flat sole with neutral midsole. Motion capture data utilized a full-body marker set with one

marker at each toe tip, three markers on each hindfoot, shank, and thigh, three markers on the pelvis,

and one marker on each acromion, elbow, and wrist (Reinbolt et al., 2005; Fregly et al., 2007). Ground

reaction data from each treadmill force plate included three force and moment components along with

the location of the fixed point used for moment calculations. EMG data included a combination of

surface and fine-wire electrodes collected from 16 muscles on each leg, including deep muscles

adductor longus, iliopsoas, tibialis posterior, extensor digitorum longus, and flexor digitorum longus.

Processing of marker motion, ground reaction, and EMG data followed a previously published

protocol.[41] Marker motion and ground reaction data were filtered at a variable cut-off frequency of 7/tf

Hz, where tf is the period of the gait cycle being analyzed, using a fourth-order zero phase lag

Butterworth filter.[134] EMG data were high-pass filtered at 40 Hz,[75] demeaned, rectified, and low-pass

filtered at a variable cut-off frequency 3.5/tf Hz using a fourth-order zero phase lag Butterworth filter.

Each processed EMG signal was normalized by the maximum value over all walking cycles and then

offset so that the minimum value was zero. For both walking speeds, the single most periodic walking

cycle (heel strike to heel strike for the paretic right leg) was selected for analysis, and all data for this

one cycle were resampled to 101 time points. After resampling, EMG data were padded with 200

milliseconds (18 time points) before the start of the cycle to account for electromechanical delay.

4.3 Model Personalization Process

We utilized all four tools in the Model Personalization toolset to personalize a full-body

neuromusculoskeletal model of the subject being studied. The starting point for the model

personalization process was a scaled RCNL2023 full-body OpenSim model, where scaling was performed

using the OpenSim Model Scaling tool with experimental marker data collected from the subject during

a static standing trial. All subsequent NMSM Pipeline tool runs were performed on a Dell PC workstation

possessing 48 cores.

First, the JMP tool was used to personalize lower body joint parameters and lower body scaling by

minimizing IK marker distance errors. The selected 0.8 m/s gait cycle marker data were used for all JMP

tool tasks. To avoid non-anatomical muscle paths around the hip complex, the left and right hip joint

parameters were not personalized. The left and right knee and ankle joints were personalized, but the

subtalar joint was not personalized because the joint did not move through a sufficient range of motion

to personalize the joint's parameter values accurately. The JMP tool reduced marker distance errors for

the thigh, shank, and foot markers by 48.4% for the gait cycle of interest. Additional JMP results are

included in Table 1 and in the supplementary material. Convergence was achieved after approximately

90 minutes of CPU time.

738   **Marker Distance Errors Before and After Joint Model Personalization**

	RMS (mm)		Max (mm)	
	Pre-JMP	Post-JMP	Pre-JMP	Post-JMP
Right Knee	7.5	4.2	18.5	11.8
Right Ankle	6.1	3.3	16.9	9.1
Left Knee	9.5	4.1	26.3	12.8
Left Ankle	6.5	3.2	16.4	10.1

739   **Table 1:** RMS and maximum marker distance errors (mm) for the right and left knee and ankle (including

740   subtalar) joints. Markers included in each joint's JMP marker set included thigh and shank markers for

741 each knee joint and shank and foot markers for each ankle joint. These markers were used to find the

742 pre- and post-JMP RMS and maximum marker distance errors.

744  Second, the MTP tool was used to personalize the properties of all lower body muscles by

745 minimizing errors in matching inverse dynamic joint moments and changes in initial muscle-tendon

746 parameter values while also predicting missing EMG signals for deep or "small" muscles (e.g.,

747 piriformis). Before the MTP tool was run, the OpenSim Inverse Kinematics, Inverse Dynamics, and

748 Muscle Analysis tools were run from the OpenSim GUI using the selected 0.8 m/s walking cycle data.

749 Using the outputs of these GUI tools, an NMSM Pipeline utility script processed EMG data, calculated

750 muscle-tendon velocity from muscle-tendon length data, and automatically organized the trial data into

751 the directory structure required by the MTP tool. Muscle groups were added to the post-JMP OpenSim

752 model to group muscles based on normalized fiber length similarity and activation similarity. Muscle-

753 tendon Length Initialization was used to find initial values for optimal muscle fiber length and tendon

754 slack length. At that point, muscle-tendon model and activation dynamics parameter values were

755 personalized. This process was repeated for each leg separately via separate runs of the MTP tool. After

756 the MTP tool was run for both legs, the left leg was found to match lower body joint moments with an

757 average root mean square (RMS) error of 3.5 Nm and the right leg with an average RMS error of 2.1 Nm.

758 Joint-specific moment matching results are included in Table 2 with additional plots available in the

759 supplementary material. A custom script was used to combine the left and right leg results for use by

760 the NCP tool. Convergence was achieved after approximately 30 minutes of CPU time.

762  **Lower Body Joint Moment Matching Errors following Muscle-tendon Model Personalization**

Joint Coordinate	Hip Flexion	Hip Adduction	Hip Rotation	Knee Angle	Ankle Angle	Subtalar Angle

Right (Nm)	2.9	2.7	3.1	1.7	1.0	1.5
Left (Nm)	5.8	4.3	4.8	2.2	2.4	1.5

Table 2: RMS errors between net joint moments calculated by the OpenSim ID tool and those calculated

by the NMSM Pipeline MTP tool following muscle-tendon model personalization.

Third, the NCP tool was used to calculate lower body muscle synergies (i.e., synergy vectors and

activations) by minimizing errors in matching inverse dynamic joint moments and muscle activations

produced by the MTP tool. Given our treatment design rationale above, we assumed that the subject's

synergy vectors were the same while his synergy activations were different for the two legs. As a result,

the NCP tool was used with the bilateral synergy vector symmetry option enabled. Synergy sets were

defined as muscle groups denoting the right and left legs. A previous synergy analysis performed on the

subject's processed EMG data indicated that six synergies were sufficient to account for the signal

variability even with the added synergy vector symmetry constraint. Muscle Tendon Length Initialization

was not performed as part of this NCP tool run because all muscles had MTP-derived muscle activations

and thus the activation minimization term was not used. The muscle synergies found by the NCP tool

reproduced all lower body joint moments with an average RMSE of 2.2 Nm and all MTP-derived muscle

activations with an average RMSE of 0.034. Additional NCP results are included in Table 3 and in the

supplementary material. Convergence was achieved after approximately 3 hours of CPU time.

Lower Body Joint Moment Matching Errors following Neural Control Model Personalization

Joint Coordinate	Hip Flexion	Hip Adduction	Hip Rotation	Knee Angle	Ankle Angle	Subtalar Angle
Right (Nm)	1.2	2.2	2.9	2.7	1.0	1.5
Left (Nm)	1.6	3.0	3.4	2.8	2.4	1.7

Table 3: RMS errors between net joint moments calculated by the OpenSim ID tool and those calculated

by the NMSM Pipeline NCP tool following neural control model personalization using muscle synergies.

Fourth, the GCP tool was used to personalize foot-ground contact model parameter values by

minimizing errors in matching ground reaction forces, ground reaction moments, and foot kinematics. A

contact element grid size of 5 by 11 was selected to match previous successful investigations.[79] The cost

functions for the three tasks performed by the tool were dominated by terms that emphasized matching

the vertical GRF, vertical and horizontal GRF, and vertical and horizontal GRF as well as ground reaction

moments, respectively, with each task starting from the solution of the previous task to track additional

quantities dependent on the previous quantities. To facilitate smooth ground reaction forces during

Treatment Optimization, we used the viscous friction coefficient as a design variable and turned off

dynamic friction. The viscous friction model penalizes excessive foot velocity with respect to the ground

during ground contact, which could lead to excessive horizontal GRFs in predictive simulations. The GCP

tool produced a personalized non-uniform distribution of spring stiffness coefficients and matched

ground reaction forces, ground reaction moments, foot positions, and foot orientations with RMSEs of

4.6 N, 2.1 Nm, 6.4 mm, and 1.7 degrees, respectively.[135,136] Additional GCP results are included in Table 4

and in the supplementary material. Convergence was achieved after approximately 4 hours of CPU time.

Ground Reaction Force/Moment and Foot Position/Orientation Errors following Ground Contact

800   **Model Personalization**

Ground Reaction Forces and Moments	Anterior Force (N)	Vertical Force (N)	Lateral Force (N)	X Moment (Nm)	Y Moment (Nm)	Z Moment (Nm)	
Right	3.5	10.2	0.9	4.6	0.9	2.0	
Left	4.1	7.4	1.3	1.8	1.1	2.1	

Foot Positions and Orientations	X Translation (mm)	Y Translation (mm)	Z Translation (mm)	X Rotation (deg)	Y Rotation (deg)	Z Rotation (deg)	Toe Angle (deg)
Right	5.6	10.1	6.5	0.5	1.1	3.7	1.3
Left	4.9	6.6	4.8	2.1	1.7	2.5	1.2

Table 4: RMS errors between ground reaction forces and moments measured experimentally, and foot

positions and orientations measured experimentally and those calculated by the NMSM Pipeline GCP

tool following ground contact model personalization.

4.4 Treatment Optimization Process

After personalizing the subject's neuromusculoskeletal model using all four Model Personalization

tools, we ran all three Treatment Optimization tools to predict how underutilized paretic and non-

paretic leg synergy activations should be upregulated to achieve a 0.8 m/s self-selected walking speed

without increasing metabolic cost per unit time above the subject's 0.5 m/s level.

