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# Optimal control of acute myeloid leukaemia

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### Abstract

Acute myeloid leukaemia (AML) is a blood cancer affecting the haematopoietic stem cells of the myeloid cell line. AML is routinely treated with chemotherapy, and so it is of great interest to develop optimal chemotherapy treatment strategies. In this work, we incorporate an immune response into a stem cell model of AML, since we find that previous models lacking an immune response are inappropriate for deriving optimal control strategies. Using optimal control theory, we produce continuous controls and bang-bang controls, corresponding to a range of objectives and parameter choices. Through example calculations, we provide a practical approach to applying optimal control using Pontryagin's maximum principle. In particular, we describe and explore factors that have a profound influence on numerical convergence. We find that the convergence behaviour is sensitive to the method of control updating, the nature of the control, and to the relative weighting of terms in the objective function. All codes we use to implement optimal control are made available.

Key words: Leukaemia; Stem cells; Immune response; Optimal treatment.

# 1 1 Introduction

Acute Myeloid Leukaemia (AML) is a blood cancer that is characterised by 2 haematopoietic stem cells of the myeloid cell line, primarily in the bone marrow, transforming into leukaemic blast cells [21,46]. These blast cells no longer undergo normal differentiation or maturation and stop responding to normal 5 regulators of proliferation [22]; their presence in the bone marrow niche dis-6 rupts normal haematopoiesis [21]. AML has significant mortality rates, with 7 a five-year survival rate of 24.5% [7], and challenges in treatment arise not 8 only in eradication of the leukaemic cells but also prophylaxis and treatment 9 of numerous life threatening complications that arise due to the absence of 10 sufficient healthy blood cells [61]. Multiple interventions are employed in the 11 management and treatment of AML, including: leukapheresis; haematopoi-12 etic stem cell transplants; radiotherapy; chemotherapy and immunotherapy 13 [4, 46, 51].14

Mathematical models are widely used to gain insight into complex biologi-15 cal processes [28,47]. Mathematical models facilitate the development of novel 16 hypotheses, allow us to test assumptions, improve our understanding of bio-17 logical interactions, interpret experimental data and assist in the generating 18 parameter estimates. Furthermore, mathematical models provide a convenient, 19 low-cost mechanism for investigating biological processes and interventions for 20 which experimental data may be scarce, cost-prohibitive or difficult to obtain 21 owing to ethical issues. Mathematical models are routinely used to interro-22 gate a variety of processes relating to cancer research including; incidence; 23 development and metastasis; tumour growth; immune reaction and treatment 24 [12,15,21,30,42,58]. Recently, mathematical models have been used to inves-25 tigate various aspects of AML, including: incidence [40]; pathogenesis [18]; 26

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<sup>27</sup> interactions between cancer and healthy haematopoietic stem cells within the

<sup>28</sup> bone marrow niche [21]; and recurrence following remission [49].

Determining how to apply optimally a treatment such as chemotherapy is of 29 great practical and theoretical interest. Chemotherapy, a common treatment 30 for AML [20], is associated with significant health costs related to the cyto-31 toxicity of chemotherapeutic agents [10,46], but also substantial economic cost 32 [63]. Optimal control theory provides us with tools for determining the optimal 33 way to apply a control to a model such that some desired quantities of interest 34 are minimised or maximised. Optimal control has been applied to a range of 35 medically motivated biological models recently; including vaccination, tumour 36 therapy and drug scheduling [14, 16, 34, 35, 43]. 37

In this work we consider a recent haematopoietic stem cell model of AML [21]. After examining the steady state behaviour associated with this model, we make a biologically appropriate and mathematically convenient modification by incorporating an immune response in the form of a Michaelis-Menten kinetic function. Overall, in this work we pursue two broad aims:

(1) Determine how to apply optimal control to the model, accounting for key
clinical features such as the competition between the negative effects of
the disease and the negative effects of the treatment;

(2) Provide a concise and insightful discussion of the methodology and numerical implementation of optimal control, as we find that much of the
existing literature is opaque with regard to practical implementation.

<sup>49</sup> In addressing these aims, we provide a brief introduction to the theory of <sup>50</sup> optimal control and apply optimal control techniques to the modified model, <sup>51</sup> identifying optimal treatment strategies under a variety of circumstances. This <sup>52</sup> leads us to consider both continuous and discontinuous bang-bang optimal <sup>53</sup> controls. Our work provides a comprehensive discussion of practical issues <sup>54</sup> that can arise when applying optimal control, and we explore key factors that influence numerical convergence when using a forward-backward sweep
algorithm to solve two-point boundary value problems that arise. The codes we
use to implement the algorithms associated with the optimal control solutions
is freely available on GitHub.

In Section 2 we present a haemotopoietic stem cell model of AML [21], and discuss the steady states. In Section 3 the importance of an immune response is outlined, and the model is modified to include such a response. In Section 4, we present discussion and results of optimal control applied to the modified AML model. Finally, concluding remarks are provided in Section 5

# 64 2 Acute myeloid leukaemia model

<sup>65</sup> Crowell, MacLean and Stumpf [21] propose a system of ordinary differential
<sup>66</sup> equations (ODEs) to model AML. Their model can be written as,

$$\frac{\mathrm{d}S}{\mathrm{d}t} = \rho_s S(K_1 - Z_1) - \delta_S S,$$

$$\frac{\mathrm{d}A}{\mathrm{d}t} = \delta_S S + \rho_A A(K_2 - Z_2) - \delta_A A,$$

$$\frac{\mathrm{d}D}{\mathrm{d}t} = \delta_A A - \mu_D D,$$

$$\frac{\mathrm{d}L}{\mathrm{d}t} = \rho_L L(K_2 - Z_2) - \delta_L L,$$

$$\frac{\mathrm{d}T}{\mathrm{d}t} = \delta_L L - \mu_T T.$$
(1)

Here S(t), A(t), D(t), L(t) and T(t) represent haematopoietic stem cells, progenitor cells, terminally differentiated cells of S(t), leukaemia stem cells and fully differentiated leukaemia cells, respectively.  $Z_1(t) = S(t)$  and  $Z_2(t) =$ A(t) + L(t), where A(t) and L(t) are coupled as the proliferating leukaemia population (L(t)) competes with the haematopoietic progenitor cell popu-

lation (A(t)). This competition is motivated in [21] by the hypothesis that 72 leukaemic stem cells and haematopoietic stem cells occupy the same niche 73 within the bone marrow [25,57] and hence compete for resources. This niche 74 interaction has been demonstrated as being crucial to similar haematopoietic 75 and leukaemic cell models of chronic myeloid leukaemia [42]. Throughout this 76 work we present numerical solutions to this model and other related mod-77 els. In all solutions presented the parameters are dimensionless, such that the 78 time scale is arbitrary and cell population sizes within the bone marrow are 79 expressed as a portion of the carrying capacities, such that  $K_1 = K_2 = 1$ . Set-80 ting these carrying capacities to be of equal size is a simplifying assumption 81 in our analysis, though we note that this is not required, and could be relaxed 82 if suitable alternative estimates of the carrying capacities were identified. 83

<sup>84</sup> Crowell, MacLean and Stumpf use numerical solutions of Equation (1) to iden-<sup>85</sup> tify parameter values that lead to particular long time steady state solutions <sup>86</sup> of the model. In this work we will use standard variables to denote time de-<sup>87</sup> pendent quantities, such as S(t), and an overbar to denote long-time steady <sup>88</sup> quantities, such as  $\lim_{t\to\infty} S(t) = \bar{S}$ . The parameters we use are summarised in <sup>89</sup> Table 1, and we note that the model supports three non-trivial steady states:

(1) The *healthy* steady state consists of  $\bar{S}, \bar{A}, \bar{D} > 0$  and  $\bar{L} = \bar{T} = 0$ , such that there is a population of each healthy cell species and no leukaemia is present.

