

Optimal control of acute myeloid leukaemia

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Abstract

Acute myeloid leukaemia (AML) is a blood cancer affecting haematopoietic stem cells. AML is routinely treated with chemotherapy, and so it is of great interest to develop optimal chemotherapy treatment strategies. In this work, we incorporate an immune response into a stem cell model of AML, since we find that previous models lacking an immune response are inappropriate for deriving optimal control strategies. Using optimal control theory, we produce continuous controls and bang-bang controls, corresponding to a range of objectives and parameter choices. Through example calculations, we provide a practical approach to applying optimal control using Pontryagin's Maximum Principle. In particular, we describe and explore factors that have a profound influence on numerical convergence. We find that the convergence behaviour is sensitive to the method of control updating, the nature of the control, and to the relative weighting of terms in the objective function. All codes we use to implement optimal control are made available.

Key words: Leukaemia; Stem cells; Immune response; Optimal treatment.

1 Introduction

2 Acute Myeloid Leukaemia (AML) is a blood cancer that is characterised
3 by haematopoietic stem cells, primarily in the bone marrow, transforming
4 into leukaemic blast cells [22,47]. These blast cells no longer undergo nor-
5 mal differentiation or maturation and stop responding to normal regulators
6 of proliferation [23]; their presence in the bone marrow niche disrupts nor-
7 mal haematopoiesis [22]. AML has significant mortality rates, with a five-year
8 survival rate of 24.5% [8], and challenges in treatment arise not only in eradica-
9 tion of the leukaemic cells but also prophylaxis and treatment of numerous life
10 threatening complications that arise due to the absence of sufficient healthy
11 blood cells [62]. Multiple interventions are employed in the management and
12 treatment of AML, including: leukapheresis; haematopoietic stem cell trans-
13 plants; radiotherapy; chemotherapy and immunotherapy [4,47,52].

14 Mathematical models are widely used to gain insight into complex biologi-
15 cal processes [29,48]. Mathematical models facilitate the development of novel
16 hypotheses, allow us to test assumptions, improve our understanding of bio-
17 logical interactions, interpret experimental data and assist in generating pa-
18 rameter estimates. Furthermore, mathematical models provide a convenient,
19 low-cost mechanism for investigating biological processes and interventions for
20 which experimental data may be scarce, cost-prohibitive or difficult to obtain
21 owing to ethical issues. Mathematical models are routinely used to interro-
22 gate a variety of processes relating to cancer research including: incidence;
23 development and metastasis; tumour growth; immune reaction and treatment
24 [13,16,22,31,43,59]. Recently, mathematical models have been used to inves-
25 tigate various aspects of AML, including: incidence [41]; pathogenesis [19];
26 interactions between cancer and healthy haematopoietic stem cells within the

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27 bone marrow niche [22]; and recurrence following remission [50].

28 Determining how to apply optimally a treatment such as chemotherapy is of
29 great practical and theoretical interest. Chemotherapy, a common treatment
30 for AML [21], is associated with significant health costs related to the cy-
31 totoxicity of chemotherapeutic agents [11,47], but also substantial economic
32 cost [64]. Optimal control theory provides us with tools for determining the
33 optimal way to apply a control to a model such that some desired quantities
34 of interest are minimised or maximised. Further, it facilitates assessment of
35 the efficacy of hypothetical treatment protocols relative to a theoretical op-
36 timal treatment. Optimal control has been applied to a range of medically
37 motivated biological models recently; including vaccination, tumour therapy
38 and drug scheduling [15,17,35,36,44].

39 In this work we consider a recent haematopoietic stem cell model of AML
40 [22]. After examining the steady state behaviour associated with this model,
41 we make a biologically appropriate and mathematically convenient modifica-
42 tion by incorporating an immune response in the form of a Michaelis-Menten
43 kinetic function. Overall, in this work we pursue two broad aims:

- 44 (1) Determine how to apply optimal control to the model, accounting for key
45 clinical features such as the competition between the negative effects of
46 the disease and the negative effects of the treatment;
- 47 (2) Provide a concise and insightful discussion of the methodology and nu-
48 merical implementation of optimal control, as we find that much of the
49 existing literature is opaque with regard to practical implementation.

50 In addressing these aims, we provide a brief introduction to the theory of
51 optimal control and apply optimal control techniques to the modified model,
52 identifying optimal treatment strategies under a variety of circumstances. This
53 leads us to consider both continuous and discontinuous bang-bang optimal
54 controls. Our work provides a comprehensive discussion of practical issues

55 that can arise when applying optimal control, and we explore key factors
56 that influence numerical convergence when using a forward-backward sweep
57 algorithm to solve two-point boundary value problems that arise. The code we
58 use to implement the algorithms associated with the optimal control solutions
59 is freely available on GitHub.

60 In Section 2 we present a haematopoietic stem cell model of AML [22], and
61 discuss the steady states. In Section 3 the importance of an immune response
62 is outlined, and the model is modified to include such a response. In Section
63 4, we present discussion and results of optimal control applied to the modified
64 AML model. Finally, concluding remarks are provided in Section 5. In the
65 supplementary material document we extend the work in this document to
66 consider: (i) arbitrary initial conditions, and; (ii) controls that impact multiple
67 species.

68 **2 Acute myeloid leukaemia model**

69 Crowell, MacLean and Stumpf [22] propose a system of ordinary differential
70 equations (ODEs) to model AML. Their model can be written as,

$$\begin{aligned}\frac{dS}{dt} &= \rho_s S(K_1 - Z_1) - \delta_S S, \\ \frac{dA}{dt} &= \delta_S S + \rho_A A(K_2 - Z_2) - \delta_A A, \\ \frac{dD}{dt} &= \delta_A A - \mu_D D, \\ \frac{dL}{dt} &= \rho_L L(K_2 - Z_2) - \delta_L L, \\ \frac{dT}{dt} &= \delta_L L - \mu_T T.\end{aligned}\tag{1}$$

71 Here $S(t)$, $A(t)$, $D(t)$, $L(t)$ and $T(t)$ represent haematopoietic stem cells, pro-

72 genitor cells, terminally differentiated cells of $S(t)$, leukaemia stem cells and
73 fully differentiated leukaemia cells, respectively. $Z_1(t) = S(t)$ and $Z_2(t) =$
74 $A(t) + L(t)$, where $A(t)$ and $L(t)$ are coupled as the proliferating leukaemia
75 population ($L(t)$) competes with the haematopoietic progenitor cell popu-
76 lation ($A(t)$). This competition is motivated in [22] by the hypothesis that
77 leukaemic stem cells and haematopoietic stem cells occupy the same niche
78 within the bone marrow [26,58] and hence compete for resources. This niche
79 interaction has been demonstrated as being crucial to similar haematopoietic
80 and leukaemic cell models of chronic myeloid leukaemia [43]. Throughout this
81 work we present numerical solutions to this model and other related mod-
82 els. In all solutions presented the parameters are dimensionless, such that the
83 time scale is arbitrary and cell population sizes within the bone marrow are
84 expressed as a portion of the carrying capacities; $K_1 = K_2 = 1$. Setting these
85 carrying capacities to be of equal size is a simplifying assumption in our anal-
86 ysis, though we note that this is not required, and could be relaxed if suitable
87 alternative estimates of the carrying capacities were identified.

88 Crowell, Mac Lean and Stumpf use numerical solutions of Equation (1) to
89 identify parameter values that lead to particular long time steady state solu-
90 tions of the model. In this work we will use standard variables to denote time
91 dependent quantities, such as $S(t)$, and an overbar to denote long-time steady
92 quantities, such as $\lim_{t \rightarrow \infty} S(t) = \bar{S}$. The parameters we use are summarised in
93 Table 1, and we note that the model supports three non-trivial steady states:

- 94 (1) The *coexisting* steady state requires $\bar{S}, \bar{A}, \bar{D}, \bar{L}, \bar{T} > 0$ simultaneously.
95 In this work we are interested in modelling the optimal application of
96 an intervention (or control) such as chemotherapy to the system that
97 shifts it from the coexisting steady state towards the healthy steady state.
98 Examples trajectories resulting in the coexisting steady state are given
99 in Figure 2a and Figure 2b.
- 100 (2) The *healthy* steady state consists of $\bar{S}, \bar{A}, \bar{D} > 0$ and $\bar{L} = \bar{T} = 0$, such

101 that there is a population of each healthy cell species and no leukaemia
 102 is present. The healthy steady state is demonstrated in Figure 2c.
 103 (3) The third steady state is *leukaemic*, characterised by $\bar{S} = \bar{A} = \bar{D} = 0$
 104 and $\bar{L}, \bar{T} > 0$, such that only leukaemic cells are present. The leukaemic
 105 steady state is demonstrated in Figure 2d.

106 The leukaemic steady state is less interesting from an intervention perspective
 107 as it cannot be steered towards the healthy steady state via a control such as
 108 chemotherapy alone; requiring in addition a source of healthy cells.

Table 1: Parameters values used in this work.

Parameter description	Value
Proliferation of S	$\rho_S = 0.5$
Proliferation of A	$\rho_A = 0.43$
Proliferation of L	$\rho_L = 0.27$
Differentiation of S into A	$\delta_S = 0.14$
Differentiation of A into D	$\delta_A = 0.44$
109 Differentiation of L into T	$\delta_L = 0.05$
Migration of D into the blood stream	$\mu_D = 0.275$
Migration of T into the blood stream	$\mu_T = 0.3$
Carrying capacity of the compartment with S	$K_1 = 1$
Carrying capacity of the compartment with A and L	$K_2 = 1$
Characteristic rate of the immune response	$\alpha = 0.015$
Half saturation constant of the immune response	$\gamma = 0.01$

110 Parameter values in Table 1 are used in all numerical solutions presented in this
 111 work, unless otherwise indicated. These values match those specified in [22]
 112 to produce a healthy steady state, noting that [22] included parameter sweeps
 113 over ρ_S, ρ_A, δ_S and δ_A , with the exception of δ_L . We have set $\delta_L = 0.05$ to
 114 produce the coexisting steady state, although other values for δ_L also produce
 115 this coexisting steady state.