First, the TO tool was used to generate a dynamically consistent full body walking motion at 0.8 m/s

that closely reproduced the subject's joint motion, joint moment, ground reaction, and muscle

activation data simultaneously using muscle synergy controls for the lower body and joint torque

controls for the back and upper body. Since synergy-driven TO requires an initial guess for synergy

vectors and activations, the TO tool XML settings file was configured such that the initial guess directly

was defined to be the NCP results directory while the tracked quantities directory was defined to be the

preprocessed data directory created after running the JMP tool. Other information, including an NMSM

Pipeline model file (.osimx), the post-JMP RCNL2023 OpenSim model, and the specified output

directory, were also included in the TO tool XML settings file. All lower body joints were controlled by

synergy controllers except for the toes coordinate, which was left uncontrolled, and all other joints were

controlled by torque controllers. Cost function terms tracked joint positions and velocities found by a

post-JMP IK analysis, joint moments found by a post-JMP ID analysis (excluding pelvis residual loads),

muscle activations found by MTP, and external loads consisting of processed experimental ground

reaction data. Constraint terms included bounded kinetic consistency errors (0.01 Nm) for all controlled

joints, root segment residual loads for the pelvis (1 N for forces and 0.1 Nm for moments), and joint

position periodicity errors (0.05 rad for joints below the pelvis and 0.1 rad for joints above it). The

solution produced by the TO tool matched tracked joint positions with an average RMSE of 2.1 degrees,

joint moments with an average RMSE of 5.1 Nm, ground reaction forces with an average RMSE of 25.3

N, ground reaction moments with an average RMSE of 4.0 Nm, and muscle activations with an average

RMSE of 0.038. Additional TO results are included in Table 5 and in the supplementary material.

Convergence was achieved after 305 IPOPT iterations, which required approximately 770 minutes of

CPU time.

832   **Lower Body Tracking Optimization Errors Relative to Experimental Data**

	Joint Angles (deg)	Joint Moments (Nm)	Ground Reaction Forces (N)	Ground Reaction Moments (Nm)	Muscle Activations
Right	2.7	4.0	22.8	4.3	0.037
Left	3.1	4.8	27.9	3.7	0.039

Table 5: RMS errors between joint angles, joint moments, ground reaction forces, ground reaction

moments, and muscle activations for the right and left legs obtained from experimental data and

corresponding quantities predicted by the NMSM Pipeline TO tool.

Second, the VO tool was used to verify that tracking the muscle synergy controls and upper body

joint kinematics found by the TO tool reproduced the joint motions, joint moments, and ground

reactions predicted by the TO tool without tracking those quantities explicitly. For the VO run, the

results of the previous TO run were used for both the initial guess and tracked quantities data. Cost

841 function terms tracked TO-found synergy controls and TO-found torque-controlled joint positions.

842 Constraint terms included bounded kinetic consistency errors (0.01 Nm) for all controlled joints, root

843 segment residual loads for the pelvis (1 N for forces and 0.1 Nm for moments), and joint position

844 periodicity errors (0.05 rad for joints below the pelvis and 0.1 rad for joints above it). The solution

845 produced by the VO tool matched tracked joint positions with an average RMSE of 0.1 deg, joint

846 moments with an average RMSE of 0.1 Nm, ground reaction forces with an average RMSE of 0.7 N,

847 ground reaction moments with an average RMSE of 0.1 Nm, and muscle activations with an average

848 RMSE of 0.01. Additional MTP results are included in Table 6 and in the supplementary material.

849 Convergence was achieved after 101 IPOPT iterations, which required approximately 170 minutes of

850 CPU time. Since the VO results closely matched the TO results, we were confident that the controller

851 and joint position tracking cost function terms and associated constraint terms selected for the

852 verification optimization could be used as the basis for the design optimization.

853 **Lower Body Verification Optimization Errors Relative to Tracking Optimization Results**

	Joint Angles (deg)	Joint Moments (Nm)	Ground Reaction Forces (N)	Ground Reaction Moments (Nm)	Muscle Activations
Right	0.09	0.06	0.44	0.06	0.01
Left	0.08	0.09	0.97	0.09	0.01

854 **Table 6:** RMS errors between joint angles, joint moments, ground reaction forces, ground reaction

855 moments, and muscle activations for the right and left legs obtained from the NMSM Pipeline TO tool

856 and corresponding quantities predicted by the NMSM Pipeline VO tool.

858 Finally, the DO tool was used to explore whether upregulating underutilized synergy activations in

859 the paretic leg and downregulating overutilized synergy activations in the non-paretic legs could

860 produce a faster self-selected walking speed of 0.8 m/s while maintaining the same metabolic cost per

unit time calculated for the subject's original self-selected walking speed of 0.5 m/s. The hypothesis in

this problem formulation is that large differences in synergy activation amplitudes between the two legs

are indicative of impaired paretic leg synergy activations that are smaller than desired and

compensatory non-paretic leg synergy activations that are larger than desired. When we evaluated the

synergy activations found by VO for the two legs, we identified four pairs that varied significantly in

amplitude between the left and right sides. Based on this observation, we formulated a DO problem that

sought to bring these four synergy activations with disparate amplitudes in the two legs closer to each

other. Each pair of asymmetric synergy activations contained a "weak" and "strong" side. First, scaled-

up "weak" synergy activations were tracked for each pair to increase their amplitudes. Second, a custom

user-defined cost function was written to reward synergy amplitude similarities between the "weak"

and "strong" synergy activations. A user-defined static parameter was added for each of the four

synergy pairs representing the amplitude scale factor to be applied to the "strong" synergy activation

using a user-defined model modification function. These two terms increased weak synergy activations

and encouraged over-active synergy activations to reduce to more symmetric magnitudes while not

overconstraining the control space. In addition, a cost function term was added to find a solution with a

metabolic cost per unit time that matched the value calculated for the subject's original 0.5 m/s self-

selected walking speed. This value was 90% of the original value calculated for the subject's 0.8 m/s self-

selected walking speed, making a 10% reduction to the target value. Cost function terms also tracked

VO-found synergy controls for the two symmetric control pairs and VO-found torque controls.

Constraint terms included bounded kinetic consistency errors (0.01 Nm) for all controlled joints, root

segment residual loads for the pelvis (1 N for forces and 0.1 Nm for moments), and joint position

periodicity errors (0.05 rad for joints below the pelvis and 0.1 rad for joints above it). The VO results

were used in both the initial guess and tracked quantities data directories, and the final time was fixed

at the value determined experimentally for the selected 0.8 m/s walking trial.

The DO predictive simulation produced modified kinematics, synergy activations, and ground

reactions that reduced the subject's metabolic cost per unit time by 9.9% for the selected gait cycle and

achieved closely matching maximum amplitudes for the four modified synergy activations. Final results

are plotted in Figure 11. Convergence was achieved after 489 IPOPT iterations, which required

approximately 730 minutes of CPU time. These DO results suggest that upregulating weak paretic leg

synergy activations while downregulating paired non-paretic leg synergy activations could potentially

allow the modeled subject to increase his self-selected walking speed by 60% without increasing his

metabolic cost per unit time.

Figure 11: Plots showing the final results of the DO tool. Subfigures A) kinematics, B) synergy activations,

C) muscle activations, and D) ground reaction forces and moments after VO (blue) and DO (red),

respectively.

Discussion

The primary objective of this work was to develop a novel set of easy-to-use computational tools

that facilitate the creation of personalized neuromusculoskeletal models and the subsequent design of

personalized clinical treatments by researchers and clinicians with little to no programming experience.

These tools dramatically reduce the barrier to entry for researchers and clinicians working together who

would like to explore using personalized computational neuromusculoskeletal models to design

personalized treatment approaches. As shown in the example application, the NMSM Pipeline has the

potential to change the way treatments are investigated and applied throughout the

neuromusculoskeletal injury space.

Going forward, two key questions need to be addressed if the NMSM Pipeline is to be used to design

actual clinical treatments for actual patients. The first question is, how should the patient's personalized

model and neural control strategy be changed in response to the simulated treatment? The second

question is, how can one validate a patient's predicted post-treatment movement function? The

answers to these two questions will depend on the specific clinical application and which aspects of the

patient's neuromusculoskeletal system need to be modeled and personalized to investigate that

application. The answers will also involve developing an understanding of how the planned intervention

will affect a patient's model parameter values and neural control strategy. Collection of post-

intervention movement data will be required so that the entire Model Personalization and Treatment

Optimization process can be evaluated, refined, and ultimately validated for one clinical application at a

time.

To conceptualize how these two important questions could be addressed, one can consider two

NSM Pipeline clinical applications being explored by the authors - one involving knee osteoarthritis

rehabilitation design, and one involving pelvic cancer surgical planning. Past computational research

involving a subject with bilateral medial compartment knee osteoarthritis investigated whether

personalized gait modifications could be designed to reduce the subject's peak adduction moment in

both knees to an extent comparable to invasive high tibial osteotomy surgery [write reference in

(author, year) form]. For this treatment optimization problem, no muscles or neural control needed to

be modeled, which simplified the treatment design process. The computational treatment design

process involved: a) creating a personalized full-body dynamic skeletal model of the subject using pre-

rehabilitation gait data, b) selecting a post-treatment control approach to be used when predicting post-

treatment walking function (in this case, minimize changes in lower body joint moments relative to pre-

rehabilitation gait data), c) performing a treatment optimization process with the personalized model

and selected control approach to identify gait modifications that would offload the medial compartment

of both knees, d) training the subject to perform and consolidate the modified walking motion, and

finally e) re-testing the subject in a gait lab to evaluate how well the predicted gait modifications could

reduce both peak adduction moment peaks. After informal training, the subject was able to perform the

predicted gait modifications and achieve bilateral reductions in the peak knee adduction moment that

were comparable to the treatment optimization predictions. A similar computational treatment design

process is currently being repeated using the NMSM Pipeline except with greater flexibility in the range

of potential gait modifications that can be predicted.

Ongoing computational research involving subjects with pelvic cancer is investigating whether

surgical decisions can be planned to achieve a post-surgery gait motion and self-selected walking speed

that is as close to normal as possible for each patient[68,137]. For this treatment optimization problem,

both muscles and neural control need to be modeled, which complicates the treatment design process.

The computational treatment design process being explored involves: a) creating a personalized full-

body dynamic neuromusculoskeletal model of the patient using pre-surgery gait, EMG, and imaging data

(to personalize pelvis bony geometry), b) selecting a post-surgery control approach to be used when

predicting post-surgery walking function (in this case, minimize changes in muscle synergy quantities

relative to pre-surgery EMG data)[137], c) performing a treatment optimization process with the

personalized model and selected control approach to identify surgical decisions that achieve clear

margins while also maximizing recovery of normal walking function[68], d) having the orthopedic

oncologist perform the patient's surgery using the optimized surgical plan, and finally e) re-testing the

patient in a gait lab following plateau in recovery to evaluate how well the predicted surgical plan

allowed the patient to achieve the predicted post-surgery gait motion and speed. Since trial and error

treatment is not possible with orthopedic surgeries, extensive testing, evaluation, and refinement of this

treatment optimization process must be performed before actual surgical plans can be designed for

actual pelvic cancer patients. To this end, the authors are collecting extensive pre- and post-surgery gait,

EMG, and imaging data sets from this patient population, along with the implemented surgical

decisions. Only after the NMSM Pipeline can predict post-surgery walking function reliably for multiple

patients when post-surgery walking function and the implemented surgical decisions are known can the

NMSM Pipeline be considered for actual use in this clinical application. A similar process would need to

be followed for any other clinical problem to which the NMSM Pipeline would be applied.

