Acoustic prediction and biomechanical validation of primary stability in uncemented

short-stem hip prostheses: an experimental study

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Abstract

Background

In uncemented hip arthroplasty, achieving sufficient primary stability is essential for long-

term implant success. However, objective intraoperative assessment of fixation quality

remains challenging. Acoustic analysis of stem impaction sounds offers a promising tool for

real-time evaluation, but its diagnostic accuracy and biomechanical correlation require further

validation.

Methods

Twelve formalin-fixed human femora were implanted with cementless Metha® short stems

under three predefined anchorage conditions: loose, optimal (fit), and fracture-inducing press-

fit. Impaction sounds were recorded using calibrated microphones and processed via

frequency-domain analysis. Relative micromotions were quantified under torsional loading to

biomechanically assess primary stability.

Results

Spectral markers reliably differentiated between anchorage states. The transition from loose to

fit showed minimal spectral change, while fit-to-fracture was characterized by a significant

increase in low-frequency energy (<2.5 kHz) and pronounced attenuation in high-frequency

bands (>15 kHz). These acoustic signatures closely correlated with biomechanically measured

micromotions, which showed a distinct hierarchy: fracture < fit < loose. Cluster permutation

analysis confirmed statistically significant differences, particularly in the fracture group.

Conclusion

This in vitro study demonstrates that frequency-based acoustic analysis can distinguish

between stable, insufficient, and over-press-fit conditions during stem implantation. The

findings support the potential of intraoperative acoustic monitoring as a real-time, objective

tool to enhance implant safety and detect cortical compromise before it becomes clinically

apparent.

Keywords: cementless hip arthroplasty, acoustic analysis, stem impaction, primary

stability, frequency-domain analysis, micromotion

Introduction

The implantation of hip endoprostheses is one of the most common surgical procedures in orthopaedic surgery and in many cases leads to a significant improvement in quality of life (Grubor et al. 2013). Despite established surgical techniques and the use of high-quality implant systems, complications such as loosening, periprosthetic fractures or the need for revision surgery remain a relevant clinical problem. Intraoperative fractures in particular occur with a frequency of around 1-5% (Kenanidis et al. 2020). With uncemented implants, this risk is particularly relevant due to the necessary interference fit, which results from an undersized prosthesis bearing in the bone and into which the prosthesis is driven (Hailer et al. 2010).

Postoperative primary stability, i.e. the direct mechanical anchoring of the prosthesis in the bone, is crucial for the success of the treatment. It is the prerequisite for subsequent bony integration and thus for the long-term stability of the implant (Bürkner et al. 2012). However, there is currently no reliable, commercially available system for the objective intraoperative assessment of this stability. Surgeons are currently highly dependent on their experience and subjective perception during implantation - for example through tactile feedback when the prosthesis is inserted. Whether this results in fine fissures or even fractures can often not be determined with certainty intraoperatively. Even imaging procedures such as intraoperative X-ray checks offer only limited certainty here, as possible fractures can easily be overlooked due to the overlapping of the prosthesis in the bone (Hassan et al. 1998; HARRIS et al. 1991).

Promising approaches to improving intraoperative assessment are currently focusing on analyzing acoustic signals that are generated during implantation. These change depending on the anchoring of the implant in the bone and allow conclusions to be drawn about the strength of the connection and possible microfractures (García-Vilana et al. 2025; Aggelis et al. 2015; Sakai et al. 2011). In a previous study, it was shown that the stability of the femoral stem can

be reliably monitored in real time using acoustic methods. The results underline the

importance of sufficient primary stability for successful bony integration and the long-term

function of the implant (Fonseca Ulloa et al. 2023). Acoustic methods could therefore make

an important contribution to optimizing surgical results by providing immediate feedback.

This in vitro study aims to determine whether frequency-domain analysis of impaction sounds

can serve as a reliable, objective predictor of primary stability in uncemented short-stem hip

prostheses. Furthermore, it seeks to validate the diagnostic value of acoustic signatures by

correlating them with biomechanically quantified micromotions under controlled torsional

loading.

Material and Methods

<u>Human specimen</u>

A total of n=12 formalin-fixed human femora (nine right, three left) were used for the present

study. The specimens came from body donors of the Anatomical Institute of the Justus Liebig

University Giessen. Ethical approval for the use of the specimens has been granted under file

number 160/19.

<u>Prostheses</u>

The cementless Metha® short stem prostheses (B. Braun, Aesculap AG, Tuttlingen, Germany)

were used. Prosthesis sizes 4 to 7 with a caput-collum-diaphyseal angle of 120° were used.

