

1 Time-to-target simplifies optimal 2 control of visuomotor feedback 3 responses

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7 Abstract

8 Visuomotor feedback responses vary in intensity throughout a reach, commonly explained by
9 optimal control. Here we show that the optimal control for a range of movements with the same
10 goal can be simplified to a time-to-target dependent control scheme. We measure participants'
11 visuomotor responses in five reaching conditions, each with different hand or cursor kinematics.
12 Participants only produced different feedback responses when these kinematic changes resulted in
13 different times-to-target. We complement our experimental data with a range of finite and
14 non-finite horizon optimal feedback control models, finding that only the model with time-to-target
15 as one of the input parameters can successfully replicate the experimental data. Overall, this
16 suggests that time-to-target is a critical control parameter in online feedback control. Moreover, we
17 propose that for a specific task and known dynamics, humans can instantly produce a control
18 signal without any computation allowing rapid response onset and close to optimal control.

20 Introduction

21 From intercepting a basketball pass between opponents to catching a vase accidentally knocked
22 off the shelf – visuomotor feedback responses play a familiar role in human motor behaviour.
23 Previous research has extensively analysed these responses in human reaching movements (*Day*
24 *and Lyon (2000)*; *Reichenbach et al. (2014)*; *de Brouwer et al. (2017, 2018)*; *Saunders and Knill*
25 *(2003)*; *Saunders (2004)*; *Saunders and Knill (2005)*; *Sarlegna et al. (2003)*; *Knill et al. (2011)*), and
26 showed an interesting combination of task-dependent variability on the timescale of a single move-
27 ment (*Dimitriou et al. (2013)*; *Franklin et al. (2014, 2017)*), as well as sub-voluntary feedback onset
28 times (*Prablanc and Martin (1992)*; *Day and Lyon (2000)*; *Franklin and Wolpert (2008)*; *Zhang et al.*
29 *(2018)*; *Oostwoud Wijdenes et al. (2011)*). These visuomotor feedback responses have been shown
30 to modulate throughout a movement depending on the perturbation onset location (*Dimitriou*
31 *et al. (2013)*). This observation was explained through optimality principles, however such control
32 was modelled only indirectly, by replicating velocity profiles and trajectories of visually perturbed
33 movements (*Liu and Todorov (2007)*; *Rigoux and Guigon (2012)*). In this study we test to what de-
34 gree optimal feedback control, as opposed to other control methods, can be used to model the
35 visuomotor feedback responses directly.

36 Optimal control as a theory of human movement has normally been compared against other
37 theories in terms of prediction of kinematics and dynamics (*Todorov and Jordan (2002)*; *Izawa*
38 *et al. (2008)*; *Nagengast et al. (2009)*; *Yeo et al. (2016)*; *Guigon et al. (2007, 2008)*). Nevertheless,
39 optimal feedback control has been used to motivate extensive studies investigating the control and
40 task-dependent modulation of feedback responses (*Knill et al. (2011)*; *Pruszynski and Scott (2012)*;
41 *Nashed et al. (2012, 2014)*). The results of these and other studies have highlighted the flexibility of

42 the modulation of these feedback responses. While a few studies have compared the predictions of
43 the controller feedback gains against the feedback responses in human subjects (*Knill et al. (2011)*),
44 such predictions have not been made about the temporal evolution of these feedback responses
45 during reaching. For example, *Dimitriou et al. (2013)* show temporal evolution of feedback response
46 intensity throughout a reaching movement, suggesting that this is similar to the feedback gain
47 predictions of *Liu and Todorov (2007)*. However a direct comparison of these feedback intensities
48 has not been made. Here we directly compare the temporal evolution of visuomotor feedback
49 response intensities in human participants with the prediction of these intensities in an optimal
50 feedback control model.

51 Visuomotor feedback response intensity over a goal directed reaching movement follows a
52 roughly bell-shaped profile, with peak intensity in the middle and decay towards the beginning and
53 the end of the movement (*Dimitriou et al. (2013)*). The results of *Liu and Todorov (2007)* suggest that
54 such modulation is a combination of gains related to movement position, velocity and acceleration.
55 However, we do not yet know whether these would be related to the visual or haptic kinematics.
56 In addition, models of ball catching were shown to produce systematic errors in the prediction of
57 the hand kinematics when using only velocity or acceleration based gains (*Dessing et al. (2002)*),
58 suggesting an integration of multiple state variables to produce the feedback response. Evidence
59 of such integration then raises two important questions. First, could there be other states than
60 position and its derivatives that also contribute to such control? Second, how can these responses
61 be produced so rapidly, when multiple inputs need to be integrated into one solution?