Although the decision to use MATLAB for the NMSM Pipeline facilitates development and ease of

access for users, the decision does create several limitations. C++ and other similar compiled

programming languages generally run significantly faster than interpreted programming languages like

MATLAB. However, they also introduce challenges since few engineering researchers are strong C++

programmers, and system-specific build procedures can often be complicated.[138,139] Due to these

drawbacks, most biomechanics software written in compiled languages can be modified only by

reporting a bug or requesting a feature and waiting for experienced software developers to release a

new version of the software. The NMSM Pipeline actively encourages modifications, bug fixes, and

improvements through open-source easy-to-modify MATLAB toolsets. Other interpreted programming

languages like Python can struggle with package management, virtual environments, and/or

dependency version mismatches that increase barriers to use. MATLAB's native debugging tools,

English-readable error messages, and robust, stable core functions allow for development with

confidence, making the NMSM Pipeline robust to issues common to other interpreted languages.

Our hope is that the NMSM Pipeline's open-source, easy-to-use framework will encourage

investigations by the research community into "best practices" for each of the included tools. With the

availability of seven new tools, each with many optional features, the research community is

encouraged to explore novel approaches to achieving the best results from each tool. Investigations into

changes in task order, data processing/organization, cost function error centers and maximum allowable

errors, among others, will inform the entire research community on the best ways to leverage these

unique tools for successful future research and clinical outcomes.

We are already planning future enhancements to improve the versatility and applicability of the

NMSM Pipeline to a broader range of clinical and research problems. Potential enhancements would

allow greater flexibility and customization during use of the Model Personalization toolset. Support for

compliant tendon muscle models and muscle models that differentiate between fast and slow twitch

fibers in the MTP tool could facilitate muscle-tendon model personalization and simulation for "fast"

activities like running or jumping.[61,140] Support for time-delayed sensory feedback models in the NCP

tool could enable investigation of how spasticity, hyperreflexia, and hypertonia interact with

incoordination and weakness to produce functional impairment in individuals with an upper motor

neuron pathology. Support for multi-segment foot models in the GCP tool could facilitate higher fidelity

simulations of foot biomechanics and better reproduction of ground reaction moments. Other potential

enhancements could facilitate novel use of the Treatment Optimization toolset. User-defined controls,

time-delayed sensory feedback controls, and individual muscle controls could facilitate computational

design of personalized functional electrical stimulation protocols[67] and prediction of how

downregulating overactive reflexes could improve an individual's movement function. Support for user-

defined loads as a function of model states and controls and making it easy to add new states and

controls to a DO problem could facilitate computational design of personalized passive and/or active

exoskeletons, which would be added to a subject's personalized model after TO and VO had been

performed. An enhancement supporting multi-phase optimal control problems, where each phase

simulates a different movement cycle with control information shared across phases, could facilitate

simulating neural feedback mechanisms, neural adaptation, and cycle-to-cycle motion and control

variability. Enhancements supporting the use of closed-chain kinematic models would facilitate

simulation of shoulder models with improved kinematic fidelity for surgical, exoskeleton, and exercise

equipment applications. Support for connecting NMSM Pipeline controls to any type of OpenSim

actuator could allow exploration of alternative optimal control problem formulations that significantly

improve IPOPT convergence rate, especially for TO. Finally, for both toolsets, development of easy-to-

use MATLAB utility functions that automatically process experimental movement data and put it into a

format that can be used directly by NMSM Pipeline tools, without requiring any manual data

manipulation, would make the toolsets accessible to a wider user base.

With all of these potential future enhancements, several limitations and challenges in future NMSM

Pipeline development exist. First, the quality of the personalization results found by the Model

Personalization tools is limited by the quality and quantity of collected experimental data. At this time, it

can be challenging to collect all of the experimental data needed to exercise all seven NMSM Pipeline

tools with a synergy-driven neuromusculoskeletal model. Leveraging markerless motion capture or

inertial measurement units could potentially increase the ability of researchers to collect the movement

data required to perform a high-quality pipeline run-through. For Model Personalization, because

gradient-based optimization techniques are used, solutions may become entrapped in a local minimum,

though the final solution will still be better than the initial guess. The use of muscle activations rather

than excitations for the NCP tool and the Treatment Optimization toolset is another limitation, though

back calculation of muscle excitations from muscle activations could potentially be performed given

estimates of activation dynamics parameter values. Using the OpenSim framework through the

OpenSim MATLAB API prevents the NMSM Pipeline from using automatic differentiation to speed up

optimizations performed during the Model Personalization or Treatment Optimization process.

Computations leveraging the OpenSim MATLAB API are inefficient, and speed limitations inherent to this

framework cannot be overcome.

Several research teams have released novel software tools for the musculoskeletal modeling

research community[51–58], and these tools could be used synergistically with the NMSM Pipeline. As

shown in Table 7, though none of these tools possess the broad range of model personalization and

treatment optimization capabilities available in the NMSM Pipeline, all of these tools facilitate some

aspect of creating scaled musculoskeletal models that incorporate personalized bone geometry and

muscle attachment locations. Consequently, these tools can provide the scaled musculoskeletal model

required as a starting point for the NMSM Pipeline Model Personalization process. For example,

NMSBuilder, MAP Client, Torsion Tool, Bone Deformation Tool, or OpenSim Creator could be used to

create personalized bone models from imaging data or physical measurements[52–55,57,141,142]. SimCP,

NMSBuilder, MAP Client, or OpenSim Creator could then be used to personalize muscle attachment

locations[51–53,57]. Next, SimCP, NMSBuilder, MAP Client, AddBiomechanics, or Scale Tool could be used to

create a scaled OpenSim musculoskeletal model possessing the personalized bone geometry and muscle

attachments[51–53,56]. In addition, AddBiomechanics could potentially be used to perform limited initial

personalization of joint functional axes[56], while SimCP could be used to perform initial personalization of

optimal muscle fiber lengths, tendon slack lengths, and synergy control properties[51].

1038

1039 **Comparison of Functionality Available in the NMSM Pipeline and Other Musculoskeletal Modeling Software Tools**

Software Tool	Personalize Bone Geometry	Personalize Muscle Attachments	Scale Generic Models	JMP	MTP	NCP	GCP	TO	VO	DO
NMSM Pipeline	No (1)	No	No	Yes	Yes	Yes	Yes	Yes	Yes	Yes
SimCP	No (1)	Yes	Yes	No	Yes	Yes	No	No	No	No
NMS Builder	Yes	Yes	Yes	No	No	No	No	No	No	No
MAP Client	Yes	Yes	Yes	No	No	No	No	No	No	No
Torsion Tool	Yes	No	No	No	No	No	No	No	No	No
Bone Deformation Tool	Yes	No	No	No	No	No	No	No	No	No
AddBiomechanics	No	No	Yes	Yes (2)	No	No	No	No	No	No
OpenSim Creator	Yes	Yes	No	No	No	No	No	No	No	No
Automatic Scale Tool	No	No	Yes	No	No	No	No	No	No	No

1040 (1) Personalized bone models produced using image processing and surface fitting software (e.g., Mimics, Materialize, Leuven, Belgium;
1041   Geomagic Wrap, Oqton, Ghent, Belgium) can be added.
1042 (2) Some, but not all, of the features of JMP

1043

As shown in Table 7 above, a current limitation of the NMSM Pipeline is the lack of functionality to

personalize a patient's bone morphology to clinical imaging data. The NMSM Pipeline was specifically

designed to avoid the use of imaging data and require only experimental data typically collected in a

human movement lab. However, personalized bone geometry generated using existing methods and

software tools[143,53,137] can easily be incorporated into scaled generic OpenSim models with personalized

joint functional axes[137] to produce more accurate muscle tendon lengths, moment arms, and joint and

bone loading scenarios.

Treatment Optimization also does not currently include a muscle fatigue model. To date, few muscle

fatigue models for neuromusculoskeletal modeling applications have been published in the

literature[144,145]. Thus, selecting an appropriate existing muscle fatigue model would be challenging.

Availability of a muscle fatigue model could improve the utility of predictive simulations for athletic,

other high-intensity, or long duration movements, making this research area an important one for

future investigation.

The NMSM Pipeline's Treatment Optimization toolset has key differences in design and

implementation from the existing OpenSim Moco tool. While Moco is generally the faster software due

to its C++-based implementation, Treatment Optimization leverages the flexibility of MATLAB and

GPOPS-II to facilitate novel features. Current unique features include user-defined functions and the use

of .osimx personalized model components, while future unique features could include support for multi-

phase optimal control problems, as discussed above. Treatment Optimization was designed to be

accessible to both novice and advanced users through intuitive XML settings files, whereas Moco users

typically set up problems through MATLAB or Python scripts. Even so, Moco's implementation facilitates

potential use of C++ automatic differentiation libraries to improve computational speed for gradient

calculations, resulting in more efficient optimizations. Lastly, Moco is free while both MATLAB and

GPOPS-II are commercial products with significant academic discounts. By incorporating NMSM Pipeline

model components into native OpenSim in the future, we plan to give users the option of using their

NMSM Pipeline personalized models in either our Treatment Optimization toolset or OpenSim Moco,

allowing the research community to explore the tradeoffs between these two approaches to developing

predictive simulations.

In conclusion, the NMSM Pipeline represents a significant step forward in the ability to personalize

neuromusculoskeletal computer models to patient movement data and then optimize parameters of

potential treatments using the personalized models. The software assembles over two decades of

biomechanics research into a well-designed and accessible framework that makes previously "high end"

modeling, simulation, and optimization techniques accessible to the entire research community. Our

hope is that by empowering researchers and clinicians working together to explore clinically relevant

questions and to design novel personalized interventions, the NMSM Pipeline will bring

neuromusculoskeletal computer modeling not only to the doorstep of clinical utility but also across it.

