

Thermoelectric Heat Exchange and Growth Regulation in a Continuous Yeast Culture

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Abstract

We have designed a thermoelectric heat exchanger (TEHE) for microbial fermentations, able to control the temperature of a microbial continuous culture, and produce electric power. The system proved able to stably maintain both the temperature and the optical density of the culture during the exponential, highly productive phase.

Keywords: heat exchange; continuous culture; temperature regulation; power production; Peltier-Seebeck effect

1. Introduction

2 A range of parameters such as temperature, pH, or substrate concentra-
3 tion need to be stable in order to sustain a suitable microbial growth and/or
4 the stable biosynthesis of a bioproduct [1]. Temperature strongly affects a
5 range of fundamental cellular processes [2, 3]; and thus keeping a microbial
6 culture in a suitable range of temperatures is of high importance in terms of
7 strain performance [4]. Large-scale growth of most microorganisms is accom-
8 panied by the production of heat [5], which, when large culture volumes are
9 set, often results in an undesirable increase in the temperature of the batch
10 culture that has to be alleviated through refrigeration [6, 7].

11

12 In a previous work, we described the first Microbial Thermoelectric Cell
13 (MTC), a system designed for batch cultures allowing the partial conversion

14 of microbial metabolic heat into electricity [8]. A range of industrial fermentations are carried out in continuous culture, where stable cellular densities can be maintained during long periods thanks to the supply of fresh medium, which is introduced at a rate that is equal to the volume of product that is removed from the fermenter. In this work, we aimed at the design, construction and characterization of a continuous culture system where temperature is automatically controlled and electric power is constantly obtained during all the fermentation process. To do that, we envisaged, constructed, and set in place a ThermoElectric Heat Exchanger (hereafter called TEHE), a device based on the Seebeck effect, which allows a fine control of temperature and fresh medium input and thus microbial growth- while electric power is produced.

26 **2. Materials and Methods**

27 *2.1. Experimental set-up*

28 A medium-scale continuous culture of budding yeast *Saccharomyces cerevisiae* strain D170 (kindly provided by Prof. Emilia Matallana, IATA, Valencia, Spain) in YPD medium supplemented with 18 % sucrose was set up in the laboratory as schematically represented in Fig. 1A. The TEHE consisted of two aluminum pipes of squared section and a serial connection of ten thermogenerators (MCPE-071-10-13, Multicomp) placed in direct contact with the pipes. The whole device was thermally insulated with expanded polystyrene (EPS) and polyurethane foam spray (Silicex Fischer, Fisher Iberica, Tarragona, Spain) (Fig. 1B). The TEHE was coupled to a thermally isolated 40 L Dewar flask (Scharlab, Barcelona, Spain) combined with a MM-1000 overhead anchor stirrer (Labnet International, Edison, NJ, USA), and two peristaltic pumps (Lambda Laboratory Instruments, Baar, Switzerland), which were programmed to control the flow of fresh and wasted medium.

41 *2.2. Data Acquisition, Monitoring and Recording*

42 The whole system was connected to a PC in order to record temperature values as well as output electrical current. Temperature measurements were performed by thin T-type thermocouples inserted into the different parts of the system and connected to a PC through a data logger. As in previous studies [8], the connections between the thermocouples and the data logger were performed on an ice-water mixture to take into account the unwanted background electric voltage, due to the junction of dissimilar metals in the

49 thermocouple-data logger connection. Temperature and electrical current
50 records were taken every 6 minutes throughout the experiment. Both feed
51 and effluent flows were automatically modulated during all the experiment
52 with the LabVIEW control software.