62 One method to solve these two problems would be a controller based on time-to-target. Within
63 a state-space system, all state variables are constantly changing with time with a fixed relationship
64 to one another as described by the state transition and control matrices. Such a system can
65 then be re-imagined as a system with time as its input, and these physical states as the hidden
66 states. Such mapping simplifies the multiple input system where the inputs are state variables,
67 to a one-input (time) system. Indeed, the expected time-to-target (or time-to-contact) has been
68 shown to be related to the control in finger pointing (*Oostwoud Wijdenes et al. (2011)*) and catching
69 tasks (*Dessing et al. (2002)*). Therefore, we test whether a simple relation to the time-to-target can
70 explain the temporal profile of visuomotor feedback responses in humans. To test our hypotheses,
71 we devised an experimental paradigm where we offset the usual bell-shaped velocity profile in the
72 aim to separate the effect of the times-to-target from the effect of kinematics on the visuomotor
73 feedback responses. Finally, we compare these results with a normative optimal feedback control
74 model of visuomotor feedback responses in order to better understand how and whether these
75 responses can be the result of optimality and still maintain rapid onset times.

76 Results

77 Experimental results

78 In this study we examine the relation between time-to-target and the visuomotor feedback re-
79 sponses. To do so, we devised an experiment consisting of five different kinematic conditions.
80 The baseline condition required movements with a natural, bell-shaped velocity profile, while the
81 velocity profiles were modified for the four other conditions. In these four conditions we introduced
82 a manipulation between the hand velocity and the cursor velocity in the forward direction, such
83 that the cursor and hand had different velocity profiles, but their positions matched at the start and
84 end of the movement (Figure 1). Two of these four conditions (matched-cursor conditions) required
85 different kinematics of the physical movement to successfully complete the task, but the cursor
86 velocity profiles matched the baseline. This manipulation of hand velocity profiles also resulted in
87 different times-to-target at the same distance in the movement. The two other conditions (matched-
88 hand conditions) required the same hand movement as for the baseline condition, but as a result
89 the cursor moved with different velocity profiles (see Materials and Methods). This manipulation
90 of the cursor velocity profiles separates the relative contributions of physical and visual hand