<u>Preparation and planning</u>

After harvesting, the femur specimens were largely freed of soft tissue and radiologically

measured in the anterior-posterior beam path to determine the appropriate prosthesis size. The

collum was then prepared according to the radiological planning using the MediCAD

software (mediCAD Hectec GmbH, Altdorf /Landshut, Germany). The medullary cavity was

rasped to the respective size using the manufacturer's instruments. The bones were numbered

and deep-frozen at -20°C until the day of implantation.

<u>Implantation of the prostheses</u>

Before implantation, the bones were thawed at $16 \pm 1°C$ room temperature for 3 hours. The

distal end of the prostheses was drilled in advance with a 1.9 mm drill for the subsequent

application of a measuring pin for primary stability measurement. To prevent excessive

movement during implantation, the femora were fixed in the desired position in a non-slip

hard foam block (PE block foam, Wilhelm Julius Teufel GmbH, Germany). This was then

pressed against the laboratory operating table using two clamps and an assistant (A. T.). The

implantation itself was performed by an experienced specialist (BA. I.). The specimens were

randomly assigned to three different study groups with n=4 specimens each: too loose (*loose*),

correct (*fit* - which refers to the surgeon's intraoperative assessment of optimal press-fit

without visible cortical damage) and up to fracture of the bone (*fracture*). These conditions

were documented and recorded by the surgeon. A detailed overview of the femoral specimens

and prosthesis sizes in the different groups is shown in Table 1 (Table 1).

Table 1: Status assignment of the femora (R = right, L = left) and prosthesis sizes

State	Specimen	Prosthesis size
fit	#13 R	4
fit	#13 L	4
fit	#3 R	6
fit	#9 R	7

loose	#5 L	4
loose	#4 R	4
loose	#14 L	5
loose	#14 R	6
fracture	#3 L	4
fracture	#10 R	5
fracture	#5 R	6
fracture	#9 L	7

<u>Acoustic instrumentation</u>

Impaction sounds were recorded with a laboratory-calibrated measurement microphone (MM

1, beyerdynamic, Heilbronn, Germany; free-field response 20 Hz – 20 kHz, ±1.5 dB). The

capsule was positioned 50 cm from the prosthesis axis, aimed directly at the stem shoulder.

The microphone fed a four-channel USB interface (Rubix 44, Roland Corporation,

Hamamatsu, Japan; 24-bit, 192 kHz, ASIO), which served as external A/D converter. Prior to

the first implantation a calibration blow was used to set the analogue gain such that the

loudest strike remained ≥6 dB below full scale; the setting was kept unchanged for all

specimens. Signals were stored as 44.1 kHz/24-bit PCM.

<u>Signal processing</u>

Individual hammer blows were isolated by a back-tracked spectral flux onset detector

implemented in *librosa 0.10.1*. Each segment was zero-padded or truncated and transformed

with a single-sided FFT of equal length. The amplitude spectrum P_1 was energy-normalised

$(P_{1,norm} = \frac{|FFT|}{\sum|FFT|})$ to compensate for amplitude variability; segments whose total energy fell

below five percent of the median were discarded. Four regions of interest (ROI) reproduced

the "original bands" reported by Fonseca et al. (Fonseca Ulloa et al. 2023): Low (0–2.5 kHz),

2.9 kHz (2.7–3.1 kHz), 4.4 kHz (4.2–4.6 kHz) and 8.7 kHz (8.5–8.9 kHz).

<u>Software environment</u>

All signal processing and statistical procedures were executed in Python 3.9 under Anaconda

(Win-64). Core numerical operations relied on NumPy 1.26.1 and SciPy 1.13.1, whereas

audio segmentation and resampling were handled by librosa 0.10.1 and soundfile 0.12.1. The

non‑parametric statistics were implemented with MNE-Python 1.8.0 (cluster permutation)

and Pingouin 0.5.5 (permutation *t*, effect sizes). Data management used pandas 2.1.1;

graphics were created with Matplotlib 3.8.0. Machine-learning benchmarks employed scikit-

learn 1.3.1. Low-level FFT kernels were accelerated by Numba 0.58.1.