116 Schematics showing the key features of the original model, a modified model
117 that incorporates an immune response (Section 3), and the modified model
118 subject to a control (Section 4) are presented in Figure 1. Typical numerical
119 solutions of the original model are presented in Figure 2. All numerical results
120 presented in this study are obtained using a fourth-order Runge-Kutta method
121 [53] with a constant time step of $\delta t = 0.001$. We find that this choice is
122 sufficient to produce numerical solutions that are grid-independent. From the
123 numerical results we observe that for the parameter values given in Table 1,
124 provided that initially $S(0) > 0$ and $L(0) > 0$, the system will tend towards
125 the coexisting steady state. In Section 3 we modify the model to incorporate
126 an immune response, such that sufficiently small leukaemic populations will
127 decay without intervention.

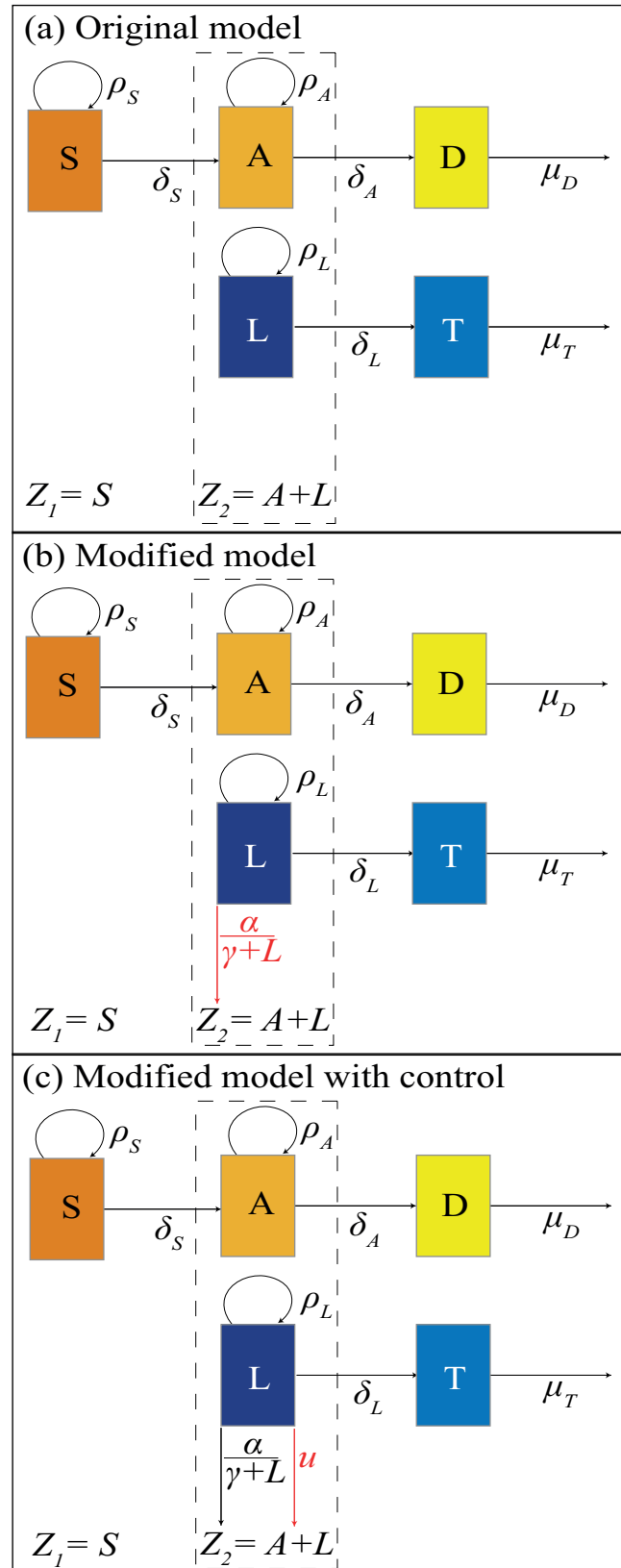


Fig. 1. Schematics present the interactions and associated parameters for the (a) original model [22], (b) modified model with immune response and (c) modified model subject to a control, u . In each schematic the additional response is highlighted in red.

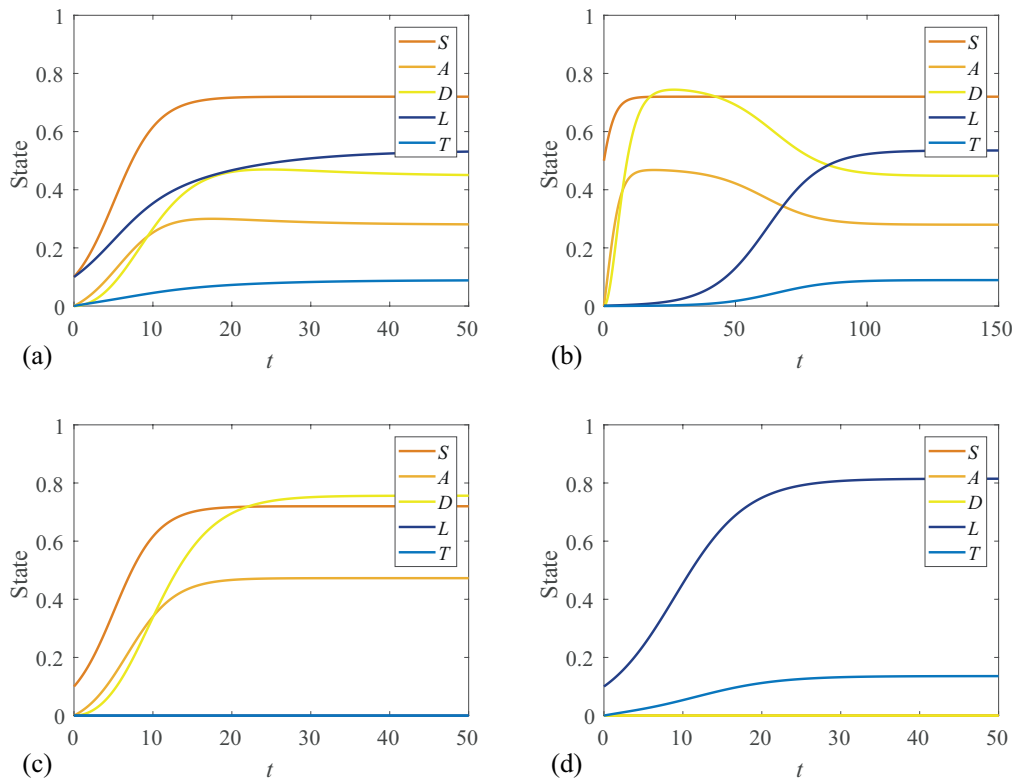


Fig. 2. Numerical solutions of Equations 1 for various initial conditions: (a) Coexisting steady state solution with $[S(0), A(0), D(0), L(0), T(0)] = [0.1, 0, 0, 0.1, 0]$. (b) Coexisting steady state with $[0.5, 0, 0, 10^{-3}, 0]$. (c) Healthy steady state with $[0.1, 0, 0, 0, 0]$. (d) Leukaemic steady state with $[0, 0, 0, 0.1, 0]$.

128 In Figure 2b we note that although the initial leukaemia stem cell population is
 129 small compared to the initial haematopoietic stem cell population, the system
 130 eventually evolves to the same coexisting steady state as in Figure 2a. However,
 131 this steady state condition requires a longer timescale to develop from the
 132 different initial conditions.

133 3 Incorporating the immune response

134 The immune system is known to play a critical role in the development, metas-
 135 tasis, treatment and recurrence of cancers [25,27]. This knowledge is supported
 136 by a range of clinical evidence, including a well-documented increased risk
 137 of cancer incidence in patients with immunodeficiency [18]. This is exempli-

138 fied by experimental mouse models where mice are typically immunocompro-
139 mised to avoid transplanted cancers being destroyed by the immune response
140 in xenograft studies [20]. Furthermore, tumours found in immunocompetent
141 hosts are observed to exhibit mechanisms for avoiding immune response [46].

142 The behaviour exhibited in Figure 2b indicates that the system cannot reach
143 a healthy non-leukaemic steady state in the presence of even small leukaemic
144 stem cell populations. It is reasonable to expect that under some circum-
145 stances a small leukaemic population may be outcompeted by healthy cells
146 occupying the same niche [42], without intervention. Therefore, we consider a
147 modification to the model proposed by Crowell, MacLean and Stumpf to incor-
148 porate an immune response. We expect this immune response to be effective
149 for small L and ineffective for large L , and so we mimic this by introducing a
150 Michaelis-Menten term to represent the immune response, giving,

$$\begin{aligned}\frac{dS}{dt} &= \rho_s S(K_1 - Z_1) - \delta_S S, \\ \frac{dA}{dt} &= \delta_S S + \rho_A A(K_2 - Z_2) - \delta_A A, \\ \frac{dD}{dt} &= \delta_A A - \mu_D D, \\ \frac{dL}{dt} &= \rho_L L(K_2 - Z_2) - \delta_L L - \underbrace{\frac{\alpha L}{\gamma + L}}_{\text{immune response}}, \\ \frac{dT}{dt} &= \delta_L L - \mu_T T.\end{aligned}\tag{2}$$

151 Including an immune response in the model is not only mathematically con-
152 venient in that it provides desirable steady states that we discuss later in this
153 section, but also biologically relevant. Immune responses are widely studied
154 in both the theoretical and experimental biology literature and acknowledged
155 as an important contributor to pathogenesis and tumour dynamics in AML
156 [7,32,61]. Additionally, immunotherapy is being investigated as an alternative
157 to chemotherapy for treatment of AML and many other cancers [10,40,45].