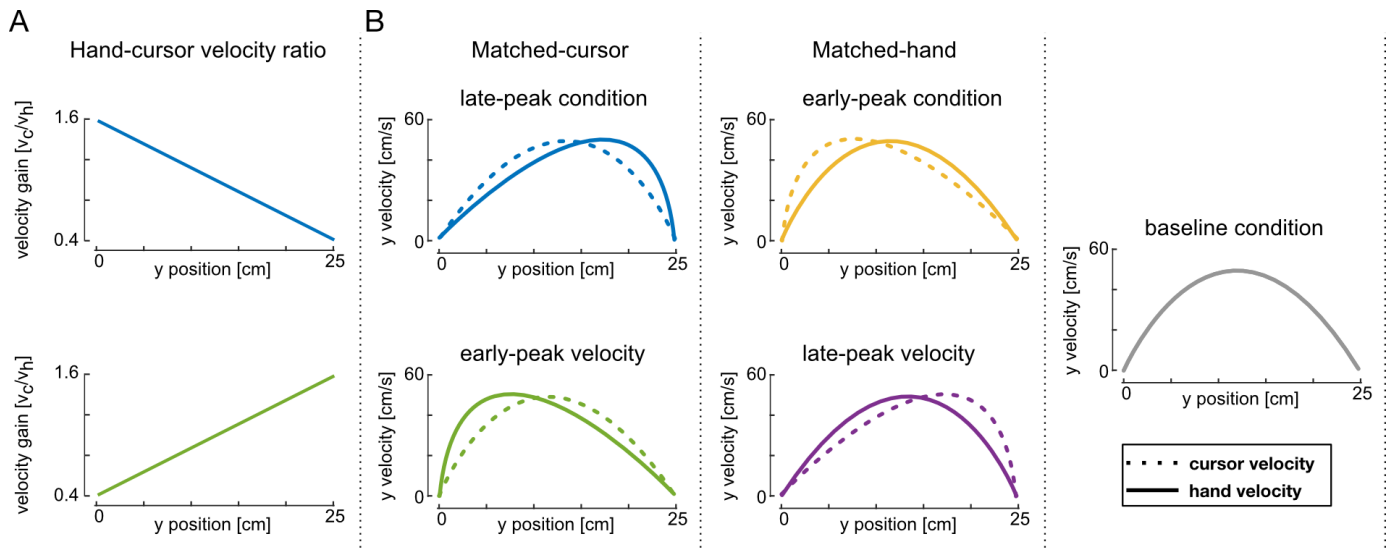


Figure 1. Experimental design. **(A)** Top: hand-cursor velocity scaling for conditions where the cursor position leads the hand position in y axis (matched-cursor late-peak hand velocity condition, blue, and matched-hand early-peak cursor velocity condition, yellow). Bottom: hand-cursor velocity scaling for conditions where the cursor position lags the hand position in y axis (matched-cursor early-peak hand velocity condition, green, and matched-hand late-peak cursor velocity condition, purple). **(B)** Hand and cursor velocity-position profiles required to achieve the ideal movement to the target. Left: matched-cursor velocity conditions; middle: baseline condition, where cursor position and hand position are consistent; right: matched-hand velocity conditions.

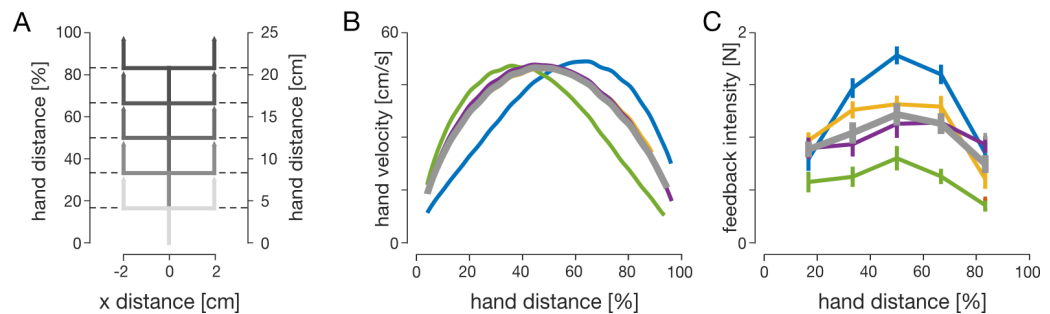


Figure 2. Human visuomotor feedback responses are modulated across the five experimental conditions. **(A)** Lateral perturbations of the cursor were applied in all five conditions. Perturbations were introduced as 2 cm cursor jumps perpendicular to the movement direction. The perturbation onset occurred at one of five equally spaced hand locations. **(B)** Mean velocity profiles of the hand in five experimental conditions: matched-cursor early-peak (green), matched-cursor late-peak (blue), matched-hand early-peak (yellow), matched-hand late-peak (purple) and baseline (grey). Participants successfully modulated forward movement kinematics to meet task demands – velocity profiles are skewed for matched-cursor conditions, and are similar to the baseline for matched-hand conditions. **(C)** Mean visuomotor feedback intensities (mean lateral force from 180-230 ms after perturbation onset) across all participants to cursor perturbations as a function of the hand distance in the movement. Error bars represent 1 SEM. Significant regulation is observed for matched-cursor early-peak and matched-cursor late-peak conditions (blue and green), but no significant regulation is seen for matched-hand conditions (yellow and purple), relative to the baseline.