<u>Preparation of the primary stability measurement</u>

For the primary stability measurement, the femora were then embedded in epoxy resin (GP

010 A/B, Gößl + Pfaff GmbH, Germany) at the condyles. A reference frame was then fixed at

the level of the lesser trochanter. This served as a base for attaching the measuring frame with

integrated measuring sensors and as a reference point. Starting from this reference point, the

positions of the bone measuring points could be precisely determined. The bone measuring

points were 45 mm proximal (B_1) and 30 mm (B_2) and 80 mm (B_3) distal to the lesser

trochanter. Holes with a diameter of 1.9 mm were drilled at each of the previously defined

measuring points and the measuring pins were fixed in place using superglue. In addition,

another pin was attached to the proximal shoulder of the prosthesis (P_p). At the distal end of

the prosthesis, the surrounding bone was specifically expanded with a 10 mm drill to expose

the hole previously made. The distal measuring point (P_d) could then be precisely inserted and

fixed in this hole.

<u>Primary stability measurement</u>

Based on previous studies, retrograde and reaction-free axial torsional moments around the

longitudinal Z-axis of the femoral stem were applied into the prosthesis. These torques were

increased in a continuous process up to a maximum value of ±3.5 Nm (for *fit* and *loose*) and

±1.75 Nm (for *fracture*) in 80 incremental steps. The maximum torque was reached twice in

each direction of rotation, resulting in 480 individual measurements per series. Each series of

measurements was repeated three times for each measuring point (Fölsch et al. 2024; Jahnke

et al. 2020; Fölsch et al. 2023).

This method was used to generate very small but measurable micromovements, if possible

without impairing the respective anchoring stability of the prosthesis. To record these

movements, the measuring pins at the bone measuring points (B_1-B_3) as well as at the

prosthesis ($P_p + P_d$) were connected to the individual measuring points one after the other via

a measuring cube. This cube served as a local coordinate system. After each torsion step, the

spatial position of the measuring cube was recorded using 9 non-contact eddy current sensors

(NCDT 3010-S2, Micro-Epsilon Messtechnik GmbH & Co. KG, Ortenburg, Germany) in a 3-

3-3 arrangement per plane with a resolution of 0.1 μm. The normalized rotational stability was

then calculated for each measurement point as a function of the applied torque (mdeg/Nm) in

order to characterize the anchoring behaviour of the prosthesis. The proximal and distal

relative micromovements (rm_1 and rm_2) were calculated as the difference between the

corresponding measuring point heights of the prosthesis and bone measuring points P_p-B_1

(rm_1) and P_d - B_2 (rm_2) (Figure 1).

Figure 1: Experimental setup and measurement protocol for quantifying primary stability via

torsion-induced micromovements

Due to the different lengths of the prosthesis models used, the relative movements rm_1 and

rm_2 were transferred to the level of the corresponding bone measuring points B_1 and B_2 using

linear interpolation. This ensures a methodologically consistent and statistically comparable

evaluation of the different stem designs (Jahnke et al. 2020).

<u>Statistics</u>

Band-wise differences ($\Delta\mu$) between conditions were assessed with independent permutation

t-tests (10 000 resamples, two-tailed); effect size was expressed as Cohen's *d*. Whole-

spectrum differences were quantified by the two-sample Kolmogorov–Smirnov statistic.

Frequency-resolved effects were detected with a one-dimensional cluster permutation test (5

000 permutations, $\alpha = 0.05$). An adjacency matrix connected frequency bins within a gap of

≤ 20 bins, preventing fragmentation; clusters with family-wise $p < 0.05$ were deemed

significant. The statistical evaluation of the measurement results of the primary stability

analysis was carried out using SPSS software (version 29.0, IBM, New York, United States).

A non-paremetric Kruskal-Wallis test was performed to identify significant differences

between the groups. The results were evaluated at a significance level of $p < 0.05$.

Results

<u>Band-wise permutation analysis</u>

Table 2 summarises the permutation-based comparisons (10 000 resamples, two-tailed) within

the four frequency windows originally reported by Fonseca et al. (Fonseca Ulloa et al. 2023).

Effect sizes are expressed as Cohen's *d*. Only the fit–fracture and loose–fracture contrasts

revealed statistically relevant differences ($\alpha<0.05$, family-wise), predominantly in the low-

frequency band (< 2.5 kHz) and the first high-frequency window around 8.7 kHz. In contrast,

loose–fit differences were negligible ($|d| \leq 0.14$, $p>0.3$).