158 Michaelis-Menten terms are commonly used to incorporate immune responses
159 in other biologically motivated models [2,24,38]. However, it is unclear, simply
160 by inspection, what parameter values are required to obtain two stable steady
161 states: one coexisting and one healthy. For $\gamma \ll \alpha$ the Michaelis-Menten term
162 behaves as exponential decay at a rate of α , while for $\gamma \gg L$ it behaves as a
163 linear sink term [56,57]. Intuitively, we expect setting $\gamma = \mathcal{O}(L)$ will produce
164 the desired dynamics whereby the immune response is effective for small L
165 and ineffective for large L .

166 We investigate further by considering the potential steady states permitted
167 by Equation (2). We note that S is governed by a logistic growth mechanism
168 that does not depend on any of the other species so we have $\bar{S} = 1 - \delta_S/\rho_S$.
169 Similarly, D and T do not influence the other populations and hence can be
170 neglected in the consideration of the steady states. Therefore, we consider a
171 reduced system in terms of A, L with $\bar{S} = 1 - \delta_S/\rho_S$, recalling that $Z_2 = A + L$,
172 and through scaling $K_2 = 1$,

$$\frac{dA}{dt} = f(A, L) = \delta_S \left(1 - \frac{\delta_S}{\rho_S} \right) + \rho_A A (1 - A - L) - \delta_A A, \quad (3)$$

$$\frac{dL}{dt} = g(A, L) = \rho_L L (1 - A - L) - \delta_L L - \frac{\alpha L}{\gamma + L}. \quad (4)$$

173 By inspection, there is a trivial L-nullcline at $\bar{L} = 0$. We can find the A-
174 nullcline by setting $f(A, L) = 0$ in Equation (3),

$$\bar{L} = \frac{\delta_S \bar{S}}{\rho_A A} + 1 - A - \frac{\delta_A}{\rho_A}. \quad (5)$$

175 Similarly, we can find the non-trivial L-nullcline by setting $g(A, L) = 0$ in
176 Equation (4),

$$\bar{A} = 1 - L - \frac{\delta_L}{\rho_L} - \frac{\alpha}{\rho_L(\gamma + L)}. \quad (6)$$

177 The nullclines, given by Equations (5) and (6), are hyperbolas. In Figure 3
 178 we present phase planes for both the modified (with immune response) and
 179 unmodified (no immune response) models showing dynamics of the A and L
 180 populations within the physically meaningful region, $A + L \leq 1$.

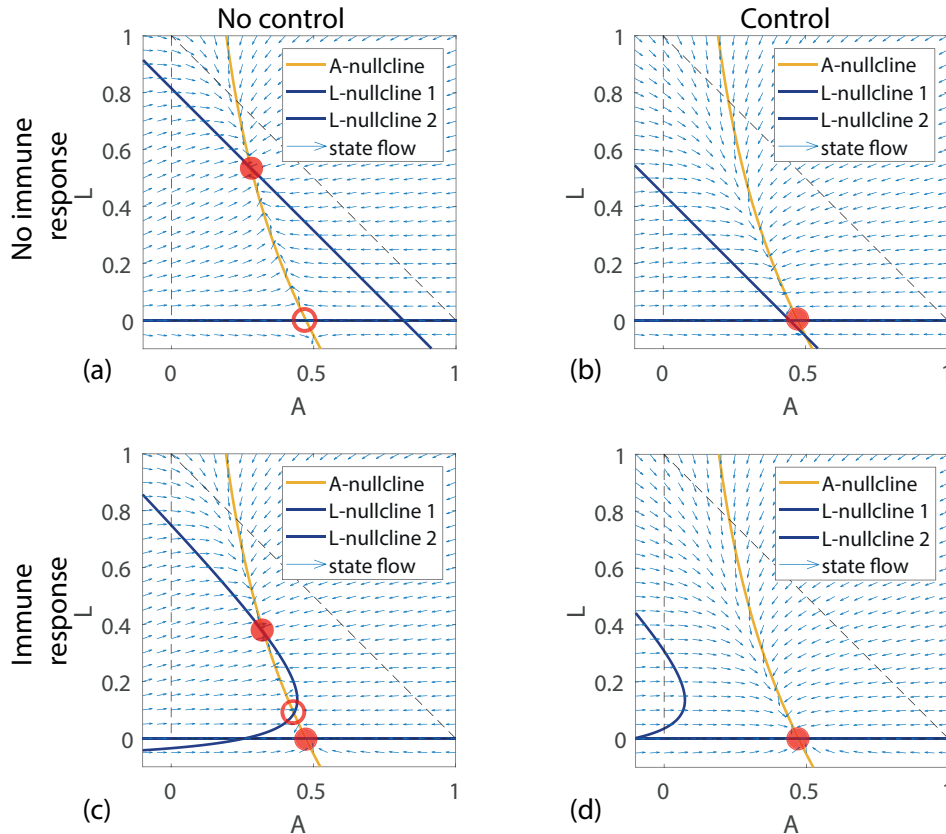


Fig. 3. Nullclines and steady states of the model with (a) no immune response and no control, (b) no immune response with control, (c) immune response with no control and (d) immune response with control, using parameters for a coexistence steady state; $[\rho_S, \rho_A, \rho_L, \delta_S, \delta_A, \delta_L] = [0.5, 0.43, .027, 0.14, 0.44, 0.05]$. Physically realistic fixed points are marked with closed discs if stable or open discs if unstable. The application of a control in (b) and (d) corresponds to $u \equiv 0.1$, effectively increasing δ_L to 0.15 (a control could be a treatment such as chemotherapy that increases the rate of decay of leukaemic stem cells, this is discussed in Section 4). In (c), for particular choices of the introduced parameters α and γ it is possible for the hyperbolas to intersect twice within the physically realistic region (dashed triangle). Figures (c) and (d) are produced with $\alpha = 0.015$, $\gamma = 0.1$. Without an immune response, as illustrated in (a) and (b), application of a control can steer the system towards a stable healthy steady state, however this fixed point becomes unstable if the control is ceased, causing the system to revert to the coexisting steady state. With an immune response, as illustrated in (c) and (d), once the control steers the system into the attractor region of the healthy fixed point, the system does not revert to the coexisting steady state upon ceasing the control.

181 This system has the desired property that we outlined previously, namely
182 that there is a stable steady state of coexistence that we aim to steer to the
183 stable state with no leukaemia through applying optimal control. Numerical
184 solutions of the modified model with no control are presented in Figure 4.

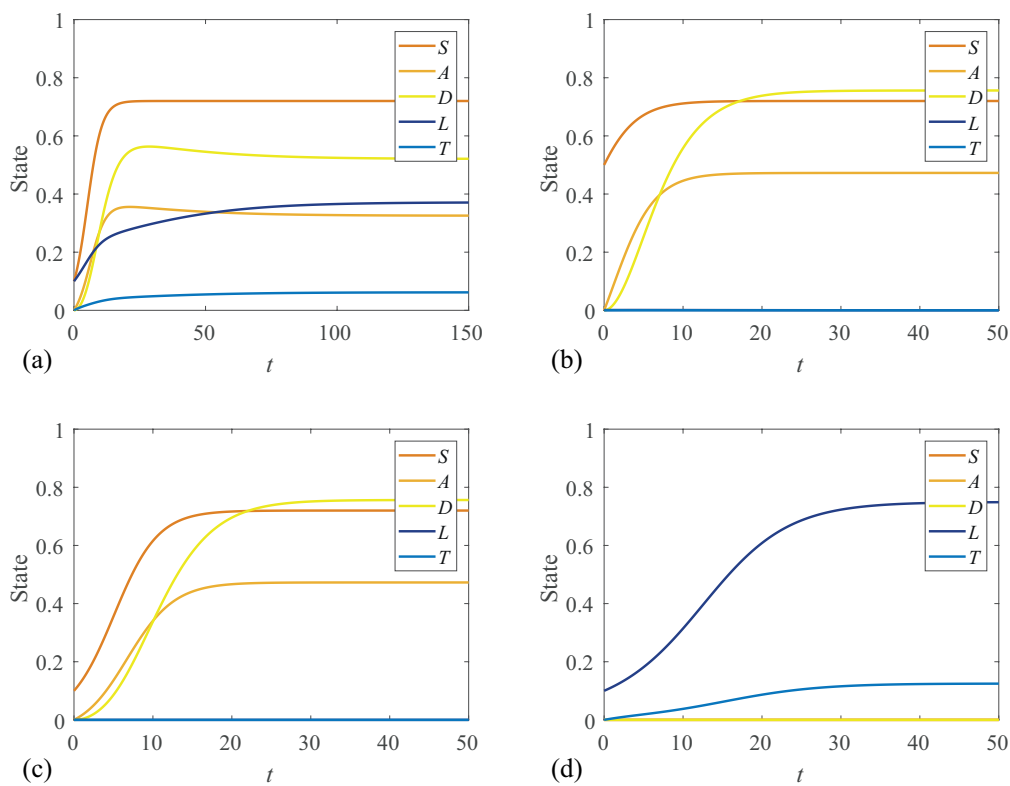


Fig. 4. Numerical solutions to the modified model with an immune response for initial conditions corresponding to Figure 2. In (a) we observe coexistence, though it takes longer for the solutions to approach steady state when compared with the original model (Figure 2a). This result is presented over a larger time-scale. With the introduction of the Michaelis-Menten style immune response to leukaemia, we observe in (b) that a small leukaemia stem cell population does not survive in the presence of a haematopoietic stem cell population. This is in contrast to Figure 2b, where a minute population of leukaemic stem cells was sufficient to grow to a coexisting steady state. These figures are produced with immune response parameters $\alpha = 0.015$, $\gamma = 0.1$.