- (2) The *coexisting* steady state requires  $\bar{S}, \bar{A}, \bar{D}, \bar{L}, \bar{T} > 0$  simultaneously. In this work we are interested in modelling the optimal application of an intervention (or control) such as chemotherapy to the system that shifts it from the coexisting steady state towards the healthy steady state.
- <sup>97</sup> (3) The third steady state is *leukaemic*, characterised by  $\bar{S} = \bar{A} = \bar{D} = 0$ <sup>98</sup> and  $\bar{L}, \bar{T} > 0$ , such that only leukaemic cells are present.

<sup>99</sup> The leukaemic steady state is less interesting from an intervention perspective

as it cannot be steered towards the healthy steady state via a control such as
chemotherapy alone; requiring in addition a source of healthy cells.

Parameter description	Value
Proliferation of $S$	$\rho_S = 0.5$
Proliferation of $A$	$\rho_A = 0.43$
Proliferation of $L$	$\rho_L = 0.27$
Differentiation of $S$ into $A$	$\delta_S = 0.14$
Differentiation of $A$ into $D$	$\delta_A = 0.44$
Differentiation of $L$ into $T$	$\delta_L = 0.05$
Migration of $D$ into the blood stream	$\mu_D = 0.275$
Migration of $T$ into the blood stream	$\mu_T = 0.3$
Carrying capacity of the compartment with $S$	$K_1 = 1$
Carrying capacity of the compartment with $A$ and $L$	$K_2 = 1$
Characteristic rate of the immune response	$\alpha=0.015$
Half saturation constant of the immune response	$\gamma=0.01$

102

Table 1: Parameters values used in this work.

Parameter values in Table 1 are used in all numerical solutions presented in this work, unless otherwise indicated. These values match those specified in [21] to produce a healthy steady state, noting that [21] included parameter sweeps over  $\rho_S$ ,  $\rho_A$ ,  $\delta_S$  and  $\delta_A$ , with the exception of  $\delta_L$ . We have set  $\delta_L = 0.05$  to produce the coexisting steady state, although other values for  $\delta_L$  also produce this coexisting steady state.

Schematics showing the key features of the original model, a modified model that incorporates an immune response (Section 3), and the modified model subject to a control (Section 4) are presented in Figure 1. Typical numerical solutions of the original model are presented in Figure 2. All numerical results presented in this study are obtained using a fourth-order Runge-Kutta method [52] with a constant time step of  $\delta t = 0.001$ . We find that this choice is <sup>115</sup> sufficient to produce numerical solutions that are grid-independent. From the <sup>116</sup> numerical results we observe that for the parameter values given in Table 1, <sup>117</sup> provided that initially S(0) > 0 and L(0) > 0, the system will tend towards <sup>118</sup> the coexisting steady state. In Section 3 we modify the model to incorporate <sup>119</sup> an immune response, such that sufficiently small leukaemic populations will <sup>120</sup> decay without intervention.

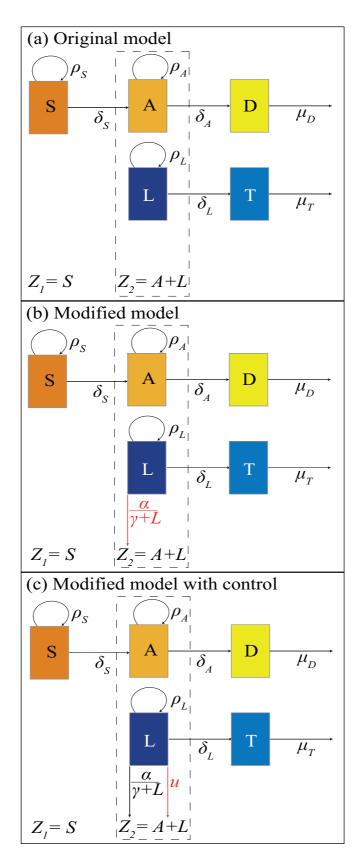


Fig. 1. Schematics present the interactions and associated parameters for the (a) original model [21], (b) modified model with immune response and (c) modified model subject to a control, u. In each schematic the additional response is highlighted in red.

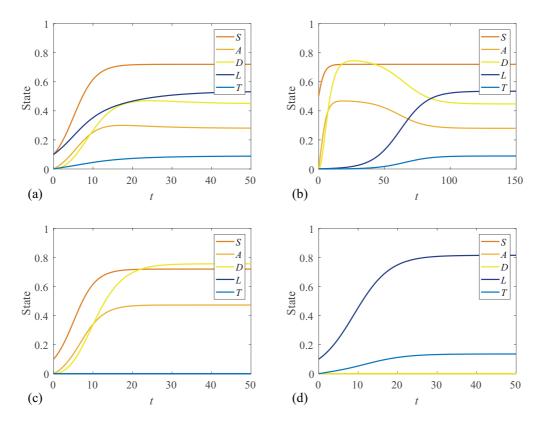


Fig. 2. Numerical solutions of Equations 1 for various initial conditions: (a) Coexisting steady state solution with [S(0), A(0), D(0), L(0), T(0)] = [0.1, 0, 0, 0.1, 0]. (b) Coexisting steady state with  $[0.5, 0, 0, 10^{-3}, 0]$ . (c) Healthy steady state with [0.1, 0, 0, 0, 0]. (d) Leukaemic steady state with [0, 0, 0, 0.1, 0].

In Figure 2b we note that although the initial leukaemia stem cell population is small compared to the initial haematopoietic stem cell population, the system eventually evolves to the same coexisting steady state as in Figure 2a. However, this steady state condition requires a longer timescale to develop from the different initial conditions.

## <sup>126</sup> 3 Incorporating the immune response

The immune system is known to play a critical role in the development, metastasis, treatment and recurrence of cancers [24,26]. This knowledge is supported by a range of clinical evidence, including a well-documented increased risk of cancer incidence in patients with immunodeficiency [17]. This is exemplified by experimental mouse models where mice are typically immunocompromised to avoid transplanted cancers being destroyed by the immune response
in xenograft studies [19]. Furthermore, tumours found in immunocompetent
hosts are observed to exhibit mechanisms for avoiding immune response [45].

The behaviour exhibited in Figure 2b indicates that the system cannot reach 135 a healthy non-leukaemic steady state in the presence of even small leukaemic 136 stem cell populations. It is reasonable to expect that under some circum-137 stances a small leukaemic population may be outcompeted by healthy cells 138 occupying the same niche [41], without intervention. Therefore, we consider a 139 modification to the model proposed by Crowell, MacLean and Stumpf to incor-140 porate an immune response. We expect this immune response to be effective 141 for small L and ineffective for large L, and so we mimic this by introducing a 142 Michaelis-Menten term to represent the immune response, giving, 143

$$\frac{\mathrm{d}S}{\mathrm{d}t} = \rho_s S(K_1 - Z_1) - \delta_S S,$$

$$\frac{\mathrm{d}A}{\mathrm{d}t} = \delta_S S + \rho_A A(K_2 - Z_2) - \delta_A A,$$

$$\frac{\mathrm{d}D}{\mathrm{d}t} = \delta_A A - \mu_D D,$$

$$\frac{\mathrm{d}L}{\mathrm{d}t} = \rho_L L(K_2 - Z_2) - \delta_L L - \underbrace{\frac{\alpha L}{\gamma + L}}_{\text{immune response}},$$

$$\frac{\mathrm{d}T}{\mathrm{d}t} = \delta_L L - \mu_T T.$$
(2)

Including an immune response in the model is not only mathematically convenient in that it provides desirable steady states that we discuss later in this section, but also biologically relevant. Immune responses are widely studied in both the theoretical and experimental biology literature and acknowledged as an important contributor to pathogenesis and tumour dynamics in AML [6,31,60]. Additionally, immunotherapy is being investigated as an alternative to chemotherapy for treatment of AML and many other cancers [9,39,44].