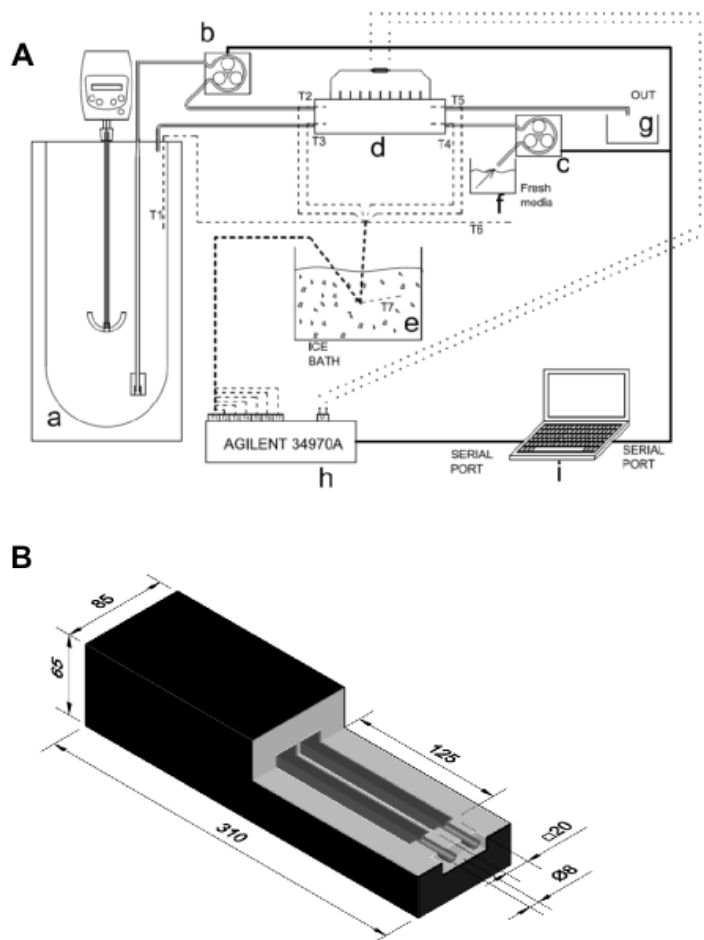


Figure 1: **(A)** Schematic representation of the continuous culture system. (a) Thermally insulated fermenter; (b, c) peristaltic pumps; (d) ThermoElectric Heat Exchanger (TEHE); (e) ice bath for the compensation of temperature measurements; (f) refrigerated fresh medium tank; (g) wasted medium tank; (h) data logger; and (i) PC with a software (Rodrguez-Barreiro et al., 2013) for data recording and automatic control of the peristaltic pumps. All temperature measurements were performed with T-type thermocouples. **(B)** Tridimensional representation of the TEHE constructed in this work. Sizes given in mm.

53 *2.3. Mathematical modelling*

54 The global thermal resistance (R_g) and the whole heat capacity (mc_p) of
55 the fermenter were estimated from Equation 1:

$$m \cdot c_p \cdot \frac{dT_{ce}}{dt} = Q \cdot \rho \cdot c_p \cdot (T_{fs} - T_{ce}) + Pc - \frac{T_{ce} - T_{env}}{R_g} \quad (1)$$

56 Where m , c_p , and T_{ce} are broth mass, specific heat, density, and tem-
57 perature, respectively, whereas Q is the flow rate and Pc is the metabolic
58 heat produced by yeasts. T_{fs} and T_{env} correspond to the fresh medium enter-
59 ing the fermenter and room temperatures, respectively. Equations 2 and
60 3, describing a Logarithmic Mean Temperature Difference (*LMTD*) model of
61 a heat exchanger [9], were used to mathematically characterize the TEHE:

$$LMTD = \Delta T_{ln} = \frac{(T_{ce} - T_{fs}) - (T_{cs} - T_{fe})}{\ln \left(\frac{T_{ce} - T_{fs}}{T_{cs} - T_{fe}} \right)} \quad (2)$$

$$q = U \cdot A \cdot LMTD \quad (3)$$

62 Being T_{ce} and T_{fe} the temperature of the hot and cold inlet flows, re-
63 spectively; and T_{cs} and T_{fs} , the temperature of the hot and cold outlet
64 flows, respectively. The heat flow (q) between the hot and the cold pipe
65 depends on the temperature of the fluids entering the exchanger, the global
66 heat transmission coefficient (U), and the heat exchange surface (A).

67 In order to obtain an estimation of the UA constant, q was first calcu-
68 lated from Equation 4 in an experiment where two water flows at known
69 temperatures were entered in the TEHE.

$$q = \dot{m} \cdot c_p \cdot (T_{ce} - T_{cs}) = \dot{m} \cdot c_p \cdot (T_{fs} - T_{fe}) \quad (4)$$

70 Where \dot{m} is the inlet mass flow rate (mass of water entering the TEHE
71 per unit of time), and c_p is the specific heat of water.