185 4 Methods

186 In this section we provide a concise overview of the theory of optimal control.
187 Methods for solving optimal control problems are discussed. We determine
188 optimal controls to the model presented in Section 3. Specifically, we consider
189 continuous optimal controls corresponding to quadratic pay-off functions and
190 discontinuous bang-bang optimal controls corresponding to linear pay-off func-
191 tions. Numerical solutions are produced for several different pay-off weighting
192 parameter combinations.

193 4.1 Optimal control theory

194 The basic principle of optimal control is to apply an external force, the *control*,
195 to a system of differential equations, the *state equations*, to cause the solution,
196 the *state*, to follow a new trajectory and/or arrive at a different final state.
197 The goal of optimal control is to select a particular control that maximises or
198 minimises a chosen objective functional, the *pay-off*; typically a function of the
199 state and the control. The pay-off is chosen such that the new trajectory/final
200 state are preferred to that of the uncontrolled state, accounting for any cost
201 associated with applying the control.

202 A typical optimal control problem will introduce the state equations as func-
203 tions of the state $\mathbf{x}(t)$ and the control $u(t)$, with initial state $\mathbf{x}(0) = \mathbf{x}_0$,

$$\frac{d\mathbf{x}}{dt} = f(t, \mathbf{x}(t), u(t)), \quad \mathbf{x}(t) \in \mathbb{R}^n. \quad (7)$$

204 It is also necessary to specify either a final time t_f with the final state free, or
205 a final state $\mathbf{x}(t_f)$, with the final time free.

206 A pay-off function J is defined as a function of the final state, $\mathbf{x}(t_f)$, and a

207 cost function $\mathcal{L}(t, \mathbf{x}(t), u(t))$ integrated from initial time (t_0) to final time (t_f).
208 Through choosing an optimal control $u^*(t)$ and solving for the corresponding
209 optimal state $\mathbf{x}^*(t)$, we seek to maximise or minimise this objective function.
210 Selecting the pay-off enables us to incorporate the context of our application
211 and determine the meaning of *optimality*. In general, the pay-off function can
212 be written as,

$$J = \phi(\mathbf{x}(t_f)) + \int_{t_0}^{t_f} \mathcal{L}(t, \mathbf{x}(t), u(t)) dt. \quad (8)$$

213 Depending on the form of ϕ , it may be possible to incorporate ϕ into \mathcal{L} by
214 restating the final state constraint in terms of an integral expression using
215 the Fundamental Theorem of Calculus, and noting that $\phi(\mathbf{x}(t_0))$ is constant
216 and hence does not impact the optimal control. The resulting unconstrained
217 optimal control problem is often more straightforward to solve than the con-
218 strained problem.

219 The optimal control can be found by solving necessary conditions obtained
220 through application of Pontryagin's Maximum Principle (PMP) [51], or a nec-
221 essary and sufficient condition by forming and solving the Hamilton-Jacobi-
222 Bellman partial differential equation; a dynamic programming approach [9]. In
223 this work we use the PMP and we construct the Hamiltonian, $H(t, \mathbf{x}, u, \boldsymbol{\lambda}) =$
224 $\mathcal{L}(t, \mathbf{x}, u) + \boldsymbol{\lambda}f$, where $\boldsymbol{\lambda} = [\lambda_1(t), \lambda_2(t), \dots, \lambda_n(t)]$ are the adjoint variables for
225 an n -dimensional state. The adjoint is analogous to Lagrange multipliers for
226 unconstrained optimisation problems. Through the Hamiltonian, the adjoint
227 allows us to link our state to our pay-off function. The necessary conditions
228 can be expressed in terms of the Hamiltonian,

230 (1) The optimality condition is obtained by minimising the Hamiltonian,
$$\frac{\partial H}{\partial u} = 0 \text{ gives } \left(\frac{\partial \mathcal{L}}{\partial u} + \boldsymbol{\lambda} \frac{\partial f}{\partial u} \right) = 0, \quad (9)$$

231 (2) the adjoint, also referred to as *co-state*, is found by setting,

232

$$\frac{\partial H}{\partial \mathbf{x}} = -\frac{d\boldsymbol{\lambda}}{dt}, \text{ giving } \frac{d\boldsymbol{\lambda}}{dt} = -\left(\frac{\partial \mathcal{L}}{\partial \mathbf{x}} + \boldsymbol{\lambda} \frac{\partial f}{\partial \mathbf{x}}\right), \text{ and} \quad (10)$$

233 (3) satisfying the transversality condition,

$$\boldsymbol{\lambda}(t_f) = \frac{\partial \phi}{\partial \mathbf{x}} \Big|_{t=t_f}. \quad (11)$$

235 4.2 Continuous optimal control

236 In this section we consider optimal control applied to the AML model pre-
 237 sented in Section 3. From this point we omit the implied time dependence of
 238 all control, state and co-state variables for notational convenience. Consider
 239 the steady states we observed for the coexistent parameter values of model
 240 1. Suppose we wish to apply an optimal control that steers the system from
 241 a steady state observed in Figure 4a towards a healthy steady state (Figure
 242 4b). This could be achieved by applying a drug $u(t)$, the dosage of which may
 243 vary over time, that kills leukaemic stem cells,

$$\begin{aligned} \frac{dS}{dt} &= \rho_S S(K_1 - Z_1) - \delta_S S, \\ \frac{dA}{dt} &= \delta_S S + \rho_A A(K_2 - Z_2) - \delta_A A, \\ \frac{dD}{dt} &= \delta_A A - \mu_D D, \\ \frac{dL}{dt} &= \rho_L L(K_2 - Z_2) - \delta_L L - \frac{\alpha L}{\gamma + L} - uL, \\ \frac{dT}{dt} &= \delta_L L - \mu_T T. \end{aligned} \quad (12)$$

244 A potential pay-off function for this optimal control problem is to minimise,

$$J = \int_0^{t_f} (a_1 u^2 + a_2 L^2) dt, \quad (13)$$

245 where the control problem is assumed to start at time zero and run until a
246 fixed end time of t_f . In defining a pay-off function there is significant scope
247 for flexibility, and what constitutes an appropriate choice depends on the
248 application. The parameters $a_1 > 0$ and $a_2 > 0$ are chosen to weight the
249 importance of each term in the pay-off, and can be adjusted to best suit a
250 particular application. Through scaling it can be seen that for this example
251 only the relative weighting (a_1/a_2) is important, however we specify a_1 and a_2
252 separately for clarity.

253 Quadratic pay-off functions have several desirable mathematical properties
254 that increase the ease of finding optimal solutions; they are smooth and have
255 only a single extremum. Furthermore, quadratic pay-off functions help to avoid
256 non-physical controls that may otherwise be found. For example; if the pay-off
257 was a cubic function of u , setting u to be large and negative may minimise
258 the pay-off but be physically unrealisable. Quadratic pay-off functions also
259 have some desirable physical properties; a quadratic term will apply a harsher
260 penalty to large amounts of control than small amounts [6], which in many
261 treatments, such as chemotherapy, is desirable [30]. In control engineering
262 applications, the control, u , is thought to be proportional to a voltage or
263 current, in which case a quadratic pay-off has a convenient interpretation, as
264 u^2 is proportional to power, and the integral of this power over an interval is
265 proportional to the energy expended [6]. Pay-off functions that are quadratic
266 in the control variable are used in many biological [39,54] and engineering
267 applications [3,49].

268 We can construct the Hamiltonian as $H = \mathcal{L} + \boldsymbol{\lambda}f$; where f is the right hand
269 side of Equation (12), $\boldsymbol{\lambda} = [\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5]$, and from Equation (13), we have

270 $\mathcal{L} = a_1 u^2 + a_2 L^2$, giving,

$$\begin{aligned}
 H &= a_2 L^2 + a_1 u^2 + \lambda_1 [\rho_S S(1 - S) - \delta_S S] \\
 &+ \lambda_2 [\delta_S S + \rho_A A(1 - A - L) - \delta_A A] \\
 &+ \lambda_3 (\delta_A A - \mu_D D) \\
 &+ \lambda_4 [\rho_L L(1 - A - L) - \delta_L L - \alpha L / (\gamma + L) - uL] \\
 &+ \lambda_5 (\delta_L L - \mu_T T). \tag{14}
 \end{aligned}$$

271 From Equation (9), we find the optimal control by setting $\partial H / \partial u = 0$, giving
 272 $u^* = \lambda_4 L / 2a_1$. Following Equation (10), the co-state equations for $\boldsymbol{\lambda}$ are found
 273 by setting $d\boldsymbol{\lambda} / dt = -\partial H / \partial \mathbf{x}$,

$$\begin{aligned}
 \frac{d\lambda_1}{dt} &= 2S\lambda_1\rho_S + \delta_S\lambda_1 - \delta_S\lambda_2 - \lambda_1\rho_S, \\
 \frac{d\lambda_2}{dt} &= 2A\lambda_2\rho_A + L\lambda_2\rho_A + L\lambda_4\rho_L + \delta_A\lambda_2 - \delta_A\lambda_3 - \lambda_2\rho_A, \\
 \frac{d\lambda_3}{dt} &= \mu_D\lambda_3, \\
 \frac{d\lambda_4}{dt} &= -2a_2L + \rho_AA\lambda_2 + \lambda_4\rho_LA + 2\rho_LL\lambda_4 - \lambda_4\rho_L \\
 &+ \lambda_4\delta_L + \frac{\alpha\gamma\lambda_4}{(\gamma + L)^2} + \lambda_4u - \delta_L\lambda_5, \\
 \frac{d\lambda_5}{dt} &= \mu_T\lambda_5. \tag{15}
 \end{aligned}$$

274 The transversality condition, Equation (11), gives final time conditions on
 275 the co-state, Equation (15); $\boldsymbol{\lambda}(t_f) = [0, 0, 0, 0, 0]$. Assuming that the initial
 276 state is known; $[S(0), A(0), D(0), L(0), T(0)]$, it is now possible to determine
 277 the optimal control and corresponding state and co-state through solving a
 278 two-point boundary value problem (BVP).