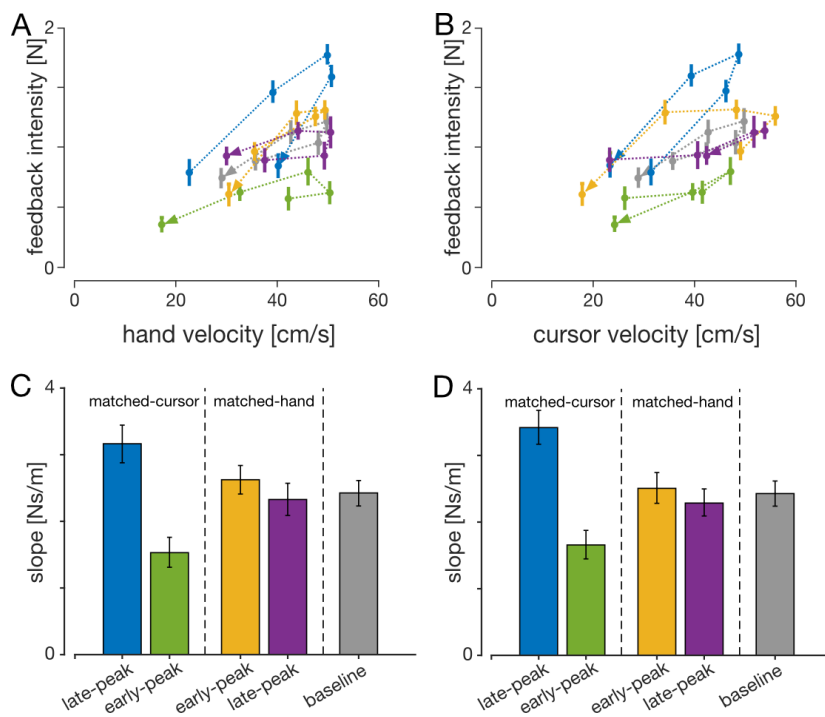


Figure 3. Visuomotor feedback intensities as a function of (A) Hand velocity and (B) cursor velocity at the time of perturbation for all experimental conditions. Error bars represent 1 SEM, and the arrowheads represent the order of the perturbation locations. (C), (D) Regression slopes of feedback intensities for each condition as a function of hand and cursor velocities respectively. Error bars represent 95% confidence intervals of the slopes. The slopes for the two matched-cursor conditions were significantly different (based on the confidence intervals) than for the baseline condition.

91 information in regulating the feedback responses. For each condition we measured the visuomotor
 92 feedback intensities (mean corrective force applied during 180-230 ms time window after a visual
 93 perturbation) at five different locations in the movement (Figure 2A). Overall our paradigm allowed
 94 us to modulate the times-to-target across conditions, as well as separate proprioceptive (hand)
 95 and visual (cursor) kinematics to examine their individual contribution to visuomotor feedback
 96 responses.

97 Different movement conditions exhibited differences in visuomotor feedback intensities (Figure
 98 2 and Figure supplement 1). Two-way repeated-measures ANOVA (both frequentist and Bayesian;
 99 Materials and Methods) showed significant main effects for both condition ($F_{4,36} = 10.807$, $p < 0.001$,
 100 and $BF_{10} = 9.136 \times 10^{12}$), and perturbation location ($F_{4,36} = 33.928$, $p < 0.001$, and $BF_{10} = 6.870 \times 10^9$).
 101 Post-hoc analysis on movement conditions revealed significant differences between baseline (grey
 102 line) and matched-cursor late-peak hand velocity condition (blue line; $t_9 = 4.262$, $p_{bonf} < 0.001$
 103 and $BF_{10} = 247.868$), and between baseline and matched-cursor early-peak hand velocity condition
 104 (green line; $t_9 = -8.287$, $p_{bonf} < 0.001$ and $BF_{10} = 1.425 \times 10^8$). However, no significant differences were
 105 found between the baseline and the two matched hand velocity conditions ($t_9 = 1.342$, $p_{bonf} = 1.0$
 106 and $BF_{10} = 0.357$ for early-peak cursor velocity, yellow; $t_9 = 0.025$, $p_{bonf} = 1.0$ and $BF_{10} = 0.154$ for
 107 late-peak cursor velocity, purple). Our results show that different kinematics of the hand movement
 108 have a significant effect on visuomotor feedback response regulation, but that different kinematics
 109 of the cursor movement do not.

110 One possible explanation for differences between the two matched-cursor conditions (blue and
 111 green in Figure 2C and Figure supplement 1) and the baseline condition (grey) might arise from a
 112 different mapping between cursor and hand velocities (Figure 1A) that had to be learned. Alter-
 113 natively, the incongruity between the vision and proprioception might be another explanation.
 114 However, the two matched-hand conditions (yellow and purple) had the identical mappings (and
 115 incongruities) as the two matched-cursor conditions (blue and green respectively) and yet no
 116 differences were found in these conditions. Instead, the only conditions in which differences in
 117 the feedback gains were found, were conditions in which the timing of the peak hand velocity was
 118 shifted.