72 **3. Results and Discussion**

73 The output of a typical experiment carried out in the continuous culture
74 system set as described above is shown in Fig. 2. The broth (35 L) was
75 inoculated with 700 mL (1:50) of an overnight yeast culture, and cultivated

76 in the thermally isolated flask under shaking (180 rpm). Broth temperature
77 rose in an exponential fashion and reached 35 °C after 24 h, (Fig. 2A). At
78 this point, culture temperature was kept constant by means of introducing
79 fresh, cool medium in the fermenter (feed flow) at the same rate that wasted
80 (warm) medium was extracted (effluent flow), in such a way that the volume
81 of the culture did not change during the experiment. The heat flow through
82 both aluminum pipes warmed the fresh medium (from 18 up to 22°C, approx-
83 imately) prior to its entrance to the fermenter (Fig. 2B); and, reciprocally,
84 cooled the waste warm (temperature at the TEHE input, around 30°C) down
85 to around 25 °C, approximately. As a result, a rather stable voltage of 1-1,3
86 V was recorded (Fig. 2C). In order for the TEHE to produce the maximum
87 electric power, a load resistance of 120 Ω was coupled to the terminals of the
88 thermogenerators, yielding 10-12 mW. When the feed and effluent flows were
89 halted and the TEHE was not used, the temperature of the broth started
90 rising immediately, peaked at 42 °C, and then started to drop (Fig. 2A).

91

92 The thermal behavior of the two main components of the system (the
93 fermenter and the TEHE) was experimentally characterized and mathemat-
94 ically modeled. Following a simplified experimental set up where no fresh
95 medium ($Q=0$) nor cells ($Pc=0$) were introduced in the fermenter, an iden-
96 tification assay was performed to estimate Rg and mc_p , obtaining values of
97 5,92 K/W and 146,547 kJ/K, respectively. The UA constant was estimated
98 also estimated as explained in the Materials and Methods section, yielding a
99 value of 1,039 W/K.

100

101 The evolution of the yeast culture was studied in a typical experiment
102 where optical density (OD) at 600 nm was periodically measured. As shown
103 in Fig. 3, yeast population and temperature during the first part of the ex-
104 periment exhibited a similar pattern. When the TEHE was connected and
105 temperature was kept constant, the OD₆₀₀ of the broth was relatively stable
106 at around 8, indicating that the number of cells present in the fermenter
107 was maintained stable despite the large flow of broth removal (2,4 L/h on
108 average).

109

110 Taken together, our results prove the ability of this thermoelectric heat
111 exchanger-based system to autonomously regulate the broth temperature and
112 to produce electric power by harvesting metabolic heat.