Declarations

Ethics Approval and Consent to Participate

The de-identified experimental walking data used in this study were collected and disseminated as part

of a previously published study.[41]

Consent for Publication

Not applicable.

Availability of Data and Materials

The NMSM Pipeline software, along with all data, models, and settings files described in this article, are

available from the "Neuromusculoskeletal Modeling (NMSM) Pipeline" project on SimTK.org

(https://simtk.org/projects/nmsm). Users are welcome to share feedback and request new functionality

through this project's forum. Documentation including implementation details, examples, and tutorials

is available at https://nmsm.rice.edu.

Further details on the NMSM Pipeline software are provided below:

Project name: Neuromusculoskeletal Modeling Pipeline

Project home page: https://nmsm.rice.edu

Archived version:

Operating systems: Windows, MacOS

Programming language: MATLAB

Other requirements: Version 2023a or higher

License: Apache 2.0

The software has no restrictions for use by non-academics.

Competing Interests

The authors declare no competing interests.

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1123   Pipeline software would not have been possible.

1124 References

1125   (1)   Ma, V. Y.; Chan, L.; Carruthers, K. J. The Incidence, Prevalence, Costs and Impact on Disability of
1126   Common Conditions Requiring Rehabilitation in the US: Stroke, Spinal Cord Injury, Traumatic
1127   Brain Injury, Multiple Sclerosis, Osteoarthritis, Rheumatoid Arthritis, Limb Loss, and Back Pain.
1128   *Arch. Phys. Med. Rehabil.* **2014**, *95* (5), 986-995.e1. https://doi.org/10.1016/j.apmr.2013.10.032.
1129   (2)   Ovbiagele, B.; Goldstein, L. B.; Higashida, R. T.; Howard, V. J.; Johnston, S. C.; Khavjou, O. A.;
1130   Lackland, D. T.; Lichtman, J. H.; Mohl, S.; Sacco, R. L.; Saver, J. L.; Trogdon, J. G.; American Heart
1131   Association Advocacy Coordinating Committee and Stroke Council. Forecasting the Future of
1132   Stroke in the United States: A Policy Statement from the American Heart Association and
1133   American Stroke Association. *Stroke* **2013**, *44* (8), 2361–2375.
1134   https://doi.org/10.1161/STR.0b013e31829734f2.
1135   (3)   Theis, K. A.; Roblin, D. W.; Helmick, C. G.; Luo, R. Prevalence and Causes of Work Disability among
1136   Working-Age U.S. Adults, 2011-2013, NHIS. *Disabil. Health J.* **2018**, *11* (1), 108–115.
1137   https://doi.org/10.1016/j.dhjo.2017.04.010.
1138   (4)   Praemer, A.; Furner, S.; Rice, D. P. *Musculoskeletal Conditions in the United States*; American
1139   Academy of Orthopaedic Surgeons: Rosemont, IL, 1999.
1140   (5)   Clark, M. S.; Smith, D. S. Factors Contributing to Patient Satisfaction with Rehabilitation Following
1141   Stroke. *Int. J. Rehabil. Res.* **1998**, *21* (2), 143.
1142   (6)   Brandstater, M. E.; de Bruin, H.; Gowland, C.; Clark, B. M. Hemiplegic Gait: Analysis of Temporal
1143   Variables. *Arch. Phys. Med. Rehabil.* **1983**, *64* (12), 583–587.
1144   (7)   Chen, G.; Patten, C.; Kothari, D. H.; Zajac, F. E. Gait Deviations Associated with Post-Stroke
1145   Hemiparesis: Improvement during Treadmill Walking Using Weight Support, Speed, Support

Stiffness, and Handrail Hold. *Gait Posture* **2005**, *22* (1), 57–62. https://doi.org/10.1016/j.gaitpost.2004.06.008.

(8)   Olney, S. J.; Monga, T. N.; Costigan, P. A. Mechanical Energy of Walking of Stroke Patients. *Arch. Phys. Med. Rehabil.* **1986**, *67* (2), 92–98. https://doi.org/10.1016/0003-9993(86)90109-7.

(9)   Rejnö, Å.; Nasic, S.; Bjälkefur, K.; Bertholds, E.; Jood, K. Changes in Functional Outcome over Five Years after Stroke. *Brain Behav.* **2019**, *9* (6), e01300. https://doi.org/10.1002/brb3.1300.

(10)   Barbour, K. E. Vital Signs: Prevalence of Doctor-Diagnosed Arthritis and Arthritis-Attributable Activity Limitation — United States, 2013–2015. *MMWR Morb. Mortal. Wkly. Rep.* **2017**, *66*. https://doi.org/10.15585/mmwr.mm6609e1.

(11)   Kahlenberg, C. A.; Nwachukwu, B. U.; McLawhorn, A. S.; Cross, M. B.; Cornell, C. N.; Padgett, D. E. Patient Satisfaction after Total Knee Replacement: A Systematic Review. *HSS Journal®* **2018**, *14* (2), 192–201. https://doi.org/10.1007/s11420-018-9614-8.

(12)   Muertizha, M.; Cai, X.; Ji, B.; Aimaiti, A.; Cao, L. Factors Contributing to 1-Year Dissatisfaction after Total Knee Arthroplasty: A Nomogram Prediction Model. *J. Orthop. Surg.* **2022**, *17* (1), 367. https://doi.org/10.1186/s13018-022-03205-2.

(13)   Bourne, R. B.; Chesworth, B. M.; Davis, A. M.; Mahomed, N. N.; Charron, K. D. J. Patient Satisfaction after Total Knee Arthroplasty: Who Is Satisfied and Who Is Not? *Clin. Orthop.* **2009**, *468* (1), 57. https://doi.org/10.1007/s11999-009-1119-9.

(14)   Anakwe, R. E.; Jenkins, P. J.; Moran, M. Predicting Dissatisfaction After Total Hip Arthroplasty: A Study of 850 Patients. *J. Arthroplasty* **2011**, *26* (2), 209–213. https://doi.org/10.1016/j.arth.2010.03.013.

(15)   Tilbury, C.; Haanstra, T. M.; Leichtenberg, C. S.; Verdegaal, S. H. M.; Ostelo, R. W.; Vet, H. C. W. de; Nelissen, R. G. H. H.; Vlieland, T. P. M. V. Unfulfilled Expectations After Total Hip and Knee Arthroplasty Surgery: There Is a Need for Better Preoperative Patient Information and Education. *J. Arthroplasty* **2016**, *31* (10), 2139–2145. https://doi.org/10.1016/j.arth.2016.02.061.

(16)   Kim, M. S.; Koh, I. J.; Kim, C. K.; Choi, K. Y.; Yang, J. S.; In, Y. Patient Expectations and Satisfaction After Medial Opening Wedge High Tibial Osteotomy. *J. Arthroplasty* **2020**, *35* (12), 3467–3473. https://doi.org/10.1016/j.arth.2020.06.076.

(17)   Stephan-Carlier, A.; Facione, J.; Speyer, E.; Rumilly, E.; Paysant, J. Quality of Life and Satisfaction after Multilevel Surgery in Cerebral Palsy: Confronting the Experience of Children and Their Parents. *Ann. Phys. Rehabil. Med.* **2014**, *57* (9–10), 640–652. https://doi.org/10.1016/j.rehab.2014.09.012.

(18)   Blumetti, F. C.; Wu, J. C. N.; Bau, K. V.; Martin, B.; Hobson, S. A.; Axt, M. W.; Selber, P. Orthopedic Surgery and Mobility Goals for Children with Cerebral Palsy GMFCS Level IV: What Are We Setting out to Achieve? *J. Child. Orthop.* **2012**, *6* (6), 485–490. https://doi.org/10.1007/s11832-012-0454-7.

(19)   Schwartz, M. H.; Ries, A. J.; Georgiadis, A. G.; Kainz, H. Demonstrating the Utility of Instrumented Gait Analysis in the Treatment of Children with Cerebral Palsy. *PLOS ONE* **2024**, *19* (4), e0301230. https://doi.org/10.1371/journal.pone.0301230.

(20)   DadeMatthews, O. O.; Roper, J. A.; Vazquez, A.; Shannon, D. M.; Sefton, J. M. Prosthetic Device and Service Satisfaction, Quality of Life, and Functional Performance in Lower Limb Prosthesis Clients. *Prosthet. Orthot. Int.* **2024**, *48* (4), 422–430. https://doi.org/10.1097/PXR.0000000000000285.

(21)   Datta, D.; Selvarajah, K.; Davey, N. Functional Outcome of Patients with Proximal Upper Limb Deficiency--Acquired and Congenital. *Clin. Rehabil.* **2004**, *18* (2), 172–177. https://doi.org/10.1191/0269215504cr716oa.

(22)   *The designer changing the way aircraft are built*. https://www.bbc.com/future/article/20181129-the-ai-transforming-the-way-aircraft-are-built (accessed 2024-09-13).