279 We solve Equation (2) numerically to reach the stable coexistence steady state

280 of the uncontrolled model. These steady state values in the absence of the
281 control are used as the initial state conditions to solve the BVP to find the
282 optimal control solution. The initial condition for the optimal control problem
283 is $[S(0), A(0), D(0), L(0), T(0)] = [0.7200, 0.3255, 0.5207, 0.3715, 0.0619]$. Ini-
284 tialising the optimal control solution from the uncontrolled steady state is not
285 necessary, however it helps to illustrate the role of the control. We demonstrate
286 this flexibility by generating results for a range of arbitrary initial conditions
287 and control start times. These results are presented and discussed in the sup-
288 plementary material.

289 There are a range analytical methods available for solving some forms of BVP
290 under certain conditions [1,63]. However, in this work we focus on numer-
291 ical solutions with a view to identifying and discussing typical issues that
292 may arise in implementation. Common numerical solution techniques include
293 shooting and forward-backward sweep methods (FBSM) [28,37]. The most ef-
294 fective numerical method depends on the particular BVP. The single shooting
295 method is relatively straightforward, but can be sensitive to the initial guess
296 of the co-state. Forming a suitable guess for the initial values of the co-state
297 is challenging, as the co-state does not have a straightforward physical inter-
298 pretation. Although the FBSM calls for an initial guess for the control over
299 the entire interval, this can often be straightforward to determine, as we will
300 demonstrate.

301 We apply the FBSM using an initial guess for the control, $u(t) \equiv 0$, to solve
302 for the state variables forward in time. The co-state is then solved backward
303 in time. In each case a fixed step fourth order Runge-Kutta method is applied
304 to solve the relevant system of ODEs. Using these solutions, the control is up-
305 dated and the process is repeated until convergence is achieved. The algorithm
306 for the FBSM is given in Algorithm 1.

Algorithm 1: Forward-backward sweep

- i. Make an initial guess of $u(t)$.

Typically $u(t) \equiv 0$ is sufficient, though a more thoughtful choice may result in fewer iterations required for convergence.

- ii. Using the initial condition $\mathbf{x}(0) = \mathbf{x}_0$, solve for $\mathbf{x}(t)$ forward in time using the initial guess of $u(t)$.

- iii. Using the transversality condition $\boldsymbol{\lambda}(t_f)$, solve for $\boldsymbol{\lambda}(t)$ backwards in time, using the values for $u(t)$ and $\mathbf{x}(t)$.

- iv. Calculate $u_{\text{new}}(t)$ by evaluating the expression for the optimal control $u^*(t)$ using the updated $\mathbf{x}(t)$ and $\boldsymbol{\lambda}(t)$ values.

- v. Update $u(t)$ based on a combination of $u_{\text{new}}(t)$ and the previous $u(t)$.

For continuous controls applied to relatively simple systems, it may be possible to use $u_{\text{new}}(t)$ directly ($u(t) = u_{\text{new}}(t)$), however this is not sufficient to achieve convergence in general. We discuss this further in Section 4.4.

- vi. Check for convergence.

If $\mathbf{x}(t)$, $\boldsymbol{\lambda}(t)$ and $u(t)$ are within a specified absolute or relative tolerance of the previous iteration, accept $\mathbf{x}(t)$, $\boldsymbol{\lambda}(t)$ and $u(t)$ as having converged, otherwise return to Step ii. and repeat the process using the updated $u(t)$.

307 Solutions are provided in Figure 5 for various weighting on the control param-
308 eters. As expected, when $a_1 > a_2$, placing a greater weighting on the negative
309 impact of the control than the negative impact of the leukaemic stem cells we
310 observe that the control is applied at a lower level than when $a_1 < a_2$. When
311 the pay-off weightings are equal, as shown in Figure 5b, the continuous control
312 is applied at an amount similar to the level of the leukaemic stem cell popula-
313 tion. Similarly, when the amount of control applied is larger, we observe that
314 the leukaemic stem cell population declines at a faster rate. With $a_1 > a_2$, as
315 in Figure 5c, we observe that the leukaemic population is effectively eradicated
316 by t_f , whereas when $a_1 < a_2$ we see, in Figure 5d, that a leukaemic population
317 remains at t_f . A limitation of specifying a fixed final time, as opposed to a
318 fixed final state, is that the optimal outcome is dependent on the specified final
319 time, and there is no consideration for what may happen *after* t_f . In many
320 applications, the notion of what happens beyond the control interval is not of
321 interest, though in some instances specifying a final state may be more sensi-
322 ble. In this work we consider fixed final time problems for ease of comparison
323 between controls under different parameter regimes, though we acknowledge
324 that specifying a final state, such as *no leukaemic stem cells*, may be more
325 biologically appropriate.

326 For each of the optimal controls presented in Figure 5, we include an estimate
327 of J , calculated by evaluating Equation (13) with the trapezoid rule. It is
328 critical to note that these pay-offs should not be directly compared with each
329 other. This kind of comparison would be meaningless as each result corre-
330 sponds to different choices of a_1 and a_2 , and these values explicitly contribute
331 to J . For example; suppose an optimal control with pay-off weightings a_1 and
332 a_2 is computed to have a pay-off of J_1 . Recomputing the optimal control with
333 weightings $2a_1$ and $2a_2$ would produce a near identical optimal control and
334 corresponding state, with slight deviation due to floating-point error. However,
335 the corresponding pay-off J_2 would be twice as large.

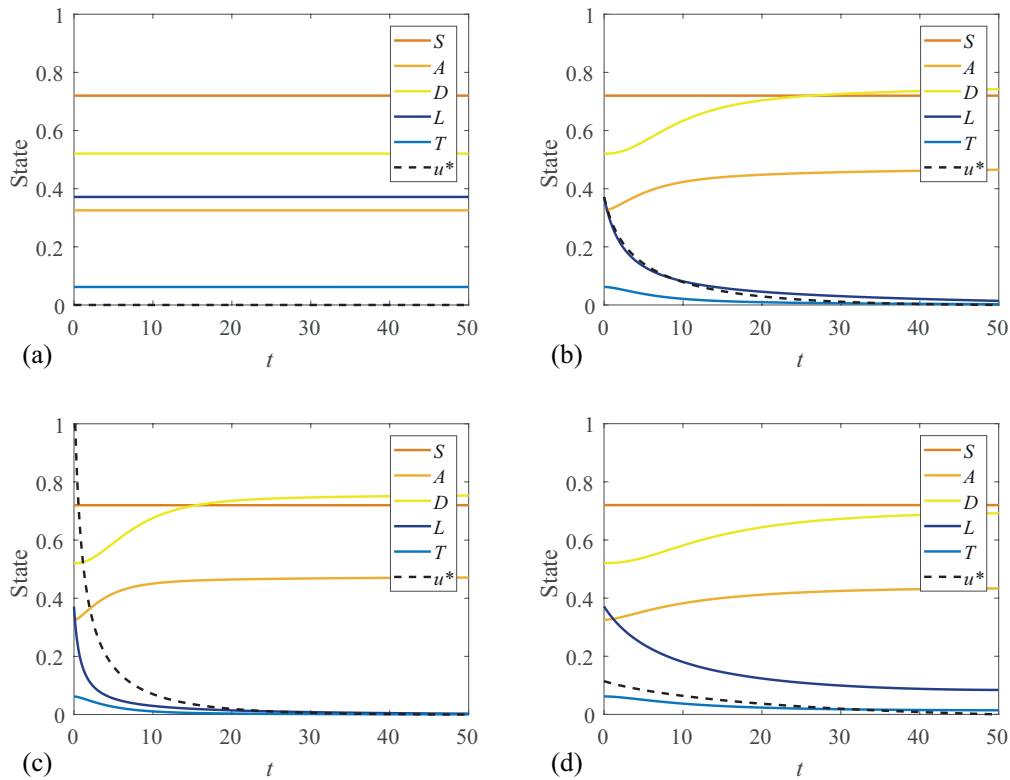


Fig. 5. Application of a continuous optimal control (black dashed line) for various pay-off weightings a_1 and a_2 . The corresponding pay-off, J , is also given. (a) Coexisting steady state solution with no control applied. (b) Equal weighting $[a_1, a_2] = [1, 1]$, $J = 0.7167$. (c) Leukaemia weighted more heavily $[a_1, a_2] = [0.1, 1]$, $J = 0.2288$. (d) Control weighted more heavily $[a_1, a_2] = [1, 0.1]$, $J = 0.2262$. These figures are produced with immune response parameters $\alpha = 0.015$, $\gamma = 0.1$.

336 No pay-off is calculated for the uncontrolled steady state solution (Figure 5a)
337 as the choice of a_1 and a_2 would be arbitrary. In this sense, computed pay-offs
338 are not useful for comparing the outcome of *treatment* versus *no treatment* as
339 there is no meaningful pay-off associated with no treatment. Rather, computed
340 pay-offs can be used for comparison with other controls applied to a system
341 with identical parameters to check whether or not they are comparable in
342 outcome to the optimal control, noting that the response of the state will also
343 change if the control changes.