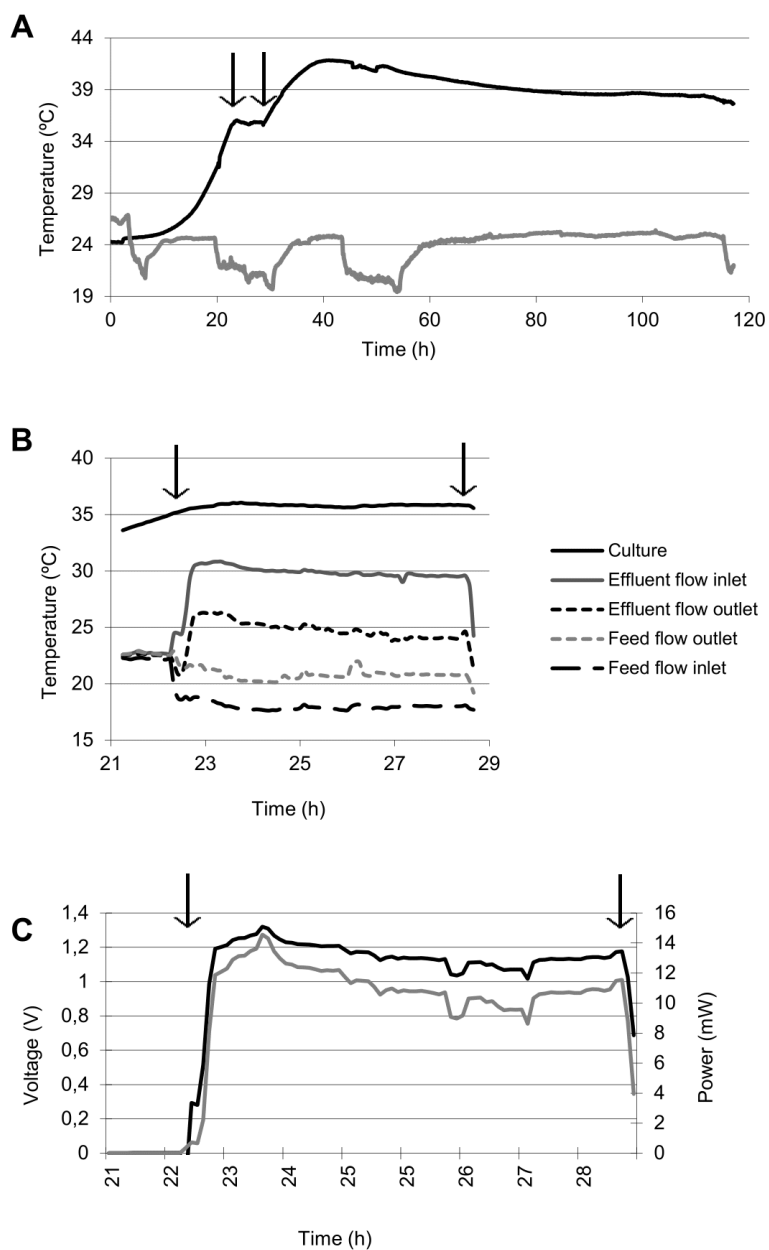


Figure 2: **(A)** Evolution of broth (black line) and room temperatures (grey line) in a typical experiment. Arrows indicate the period of time when the TEHE was connected. **(B)** Changes in the temperature of inlet and outlet flows of the TEHE. **(C)** Voltage (black line) and power (grey line) production in the TEHE.

113 In our prototype, autonomous heating of the culture was achieved and
114 reached values (42 °C) well beyond optimal temperatures for budding yeast.
115 Lower, industrially friendly temperatures could be constantly maintained by
116 means of an automatic equilibrium between the flow of fresh and product-
117 containing media through the TEHE. This resulted in the production of a
118 significant electric power during all the process. In addition, biomass concen-
119 tration proved to be constant when the temperature was controlled. This is
120 of key importance, since industrial bioprocesses require stable temperatures
121 in order to maintain a constant output of a given product [10].
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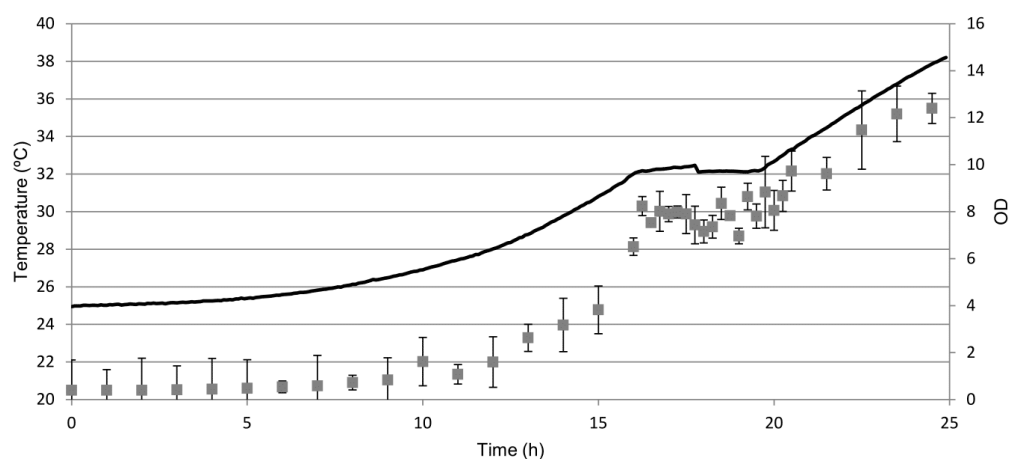


Figure 3: Evolution of broth temperature (black line) and optical density at 600 nm (grey squares). Arrows indicate the interval of time when the TEHE was connected. Error bars show the standard deviation of three independent measurements.