Table 2: Band-wise permutation analysis reveals significant fit–fracture and loose–fracture

differences in selected frequency bands

original band	Comparison	Δμ	*p*-value	*d*	Interpretation
0–2 500 Hz	loose–fit	$5.5 \times 10^{\square\square}$	0.967	+0.01	no effect
	fit–fracture	**+0.062**	**0.0002**	+1.02	substantial ↑ in fracture
	loose–fracture	+0.063	0.007	+0.58	moderate
2 700–3 100 Hz	loose–fit	+0.0020	0.38	+0.14	trivial
	fit–fracture	**+0.0069**	**0.034**	+0.46	medium
	loose–fracture	**+0.0089**	**0.0006**	+0.76	large
4 200–4 600 Hz	loose–fit	–0.00027	0.86	–0.03	none

	fit–fracture	+0.0014	0.506	+0.16	small
	loose–fracture	+0.0011	0.578	+0.12	small
8 500–8 900 Hz	loose–fit	+0.00052	0.515	+0.10	none
	fit–fracture	**–0.0040**	**0.0002**	–1.37	large ↓ in fracture
	loose–fracture	**–0.0035**	**0.011**	–0.62	moderate

Global distribution tests

Kolmogorov–Smirnov tests, performed on the complete spectra (Table 3), confirmed global distributional differences between all three conditions. The largest separations were observed for pairings that involved the fracture state.

Table 3: Kolmogorov–Smirnov tests confirm global spectral differences, with largest deviations involving the fracture condition

Pair	D	p
loose vs fit	0.087	$6.2 \times 10^{\square\square}$
fit vs fracture	**0.177**	$<10^{\square 2 \square 3}$
loose vs fracture	**0.180**	$<10^{\square 2 \square 1}$

Cluster permutation tests

A one-dimensional cluster permutation test (5 000 permutations; threshold t-value corresponding to $\alpha = 0.05$; maximum spatial gap ≤ 20 frequency bins) was applied to the log-

spectral amplitudes. Nine, 16 and 12 significant clusters (family-wise α < 0.05) were obtained

for loose–fit, fit–fracture and loose–fracture respectively (Figure 4–6).

<u>Visual summary</u>

Stacked plots (Figure 2: loose–fit, Figure 3: fit–fracture, Figure 4: loose–fracture) display

mean ± SD spectra with super-imposed cluster spans and the absolute T metrics. Legends

identify every significant cluster by its rounded 100-Hz limits and corrected p-value.

Figure 2: **Loose vs fit**: the original bands reported by Fonseca et al. (Fonseca Ulloa et al.

2023) (< 2.5 kHz, 2.9 kHz, 4.4 kHz, 8.7 kHz) were all replicated, although their summed $|T|$

ranked only second to eighth (e.g., 8 724–9 380 Hz, p=0.001).

Figure 3: **Fit vs fracture**: new, wide clusters emerged between 15–20 kHz and 7–9 kHz ($\Sigma|T|$

> 22 000; $p \leq 0.0002$), whereas the classical bands shifted upwards by ≈ 0.5 kHz.

Figure 4: **Loose vs fracture**: combined effects yielded two dominant high-frequency clusters

(15–19 kHz, 8–9 kHz) and a broad low-frequency cluster (0–255 Hz, $p=0.009$).

A representative image of an intraoperative fracture is shown in Figure 5. The cortical

disruption (indicated by the red arrow) occurred during stem impaction and reflects a critical

outcome of excessive press-fit.

Figure 5: Illustration of a bone fractured during the implantation process.

Motion graph

The motion graph illustrates the normalized relative movements between the prosthesis and

the femur as a function of the defined measurement heights rm1 (proximal) and rm2 (distal).

The respective fixation conditions – loose, fit, and fracture – display characteristic patterns. In

the loose group, significantly larger distances between the prosthesis and bone (orange lines)

are visible, indicating pronounced micromovements and reflecting a lack of force-locked

connection between implant and bone. Movement is markedly pronounced both proximally

and distally, suggesting insufficient mechanical stability. In the fit group, the lines are closer

together, indicating a stable anchorage between prosthesis and femur and biomechanically

confirming good primary fixation. The fracture group shows the smallest distances; the

movements are minimal, pointing to an almost rigid connection. However, this rigidity may

indicate overpressurization, which is associated with an increased risk of fracture. The

graphically depicted distances between prosthesis and bone measurement points thus provide

direct insight into the quality of the primary connection and allow for a clear differentiation of

stability conditions along the anatomical axis (Figure 6).