344 To illustrate this point, we compare the optimal control obtained in Figure 5b
345 to other potential treatment scenarios. In Figure 6 we compare four different
346 dosing strategies where the same total amount of drug is applied using different
347 temporal regimes. Our calculations of J provide a measure of how much the
348 optimal result (Figure 6a) outperforms the other heuristically-determined dos-
349 ing strategies. Applying the control at a constant rate for the full duration of
350 the simulation (Figure 6b) produces a worse outcome than clinically-motivated
351 cyclic treatment designs; applying the control at a greater level for a shorter
352 duration in one (Figure 6c) or two (Figure 6d) cycles [5]. Due to the quadratic
353 control term in Equation (13), despite applying the same total dosage, the
354 control contributes more to the pay-off in Figure 6c than 6d, but this is out-
355 weighed by the benefit of reducing the leukaemic population more quickly.
356 The optimal control framework provides us with tools to generate treatment
357 hypotheses and assess the efficacy of different treatment protocols relative to
358 one another and to the theoretical optimum for a given set of parameters.

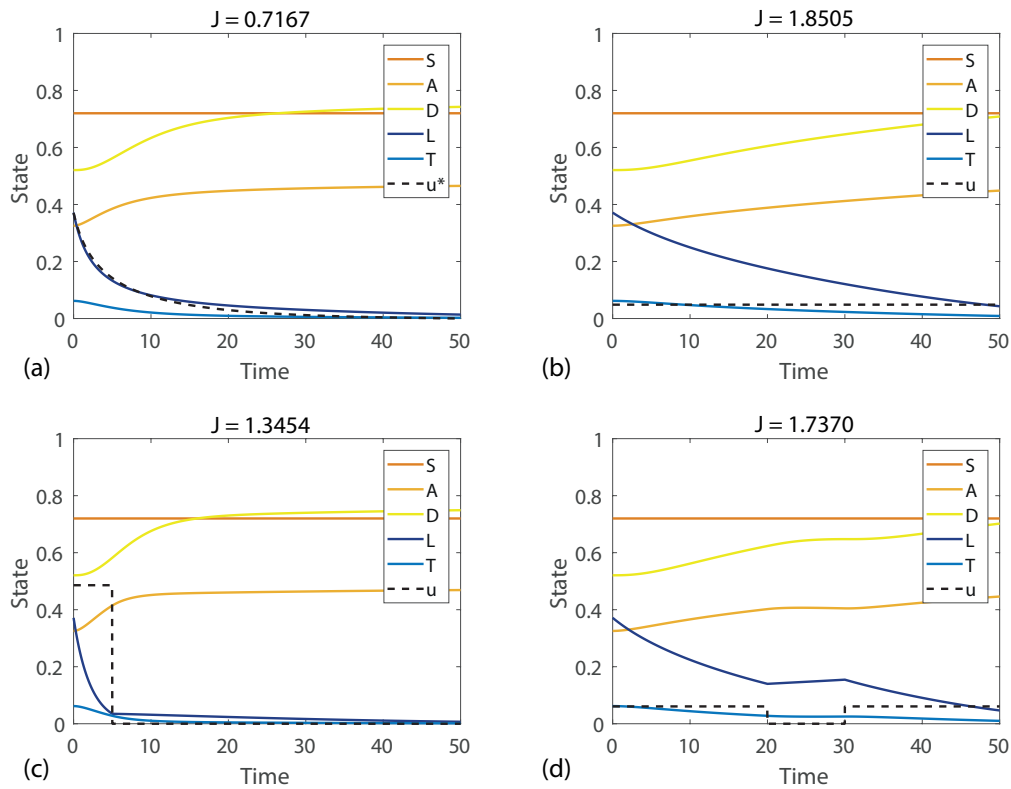


Fig. 6. Comparison of (a) continuous optimal control with other possible controls of the same total dosage; (b) control applied at a constant rate over the entire duration, (c) control applied at a higher rate over a short cycle and (d) control applied in two cycles. These figures are produced with $a_1 = a_2 = 1$ and immune response parameters $\alpha = 0.015$, $\gamma = 0.1$.

359 4.3 *Bang-bang optimal control*

360 In addition to considering continuous controls, it is also relevant to con-
 361 sider discontinuous bang-bang controls as this kind of *on-off* control could
 362 be thought to be more clinically relevant than a continuous setting. Bang-
 363 bang control problems require a specified bound on the control variable. A
 364 bang-bang optimal control takes the value of either the upper or lower bound
 365 with finitely many switching points over an interval. As a starting point we
 366 re-consider Equation (12) and note that a control will be either bang-bang op-
 367 timal or singular if the pay-off function is linear in the control term. A pay-off
 368 that should produce a bang-bang or singular optimal control of Equation (12)
 369 is to minimise

$$J = \int_0^{t_f} (a_1 u + a_2 L) dt, \quad (16)$$

370 subject to $b_1 \leq u \leq b_2$. We can construct the Hamiltonian as $H = \mathcal{L} + \boldsymbol{\lambda}f$,
 371 where \mathcal{L} is the integrand of Equation (16), $\boldsymbol{\lambda} = [\lambda_1, \lambda_2, \lambda_3, \lambda_4, \lambda_5]$ and f is the
 372 right hand side of Equation (12), giving

$$\begin{aligned} H = & a_2 L + a_1 u + \lambda_1 [\rho_S S(1 - S) - \delta_S S] \\ & + \lambda_2 [\delta_S S + \rho_A A(1 - A - L) - \delta_A A] \\ & + \lambda_3 (\delta_A A - \mu_D D) \\ & + \lambda_4 [\rho_L L(1 - A - L) - \delta_L L - \alpha L / (\gamma + L) - uL] \\ & + \lambda_5 (L\delta_L - T\mu_T). \end{aligned} \quad (17)$$

373 As for the continuous control case, we differentiate the Hamiltonian with re-
 374 spect to our control variable u . With a linear pay-off, however, the result no
 375 longer contains u . Rather than solving for u , we define a switching function,

376 $\psi(t)$, given by

$$\psi(t) = \frac{\partial H}{\partial u} = -\lambda_4(t)L(t) + a_1. \quad (18)$$

377 From PMP [51], it is implied that the Hamiltonian will be minimised under
378 the following conditions,

$$u^*(t) = \begin{cases} b_1, & \text{if } \psi(t) > 0, \\ b_2, & \text{if } \psi(t) < 0. \end{cases} \quad (19)$$

379 Conditions in Equation (19) produce a bang-bang control. Here, the control
380 variable takes a value of either its upper or lower bound. Notably, Equation
381 (19) omits the case where $\psi(t) = 0$, as a bang-bang optimal control requires
382 that $\psi(t) = 0$ only at discrete points, if at all [14]. If $\psi(t) = 0$ for any finite
383 interval aside from isolated points, the control is singular. Singular controls are
384 most commonly encountered in cases where the Hamiltonian is linear in the
385 control variable but non-linear in some state variables [12]. When $\psi(t) = 0$ over
386 an interval, the Hamiltonian is not a function of the control, so the state and
387 co-state variables no longer determine the control [12]; over this interval the
388 control is determined by requiring $\partial H/\partial u = 0$. Our control problem defined by
389 Equation (12) and Equation (16) is not singular, so we do not discuss singular
390 controls further.

391 Our co-state equations for λ are found as $\partial H/\partial \mathbf{x} = -d\lambda/dt$. The co-state in

392 the bang-bang control problem is given by,

$$\begin{aligned}
 \frac{d\lambda_1}{dt} &= 2S\lambda_1\rho_S + \delta_S\lambda_1 - \delta_S\lambda_2 - \lambda_1\rho_S, \\
 \frac{d\lambda_2}{dt} &= 2A\lambda_2\rho_A + L\lambda_2\rho_A + L\lambda_4\rho_L + \delta_A\lambda_2 - \lambda_2\rho_A, \\
 \frac{d\lambda_3}{dt} &= \mu_D\lambda_3, \\
 \frac{d\lambda_4}{dt} &= -a_2 + \rho_AA\lambda_2 + \lambda_4\rho_LA + 2\rho_LL\lambda_4 - \lambda_4\rho_L \\
 &\quad + \lambda_4\delta_L + \frac{\alpha\gamma\lambda_4}{(\gamma + L)^2} + \lambda_4u - \delta_L\lambda_5, \\
 \frac{d\lambda_5}{dt} &= \mu_T\lambda_5,
 \end{aligned} \tag{20}$$

393 and we note that Equation (20) is subtly different to Equation (15), as the first
 394 term of the fourth line of Equation (20) is the constant $-a_2$, and no longer
 395 depends on L .

396 The transversality condition, Equation (11), gives the final time conditions
 397 on the co-state, $[\lambda_1(t_f), \lambda_2(t_f), \lambda_3(t_f), \lambda_4(t_f), \lambda_5(t_f)] = [0, 0, 0, 0, 0]$. Assuming
 398 again that the initial state is known; $[S(0), A(0), D(0), L(0), T(0)]$, it is now
 399 possible to determine the optimal bang-bang control and corresponding op-
 400 timal state and co-state through a two-point BVP that we solve using the
 401 FBSM, as in the continuous control case. It is not necessary to modify the
 402 FBSM algorithm to find bang-bang optimal controls, though care must be
 403 taken in how the control is updated between iterations. This is discussed fur-
 404 ther in Section 4.4. Depending on the numerical scheme used to integrate
 405 the state and co-state equations through time, the discontinuous nature of
 406 the bang-bang control may require careful handling. Solutions are provided in
 407 Figure 7 for various weighting on the control parameters. In the continuous
 408 control case, when $a_1 > a_2$, placing a greater weighting on the negative im-
 409 pact of the control than the negative impact of the leukaemic stem cells; we
 410 observed that the control is applied at a lower level than when $a_1 < a_2$. The
 411 optimal bang-bang control must take either the upper or lower bound of the

412 specified range. As such, in the bang-bang control case the pay-off weighting
 413 parameters determine not the level at which the control is applied, but rather
 414 the times at which the control switches from one bound to the other, hence
 415 the name *switching function* given to Equation (19).