(23) *SpaceX Is Using These Simulations to Design the Rocket That'll Take Us to Mars*.
https://www.vice.com/en/article/spacex-is-using-these-simulations-to-design-the-rocket-thatll-
take-us-to-mars/ (accessed 2024-09-13).
(24) *A brief history of computing in Formula 1*. https://www.mclaren.com/racing/team/a-brief-
history-of-computing-in-f1-1052199/ (accessed 2024-09-13).
(25) *The America's Cup: nerves, skill, and computer design | PCWorld*.
https://www.pcworld.com/article/447831/the-americas-cup-nerves-skill-and-a-lot-of-
computers.html (accessed 2024-09-13).
(26) *Planning and Design of Engineering Systems | Graeme Dandy, David Walke*.
https://www.taylorfrancis.com/books/mono/10.1201/9781351228121/planning-design-
engineering-systems-graeme-dandy-trevor-daniell-robert-warner-bernadette-foley-graeme-
dandy-david-walker-trevor-daniell-robert-warner (accessed 2024-09-13).
(27) López Gualdrón, C.-I.; Bravo Ibarra, E.-R.; Murillo Bohórquez, A.-P.; Garnica Bohórquez, I. Present
and Future for Technologies to Develop Patient-Specific Medical Devices: A Systematic Review
Approach. *Med. Devices Auckl. NZ* **2019**, *12*, 253–273. https://doi.org/10.2147/MDER.S215947.
(28) U, V.; Mehrotra, D.; Howlader, D.; Singh, P. K.; Gupta, S. Patient Specific Three-Dimensional
Implant for Reconstruction of Complex Mandibular Defect. *J. Craniofac. Surg.* **2019**, *30* (4), e308–
e311. https://doi.org/10.1097/SCS.0000000000005228.
(29) Sutradhar, A.; Park, J.; Carrau, D.; Miller, M. J. Experimental Validation of 3D Printed Patient-
Specific Implants Using Digital Image Correlation and Finite Element Analysis. *Comput. Biol. Med.*
2014, *52*, 8–17. https://doi.org/10.1016/j.compbiomed.2014.06.002.
(30) Pinheiro, M.; Alves, J. L. The Feasibility of a Custom-Made Endoprosthesis in Mandibular
Reconstruction: Implant Design and Finite Element Analysis. *J. Cranio-Maxillofac. Surg.* **2015**, *43*
(10), 2116–2128. https://doi.org/10.1016/j.jcms.2015.10.004.
(31) *Transforming the Diagnosis and Management of Coronary Artery Disease*.
https://www.heartflow.com/. https://www.heartflow.com/ (accessed 2024-09-13).
(32) Hlatky, M. A.; De Bruyne, B.; Pontone, G.; Patel, M. R.; Norgaard, B. L.; Byrne, R. A.; Curzen, N.;
Purcell, I.; Gutberlet, M.; Rioufol, G.; Hink, U.; Schuchlenz, H. W.; Feuchtner, G.; Gilard, M.;
Andreini, D.; Jensen, J. M.; Hadamitzky, M.; Wilk, A.; Wang, F.; Rogers, C.; Douglas, P. S.;
PLATFORM Investigators. Quality-of-Life and Economic Outcomes of Assessing Fractional Flow
Reserve With Computed Tomography Angiography: PLATFORM. *J. Am. Coll. Cardiol.* **2015**, *66*
(21), 2315–2323. https://doi.org/10.1016/j.jacc.2015.09.051.
(33) Douglas, P. S.; Pontone, G.; Hlatky, M. A.; Patel, M. R.; Norgaard, B. L.; Byrne, R. A.; Curzen, N.;
Purcell, I.; Gutberlet, M.; Rioufol, G.; Hink, U.; Schuchlenz, H. W.; Feuchtner, G.; Gilard, M.;
Andreini, D.; Jensen, J. M.; Hadamitzky, M.; Chiswell, K.; Cyr, D.; Wilk, A.; Wang, F.; Rogers, C.; De
Bruyne, B. Clinical Outcomes of Fractional Flow Reserve by Computed Tomographic Angiography-
Guided Diagnostic Strategies vs. Usual Care in Patients with Suspected Coronary Artery Disease:
The Prospective Longitudinal Trial of FFRCT: Outcome and Resource Impacts Study. *Eur. Heart J.*
2015, *36* (47), 3359–3367. https://doi.org/10.1093/eurheartj/ehv444.
(34) Fregly, B. J. A Conceptual Blueprint for Making Neuromusculoskeletal Models Clinically Useful.
Appl. Sci. **2021**, *11* (5), 2037. https://doi.org/10.3390/app11052037.
(35) Umberger, B. R.; Miller, R. H. Optimal Control Modeling of Human Movement. In *Handbook of*
Human Motion; Müller, B., Wolf, S. I., Brueggemann, G.-P., Deng, Z., McIntosh, A., Miller, F.,
Selbie, W. S., Eds.; Springer International Publishing: Cham, 2017; pp 1–22.
https://doi.org/10.1007/978-3-319-30808-1_177-1.
(36) Lee, L.-F.; Umberger, B. R. Generating Optimal Control Simulations of Musculoskeletal Movement
Using OpenSim and MATLAB. *PeerJ* **2016**, *4*, e1638. https://doi.org/10.7717/peerj.1638.
(37) Porsa, S.; Lin, Y.-C.; Pandy, M. G. Direct Methods for Predicting Movement Biomechanics Based

Upon Optimal Control Theory with Implementation in OpenSim. *Ann. Biomed. Eng.* **2016**, *44* (8),
2542–2557. https://doi.org/10.1007/s10439-015-1538-6.
(38) Pandy, M. G.; Zajac, F. E.; Sim, E.; Levine, W. S. An Optimal Control Model for Maximum-Height
Human Jumping. *J. Biomech.* **1990**, *23* (12), 1185–1198. https://doi.org/10.1016/0021-
9290(90)90376-E.
(39) van den Bogert, A. J.; Hupperets, M.; Schlarb, H.; Krabbe, B. Predictive Musculoskeletal
Simulation Using Optimal Control: Effects of Added Limb Mass on Energy Cost and Kinematics of
Walking and Running. *Proc. Inst. Mech. Eng. Part P J. Sports Eng. Technol.* **2012**, *226* (2), 123–133.
https://doi.org/10.1177/1754337112440644.
(40) Rohani, F.; Richter, H.; Bogert, A. J. van den. Optimal Design and Control of an Electromechanical
Transfemoral Prosthesis with Energy Regeneration. *PLOS ONE* **2017**, *12* (11), e0188266.
https://doi.org/10.1371/journal.pone.0188266.
(41) Meyer, A. J.; Eskinazi, I.; Jackson, J. N.; Rao, A. V.; Patten, C.; Fregly, B. J. Muscle Synergies
Facilitate Computational Prediction of Subject-Specific Walking Motions. *Front. Bioeng.*
Biotechnol. **2016**, *4*. https://doi.org/10.3389/fbioe.2016.00077.
(42) Dorn, T. W.; Wang, J. M.; Hicks, J. L.; Delp, S. L. Predictive Simulation Generates Human
Adaptations during Loaded and Inclined Walking. *PLOS ONE* **2015**, *10* (4), e0121407.
https://doi.org/10.1371/journal.pone.0121407.
(43) Ong, C. F.; Geijtenbeek, T.; Hicks, J. L.; Delp, S. L. Predicting Gait Adaptations Due to Ankle
Plantarflexor Muscle Weakness and Contracture Using Physics-Based Musculoskeletal
Simulations. *PLOS Comput. Biol.* **2019**, *15* (10), e1006993.
https://doi.org/10.1371/journal.pcbi.1006993.
(44) Miller, R. H.; Esterson, A. Y.; Shim, J. K. Joint Contact Forces When Minimizing the External Knee
Adduction Moment by Gait Modification: A Computer Simulation Study. *The Knee* **2015**, *22* (6),
481–489. https://doi.org/10.1016/j.knee.2015.06.014.
(45) Miller, R. H. A Comparison of Muscle Energy Models for Simulating Human Walking in Three
Dimensions. *J. Biomech.* **2014**, *47* (6), 1373–1381.
https://doi.org/10.1016/j.jbiomech.2014.01.049.
(46) McGowan, C. P.; Neptune, R. R.; Clark, D. J.; Kautz, S. A. Modular Control of Human Walking:
Adaptations to Altered Mechanical Demands. *J. Biomech.* **2010**, *43* (3), 412–419.
https://doi.org/10.1016/j.jbiomech.2009.10.009.
(47) Allen, J. L.; Neptune, R. R. Three-Dimensional Modular Control of Human Walking. *J. Biomech.*
2012, *45* (12), 2157–2163. https://doi.org/10.1016/j.jbiomech.2012.05.037.
(48) Dembia, C. L.; Bianco, N. A.; Falisse, A.; Hicks, J. L.; Delp, S. L. OpenSim Moco: Musculoskeletal
Optimal Control. *PLOS Comput. Biol.* **2020**, *16* (12), e1008493.
https://doi.org/10.1371/journal.pcbi.1008493.
(49) Delp, S. L.; Anderson, F. C.; Arnold, A. S.; Loan, P.; Habib, A.; John, C. T.; Guendelman, E.; Thelen,
D. G. OpenSim: Open-Source Software to Create and Analyze Dynamic Simulations of Movement.
IEEE Trans. Biomed. Eng. **2007**, *54* (11), 1940–1950. https://doi.org/10.1109/TBME.2007.901024.
(50) Seth, A.; Hicks, J. L.; Uchida, T. K.; Habib, A.; Dembia, C. L.; Dunne, J. J.; Ong, C. F.; DeMers, M. S.;
Rajagopal, A.; Millard, M.; Hamner, S. R.; Arnold, E. M.; Yong, J. R.; Lakshmikanth, S. K.; Sherman,
M. A.; Ku, J. P.; Delp, S. L. OpenSim: Simulating Musculoskeletal Dynamics and Neuromuscular
Control to Study Human and Animal Movement. *PLOS Comput. Biol.* **2018**, *14* (7), e1006223.
https://doi.org/10.1371/journal.pcbi.1006223.
(51) Pitto, L.; Kainz, H.; Falisse, A.; Wesseling, M.; Van Rossom, S.; Hoang, H.; Papageorgiou, E.;
Hallemans, A.; Desloovere, K.; Molenaers, G.; Van Campenhout, A.; De Groote, F.; Jonkers, I.
SimCP: A Simulation Platform to Predict Gait Performance Following Orthopedic Intervention in
Children With Cerebral Palsy. *Front. Neurorobotics* **2019**, *13*.

1290 https://doi.org/10.3389/fnbot.2019.00054.

1291 (52) Valente, G.; Crimi, G.; Vanella, N.; Schileo, E.; Taddei, F. nmsBuilder: Freeware to Create Subject-
1292  Specific Musculoskeletal Models for OpenSim. *Comput. Methods Programs Biomed.* **2017**, *152*,
1293  85–92. https://doi.org/10.1016/j.cmpb.2017.09.012.

1294 (53) Zhang, J.; Sorby, H.; Clement, J.; Thomas, C. D. L.; Hunter, P.; Nielsen, P.; Lloyd, D.; Taylor, M.;
1295  Besier, T. The MAP Client: User-Friendly Musculoskeletal Modelling Workflows. In *Biomedical*
1296  *Simulation*; Bello, F., Cotin, S., Eds.; Springer International Publishing: Cham, 2014; pp 182–192.
1297  https://doi.org/10.1007/978-3-319-12057-7_21.