Michaelis-Menten terms are commonly used to incorporate immune responses 151 in other biologically motivated models [2,23,37]. However, it is unclear, simply 152 by inspection, what parameter values are required to obtain two stable steady 153 states: one coexisting and one healthy. For  $\gamma \ll \alpha$  the Michaelis-Menten term 154 behaves as exponential decay at a rate of  $\alpha$ , while for  $\gamma \gg L$  it behaves as a 155 linear sink term [55,56]. Intuitively, we expect setting  $\gamma = \mathcal{O}(L)$  will produce 156 the desired dynamics whereby the immune response is effective for small L157 and ineffective for large L. 158

We investigate further by considering the potential steady states permitted by Equation (2). We note that S is governed by a logistic growth mechanism that does not depend on any of the other species so we have  $\bar{S} = 1 - \delta_S / \rho_S$ . Similarly, D and T do not influence the other populations and hence can be neglected in the consideration of the steady states. Therefore, we consider a reduced system in terms of A, L with  $\bar{S} = 1 - \delta_S / \rho_S$ , recalling that  $Z_2 = A + L$ , and through scaling  $K_2 = 1$ ,

$$\frac{\mathrm{d}A}{\mathrm{d}t} = f(A,L) = \delta_S \left(1 - \frac{\delta_S}{\rho_S}\right) + \rho_A A (1 - A - L) - \delta_A A, \qquad (3)$$

$$\frac{\mathrm{d}L}{\mathrm{d}t} = g(A,L) = \rho_L L(1-A-L) - \delta_L L - \frac{\alpha L}{\gamma + L}.$$
(4)

By inspection, there is a trivial L-nullcline at  $\overline{L} = 0$ . We can find the Anullcline by setting f(A, L) = 0 in Equation (3),

$$\bar{L} = \frac{\delta_S \bar{S}}{\rho_A A} + 1 - A - \frac{\delta_A}{\rho_A}.$$
(5)

Similarly, we can find the non-trivial L-nullcline by setting g(A, L) = 0 in Equation (4),

$$\bar{A} = 1 - L - \frac{\delta_L}{\rho_L} - \frac{\alpha}{\rho_L(\gamma + L)}.$$
(6)

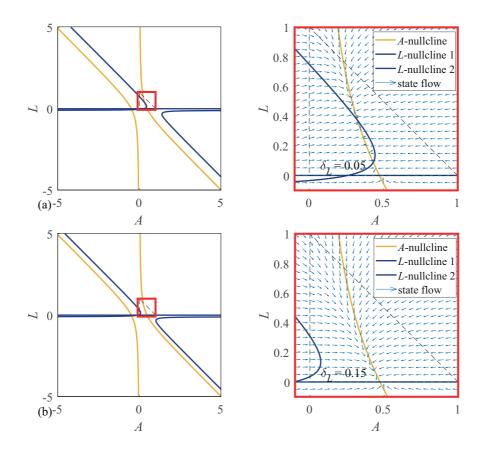


Fig. 3. Nullclines using parameters for (a) a coexistence steady state;  $[\rho_S, \rho_A, \rho_L, \delta_S, \delta_A, \delta_L] = [0.5, 0.43, .027, 0.14, 0.44, 0.05]$ , and (b) the same parameters with application of a control of  $u \equiv 0.1$ , effectively increasing  $\delta_L$  to 0.15 (a control could be a treatment such as chemotherapy that increases the rate of decay of leukaemic stem cells, this is discussed in Section 4). In (a), for particular choices of the introduced parameters  $\alpha$  and  $\gamma$  it is possible for the hyperbolas to intersect twice within the physically realistic region (dashed triangle). These figures are produced with  $\alpha = 0.015$ ,  $\gamma = 0.1$ .

- <sup>170</sup> The nullclines, given by Equations (5) and (6), are hyperbolas. In Figure 3
- <sup>171</sup> we present phase planes showing dynamics of the A and L populations within
- the physically meaningful region,  $A + L \leq 1$ .

This system has the desired property that we outlined previously, namely that there is a stable steady state of coexistence that we aim to steer to the stable state with no leukaemia through applying optimal control. Numerical solutions of the modified model with no control are presented in Figure 4.

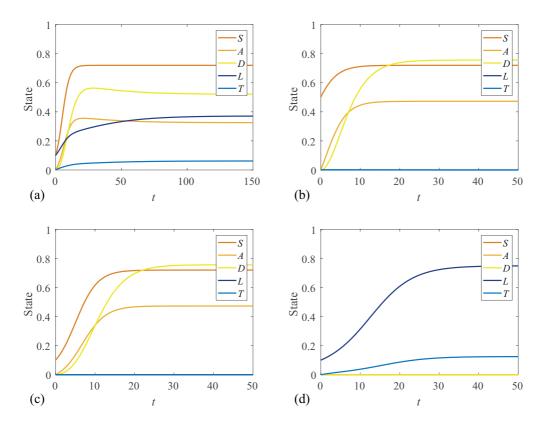


Fig. 4. Numerical solutions to the modified model with an immune response for initial conditions corresponding to Figure 2. In (a) we observe coexistence, though it takes longer for the solutions to approach steady state when compared with the original model (Figure 2a). This result is presented over a larger time-scale. With the introduction of the Michaelis-Menten style immune response to leukaemia, we observe in (b) that a small leukaemia stem cell population does not survive in the presence of a haematopoietic stem cell population. This is in contrast to Figure 2b, where a minute population of leukaemic stem cells was sufficient to grow to a coexisting steady state. These figures are produced with immune response parameters  $\alpha = 0.015$ ,  $\gamma = 0.1$ .

### 177 4 Results and discussion

In this section we provide a concise overview of the theory of optimal control. Methods for solving optimal control problems are discussed. We determine optimal controls to the model presented in Section 3. Specifically, we consider continuous optimal controls corresponding to quadratic pay-off functions and discontinuous bang-bang optimal controls corresponding to linear pay-off functions. Numerical solutions are produced for several different pay-off weighting parameter combinations.

### 185 4.1 Optimal control theory

The basic principle of optimal control is to apply an external force, the *control*, 186 to a system of differential equations, the *state equations*, to cause the solution, 187 the *state*, to follow a new trajectory and/or arrive at a different final state. 188 The goal of optimal control is to select a particular control that maximises or 189 minimises a chosen objective functional, the *pay-off*; typically a function of the 190 state and the control. The pay-off is chosen such that the new trajectory/final 191 state are preferred to that of the uncontrolled state, accounting for any cost 192 associated with applying the control. 193

<sup>194</sup> A typical optimal control problem will introduce the state equations as func-<sup>195</sup> tions of the state  $\mathbf{x}(t)$  and the control u(t), with initial state  $\mathbf{x}(0) = \mathbf{x_0}$ ,

$$\frac{\mathrm{d}\mathbf{x}}{\mathrm{d}t} = f(t, \mathbf{x}(t), u(t)), \quad \mathbf{x}(t) \in \mathbb{R}^n.$$
(7)

It is also necessary to specify either a final time  $t_f$  with the final state free, or a final state  $\mathbf{x}(t_f)$ , with the final time free.