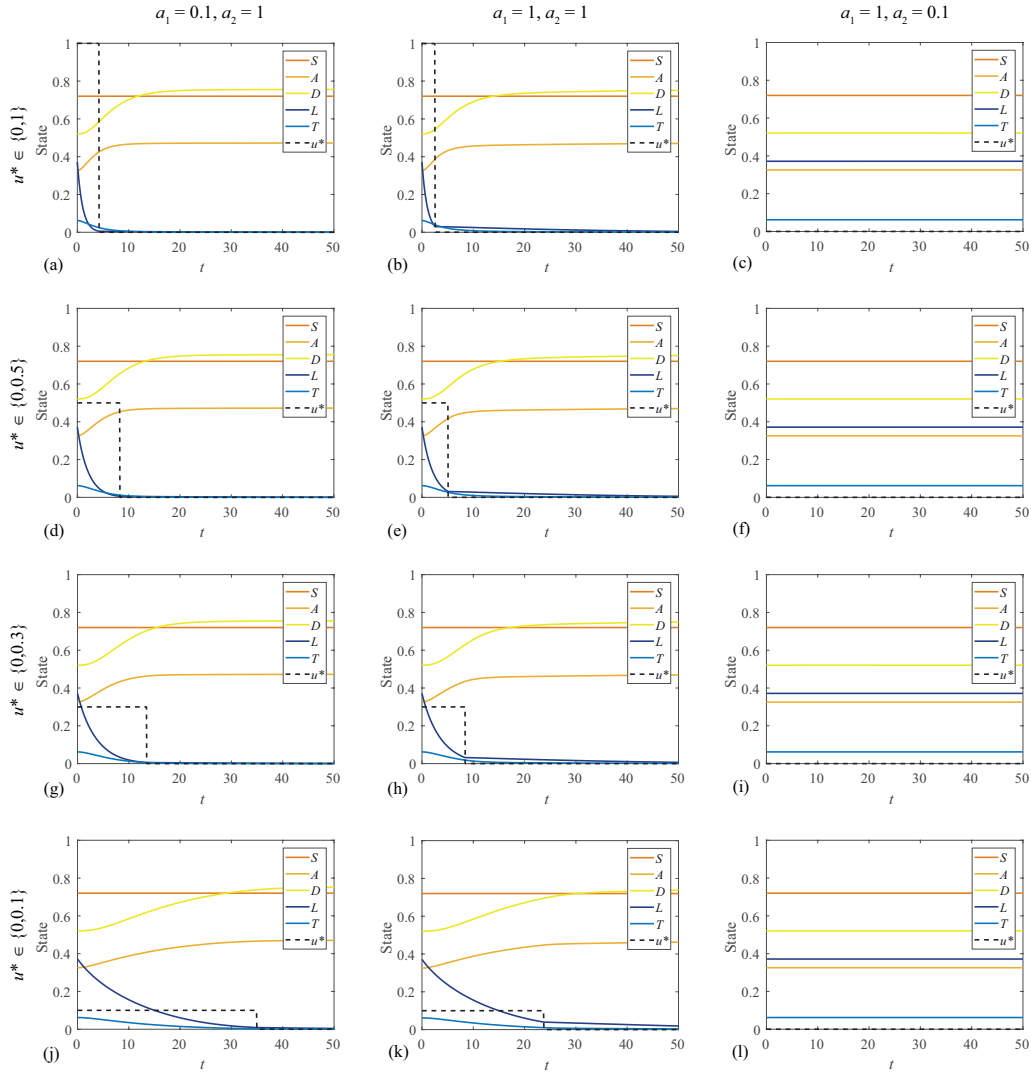


Fig. 7. Bang-bang control solutions for various weightings on control and leukaemia in the pay-off (a_1 and a_2 respectively), with different control upper bounds. These figures are produced with immune response parameters $\alpha = 0.015$, $\gamma = 0.1$.

416 In Figure 7 it is clear that when the upper bound on the control is higher,
 417 meaning in this context the maximum amount of chemotherapy that can be
 418 applied at any given time is higher, the control switches to the lower bound
 419 earlier. In this case the lower bound corresponds to $u = 0$, or no chemotherapy

420 being applied (control *switched off*), though this is not required of the method.
421 The interaction between the control and state in Equation (20) means that
422 the cumulative amount of control applied is not the same for different bounds
423 on the control. In Figure 5 we demonstrate that for a continuous control with
424 $a_1 = 1$, $a_2 = 0.1$, a small amount of control is applied. For the bang-bang case
425 with the same weighting, we observe in the rightmost column of Figure 7 that
426 for a range of control upper bounds, the control is not switched on at all -
427 implying that with such a pay-off, it is optimal not to apply the control. One
428 may suppose that for a sufficiently small upper bound that the control would
429 turn on even with this pay-off, however a lower upper bound on the control
430 also reduces the impact the control has on the state.

431 Due to the immune response incorporated in Section 3, a sufficiently small
432 leukaemic population will tend towards extinction rather than grow back to
433 a coexisting steady state. Because of this, we observe in Figure 7 that the
434 control switches off before the leukaemic stem cells are totally eradicated -
435 the immune response is sufficient once the leukaemic population is sufficiently
436 low. This is most evident in Figure 7k, where we can see that the population
437 of leukaemic stem cells is declining but has not become extinct by the final
438 time, $t = 50$. In absence of the immune response incorporated in Section 3, we
439 would observe the leukaemic population increasing as soon as the control is
440 switched off, since the healthy steady state would be unstable; applying fixed
441 final time bang-bang optimal control to the original model produces outcomes
442 that are mathematically optimal but physically undesirable.

443 In our discussion of continuous controls, we note the fixed final time as a
444 limitation, since changing the final time can change the profile of the optimal
445 control and state. In general the same is true of bang-bang controls with fixed
446 final times, though in some instances that we consider the optimal bang-bang
447 control does not change significantly if the final time is changed. For example;
448 the optimal switching times and corresponding optimal states in the leftmost

449 column of Figure 7 do not change significantly if the final time is increased to
450 $t = 100$, because by $t = 50$ we see that $L \approx 0$ and $u = 0$, so neither contributes
451 significantly to the pay-off in the interval $50 < t \leq 100$. For these cases the
452 control is not costly relative to the leukaemia ($a_1 < a_2$) so it is applied at the
453 upper bound until the leukaemic stem cell population is virtually eradicated
454 before switching off.

455 For this particular system, we only obtain bang-bang optimal controls with a
456 single switching time. We are able to verify these bang-bang optimal controls
457 through an exhaustive search of all possible bang-bang controls by specifying
458 the switching time, directly calculating the pay-off and determining the
459 switching time that minimises the pay-off. For all cases considered in Figure 7
460 the switching time identified via exhaustive search is in agreement. It is also
461 possible that the optimal bang-bang control may switch between the upper
462 and lower bounds numerous times, producing multiple ‘bangs’. Bang-bang op-
463 timal controls that exhibit multiple bangs can be identified using the FBSM
464 without modification, though it is more difficult to find a convergent bang-
465 bang optimal control with multiple bangs. Similarly, without knowing a priori
466 how many switching times to expect, an exhaustive search for multiple bangs
467 is not computationally feasible.

468 *4.4 Convergence and control updating*

469 In this section we examine the convergence behaviour of solutions to the op-
470 timal control problems presented in this work. Convergence behaviour of nu-
471 merical solutions to optimal control problems is influenced by multiple factors.
472 In particular, we discuss the initial guess of the control, convergence criteria,
473 control updating and pay-off weightings. These factors influence not only the
474 number of iterations required to reach a converged numerical solution, but
475 also whether or not a converged solution will be reached at all.

476 Holding all other factors constant, provided that the initial guess for the con-
477 trol is sensible, the initial guess does not have a significant impact on whether
478 or not a converged result is reached for the control problems considered in this
479 work. However, convergence is typically reached with fewer iterations when the
480 initial guess is relatively closer to the true value of the optimal control. For
481 simplicity we use the initial guess $u \equiv 0$ for all results presented in this work,
482 while acknowledging that more thoughtful choices may deliver convergence in
483 fewer iterations.

484 For optimal control results presented in the previous sections, we determine
485 whether convergence has been achieved after each iteration based on the rela-
486 tive difference between the updated control, u_{updated} , and the old control, u_{old} .
487 If this relative difference is sufficiently small, the updated control is accepted
488 as the optimal control. A typical relative difference convergence criterion re-
489 quires

$$\frac{|u_{\text{updated}} - u_{\text{old}}|}{|u_{\text{updated}}|} \leq \varepsilon, \quad (21)$$

490 where $0 < \varepsilon \ll 1$ is the desired relative tolerance. Following [37], we adjust
491 Equation (21) to allow for a control of the form $u \equiv 0$, giving

$$\varepsilon \sum_{i=1}^n |u_{\text{updated}}(i\Delta t)| - \sum_{i=1}^n |u_{\text{updated}}(i\Delta t) - u_{\text{old}}(i\Delta t)| \geq 0, \quad (22)$$

492 where $t = i\Delta t$, Δt is the numerical time step and n is the number of nodes
493 in the time discretisation. The absolute value is taken to ensure that positive
494 differences are not offset by negative differences that could otherwise result
495 in incorrectly detecting convergence. The choice of convergence criterion and
496 acceptable tolerance depends on the particular problem at hand, and may
497 need to be adjusted to be appropriate for another control problem. In some
498 instances, it may be necessary to check convergence of the state and co-state
499 as well as the control, particularly if the state response to control is sensitive.

500 For the control problems studied in this work, we find that state and co-
501 state respond predictably to the control, and convergence of the control is
502 accompanied by convergence of that state and co-state. As such we do not
503 explicitly check for convergence of the state and co-state.