119 In order to test whether a simple relationship between movement kinematics and visuomotor

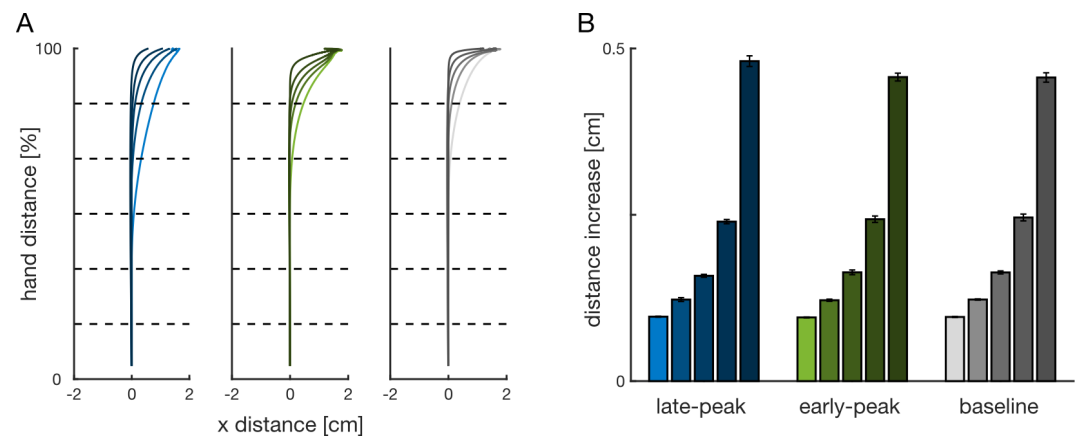


Figure 4. (A) Mean hand movement trajectories for matched-cursor late-peak (left), matched-cursor early-peak (middle) and baseline (right) conditions recorded in our participants, with perturbation onset at five locations (colour light to dark: 4.2 cm (16.7%), 8.3 cm (33.3%), 12.5 cm (50%), 16.7 cm (66.7%) and 20.8 cm (83.4%) from the start position; dashed lines). Corrections to rightward perturbations were flipped and combined with leftward corrections. (B) Distance increase for each perturbation location recorded in our participants. Perturbation locations closest to the target required the largest increases in movement distance. Error bars represent 1 SEM.

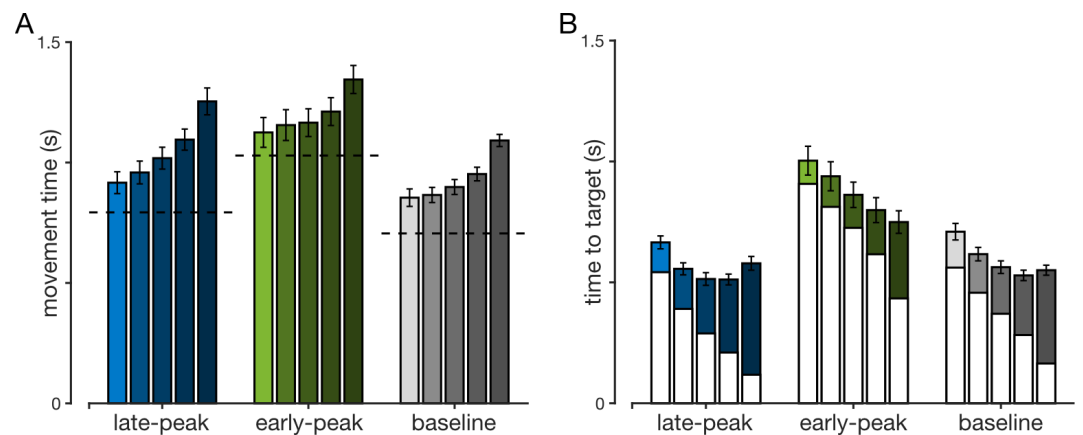


Figure 5. (A) Movement durations in maintained perturbation trials recorded by our participants in late-peak, early-peak and baseline conditions. Separate bars within the same colour block represent different perturbation onset locations (left to right: 4.2 cm, 8.3 cm, 12.5 cm, 16.7 cm and 20.8 cm from the start position). Error bars represent 1 SEM while the horizontal dashed lines represent movement durations in the same movement condition for non-perturbed movements. (B) Full bars represent times-to-target in maintained perturbation trials in our participants for late-peak, early-peak and baseline conditions. White bars represent the time-to-target for a respective non-perturbed movement, at the time when the perturbation would have happened. The coloured part of the bars shows the extension in times-to-target due to the perturbation in a non-constrained movement. Each of the five bars represents a different perturbation onset location, as in (A). Error bars represent 1 SEM.