1298 (54) Veerkamp, K.; Kainz, H.; Killen, B. A.; Jónasdóttir, H.; van der Krogt, M. M. Torsion Tool: An
1299  Automated Tool for Personalising Femoral and Tibial Geometries in OpenSim Musculoskeletal
1300  Models. *J. Biomech.* **2021**, *125*, 110589. https://doi.org/10.1016/j.jbiomech.2021.110589.

1301 (55) Modenese, L.; Barzan, M.; Carty, C. P. Dependency of Lower Limb Joint Reaction Forces on
1302  Femoral Version. *Gait Posture* **2021**, *88*, 318–321.
1303  https://doi.org/10.1016/j.gaitpost.2021.06.014.

1304 (56) Werling, K.; Bianco, N. A.; Raitor, M.; Stingel, J.; Hicks, J. L.; Collins, S. H.; Delp, S. L.; Liu, C. K.
1305  AddBiomechanics: Automating Model Scaling, Inverse Kinematics, and Inverse Dynamics from
1306  Human Motion Data through Sequential Optimization. *PLOS ONE* **2023**, *18* (11), e0295152.
1307  https://doi.org/10.1371/journal.pone.0295152.

1308 (57) Kewley, A.; Beesel, J.; Seth, A. OpenSim Creator, 2025.
1309  https://doi.org/10.5281/zenodo.14755649.

1310 (58) Di Pietro, A.; Bersani, A.; Curreli, C.; Di Puccio, F. AST: An OpenSim-Based Tool for the Automatic
1311  Scaling of Generic Musculoskeletal Models. *Comput. Biol. Med.* **2024**, *175*, 108524.
1312  https://doi.org/10.1016/j.compbiomed.2024.108524.

1313 (59) van den Bogert, A. J.; Blana, D.; Heinrich, D. Implicit Methods for Efficient Musculoskeletal
1314  Simulation and Optimal Control. *Procedia IUTAM* **2011**, *2* (2011), 297–316.
1315  https://doi.org/10.1016/j.piutam.2011.04.027.

1316 (60) Patterson, M. A.; Rao, A. V. GPOPS-II: A MATLAB Software for Solving Multiple-Phase Optimal
1317  Control Problems Using Hp-Adaptive Gaussian Quadrature Collocation Methods and Sparse
1318  Nonlinear Programming. *ACM Trans Math Softw* **2014**, *41* (1), 1:1-1:37.
1319  https://doi.org/10.1145/2558904.

1320 (61) De Groote, F.; Kinney, A. L.; Rao, A. V.; Fregly, B. J. Evaluation of Direct Collocation Optimal
1321  Control Problem Formulations for Solving the Muscle Redundancy Problem. *Ann. Biomed. Eng.*
1322  **2016**, *44* (10), 2922–2936. https://doi.org/10.1007/s10439-016-1591-9.

1323 (62) Febrer-Nafría, M.; Pallarès-López, R.; Fregly, B. J.; Font-Llagunes, J. M. Comparison of Different
1324  Optimal Control Formulations for Generating Dynamically Consistent Crutch Walking Simulations
1325  Using a Torque-Driven Model. *Mech. Mach. Theory* **2020**, *154*, 104031.
1326  https://doi.org/10.1016/j.mechmachtheory.2020.104031.

1327 (63) Butler, D. Translational Research: Crossing the Valley of Death. *Nature* **2008**, *453* (7197), 840–
1328  842. https://doi.org/10.1038/453840a.

1329 (64) Jørgensen, J. T. Twenty Years with Personalized Medicine: Past, Present, and Future of
1330  Individualized Pharmacotherapy. *The Oncologist* **2019**, *24* (7), e432–e440.
1331  https://doi.org/10.1634/theoncologist.2019-0054.

1332 (65) Rassmussen J; Vondrak V; Damsgaard M; de Zee M; Christensen ST. The AnyBody Project –
1333  Computer Analysis of the Human Body. *Comput. Anal. Hum. Body* **2002**, No. Biomechanics of
1334  Man, 270–274.

1335 (66) Wächter, A.; Biegler, L. T. On the Implementation of an Interior-Point Filter Line-Search Algorithm
1336  for Large-Scale Nonlinear Programming. *Math. Program.* **2006**, *106* (1), 25–57.
1337  https://doi.org/10.1007/s10107-004-0559-y.

(67) Sauder, N. R.; Meyer, A. J.; Allen, J. L.; Ting, L. H.; Kesar, T. M.; Fregly, B. J. Computational Design
of FastFES Treatment to Improve Propulsive Force Symmetry During Post-Stroke Gait: A
Feasibility Study. *Front. Neurorobotics* **2019**, *13*, 80. https://doi.org/10.3389/fnbot.2019.00080.
(68) Vega, M. M.; Li, G.; Shourijeh, M. S.; Ao, D.; Weinschenk, R. C.; Patten, C.; Font-Llagunes, J. M.;
Lewis, V. O.; Fregly, B. J. Computational Evaluation of Psoas Muscle Influence on Walking
Function Following Internal Hemipelvectomy with Reconstruction. *Front. Bioeng. Biotechnol.*
2022, *10*, 855870. https://doi.org/10.3389/fbioe.2022.855870.
(69) McMorland, A. J. C.; Runnalls, K. D.; Byblow, W. D. A Neuroanatomical Framework for Upper Limb
Synergies after Stroke. *Front. Hum. Neurosci.* **2015**, *9*.
https://doi.org/10.3389/fnhum.2015.00082.
(70) Akhras, M. A.; Bortoletto, R.; Madehkhaksar, F.; Tagliapietra, L. Neural and Musculoskeletal
Modeling: Its Role in Neurorehabilitation. In *Emerging Therapies in Neurorehabilitation II*; Pons, J.
L., Raya, R., González, J., Eds.; Springer International Publishing: Cham, 2016; pp 109–143.
https://doi.org/10.1007/978-3-319-24901-8_5.
(71) Meyer, A. J.; Patten, C.; Fregly, B. J. Lower Extremity EMG-Driven Modeling of Walking with
Automated Adjustment of Musculoskeletal Geometry. *PLOS ONE* **2017**, *12* (7), e0179698.
https://doi.org/10.1371/journal.pone.0179698.
(72) Reinbolt, J. A.; Haftka, R. T.; Chmielewski, T. L.; Fregly, B. J. Are Patient-Specific Joint and Inertial
Parameters Necessary for Accurate Inverse Dynamics Analyses of Gait? *IEEE Trans. Biomed. Eng.*
2007, *54* (5), 782–793. https://doi.org/10.1109/TBME.2006.889187.
(73) Serrancolí, G.; Kinney, A. L.; Fregly, B. J.; Font-Llagunes, J. M. Neuromusculoskeletal Model
Calibration Significantly Affects Predicted Knee Contact Forces for Walking. *J. Biomech. Eng.* **2016**,
138 (8), 0810011–08100111. https://doi.org/10.1115/1.4033673.
(74) Żuk, M.; Syczewska, M.; Pezowicz, C. Influence of Uncertainty in Selected Musculoskeletal Model
Parameters on Muscle Forces Estimated in Inverse Dynamics-Based Static Optimization and
Hybrid Approach. *J. Biomech. Eng.* **2018**, *140* (121001). https://doi.org/10.1115/1.4040943.
(75) Lloyd, D. G.; Besier, T. F. An EMG-Driven Musculoskeletal Model to Estimate Muscle Forces and
Knee Joint Moments in Vivo. *J. Biomech.* **2003**, *36* (6), 765–776. https://doi.org/10.1016/s0021-
9290(03)00010-1.
(76) Manal, K.; Buchanan, T. S. Use of an EMG-Driven Biomechanical Model to Study Virtual Injuries.
Med. Sci. Sports Exerc. **2005**, *37* (11), 1917–1923.
https://doi.org/10.1249/01.mss.0000176685.35442.6b.
(77) Moissenet, F.; Modenese, L.; Dumas, R. Alterations of Musculoskeletal Models for a More
Accurate Estimation of Lower Limb Joint Contact Forces during Normal Gait: A Systematic Review.
J. Biomech. **2017**, *63*, 8–20. https://doi.org/10.1016/j.jbiomech.2017.08.025.
(78) Arones, M. M.; Shourijeh, M. S.; Patten, C.; Fregly, B. J. Musculoskeletal Model Personalization
Affects Metabolic Cost Estimates for Walking. *Front. Bioeng. Biotechnol.* **2020**, *8*, 588925.
https://doi.org/10.3389/fbioe.2020.588925.
(79) Jackson, J. N.; Hass, C. J.; Fregly, B. J. Development of a Subject-Specific Foot-Ground Contact
Model for Walking. *J. Biomech. Eng.* **2016**, *138* (9), 0910021–09100212.
https://doi.org/10.1115/1.4034060.
(80) Nguyen, V. Q.; Johnson, R. T.; Sup, F. C.; Umberger, B. R. Bilevel Optimization for Cost Function
Determination in Dynamic Simulation of Human Gait. *IEEE Trans. Neural Syst. Rehabil. Eng. Publ.*
IEEE Eng. Med. Biol. Soc. **2019**, *27* (7), 1426–1435. https://doi.org/10.1109/TNSRE.2019.2922942.
(81) Kuska, E. C.; Steele, K. M. Does Crouch Alter the Effects of Neuromuscular Impairments on Gait?
A Simulation Study. *J. Biomech.* **2024**, *165*, 112015.
https://doi.org/10.1016/j.jbiomech.2024.112015.
(82) Pariser, K. M.; Higginson, J. S. Development and Validation of a Framework for Predictive

Simulation of Treadmill Gait. *J. Biomech. Eng.* **2022**, *144* (11), 114505.
https://doi.org/10.1115/1.4054867.

(83) Falisse, A.; Serrancolí, G.; Dembia, C. L.; Gillis, J.; Jonkers, I.; De Groote, F. Rapid Predictive
Simulations with Complex Musculoskeletal Models Suggest That Diverse Healthy and Pathological
Human Gaits Can Emerge from Similar Control Strategies. *J. R. Soc. Interface* **2019**, *16* (157),
20190402. https://doi.org/10.1098/rsif.2019.0402.