<sup>198</sup> A pay-off function J is defined as a function of the final state,  $\mathbf{x}(t_f)$ , and a

<sup>199</sup> cost function  $\mathcal{L}(t, \mathbf{x}(t), u(t))$  integrated from initial time  $(t_0)$  to final time  $(t_f)$ . <sup>200</sup> Through choosing an optimal control  $u^*(t)$  and solving for the corresponding <sup>201</sup> optimal state  $\mathbf{x}^*(t)$ , we seek to maximise or minimise this objective function. <sup>202</sup> Selecting the pay-off enables us to incorporate the context of our application <sup>203</sup> and determine the meaning of *optimality*. In general, the pay-off function can <sup>204</sup> be written as,

$$J = \boldsymbol{\phi}(\mathbf{x}(t_f)) + \int_{t_0}^{t_f} \mathcal{L}(t, \mathbf{x}(t), u(t)) \, \mathrm{d}t.$$
(8)

<sup>205</sup> Depending on the form of  $\phi$ , it may be possible to incorporate  $\phi$  into  $\mathcal{L}$  by <sup>206</sup> restating the final state constraint in terms of an integral expression using <sup>207</sup> the Fundamental Theorem of Calculus, and noting that  $\phi(\mathbf{x}(t_0))$  is constant <sup>208</sup> and hence does not impact the optimal control. The resulting unconstrained <sup>209</sup> optimal control problem is often more straightforward to solve than the con-<sup>210</sup> strained problem.

The optimal control can be found by solving necessary conditions obtained 211 through application of Pontryagin's Maximum Principle (PMP) [50], or a nec-212 essary and sufficient condition by forming and solving the Hamilton-Jacobi-213 Bellman partial differential equation; a dynamic programming approach [8]. In 214 this work we use the PMP and we construct the Hamiltonian,  $H(t, \mathbf{x}, u, \boldsymbol{\lambda}) =$ 215  $\mathcal{L}(t, \mathbf{x}, u) + \boldsymbol{\lambda} f$ , where  $\boldsymbol{\lambda} = [\lambda_1(t), \lambda_2(t), ..., \lambda_n(t)]$  are the adjoint variables for 216 an *n*-dimensional state. The adjoint is analogous to Lagrange multipliers for 217 unconstrained optimisation problems. Through the Hamiltonian, the adjoint 218 allows us to link our state to our pay-off function. The necessary conditions 219 can be expressed in terms of the Hamiltonian, 220

(1) The optimality condition is obtained by minimising the Hamiltonian,  

$$\frac{\partial H}{\partial u} = 0 \text{ gives } \left(\frac{\partial \mathcal{L}}{\partial u} + \lambda \frac{\partial f}{\partial u}\right) = 0, \qquad (9)$$

 $_{223}$  (2) the adjoint, also referred to as *co-state*, is found by setting,

224

$$\frac{\partial H}{\partial \mathbf{x}} = -\frac{\mathrm{d}\boldsymbol{\lambda}}{\mathrm{d}t}, \text{ giving } \frac{\mathrm{d}\boldsymbol{\lambda}}{\mathrm{d}t} = -\left(\frac{\partial \mathcal{L}}{\partial \mathbf{x}} + \boldsymbol{\lambda}\frac{\partial f}{\partial \mathbf{x}}\right), \text{ and}$$
(10)

226 (3) satisfying the transversality condition,

$$\boldsymbol{\lambda}(t_f) = \frac{\partial \boldsymbol{\phi}}{\partial \mathbf{x}} \Big|_{t=t_f}.$$
(11)

# 227 4.2 Continuous optimal control

In this section we consider optimal control applied to the AML model pre-228 sented in Section 3. From this point we omit the implied time dependence of 229 all control, state and co-state variables for notational convenience. Consider 230 the steady states we observed for the coexistent parameter values of model 231 1. Suppose we wish to apply an optimal control that steers the system from 232 a steady state observed in Figure 4a towards a healthy steady state (Figure 233 4b). This could be achieved by applying a drug u(t), the dosage of which may 234 vary over time, that kills leukaemic stem cells, 235

$$\frac{dS}{dt} = \rho_S S(K_1 - Z_1) - \delta_S S,$$

$$\frac{dA}{dt} = \delta_S S + \rho_A A(K_2 - Z_2) - \delta_A A,$$

$$\frac{dD}{dt} = \delta_A A - \mu_D D,$$

$$\frac{dL}{dt} = \rho_L L(K_2 - Z_2) - \delta_L L - \frac{\alpha L}{\gamma + L} - uL,$$

$$\frac{dT}{dt} = \delta_L L - \mu_T T.$$
(12)

<sup>236</sup> A potential pay-off function for this optimal control problem is to minimise,

$$J = \int_0^{t_f} \left( a_1 u^2 + a_2 L^2 \right) \, \mathrm{d}t, \tag{13}$$

where the control problem is assumed to start at time zero and run until a 237 fixed end time of  $t_f$ . In defining a pay-off function there is significant scope 238 for flexibility, and what constitutes an appropriate choice depends on the 239 application. The parameters  $a_1 > 0$  and  $a_2 > 0$  are chosen to weight the 240 importance of each term in the pay-off, and can be adjusted to best suit a 241 particular application. Through scaling it can be seen that for this example 242 only the relative weighting  $(a_1/a_2)$  is important, however we specify  $a_1$  and  $a_2$ 243 separately for clarity. 244

Quadratic pay-off functions have several desirable mathematical properties 245 that increase the ease of finding optimal solutions; they are smooth and have 246 only a single extremum. Furthermore, Quadratic pay-off functions help to 247 avoid non-physical controls that may otherwise be found. For example; if the 248 pay-off was a cubic function of u, setting u to be large and negative may min-249 imise the pay-off but be physically unrealisable. Quadratic pay-off functions 250 also have some desirable physical properties; a quadratic term will apply a 251 harsher penalty to large amounts of control than small amounts [5], which in 252 many treatments, such as chemotherapy, is desirable [29]. In control engineer-253 ing applications, the control, u, is thought to be proportional to a voltage or 254 current, in which case a quadratic pay-off has a convenient interpretation, as 255  $u^2$  is proportional to power, and the integral of this power over an interval is 256 proportional to the energy expended [5]. Pay-off functions that are quadratic 257 in the control variable are used in many biological [38,53] and engineering 258 applications [3,48]. 259

We can construct the Hamiltonian as  $H = \mathcal{L} + \lambda f$ ; where f is the right hand side of Equation (12),  $\lambda = [\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5]$ , and from Equation (13), we have 262  $\mathcal{L} = a_1 u^2 + a_2 L^2$ , giving,

$$H = a_{2}L^{2} + a_{1}u^{2} + \lambda_{1}[\rho_{S}S(1 - S) - \delta_{S}S] + \lambda_{2}[\delta_{S}S + \rho_{A}A(1 - A - L) - \delta_{A}A] + \lambda_{3}(\delta_{A}A - \mu_{D}D) + \lambda_{4}[\rho_{L}L(1 - A - L) - \delta_{L}L - \alpha L/(\gamma + L) - uL] + \lambda_{5}(\delta_{L}L - \mu_{T}T).$$
(14)

From Equation (9), we find the optimal control by setting  $\partial H/\partial u = 0$ , giving  $u^* = \lambda_4 L/2a_1$ . Following Equation (10), the co-state equations for  $\lambda$  are found by setting  $d\lambda/dt = -\partial H/\partial x$ ,

$$\frac{d\lambda_{1}}{dt} = 2S\lambda_{1}\rho_{S} + \delta_{S}\lambda_{1} - \delta_{S}\lambda_{2} - \lambda_{1}\rho_{S},$$

$$\frac{d\lambda_{2}}{dt} = 2A\lambda_{2}\rho_{A} + L\lambda_{2}\rho_{A} + L\lambda_{4}\rho_{L} + \delta_{A}\lambda_{2} - \lambda_{2}\rho_{A},$$

$$\frac{d\lambda_{3}}{dt} = \mu_{D}\lambda_{3},$$

$$\frac{d\lambda_{4}}{dt} = -2a_{2}L + \rho_{A}A\lambda_{2} + \lambda_{4}\rho_{L}A + 2\rho_{L}L\lambda_{4} - \lambda_{4}\rho_{L},$$

$$+ \lambda_{4}\delta_{L} + \frac{\alpha\gamma\lambda_{4}}{(\gamma + L)^{2}} + \lambda_{4}u - \gamma_{L}\lambda_{5},$$

$$\frac{d\lambda_{5}}{dt} = \mu_{T}\lambda_{5}.$$
(15)

The transversality condition, Equation (11), gives final time conditions on the co-state, Equation (15);  $\lambda(t_f) = [0, 0, 0, 0, 0]$ . Assuming that the initial state is known; [S(0), A(0), D(0), L(0), T(0)], it is now possible to determine the optimal control and corresponding state and co-state through solving a two-point boundary value problem (BVP).