504 In each iteration of the FBSM we recalculate the control, u_{new} , based on the
505 newly calculated state and co-state solutions and associated optimality cri-
506 terion, as discussed in Section 4.2 for the continuous control and Section 4.3
507 for the bang-bang control. Typically, u_{new} is not used directly as the control
508 for the next iteration of the FBSM, but rather we form an updated control
509 u_{updated} as a weighted combination of u_{new} and the control from the previ-
510 ous iteration, u_{old} . The motivation for this is two-fold; first, an appropriately
511 weighted control updating scheme can speed up convergence; and second, for
512 many optimal control problems, a direct update of $u_{\text{updated}} = u_{\text{new}}$ will fail
513 to produce converging results at all. A common approach is to update the
514 control based on a convex combination, such that the total weightings sum to
515 one, of the new and previous control(s). In this work we use a constant linear
516 weighting, with $0 < \omega < 1$, giving

$$u_{\text{updated}} = \omega u_{\text{old}} + (1 - \omega) u_{\text{new}}. \quad (23)$$

517 We find that the best choice for ω depends not only on the form of the control,
518 continuous or bang-bang, but also on model parameters such as the pay-off
519 weightings. There is a trade-off between the number of iterations required to
520 obtain convergence, and actually converging at all; a larger ω typically is more
521 likely to produce converging solutions, but this also means that the control
522 changes less each iteration, so more iterations are required. For example, a
523 weighting of $\omega = 0.7$ was sufficiently large that all continuous control solutions
524 presented in Figure 5 converged to a relative tolerance of $\varepsilon = 1 \times 10^{-3}$. For
525 $\omega = 0.6$ only Figure 5d converges, and for $\omega = 0.8$, all solutions in Figure 5

526 converge but require more iterations than when $\omega = 0.7$.

527 Convergence in the bang-bang control case typically requires larger ω and more
528 iterations than the continuous controls. In the rightmost column of Figure
529 7, there is no concept of convergence as the control never switches on. Only
530 Figure 7j and Figure 7k converge to a relative tolerance of 1×10^{-3} for $\omega = 0.7$,
531 with $\omega = 0.9$ being sufficient for convergence of all remaining solutions aside
532 from Figure 7b, where we set $\omega = 0.95$.

533 It is clear that the best control updating scheme depends on the particular
534 problem; and a scheme that works well for one problem may not necessarily
535 work at all for another. When solving control problems, it may be necessary
536 to try a range of updating schemes to achieve convergence. In this work we
537 only consider constant weighted updating, though there are more sophisti-
538 cated updating schemes that shift the weighting towards u_{new} as the number
539 of iterations increase [37]. In Figure 8 we examine the influence of the control
540 update weighting ω , and the pay-off weightings, a_1 and a_2 , on the convergence
541 behaviour of the bang-bang control problem studied in Section 4.3. Specifi-
542 cally, we consider the case where $0 \leq u \leq 0.5$, and determine that a solution
543 has converged if it meets a relative tolerance of $\varepsilon = 1 \times 10^{-3}$ within 250 it-
544 erations. In each panel of Figure 8 we observe three *regions*: in region I we
545 have no concept of convergence as the control never switches on; in region II
546 we find that the optimal control problem does not converge; and in region III
547 we observe convergence. Not all simulations conform strictly to these regions
548 since the boundary between the different regions is not always sharp and well-
549 defined. However, broadly speaking, these three regions capture the essence
550 of the convergence behaviour that we observe. These regions are constructed
551 based on discrete simulations of the problem for $0 < a_1 \leq 10$ and $0 \leq a_2 \leq 10$,
552 each in increments of 0.1. The case where $a_1 = 0$ is excluded as this corre-
553 sponds to no cost associated with applying the control, so there is no sense of
554 convergence.

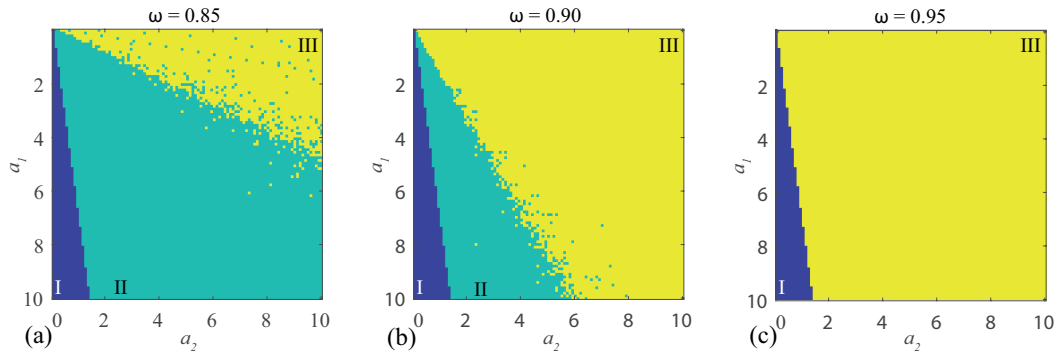


Fig. 8. Convergence behaviour for (a) $\omega = 0.85$, (b) $\omega = 0.9$, and (c) $\omega = 0.95$, with a_1 and a_2 ranging from 0 to 10 in increments of 0.1, excluding $a_1 = 0$. In region I (dark blue) we have no concept of convergence as the control never switches on. In region II (light blue) we find that the optimal control problem does not converge, and in region III (yellow) we observe convergence. These figures are produced with immune response parameters $\alpha = 0.015$, $\gamma = 0.1$.

555 From Figure 8 it is clear that convergence is achieved in a larger region of the
556 (a_1, a_2) parameter space when ω is increased. However, it is important to note
557 that achieving convergence in this context only implies that Equation (22) is
558 satisfied, and does not necessarily mean that a suitable bang-bang control is
559 obtained. While some controls corresponding to individual simulations in Fig-
560 ure 8c are suitable bang-bang controls; a portion are approaching bang-bang
561 but require additional iterations to accurately calculate the control around
562 the switching point. The weighting applied in Equation (23) has the effect
563 of smoothing u during intermediate iterations of the FBSM; this smoothness
564 is gradually reduced as the control converges to the optimal switching point.
565 Since ω explicitly influences the relative amount that the control can differ
566 between iterations, if a larger ω is required to achieve convergence for a given
567 problem, it may also be necessary to reduce the convergence tolerance ε to
568 ensure that the resulting control is sufficiently bang-bang.

569 **5 Conclusion and Outlook**

570 In this work we consider a haematopoietic stem cell model of AML that incor-
571 porates competition between leukaemic stem cells and blood progenitor cells
572 within the bone marrow niche. We incorporate a biologically appropriate im-
573 mune response in the form of a Michaelis-Menten term. This modification is
574 mathematically convenient because of the impact it has on the steady states,
575 and biologically relevant because the immune response is known to play an
576 important role in cancer progression and treatment. With a view to identify-
577 ing the optimal way to apply a treatment such as chemotherapy to the model,
578 we formulate and solve optimal control problems corresponding to multiple
579 objectives and constraints. This includes quadratic pay-off functions, yielding
580 continuous controls, as well as linear pay-off functions, yielding discontinuous
581 bang-bang controls.

582 We provide a brief overview of optimal control theory, with a focus on the
583 necessary conditions derived from Pontryagin's Maximum Principle. This ap-
584 proach formulates the optimal control problem as a coupled multi-species
585 two-point boundary value problem. The resulting optimal control problem
586 is solved numerically using the iterative FBSM. The algorithm for the FBSM
587 is discussed, with a focus on highlighting typical issues that may arise in im-
588 plementing optimal control. Suggestions are provided for overcoming these
589 issues. In particular, we focus on factors that influence the convergence of
590 the FBSM; not only in terms of the number of iterations required, but also
591 whether it converges at all. These factors include the initial guess for the
592 control, the convergence criterion, the method of updating the control, the
593 associated weighting placed on controls from prior iterations and parameters
594 such as pay-off weightings, and in the bang-bang control case, the control
595 bounds.

596 For the model we consider; a well informed initial guess for the control may re-

597 duce the number of iterations required for convergence, but any sensible guess
598 should not prevent convergence. Most critically, we show that the method of
599 updating the control and the associated weight placed on the control from the
600 previous iteration has a significant impact on whether or not convergence will
601 be achieved, as do the weights in the pay-off function. In the bang-bang control
602 case, we observe that increasing the upper bound on the control can prevent
603 convergence, holding all other factors constant; in this case, placing a greater
604 weight on the solution from the previous iteration may produce convergence.

605 There are many potential avenues to extend the ideas explored in this work.
606 Here, we have incorporated the control via a simple mechanism, and more so-
607 phisticated pharmacokinetic processes such as drug absorption and metabolism
608 could be incorporated to increase the biological detail captured by the model,
609 but this additional biological detail comes at the cost of increasing the number
610 of unknown, and possibly unmeasurable parameters. Therefore, care must be
611 exercised in following up this kind of extension. In the main document we
612 consider the most fundamental case of a control that only impacts leukaemic
613 cells, however the methodology extends to a control affecting multiple species.
614 We demonstrate this extension in the supplementary material. The control
615 problems presented in this work could be reformulated as fixed final state
616 problems, leaving the final time free to vary which could be more clinically
617 relevant than specifying the final time. With the introduction of an immune
618 mechanism to the model, it is also possible to consider a control based around
619 immunotherapy.

620 A recent idea of great interest in clinical cancer research is the possibility of
621 introducing an interval of time during treatment in which no chemotherapy is
622 applied. This kind of intervention is reminiscent of a bang-bang control, and
623 is often referred to as a *drug holiday* [60]. There is some evidence to suggest
624 that drug resistance of tumour cells may reduce with time so that patients
625 experience an improved response to chemotherapy following a drug holiday

626 [33,34,55]. This application of a drug in an *on-off* fashion parallels the idea of
627 the bang-bang controls we consider in this work and so it would be interesting
628 to formulate the concept of designing a drug holiday in terms of a bang-bang
629 optimal control problem by extending the model to include acquired drug
630 resistance and using the algorithms and concepts demonstrated in this work.

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