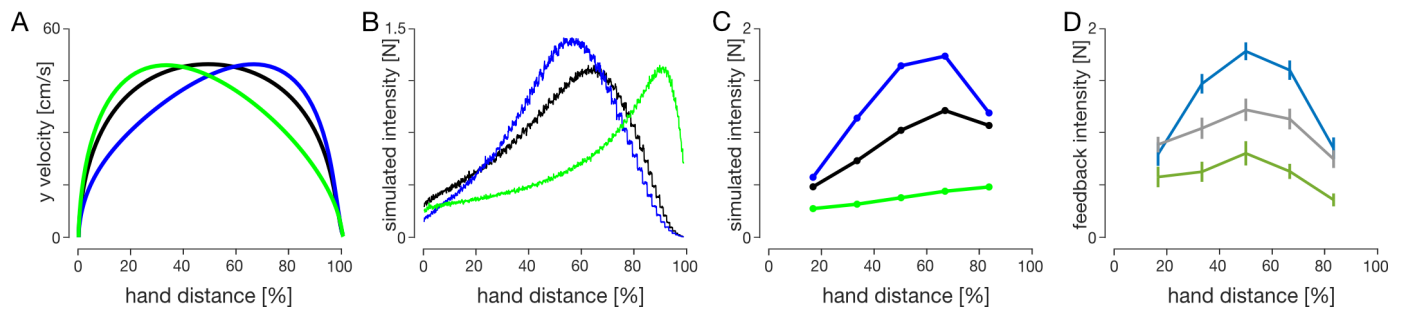


Figure 6. Comparison of feedback intensities between the two OFC models and experimental data. **(A)** Simulated velocity profiles, and **(B)** Simulated feedback intensity profiles of baseline (black), early-peak (green) and late-peak (blue) velocity condition simulations for the classical OFC model. Velocity profiles were obtained by constraining the velocity peak location and magnitude and optimising for movement duration and activation cost function. Simulated feedback intensity profiles were obtained by applying virtual target jumps perpendicular to the movement direction during these movements and calculating the force exerted by the controller in the direction of the target jumps. **(C)** Simulated feedback intensities obtained via the time-to-target OFC model. Pre-perturbation movements were simulated as if no perturbation would occur, in order to keep the controller naive to an upcoming perturbation. At the perturbation onset the remaining movement duration is adjusted to match the mean time-to-target for a similar perturbation onset in human participants (Figure 5B). The velocity profiles for the time-to-target model match the velocity profiles of the classical model, shown in **(A)**. **(D)** Visuomotor feedback intensities recorded in human participants.

120 feedback intensities exists, we mapped visuomotor feedback intensity magnitudes as a linear
121 function of the hand velocity and the cursor velocity. For each experimental condition, we find a
122 different regression slope between the velocity and the feedback intensities regardless of whether
123 this is the cursor or the hand velocity (Figure 3AB). Consistent with our previous results, this
124 difference in slopes is significant for conditions where the hand, but not cursor, movement was
125 different (Figure 3CD). Although feedback intensities increase with increasing velocity in both cursor
126 and hand coordinates, no one coordinate modality could predict the changes in the feedback
127 intensity.

128 To successfully complete each trial, participants were required to reach the target. However,
129 the distance to reach the target is affected by the perturbation onset – later perturbation locations
130 lead to larger correction angles (Figure 4A) and thus longer movement distances (Figure 4B). This
131 effect is clearly seen where the extension of movement distance is enhanced for the perturbations
132 closest to the target, with movement distance extended by almost half a centimetre compared to
133 less than one millimetre for the closest perturbations. Any extension of the movement distance
134 requires an appropriate increase in movement duration. Consequently, participants extended
135 their movement time, with longest durations for perturbations close to the target (Figure 5A). This
136 increase in movement duration increases the time-to-target for these late perturbations (Figure 5B),
137 and now allows sufficient time for the controller to issue any corrective commands.

138 Finite horizon optimal feedback control

139 As optimal control has been suggested to predict the temporal evolution of feedback intensities
140 (*Dimitriou et al. (2013); Liu and Todorov (2007)*), we built two finite-horizon optimal feedback control
141 (OFC) models: the classical model (*Liu and Todorov (2007)*), and a time-to-target model. For the
142 classical model we implemented an OFC (*Todorov (2005)*) to simulate movements with different
143 velocity profiles, similar to the experiments performed by our participants. We extended this
144 classical model to the time-to-target model, by increasing the movement duration after each
145 perturbation onset according to experimental results (Figure 5). For both models we only simulated
146 different hand kinematics for computational ease and as our participants showed little effect of
147 cursor kinematics on their feedback intensities.