(84) Dorschky, E.; Nitschke, M.; Seifer, A.-K.; van den Bogert, A. J.; Eskofier, B. M. Estimation of Gait
Kinematics and Kinetics from Inertial Sensor Data Using Optimal Control of Musculoskeletal
Models. *J. Biomech.* **2019**, *95*, 109278. https://doi.org/10.1016/j.jbiomech.2019.07.022.

(85) Ackermann, M.; van den Bogert, A. J. Optimality Principles for Model-Based Prediction of Human
Gait. *J. Biomech.* **2010**, *43* (6), 1055–1060. https://doi.org/10.1016/j.jbiomech.2009.12.012.

(86) Johnson, R. T.; Bianco, N. A.; Finley, J. M. Patterns of Asymmetry and Energy Cost Generated from
Predictive Simulations of Hemiparetic Gait. *PLoS Comput. Biol.* **2022**, *18* (9), e1010466.
https://doi.org/10.1371/journal.pcbi.1010466.

(87) Miller, R. H.; Russell Esposito, E. Transtibial Limb Loss Does Not Increase Metabolic Cost in Three-
Dimensional Computer Simulations of Human Walking. *PeerJ* **2021**, *9*, e11960.
https://doi.org/10.7717/peerj.11960.

(88) Weng, J.; Hashemi, E.; Arami, A. Adaptive Reference Inverse Optimal Control for Natural Walking
With Musculoskeletal Models. *IEEE Trans. Neural Syst. Rehabil. Eng.* **2022**, *30*, 1567–1575.
https://doi.org/10.1109/TNSRE.2022.3180690.

(89) Tresch, M. C.; Saltiel, P.; Bizzi, E. The Construction of Movement by the Spinal Cord. *Nat.
Neurosci.* **1999**, *2* (2), 162–167. https://doi.org/10.1038/5721.

(90) Lee, D.; Seung, H. Algorithms for Non-Negative Matrix Factorization. *Adv Neural Inf. Process Syst*
2001, *13*.

(91) Ivanenko, Y. P.; Poppele, R. E.; Lacquaniti, F. Five Basic Muscle Activation Patterns Account for
Muscle Activity during Human Locomotion. *J. Physiol.* **2004**, *556* (Pt 1), 267–282.
https://doi.org/10.1113/jphysiol.2003.057174.

(92) Cheung, V. C. K.; Piron, L.; Agostini, M.; Silvoni, S.; Turolla, A.; Bizzi, E. Stability of Muscle
Synergies for Voluntary Actions after Cortical Stroke in Humans. *Proc. Natl. Acad. Sci. U. S. A.*
2009, *106* (46), 19563. https://doi.org/10.1073/pnas.0910114106.

(93) Clark, D. J.; Ting, L. H.; Zajac, F. E.; Neptune, R. R.; Kautz, S. A. Merging of Healthy Motor Modules
Predicts Reduced Locomotor Performance and Muscle Coordination Complexity Post-Stroke. *J.
Neurophysiol.* **2010**, *103* (2), 844–857. https://doi.org/10.1152/jn.00825.2009.

(94) Gizzi, L.; Nielsen, J. F.; Felici, F.; Ivanenko, Y. P.; Farina, D. Impulses of Activation but Not Motor
Modules Are Preserved in the Locomotion of Subacute Stroke Patients. *J. Neurophysiol.* **2011**, *106*
(1), 202–210. https://doi.org/10.1152/jn.00727.2010.

(95) Routson, R. L.; Clark, D. J.; Bowden, M. G.; Kautz, S. A.; Neptune, R. R. The Influence of Locomotor
Rehabilitation on Module Quality and Post-Stroke Hemiparetic Walking Performance. *Gait
Posture* **2013**, *38* (3), 511–517. https://doi.org/10.1016/j.gaitpost.2013.01.020.

(96) Roh, J.; Rymer, W. Z.; Perreault, E. J.; Yoo, S. B.; Beer, R. F. Alterations in Upper Limb Muscle
Synergy Structure in Chronic Stroke Survivors. *J. Neurophysiol.* **2013**, *109* (3), 768–781.
https://doi.org/10.1152/jn.00670.2012.

(97) Pitto, L.; Rossom, S. van; Desloovere, K.; Molenaers, G.; Huenaerts, C.; Groote, F. D.; Jonkers, I.
Pre-Treatment EMG Can Be Used to Model Post-Treatment Muscle Coordination during Walking
in Children with Cerebral Palsy. *PLOS ONE* **2020**, *15* (2), e0228851.
https://doi.org/10.1371/journal.pone.0228851.

(98) Rabbi, M. F.; Pizzolato, C.; Lloyd, D. G.; Carty, C. P.; Devaprakash, D.; Diamond, L. E. Non-Negative
Matrix Factorisation Is the Most Appropriate Method for Extraction of Muscle Synergies in

Walking and Running. *Sci. Rep.* **2020**, *10* (1), 8266. https://doi.org/10.1038/s41598-020-65257-w.

(99)   Rajagopal, A.; Dembia, C. L.; DeMers, M. S.; Delp, D. D.; Hicks, J. L.; Delp, S. L. Full-Body
Musculoskeletal Model for Muscle-Driven Simulation of Human Gait. *IEEE Trans. Biomed. Eng.*
2016, *63* (10), 2068–2079. https://doi.org/10.1109/TBME.2016.2586891.

(100) van den Bogert, A. J.; Smith, G. D.; Nigg, B. M. In Vivo Determination of the Anatomical Axes of
the Ankle Joint Complex: An Optimization Approach. *J. Biomech.* **1994**, *27* (12), 1477–1488.
https://doi.org/10.1016/0021-9290(94)90197-x.

(101) Reinbolt, J. A.; Schutte, J. F.; Fregly, B. J.; Koh, B. I.; Haftka, R. T.; George, A. D.; Mitchell, K. H.
Determination of Patient-Specific Multi-Joint Kinematic Models through Two-Level Optimization.
J. Biomech. **2005**, *38* (3), 621–626. https://doi.org/10.1016/j.jbiomech.2004.03.031.

(102) Price, M. A.; LaPrè, A. K.; Johnson, R. T.; Umberger, B. R.; Sup IV, F. C. A Model-Based Motion
Capture Marker Location Refinement Approach Using Inverse Kinematics from Dynamic Trials.
Int. J. Numer. Methods Biomed. Eng. **2020**, *36* (1), e3283. https://doi.org/10.1002/cnm.3283.

(103) Xu, D.; Carlton, L. G.; Rosengren, K. S. Anticipatory Postural Adjustments for Altering Direction
during Walking. *J. Mot. Behav.* **2004**, *36* (3), 316–326. https://doi.org/10.3200/JMBR.36.3.316-
326.

(104) Bell, A. L.; Pedersen, D. R.; Brand, R. A. A Comparison of the Accuracy of Several Hip Center
Location Prediction Methods. *J. Biomech.* **1990**, *23* (6), 617–621. https://doi.org/10.1016/0021-
9290(90)90054-7.

(105) Leardini, A.; Cappozzo, A.; Catani, F.; Toksvig-Larsen, S.; Petitto, A.; Sforza, V.; Cassanelli, G.;
Giannini, S. Validation of a Functional Method for the Estimation of Hip Joint Centre Location. *J.*
Biomech. **1999**, *32* (1), 99–103. https://doi.org/10.1016/S0021-9290(98)00148-1.

(106) Charlton, I. W.; Tate, P.; Smyth, P.; Roren, L. Repeatability of an Optimised Lower Body Model.
Gait Posture **2004**, *20* (2), 213–221. https://doi.org/10.1016/j.gaitpost.2003.09.004.

(107) Chèze, L.; Fregly, B. J.; Dimnet, J. Determination of Joint Functional Axes from Noisy Marker Data
Using the Finite Helical Axis. *Hum. Mov. Sci.* **1998**, *17* (1), 1–15. https://doi.org/10.1016/S0167-
9457(97)00018-3.

(108) Sartori, M.; Reggiani, M.; Farina, D.; Lloyd, D. G. EMG-Driven Forward-Dynamic Estimation of
Muscle Force and Joint Moment about Multiple Degrees of Freedom in the Human Lower
Extremity. *PLOS ONE* **2012**, *7* (12), e52618. https://doi.org/10.1371/journal.pone.0052618.

(109) Pizzolato, C.; Lloyd, D. G.; Sartori, M.; Ceseracciu, E.; Besier, T. F.; Fregly, B. J.; Reggiani, M.
CEINMS: A Toolbox to Investigate the Influence of Different Neural Control Solutions on the
Prediction of Muscle Excitation and Joint Moments during Dynamic Motor Tasks. *J. Biomech.*
2015, *48* (14), 3929–3936. https://doi.org/10.1016/j.jbiomech.2015.09.021.

(110) De Groote, F.; Van Campen, A.; Jonkers, I.; De Schutter, J. Sensitivity of Dynamic Simulations of
Gait and Dynamometer Experiments to Hill Muscle Model Parameters of Knee Flexors and
Extensors. *J. Biomech.* **2010**, *43* (10), 1876–1883.
https://doi.org/10.1016/j.jbiomech.2010.03.022.

(111) Anderson, F. C.; Pandy, M. G. Static and Dynamic Optimization Solutions for Gait Are Practically
Equivalent. *J. Biomech.* **2001**, *34* (2), 153–161. https://doi.org/10.1016/S0021-9290(00)00155-X.

(112) Millard, M.; Uchida, T.; Seth, A.; Delp, S. L. Flexing Computational Muscle: Modeling and
Simulation of Musculotendon Dynamics. *J. Biomech. Eng.* **2013**, *135* (2), 0210051–02100511.
https://doi.org/10.1115/1.4023390.

(113) Buchanan, T. S.; Lloyd, D. G.; Manal, K.; Besier, T. F. Estimation of Muscle Forces and Joint
Moments Using a Forward-Inverse Dynamics Model. *Med. Sci. Sports Exerc.* **2005**, *37* (11), 1911–
1916. https://doi.org/10.1249/01.mss.0000176684.24008.6f.

(114) Handsfield, G. G.; Meyer, C. H.; Hart, J. M.; Abel, M. F.; Blemker, S. S. Relationships of 35 Lower
Limb Muscles to Height and Body Mass Quantified Using MRI. *J. Biomech.* **2014**, *47* (3), 631–638.