123 The generation of electric power in heat exchangers through the Peltier-
124 Seebeck effect has been previously reported [11-13]. However, this is, to the
125 best of our knowledge, the first time that a heat exchanger with thermogener-
126 ator ability has been coupled to a bioprocess. The difference of temperatures
127 that can be achieved between both sides of the thermogenerators is obviously
128 limited by the narrow range of temperatures mesophiles can tolerate; and,
129 therefore, the electric power that can be produced is lower than that of other
130 type of industrial processes [14]. Albeit low, TEHE-based power produc-
131 tion proved twice more efficient compared to our previous MTC designed for
132 batch culture. Indeed, a 40-fold increase in electrical power production was

133 obtained in the TEHE compared to MTC, which was 20-fold smaller [8].

134

135 Our results are the first step towards controlling microbial growth towards
136 thermoelectric exchangers producing electric power. Scaling up fermentation
137 volumes would accordingly increase electrical power production, which might
138 allow a at least- partial self-control of the culture based on its temperature,
139 with the TEHE contributing to power the peristaltic pumps that regulate
140 broth renovation rates.

141 References

142 1. Walker GM, Yeast Physiology and Biotechnology, John Wiley & Sons,
143 Hoboken, 1998.

144 2. Goldberg AL. Protein degradation and protection against misfolded
145 or damaged proteins. *Nature* 2003;426:89599.

146 3. Haas AL. Regulating the Regulator: Rsp5 Ubiquitinates the Protea-
147 some. *Mol Cell* 2010;38:62324.

148 4. Amillastre E, Aceves-Lara CA, UribeLarrea JL, Alfenore S. Dynamic
149 model of temperature impact on cell viability and major product formation
150 during fed-batch and continuous ethanolic fermentation in *Saccharomyces*
151 *cerevisiae*. *Bioresour Technol* 2012;117:24250.

152 5. Brettel R, Lamprecht I, Schaarschmidt B. Microcalorimetric investi-
153 gations of the metabolism of yeasts growth in batch and chemostat cultures
154 on ethanol medium. *Appl Microbiol Biotechnol* 1981;11:21215.

155 6. von Stockar U, van der Wielen LAM. Thermodynamics in biochemical
156 engineering. *J Biotechnol* 1997;59:2537.

157 7. Trker M. Development of biocalorimetry as a technique for process
158 monitoring and control in technical scale fermentations. *Thermochim Acta*
159 2004;419:7381 (2004).

160 8. Rodriguez-Barreiro R, Abendroth C, Vilanova C, Moya A. Towards a
161 microbial thermoelectric cell. *PloS One* 2013;8:e56358.

162 9. Mizutani FT, Pessoa FLP, Queiroz EM, Hauan S. Mathematical Pro-
163 gramming Model for Heat-Exchanger Network Synthesis Including Detailed
164 Heat-Exchanger Designs. 1. Shell-and-Tube Heat-Exchanger Design. *Ind*
165 *Eng Chem Res* 2003;42:400918.

166 10. Park BG, Lee WG, Chang YK, Chang HN. Long-term operation of
167 continuous high cell density culture of *Saccharomyces cerevisiae* with mem-

168 brane filtration and on-line cell concentration monitoring. *Bioprocess Eng*
169 1999;21:97100.

170 11. Riffat S, Ma X. Thermoelectrics: a review of present and potential
171 applications. *Appl Therm Eng* 2003;23:91335.

172 12. Bell LE. Cooling, heating, generating power, and recovering waste
173 heat with thermoelectric systems. *Science* 2008;321:1457-61.

174 13. Takahashi K, Kanno T, Sakai A, Tamaki H. Bifunctional thermo-
175 electric tube made of tilted multilayer material as an alternative to standard
176 heat exchangers. *Sci Rep* 2013;3:1501 (2013).

177 14. Weng CC, Huang MJ. A simulation study of automotive waste
178 heat recovery using a thermoelectric power generator. *Int J Therm Sci*
179 2013;71:30209 (2013).

180 **Conflict of interest**

181 The authors declare no conflict of interest.

182 **Acknowledgments**

183 We are very grateful to Julin Heredero, from ICMUV (Institut Cincia
184 Materials Universitat Valncia) for manufacturing the TEHE pipes. This
185 work was funded by the Valoritza i Transfereix program (CPI-13-128) from
186 the University of Valencia. The technology described in this work is sub-
187 jected to industrial protection (Patent Cooperation Treaty reference number:
188 PCT/ES2013/000212). The authors have prepared the patent and the reg-
189 istration in collaboration with the Research Transfer Office (OTRI) of the
190 University of Valencia (contact person, Marta Garces: marta.garces@uv.es).