Figure 6: Relative micromovement patterns reveal distinct primary stability states across

fixation conditions

<u>Primary stability analysis</u>

The results of the primary stability analysis revealed clear differences between the three

anchorage conditions (*loose*, *fit* and *fracture*), which were statistically evaluated using a non-

parametric Kruskal–Wallis test. The *fit* group showed low relative micromotions (rm_1 = 4.41

± 2.43 mdeg/Nm; rm_2 = 5.59 ± 4.77 mdeg/Nm). Even lower values were observed in the

fracture group (rm_1 = 1.67 ± 0.60 mdeg/Nm; rm_2 = 2.72 ± 1.97 mdeg/Nm). In contrast, the

loose group exhibited significantly higher relative micromotions (rm_1 = 132.78 ± 171.4

mdeg/Nm; rm_2 = 124.69 ± 125.07 mdeg/Nm), indicating insufficient mechanical fixation and

a potentially increased risk of early loosening. Statistically significant differences were

particularly evident between *fit* and *loose* (p = 0.003 for rm_1) as well as between *fracture* and

loose (p = 0.006 for rm_2). A significant difference was also found between *fit* and *fracture* for

rm_2 (p = 0.05; see Table 4).

Table 4: Relative micromotions (rm_1, rm_2) distinguish anchorage quality, with significant differences between *loose*, *fit* and *fracture* conditions. Small superscript letters indicate significant differences in pairwise comparison.

state	ID	Measurement levels	
		rm_1 [mdeg/Nm]	rm_2 [mdeg/Nm]
loose	#1	95.95	187.83
	#2	13.27	27.16
	#3	384.55	270.02
	#4	37.35	13.74
	MEAN	**132.78** [a]	**124.69** [a,b]
	SD	**171.4**	**125.07**
fit	#1	6.59	12.32
	#2	3.14	5.65
	#3	6.30	2.21
	#4	1.63	2.19
	MEAN	**4.41**	**5.59** [a]
	SD	**2.43**	**4.77**
fracture	#1	1.25	0.96
	#2	2.04	4.32
	#3	1.08	1.07
	#4	2.32	4.53

	MEAN	1.67[a]	2.72[b]
	SD	0.60	1.97
p-values		a=0.003	a=0.05, b=0.006

Discussion

The present study aimed to determine whether frequency-domain analysis of impaction

sounds can reproduce the spectral markers of primary stability described by Fonseca et al.

(Fonseca Ulloa et al. 2023) and, more importantly, whether it can distinguish a clinically

hazardous "over-impaction" that culminates in cortical fracture. All hammer blows were

recorded under strictly standardized acoustic conditions and processed with an identical FFT-

based workflow; statistical inference relied on permutation statistics and family-wise–

controlled cluster analysis, thereby avoiding distributional assumptions and α-inflation.

<u>Re-appearance and shift of the original bands</u>

For the *loose* to *fit* transition the four canonical bands (< 2.5 kHz, 2.9 kHz, 4.4 kHz, 8.7 kHz)

were confirmed by cluster permutation, although their effect sizes were small ($d \leq 0.14$) and

global separation minimal (KS = 0.087). The findings are congruent with the original report in

which spectral change was attributed primarily to a shift of energy from the low-frequency

band to the first two high-frequency bands (Fonseca Ulloa et al. 2023). In the current data this

shift is still present but its amplitude is ≤ 0.2 dB, suggesting that the surgeon's subjective *fit*

criterion already limits further seating and thus attenuates the spectral contrast observed in

strictly incremental laboratory insertions.

<u>Emergence of fracture-specific signatures</u>

The transition from *fit* to *fracture* produced a qualitatively different acoustic fingerprint. In the

low-frequency window (< 2.5 kHz) band power increased by +6 % ($\Delta\mu = 0.062$, $d \approx 1$),

whereas energy between 15 and 20 kHz dropped sharply, forming two broad, highly

significant clusters ($\Sigma\|T\| > 5 \times 10\square$). Such high-frequency deficits are characteristic of loss of

cortical continuity and the concomitant damping of flexural modes; similar shifts have been

reported for microscopic fatigue cracks in cortical bone specimens (Aggelis et al. 2015;

García-Vilana et al. 2025; Sakai et al. 2011). The discovery of additional narrow clusters at 7–

9 kHz provides further evidence that the spectral content of the hammer blow is sensitive to

small changes in stem-bone coupling long before gross displacement becomes apparent.