<sup>271</sup> We solve Equation (2) numerically to reach the stable coexistence steady state

of the uncontrolled model. These steady state values in the absence of the control are used as the initial state conditions to solve the BVP to find the optimal control solution. The initial condition for the optimal control problem is [S(0), A(0), D(0), L(0), T(0)] = [0.7200, 0.3255, 0.5207, 0.3715, 0.0619].Initialising the optimal control solution from the uncontrolled steady state is not necessary, however it helps to illustrate the role of the control.

There are a range analytical methods available for solving some forms of BVP 278 under certain restrictions conditions [1,62]. However, in this work we focus on 279 numerical solutions with a view to identifying and discussing typical issues 280 that may arise in implementation. Common numerical solution techniques 281 include shooting and forward backward sweep methods (FBSM) [27,36]. The 282 most effective numerical method depends on the particular BVP. The single 283 shooting method is relatively straightforward, but can be sensitive to the initial 284 guess of the co-state. Forming a suitable guess for the initial values of the co-285 state is challenging, as the co-state does not have a straightforward physical 286 interpretation. Although the FBSM calls for an initial guess for the control 287 over the entire interval, this can often be straightforward to determine, as we 288 will demonstrate. 289

We apply the FBSM using an initial guess for the control,  $u(t) \equiv 0$ , to solve for the state variables forward in time. The co-state is then solved backward in time. In each case a fixed step fourth order Runge-Kutta method is applied to solve the relevant system of ODEs. Using these solutions, the control is updated and the process is repeated until convergence is achieved. The algorithm for the forward-backward sweep method is given in Algorithm 1.

# Algorithm 1: Forward-backward sweep

- i. Make an initial guess of u(t).
  Typically u(t) ≡ 0 is sufficient, though a more thoughtful choice may result in fewer iterations required for convergence.
- ii. Using the initial condition  $\mathbf{x}(0) = \mathbf{x}_0$ , solve for  $\mathbf{x}(t)$  forward in time using the initial guess of u(t).
- iii. Using the transversality condition  $\lambda(t_f)$ , solve for  $\lambda(t)$  backwards in time, using the values for u(t) and  $\mathbf{x}(t)$ .
- iv. Calculate  $u_{\text{new}}(t)$  by evaluating the expression for the optimal control  $u^*(t)$  using the updated  $\mathbf{x}(t)$  and  $\boldsymbol{\lambda}(t)$  values.
- v. Update u(t) based on a combination of  $u_{\text{new}}(t)$  and the previous u(t). For continuous controls applied to relatively simple systems, it may be possible to use  $u_{new}(t)$  directly  $(u(t) = u_{\text{new}}(t))$ , however this is not sufficient to achieve convergence in general. We discuss this further in Section 4.4.
- vi. Check for convergence.

If  $\mathbf{x}(t)$ ,  $\boldsymbol{\lambda}(t)$  and u(t) are within a specified absolute or relative tolerance of the previous iteration, accept  $\mathbf{x}(t)$ ,  $\boldsymbol{\lambda}(t)$  and u(t) as having converged, otherwise return to Step ii. and repeat the process using the updated u(t).

Solutions are provided in Figure 5 for various weighting on the control param-296 eters. As expected, when  $a_1 > a_2$ , placing a greater weighting on the negative 297 impact of the control than the negative impact of the leukaemic stem cells we 298 observe that the control is applied at a lower level than when  $a_1 < a_2$ . When 299 the pay-off weightings are equal, as shown in Figure 5b, the continuous control 300 is applied at an amount similar to the level of the leukaemic stem cell popula-301 tion. Similarly, when the amount of control applied is larger, we observe that 302 the leukaemic stem cell population declines at a faster rate. With  $a_1 > a_2$ , as 303 in Figure 5c, we observe that the leukaemic population is effectively eradicated 304

by  $t_f$ , whereas when  $a_1 < a_2$  we see, in Figure 5d, that a leukaemic population 305 remains at  $t_f$ . A limitation of specifying a fixed final time, as opposed to a 306 fixed final state, is that the optimal outcome is dependent on the specified final 307 time, and there is no consideration for what may happen after  $t_f$ . In many 308 applications, the notion of what happens beyond the control interval is not of 309 interest, though in some instances specifying a final state may be more sensi-310 ble. In this work we consider fixed final time problems for ease of comparison 311 between controls under different parameter regimes, though we acknowledge 312 that specifying a final state, such as no leukaemic stem cells, may be more 313 biologically appropriate. 314

For each of the optimal controls presented in Figure 5, we include an estimate 315 of J, calculated by evaluating Equation (13) with the trapezoid rule. It is 316 critical to note that these pay-offs should not be directly compared with each 317 another. This kind of comparison would be meaningless as each result corre-318 sponds to different choices of  $a_1$  and  $a_2$ , and these values explicitly contribute 319 to J. For example; suppose an optimal control with pay-off weightings  $a_1$  and 320  $a_2$  is computed to have a pay-off of  $J_1$ . Recomputing the optimal control with 321 weightings  $2a_1$  and  $2a_2$  would produce a near identical optimal control and 322 corresponding state, with slight deviation due to floating-point error. However, 323 the corresponding pay-off  $J_2$  would be twice as large. 324

No pay-off is calculated for the uncontrolled steady state solution (Figure 5a) 325 as the choice of  $a_1$  and  $a_2$  would be arbitrary. In this sense, computed pay-offs 326 are not useful for comparing the outcome of treatment versus no treatment as 327 there is no meaningful pay-off associated with no treatment. Rather, computed 328 pay-offs can be used for comparison with other controls applied to a system 329 with identical parameters to check whether or not they are comparable in 330 outcome to the optimal control, noting that the response of the state will also 331 change if the control changes. 332

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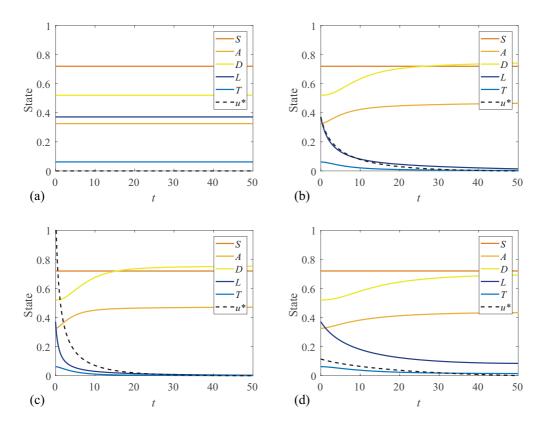


Fig. 5. Application of a continuous optimal control (black dashed line) for various pay-off weightings  $a_1$  and  $a_2$ . The corresponding pay-off, J, is also given. (a) Coexisting steady state solution with no control applied. (b) Equal weighting  $[a_1, a_2] = [1, 1], J = 0.7167$ . (c) Leukaemia weighted more heavily  $[a_1, a_2] = [0.1, 1], J = 0.2288$ . (d) Control weighted more heavily  $[a_1, a_2] = [1, 0.1], J = 0.2262$ . These figures are produced with immune response parameters  $\alpha = 0.015, \gamma = 0.1$ .