1482 https://doi.org/10.1016/j.jbiomech.2013.12.002.

(115) Ao, D.; Shourijeh, M. S.; Patten, C.; Fregly, B. J. Evaluation of Synergy Extrapolation for Predicting Unmeasured Muscle Excitations from Measured Muscle Synergies. *Front. Comput. Neurosci.* **2020**, *14*. https://doi.org/10.3389/fncom.2020.588943.

(116) Ao, D.; Vega, M. M.; Shourijeh, M. S.; Patten, C.; Fregly, B. J. EMG-Driven Musculoskeletal Model Calibration with Estimation of Unmeasured Muscle Excitations via Synergy Extrapolation. *Front. Bioeng. Biotechnol.* **2022**, *10*. https://doi.org/10.3389/fbioe.2022.962959.

(117) Di, A.; Benjamin, J. F. Comparison of Synergy Extrapolation and Static Optimization for Estimating Multiple Unmeasured Muscle Activations during Walking. *bioRxiv* **2024**, 2024.03.03.583228. https://doi.org/10.1101/2024.03.03.583228.

(118) Arnold, E. M.; Hamner, S. R.; Seth, A.; Millard, M.; Delp, S. L. How Muscle Fiber Lengths and Velocities Affect Muscle Force Generation as Humans Walk and Run at Different Speeds. *J. Exp. Biol.* **2013**, *216* (11), 2150–2160. https://doi.org/10.1242/jeb.075697.

(119) Gopalakrishnan, A.; Modenese, L.; Phillips, A. T. M. A Novel Computational Framework for Deducing Muscle Synergies from Experimental Joint Moments. *Front. Comput. Neurosci.* **2014**, *8*. https://doi.org/10.3389/fncom.2014.00153.

(120) Shourijeh, M. S.; Fregly, B. J. Muscle Synergies Modify Optimization Estimates of Joint Stiffness During Walking. *J. Biomech. Eng.* **2020**, *142* (1), 011011. https://doi.org/10.1115/1.4044310.

(121) Ivanenko, Y. P.; Cappellini, G.; Dominici, N.; Poppele, R. E.; Lacquaniti, F. Coordination of Locomotion with Voluntary Movements in Humans. *J. Neurosci.* **2005**, *25* (31), 7238–7253. https://doi.org/10.1523/JNEUROSCI.1327-05.2005.

(122) Rodriguez, K. L.; Roemmich, R. T.; Cam, B.; Fregly, B. J.; Hass, C. J. Persons with Parkinson's Disease Exhibit Decreased Neuromuscular Complexity during Gait. *Clin. Neurophysiol.* **2013**, *124* (7), 1390–1397. https://doi.org/10.1016/j.clinph.2013.02.006.

(123) Bhargava, L. J.; Pandy, M. G.; Anderson, F. C. A Phenomenological Model for Estimating Metabolic Energy Consumption in Muscle Contraction. *J. Biomech.* **2004**, *37* (1), 81–88. https://doi.org/10.1016/s0021-9290(03)00239-2.

(124) Roh, J.; Cheung, V. C. K.; Bizzi, E. Modules in the Brain Stem and Spinal Cord Underlying Motor Behaviors. *J. Neurophysiol.* **2011**, *106* (3), 1363–1378. https://doi.org/10.1152/jn.00842.2010.

(125) Cheung, V. C. K.; Piron, L.; Agostini, M.; Silvoni, S.; Turolla, A.; Bizzi, E. Stability of Muscle Synergies for Voluntary Actions after Cortical Stroke in Humans. *Proc. Natl. Acad. Sci.* **2009**, *106* (46), 19563–19568. https://doi.org/10.1073/pnas.0910114106.

(126) Raja, B.; Neptune, R. R.; Kautz, S. A. Coordination of the Non-Paretic Leg During Hemiparetic Gait: Expected and Novel Compensatory Patterns. *Clin. Biomech. Bristol Avon* **2012**, *27* (10), 1023–1030. https://doi.org/10.1016/j.clinbiomech.2012.08.005.

(127) Kautz, S. A.; Patten, C. Interlimb Influences on Paretic Leg Function in Poststroke Hemiparesis. *J. Neurophysiol.* **2005**, *93* (5), 2460–2473. https://doi.org/10.1152/jn.00963.2004.

(128) Sánchez, N.; Acosta, A. M.; López-Rosado, R.; Dewald, J. P. A. Neural Constraints Affect the Ability to Generate Hip Abduction Torques When Combined With Hip Extension or Ankle Plantarflexion in Chronic Hemiparetic Stroke. *Front. Neurol.* **2018**, *9*. https://doi.org/10.3389/fneur.2018.00564.

(129) Pandian, S.; Arya, K. N.; Kumar, D. Does Motor Training of the Nonparetic Side Influences Balance and Function in Chronic Stroke? A Pilot RCT. *Sci. World J.* **2014**, *2014* (1), 769726. https://doi.org/10.1155/2014/769726.

(130) Lim, H.; Madhavan, S. Non-Paretic Leg Movements Can Facilitate Cortical Drive to the Paretic Leg in Individuals Post Stroke with Severe Motor Impairment: Implications for Motor Priming. *Eur. J. Neurosci.* **2023**, *58* (3), 2853–2867. https://doi.org/10.1111/ejn.16069.

(131) Kramer, S.; Johnson, L.; Bernhardt, J.; Cumming, T. Energy Expenditure and Cost During Walking After Stroke: A Systematic Review. *Arch. Phys. Med. Rehabil.* **2016**, *97* (4), 619-632.e1.

https://doi.org/10.1016/j.apmr.2015.11.007.

(132) Hoxie, R. E.; Rubenstein, L. Z.; Hoenig, H.; Gallagher, B. R. The Older Pedestrian. *J. Am. Geriatr.*
Soc. **1994**, *42* (4), 444–450. https://doi.org/10.1111/j.1532-5415.1994.tb07496.x.

(133) Perry, J.; Garrett, M.; Gronley, J. K.; Mulroy, S. J. Classification of Walking Handicap in the Stroke
Population. *Stroke* **1995**, *26* (6), 982–989. https://doi.org/10.1161/01.str.26.6.982.

(134) Hug, F.; Turpin, N. A.; Couturier, A.; Dorel, S. Consistency of Muscle Synergies during Pedaling
across Different Mechanical Constraints. *J. Neurophysiol.* **2011**, *106* (1), 91–103.
https://doi.org/10.1152/jn.01096.2010.

(135) Pataky, T. C.; Goulermas, J. Y. Pedobarographic Statistical Parametric Mapping (pSPM): A Pixel-
Level Approach to Foot Pressure Image Analysis. *J. Biomech.* **2008**, *41* (10), 2136–2143.
https://doi.org/10.1016/j.jbiomech.2008.04.034.

(136) Duckworth, T.; Betts, R. P.; Franks, C. I.; Burke, J. The Measurement of Pressures under the Foot.
Foot Ankle **1982**, *3* (3), 130–141. https://doi.org/10.1177/107110078200300303.

(137) Li, G.; Ao, D.; Vega, M. M.; Zandiyeh, P.; Chang, S.-H.; Penny, A. N.; Lewis, V. O.; Fregly, B. J.
Changes in Walking Function and Neural Control Following Pelvic Cancer Surgery with
Reconstruction. *Front. Bioeng. Biotechnol.* **2024**, *12*.
https://doi.org/10.3389/fbioe.2024.1389031.

(138) Wirth, M. A.; Kovesi, P. MATLAB as an Introductory Programming Language. *Comput. Appl. Eng.*
Educ. **2006**, *14* (1), 20–30. https://doi.org/10.1002/cae.20064.

(139) Vicéns, J. L.; Zamora, B.; Ojados, D. Improvement of the Reflective Learning in Engineering
Education Using MATLAB for Problems Solving. *Comput. Appl. Eng. Educ.* **2016**, *24* (5), 755–764.
https://doi.org/10.1002/cae.21748.

(140) Anderson, F. C.; Pandy, M. G. Static and Dynamic Optimization Solutions for Gait Are Practically
Equivalent. *J. Biomech.* **2001**, *34* (2), 153–161. https://doi.org/10.1016/s0021-9290(00)00155-x.

(141) Suwarganda, E. K.; Diamond, L. E.; Lloyd, D. G.; Besier, T. F.; Zhang, J.; Killen, B. A.; Savage, T. N.;
Saxby, D. J. Minimal Medical Imaging Can Accurately Reconstruct Geometric Bone Models for
Musculoskeletal Models. *PLOS ONE* **2019**, *14* (2), e0205628.
https://doi.org/10.1371/journal.pone.0205628.

(142) Killen, B. A.; Brito da Luz, S.; Lloyd, D. G.; Carleton, A. D.; Zhang, J.; Besier, T. F.; Saxby, D. J.
Automated Creation and Tuning of Personalised Muscle Paths for OpenSim Musculoskeletal
Models of the Knee Joint. *Biomech. Model. Mechanobiol.* **2021**, *20* (2), 521–533.
https://doi.org/10.1007/s10237-020-01398-1.

(143) Kainz, H.; Wesseling, M.; Jonkers, I. Generic Scaled versus Subject-Specific Models for the
Calculation of Musculoskeletal Loading in Cerebral Palsy Gait: Effect of Personalized
Musculoskeletal Geometry Outweighs the Effect of Personalized Neural Control. *Clin. Biomech.*
2021, *87*, 105402. https://doi.org/10.1016/j.clinbiomech.2021.105402.

(144) Michaud, F.; Frey-Law, L. A.; Lugrís, U.; Cuadrado, L.; Figueroa-Rodríguez, J.; Cuadrado, J. Applying
a Muscle Fatigue Model When Optimizing Load-Sharing between Muscles for Short-Duration
High-Intensity Exercise: A Preliminary Study. *Front. Physiol.* **2023**, *14*.
https://doi.org/10.3389/fphys.2023.1167748.

(145) Ma, L.; Zhang, W.; Hu, B.; Chablat, D.; Bennis, F.; Guillaume, F. Determination of Subject-Specific
Muscle Fatigue Rates under Static Fatiguing Operations. *Ergonomics* **2013**, *56* (12), 1889–1900.
https://doi.org/10.1080/00140139.2013.851283.

Figure Captions

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