<u>Agreement with mechanical primary-stability testing</u>

Relative micromotion testing demonstrated a clear hierarchy: *fracture < fit < loose* for both

proximal (rm_1) and distal (rm_2) relative micromotions. The wide separation between *loose* and

fit confirms that acoustic changes in the incremental insertion phase mainly reflect global

stem seating, whereas the appearance of fracture-specific high-frequency clusters parallels the

sudden reduction in micromotion caused by over-press-fit and cortical cracking. The fact that

the low-frequency band (< 2.5 kHz) is significantly higher in *fracture* than in *fit* indicates that

rigid bony confinement amplifies the fundamental resonance originally observed by Fonseca

et al. in the *fit* condition (Fonseca Ulloa et al. 2023). Thus, spectral analysis not only

reproduces the classical stability markers but also provides an acoustic "warning zone" above

15 kHz that coincides with the loss of elastic compliance measured mechanically.

Clinical Implications of Primary Stability

The results underscore the essential importance of primary stability as a key factor for both

the short- and long-term success of uncemented short-stem hip prostheses. As the immediate

mechanical anchorage of the implant within the surrounding bone, primary stability is crucial

for the initial load-bearing capacity of the prosthesis and the subsequent biological integration

through osseointegration. Inadequate primary stability can lead to micromovements that

impair this integration and significantly increase the risk of aseptic loosening (Bürkner et al.

2012; Hailer et al. 2010).

Biomechanical validation through relative micromotion measurements demonstrated a clear

differentiation between anchorage conditions: prostheses in the *loose* group exhibited

significantly higher micromotions, indicating a lack of force-locked fixation and thus

potentially unstable primary anchorage. In contrast, correctly implanted *fit* prostheses showed

minimal motion, confirming sufficient mechanical stability.

Particularly critical is the assessment of the *fracture* group: although relative micromotions

were low - superficially suggesting high stability - these cases involved mechanical over-

press-fit, resulting in the onset of cortical fractures. Such fractures can easily go unnoticed

intraoperatively, especially by less experienced surgeons, as they often do not present

immediate clinical or radiographic signs (Adla et al. 2023; Berry 2002). If early-stage

fractures remain undetected, there is a considerable risk of complete or displaced fractures

during postoperative loading, for instance during early mobilization (Geest et al. 2013). These

complications often necessitate complex revision surgeries and significantly delay

rehabilitation (Simunovic et al. 2010). Against this backdrop, the combination of acoustic

analysis and biomechanical validation offers a valuable tool for intraoperative quality control.

The acoustic markers identified in this study provide real-time feedback on the anchorage

condition and could serve as an objective early warning system to detect both insufficient

fixation and excessive press-fit. This is especially relevant in training situations or in cases

with complex anatomy, where the surgeon's subjective assessment may be limited. In the long

term, the results of this study lay the foundation for data-driven decision support in the

operating room, with the potential to improve safety during uncemented prosthesis

implantation and reduce complications arising from inadequate primary stability.

Limitations

Despite promising results, this study has several limitations. All tests were conducted on

formalin-fixed human cadaveric femora, which differ biomechanically from living bone and

lack biological responses. Only one short stem design (Metha®, Aesculap) was examined,

limiting generalizability to other implant types. Standardized surgical technique, impaction

force, and microphone placement ensured consistency but only partly reflect clinical

variability. No direct comparison was made with conventional intraoperative tools (e.g.,

fluoroscopy), so the diagnostic sensitivity of the acoustic method remains unverified. Lastly,

the acoustic markers have not yet been tested in vivo, and their clinical applicability must be

assessed in future studies., limiting the ability to compare diagnostic accuracy across

modalities.

Conclusions

This in vitro study demonstrates that spectral cluster analysis of impaction sounds enables

objective differentiation between distinct anchorage states of an uncemented short stem hip

prostheses. The identified frequency-domain features correlate closely with mechanically

measured relative micromotion, thereby providing a reliable acoustic proxy for assessing

primary stability.

A particularly noteworthy finding is the detection of high-frequency spectral deficits above 15

kHz combined with a low-frequency gain below 2.5 kHz, which are indicative of incipient

cortical fractures. These fracture-specific acoustic signatures not only reflect critical changes

in stem-bone coupling but may also serve as early intraoperative warning signals - especially

valuable in situations with limited visual control or when procedures are performed by less

experienced surgeons.

Overall, the results highlight the technical feasibility and biomechanical validity of real-time

acoustic monitoring during prosthesis implantation. This approach offers a promising

foundation for developing automated, feedback-supported assistance systems that can

enhance intraoperative safety and reduce the incidence of postoperative complications such as

loosening or fracture, without disrupting the standard surgical workflow.

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Author´s contribution

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