#### 333 4.3 Bang-bang optimal control

In addition to considering continuous controls, it is also relevant to con-334 sider discontinuous bang-bang controls as this kind of on-off control could 335 be thought to be more clinically relevant than a continuous setting. Bang-336 bang control problems require a specified bound on the control variable. A 337 bang-bang optimal control takes the value of either the upper or lower bound 338 with finitely many switching points over an interval. As a starting point we 339 re-consider Equation (12) and note that a control will be either bang-bang op-340 timal or singular if the pay-off function is linear in the control term. A pay-off 341 that should produce a bang-bang or singular optimal control of Equation (12) 342 is to minimise 343

$$J = \int_0^{t_f} (a_1 u + a_2 L) \, \mathrm{d}t, \tag{16}$$

subject to  $b_1 \leq u \leq b_2$ . We can construct the Hamiltonian as  $H = \mathcal{L} + \lambda f$ , where  $\mathcal{L}$  is the integrand of Equation (16),  $\lambda = [\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5]$  and f is the right hand side of Equation (12), giving

$$H = a_2 L + a_1 u + \lambda_1 [\rho_S S(1 - S) - \delta_S S]$$
  
+  $\lambda_2 [\delta_S S + \rho_A A(1 - A - L) - \delta_A A]$   
+  $\lambda_3 (\delta_A A - \mu_D D)$   
+  $\lambda_4 [\rho_L L(1 - A - L) - \delta_L L - \alpha L/(\gamma + L) - uL]$   
+  $\lambda_5 (L\delta_L - T\mu_T).$  (17)

As for the continuous control case, we differentiate the Hamiltonian with respect to our control variable u. With a linear pay-off, however, the result no longer contains u. Rather than solving for u, we define a switching function,  $\psi(t)$ , given by

$$\psi(t) = \frac{\partial H}{\partial u} = -\lambda_4(t)L(t) + a_1.$$
(18)

From PMP [50], it is implied that the Hamiltonian will be minimised under the following conditions,

$$u^{*}(t) = \begin{cases} b_{1}, & \text{if } \psi(t) > 0, \\ b_{2}, & \text{if } \psi(t) < 0. \end{cases}$$
(19)

Conditions in Equation (19) produce a bang-bang control. Here, the control 353 variable takes a value of either its upper or lower bound. Notably, Equation 354 (19) omits the case where  $\psi(t) = 0$ , as a bang-bang optimal control requires 355 that  $\psi(t) = 0$  only at discrete points, if at all [13]. If  $\psi(t) = 0$  for any finite 356 interval aside from isolated points, the control is singular. Singular controls are 357 most commonly encountered in cases where the Hamiltonian is linear in the 358 control variable but non-linear in some state variables [11]. When  $\psi(t) = 0$  over 359 an interval, the Hamiltonian is not a function of the control, so the state and 360 co-state variables no longer determine the control [11]; over this interval the 361 control is determined by requiring  $\partial H/\partial u = 0$ . Our control problem defined by 362 Equation (12) and Equation (16) is not singular, so we do not discuss singular 363 controls further. 364

<sup>365</sup> Our co-state equations for  $\lambda$  are found as  $\partial H/\partial f = -d\lambda/dt$ . The co-state in

<sup>366</sup> the bang-bang control problem is given by,

$$\frac{d\lambda_{1}}{dt} = 2S\lambda_{1}\rho_{S} + \delta_{S}\lambda_{1} - \delta_{S}\lambda_{2} - \lambda_{1}\rho_{S},$$

$$\frac{d\lambda_{2}}{dt} = 2A\lambda_{2}\rho_{A} + L\lambda_{2}\rho_{A} + L\lambda_{4}\rho_{L} + \delta_{A}\lambda_{2} - \lambda_{2}\rho_{A},$$

$$\frac{d\lambda_{3}}{dt} = \mu_{D}\lambda_{3},$$

$$\frac{d\lambda_{4}}{dt} = -a_{2} + \rho_{A}A\lambda_{2} + \lambda_{4}\rho_{L}A + 2\rho_{L}L\lambda_{4} - \lambda_{4}\rho_{L}$$

$$+ \lambda_{4}\delta_{L} + \frac{\alpha\gamma\lambda_{4}}{(\gamma + L)^{2}} + \lambda_{4}u - \gamma_{L}\lambda_{5},$$

$$\frac{d\lambda_{5}}{dt} = \mu_{T}\lambda_{5},$$
(20)

and we note that Equation 20 is subtly different to Equation 15, as the first term of the fourth line of Equation (20) is the constant  $-a_2$ , and no longer depends on L.

The transversality condition, Equation (11), gives the final time conditions 370 on the co-state,  $[\lambda_1(t_f), \lambda_2(t_f), \lambda_3(t_f), \lambda_4(t_f), \lambda_5(t_f)] = [0, 0, 0, 0, 0]$ . Assuming 371 again that the initial state is known; [S(0), A(0), D(0), L(0), T(0)], it is now 372 possible to determine the optimal bang-bang control and corresponding opti-373 mal state and co-state through solving a two-point BVP that we solve using 374 the FBSM, as in the continuous control case. It is not necessary to modify 375 the FBSM algorithm to find bang-bang optimal controls, though care must 376 be taken in how the control is updated between iterations. This is discussed 377 further in Section 4.4. Depending on the numerical scheme used to integrate 378 the state and co-state equations through time, the discontinuous nature of 379 the bang-bang control may require careful handling. Solutions are provided in 380 Figure 6 for various weighting on the control parameters. In the continuous 381 control case, when  $a_1 > a_2$ , placing a greater weighting on the negative im-382 pact of the control than the negative impact of the leukaemic stem cells; we 383 observed that the control is applied at a lower level than when  $a_1 < a_2$ . The 384 optimal bang-bang control must take either the upper or lower bound of the 385

specified range. As such, in the bang-bang control case the pay-off weighting parameters determine not the level at which the control is applied, but rather the times at which the control switches from one bound to the other, hence the name *switching function* given to Equation (19).

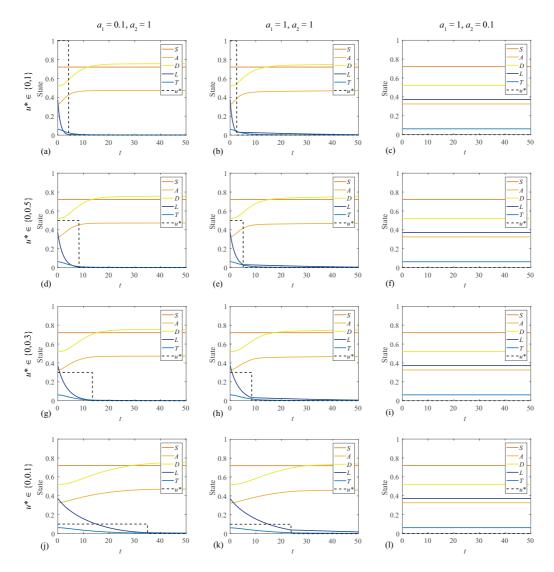


Fig. 6. Bang-bang control solutions for various weightings on control and leukaemia in the pay-off ( $a_1$  and  $a_2$  respectively), with different control upper bounds. These figures are produced with immune response parameters  $\alpha = 0.015$ ,  $\gamma = 0.1$ .

In Figure 6 it is clear that when the upper bound on the control is higher, meaning in this context the maximum amount of chemotherapy that can be applied at any given time is higher, the control switches to the lower bound earlier. In this case the lower bound corresponds to u = 0, or no chemotherapy

being applied (control *switched off*), though this is not required of the method. 394 The interaction between the control and state in Equation (20) means that 395 the cumulative amount of control applied is not the same for different bounds 396 on the control. In Figure 5 we demonstrate that for a continuous control with 397  $a_1 = 1, a_2 = 0.1$ , a small amount of control is applied. For the bang-bang case 398 with the same weighting, we observe in the rightmost column of Figure 6 that 399 for a range of control upper bounds, the control is not switched on at all -400 implying that with such a pay-off, it is optimal not to apply the control. One 401 may suppose that for a sufficiently small upper bound that the control would 402 turn on even with this pay-off, however a lower upper bound on the control 403 also reduces the impact the control has on the state. 404

Due to the immune response incorporated in Section 3, a sufficiently small 405 leukaemic population will tend towards extinction rather than grow back to 406 a coexisting steady state. Because of this, we observe in Figure 6 that the 407 control switches off before the leukaemic stem cells are totally eradicated -408 the immune response is sufficient once the leukaemic population is sufficiently 409 low. This is most evident in Figure 6k, where we can see that the population 410 of leukaemic stem cells is declining but has not become extinct by the final 411 time, t = 50. In absence of the immune response incorporated in Section 3, we 412 would observe the leukaemic population increasing as soon as the control is 413 switched off, since the healthy steady state would be unstable; applying fixed 414 final time bang-bang optimal control to the original model produces outcomes 415 that are mathematically optimal but physically undesirable. 416

In our discussion of continuous controls, we note the fixed final time as a limitation, since changing the final time can change the profile of the optimal control and state. In general the same is true of bang-bang controls with fixed final times, though in some instances that we consider the optimal bang-bang control does not change significantly if the final time is changed. For example; the optimal switching times and corresponding optimal states in the leftmost column of Figure 6 do not change significantly if the final time is increased to t = 100, because by t = 50 we see that  $L \approx 0$  and u = 0, so neither contributes significantly to the pay-off in the interval  $50 < t \leq 100$ . For these cases the control is not costly relative to the leukaemia  $(a_1 < a_2)$  so it is applied at the upper bound until the leukaemic stem cell population is virtually eradicated before switching off.

For this particular system, we only obtain bang-bang optimal controls with a 429 single switching time. We are able to verify these bang-bang optimal controls 430 through an exhaustive search of all possible bang-bang controls by specify-431 ing the switching time, directly calculating the pay-off and determining the 432 switching time that minimises the pay-off. For all cases considered in Figure 6 433 the switching time identified via exhaustive search is in agreement. It is also 434 possible that the optimal bang-bang control may switch between the upper 435 and lower bounds numerous times, producing multiple 'bangs'. Bang-bang op-436 timal controls that exhibit multiple bangs can be identified using the FBSM 437 without modification, though it is more difficult to find a convergent bang-438 bang optimal control with multiple bangs. Similarly, without knowing a priori 430 how many switching times to expect, an exhaustive search for multiple bangs 440 is not computationally feasible. 441

# 442 4.4 Convergence and control updating

In this section we examine the convergence behaviour of solutions to the optimal control problems presented in this work. Convergence behaviour of numerical solutions to optimal control problems is influenced by multiple factors. In particular, we discuss the initial guess of the control, convergence criteria, control updating and pay-off weightings. These factors influence not only the number of iterations required to reach a converged numerical solution, but also whether or not a converged solution will be reached at all.

Holding all other factors constant, provided that the initial guess for the con-450 trol is sensible, the initial guess does not have a significant impact on whether 451 or not a converged result is reached for the control problems considered in this 452 work. However, convergence is typically reached with fewer iterations when the 453 initial guess is relatively closer to the true value of the optimal control. For 454 simplicity we use the initial guess  $u \equiv 0$  for all results presented in this work, 455 while acknowledging that more thoughtful choices may deliver convergence in 456 fewer iterations. 457

For optimal control results presented in the previous sections, we determine whether convergence has been achieved after each iteration based on the relative difference between the updated control,  $u_{updated}$ , and the old control,  $u_{old}$ . If this relative difference is sufficiently small, the updated control is accepted as the optimal control. A typical relative difference convergence criterion requires

$$\frac{|u_{\rm updated} - u_{\rm old}|}{|u_{\rm updated}|} \le \varepsilon, \tag{21}$$

where  $0 < \varepsilon \ll 1$  is the desired relative tolerance. Following [36], we adjust Equation (21) to allow for a control of the form  $u \equiv 0$ , giving

$$\varepsilon \sum_{i=1}^{n} |u_{\text{updated}}(i\Delta t)| - \sum_{i=1}^{n} |u_{\text{updated}}(i\Delta t) - u_{\text{old}}(i\Delta t)| \ge 0, \quad (22)$$

where  $t = i\Delta t$ ,  $\Delta t$  is the numerical time step and n is the number of nodes 466 in the time discretisation. The absolute value is taken to ensure that positive 467 differences are not offset by negative differences that could otherwise result 468 in incorrectly detecting convergence. The choice of convergence criterion and 469 acceptable tolerance depends on the particular problem at hand, and may 470 need to be adjusted to be appropriate for another control problem. In some 471 instances, it may be necessary to check convergence of the state and co-state 472 as well as the control, particularly if the state response to control is sensitive. 473

For the control problems studied in this work, we find that state and costate respond predictably to the control, and convergence of the control is accompanied by convergence of that state and co-state. As such we do not explicitly check for convergence of the state and co-state.

In each iteration of the FBSM we recalculate the control,  $u_{\text{new}}$ , based on the 478 newly calculated state and co-state solutions and associated optimality cri-470 terion, as discussed in Section 4.2 for the continuous control and Section 4.3 480 for the bang-bang control. Typically,  $u_{new}$  is not used directly as the control 481 for the next iteration of the FBSM, but rather we form an updated control 482  $u_{\rm updated}$  as a weighted combination of  $u_{\rm new}$  and the control from the previ-483 ous iteration,  $u_{old}$ . The motivation for this is two-fold; first, an appropriately 484 weighted control updating scheme can speed up convergence; and second, for 485 many optimal control problems, a direct update of  $u_{updated} = u_{new}$  will fail 486 to produce converging results at all. A common approach is to update the 487 control based on a convex combination, such that the total weightings sum to 488 one, of the new and previous control(s). In this work we use a constant linear 489 weighting, with  $0 < \omega < 1$ , giving 490

$$u_{\text{updated}} = \omega u_{\text{old}} + (1 - \omega) u_{\text{new}}.$$
(23)

We find that the best choice for  $\omega$  depends not only on the form of the control, 491 continuous or bang-bang, but also on model parameters such as the pay-off 492 weightings. There is a trade-off between the number of iterations required to 493 obtain convergence, and actually converging at all; a larger  $\omega$  typically is more 494 likely to produce converging solutions, but this also means that the control 495 changes less each iteration, so more iterations are required. For example, a 496 weighting of  $\omega = 0.7$  was sufficiently large that all continuous control solutions 497 presented in Figure 5 converged to a relative tolerance of  $\varepsilon = 1 \times 10^{-3}$ . For 498  $\omega = 0.6$  only Figure 5d converges, and for  $\omega = 0.8$ , all solutions in Figure 5 499

converge but require more iterations than when  $\omega = 0.7$ .

<sup>501</sup> Convergence in the bang-bang control case typically requires larger  $\omega$  and more <sup>502</sup> iterations than the continuous controls. In the rightmost column of Figure <sup>503</sup> 6, there is no concept of convergence as the control never switches on. Only <sup>504</sup> Figure 6j and Figure 6k converge to a relative tolerance of  $1 \times 10^{-3}$  for  $\omega = 0.7$ , <sup>505</sup> with  $\omega = 0.9$  being sufficient for convergence of all remaining solutions aside <sup>506</sup> from Figure 6b, where we set  $\omega = 0.95$ .

It is clear that the best control updating scheme depends on the particular 507 problem; and a scheme that works well for one problem may not necessarily 508 work at all for another. When solving control problems, it may be necessary 509 to try a range of updating schemes to achieve convergence. In this work we 510 only consider constant weighted updating, though there are more sophisti-511 cated updating schemes that shift the weighting towards  $u_{\text{new}}$  as the number 512 of iterations increase [36]. In Figure 7 we examine the influence of the control 513 update weighting  $\omega$ , and the pay-off weightings,  $a_1$  and  $a_2$ , on the convergence 514 behaviour of the bang-bang control problem studied in Section 4.3. Specifi-515 cally, we consider the case where  $0 \le u \le 0.5$ , and determine that a solution 516 has converged if it meets a relative tolerance of  $\varepsilon = 1 \times 10^{-3}$  within 250 it-517 erations. In each panel of Figure 7 we observe three *regions*: in region I we 518 have no concept of convergence as the control never switches on; in region II 519 we find that the optimal control problem does not converge; and in region III 520 we observe convergence. Not all simulations conform strictly to these regions 521 since the boundary between the different regions is not always sharp and well-522 defined. However, broadly speaking, these three regions capture the essence 523 of the convergence behaviour that we observe. These regions are constructed 524 based on discrete simulations of the problem for  $0 < a_1 \le 10$  and  $0 \le a_2 \le 10$ , 525 each in increments of 0.1. The case where  $a_1 = 0$  is excluded as this corre-526 sponds to no cost associated with applying the control, so there is no sense of 527 convergence. 528

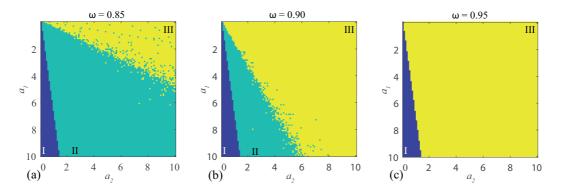


Fig. 7. Convergence behaviour for (a)  $\omega = 0.85$ , (b)  $\omega = 0.9$ , and (c)  $\omega = 0.95$ , with  $a_1$  and  $a_2$  ranging from 0 to 10 in increments of 0.1, excluding  $a_1 = 0$ . In region I (dark blue) we have no concept of convergence as the control never switches on. In region II (light blue) we find that the optimal control problem does not converge, and in region III (yellow) we observe convergence. These figures are produced with immune response parameters  $\alpha = 0.015$ ,  $\gamma = 0.1$ .

From Figure 7 it is clear that convergence is achieved in a larger region of the 529  $(a_1, a_2)$  parameter space when  $\omega$  is increased. However, it is important to note 530 that achieving convergence in this context only implies that Equation (22) is 531 satisfied, and does not necessarily mean that a suitable bang-bang control is 532 obtained. While some controls corresponding to individual simulations in Fig-533 ure 7c are suitable bang-bang controls; a portion are approaching bang-bang 534 but require additional iterations to accurately calculate the control around 535 the switching point. The weighting applied in Equation (23) has the effect 536 of smoothing u during intermediate iterations of the FBSM; this smoothness 537 is gradually reduced as the control converges to the optimal switching point. 538 Since  $\omega$  explicitly influences the relative amount that the control can differ 539 between iterations, if a larger  $\omega$  is required to achieve convergence for a given 540 problem, it may also be necessary to reduce the convergence tolerance  $\varepsilon$  to 541 ensure that the resulting control is sufficiently bang-bang. 542

### 543 5 Conclusion and Outlook

In this work we consider a haematopoietic stem cell model of AML that incor-544 porates competition between leukaemic stem cells and blood progenitor cells 545 within the bone marrow niche. We incorporate a biologically appropriate im-546 mune response in the form of a Michaelis-Menten term. This modification is 547 mathematically convenient because of the impact it has on the steady states, 548 and biologically relevant because the immune response is known to play an 549 important role in cancer progression and treatment. With a view to identify-550 ing the optimal way to apply a treatment such as chemotherapy to the model, 551 we formulate and solve optimal control problems corresponding to multiple of 552 objectives and constraints. This includes quadratic pay-off functions, yielding 553 continuous controls, as well as linear pay-off functions, yielding discontinuous 554 bang-bang controls. 555

We provide a brief overview of optimal control theory, with a focus on the 556 necessary conditions derived from Pontryagin's Maximum Principle. This ap-557 proach formulates the optimal control problem as a coupled multi-species 558 two-point boundary value problem. The resulting optimal control problem 559 is solved numerically using the iterative FBSM. The algorithm for the FBSM 560 is discussed, with a focus on highlighting typical issues that may arise in im-561 plementing optimal control. Suggestions are provided for overcoming these 562 issues. In particular, we focus on factors that influence the convergence of 563 the FBSM; not only in terms of the number of iterations required, but also 564 whether it converges at all. These factors include the initial guess for the 565 control, the convergence criterion, the method of updating the control, the 566 associated weighting placed on controls from prior iterations and parameters 567 such as pay-off weightings, and in the bang-bang control case, the control 568 bounds. 569

<sup>570</sup> For the model we consider; a well informed initial guess for the control may re-

duce the number of iterations required for convergence, but any sensible guess 571 should not prevent convergence. Most critically, we show that the method of 572 updating the control and the associated weight placed on the control from the 573 previous iteration has a significant impact on whether or not convergence will 574 be achieved, as do the weights in the pay-off function. In the bang-bang control 575 case, we observe that increasing the upper bound on the control can prevent 576 convergence, holding all other factors constant; in this case, placing a greater 577 weight on the solution from the previous iteration may produce convergence. 578

There are many potential avenues to extend the ideas explored in this work. 579 Here, we have incorporated the control via a simple mechanism, and more so-580 phisticated pharmacokinetic processes such as drug absorption and metabolism 581 could be incorporated to increase the biological detail captured by the model, 582 but this additional biological detail comes at the cost of increasing the num-583 ber of unknown, and possibly unmeasurable parameters. Therefore, care must 584 be exercised in following up this kind of extension. The control problems pre-585 sented in this work could be reformulated as fixed final state problems, leaving 586 the final time free to vary which could be more clinically relevant than spec-58 ifying the final time. With the introduction of an immune mechanism to the 588 model, it is also possible to consider a control based around immunotherapy. 580

A recent idea of great interest in clinical cancer research is the possibility of 590 introducing an interval of time during treatment in which no chemotherapy is 591 applied. This kind of intervention is reminiscent of a bang-bang control, and 592 is often referred to as a *drug holiday* [59]. There is some evidence to suggest 593 that drug resistance of tumour cells may reduce with time so that patients 594 experience an improve response to chemotherapy following a drug holiday 595 [32,33,54]. This application of a drug in an *on-off* fashion parallels the idea of 596 the bang-bang controls we consider in this work and so it would be interesting 597 to formulate the concept of designing a drug holiday in terms of a bang-bang 598 optimal control problem using the algorithms and concepts developed in this 599

600 work.

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