148 For both models we controlled the activation cost R to simulate three conditions in which
149 the location of the peak velocity was shifted to match the experimental hand kinematics (Figure
150 6A). Specifically, we solved for the activation cost R and movement duration N by optimising the
151 log-likelihood of our model's peak velocity location and magnitude using Bayesian Adaptive Direct

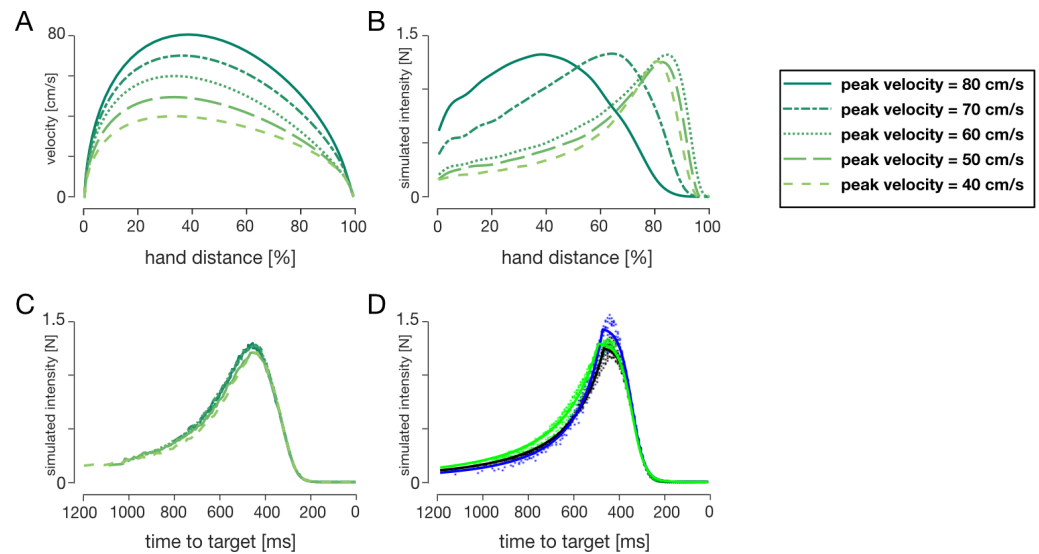


Figure 7. OFC simulations of (A) velocity profiles and (B) simulated feedback intensity profiles for different desired peak velocities (in order from light to dark line colours: 40 cm/s, 50 cm/s, 60 cm/s, 70 cm/s, 80 cm/s). (C) Simulated feedback intensities of (B) re-mapped as a function of time-to-target at the time of target perturbation. (D) Simulated feedback intensities vs time-to-target for the three kinematic conditions over the five peak velocities simulated by OFC (coloured dots). Solid lines represent the tuning curves (Equation 7) fit to the data. Both the tuning curves and the simulated feedback intensity profiles are similar across a variety of different kinematics when expressed as a function of time-to-target.

152 Search (BADs, *Acerbi and Ma (2017)*). The optimised movement durations (mean \pm SEM) were N
153 = 930 ± 0 ms for the baseline condition, N = 1050 ± 10 ms for the late-peak condition and N =
154 = 1130 ± 20 ms for the early-peak condition (10 optimisation runs per condition). In comparison,
155 experimental movement durations were N = 932 ± 30 ms for the baseline condition, N = 1048 ± 47
156 ms for the late-peak condition and 1201 ± 59 ms for the early-peak condition, matching well with
157 the OFC predictions. Overall this shows that specific constraints on the magnitude and location of
158 peak velocity that we imposed on our participants resulted in a modulation of reaching times that
159 matched OFC predictions under the same constraints.

160 For the classical model we estimated simulated feedback intensities by shifting the movement
161 target at each timepoint in the movement and measuring the mean magnitude of the simulated
162 force response over a 130-180 ms time window in the direction of this shift. The simulated feedback
163 intensity profiles follow the same general shape as in human participants – intensity increases
164 from the beginning of the movement and then falls off at the end (Figure 6B). However, the overall
165 profile of these simulated feedback intensities is very different for each of the kinematic conditions.
166 For the early-peak velocity condition, the simulated feedback intensity peaks towards the end of
167 the movement (green line), whereas for the late-peak velocity condition the simulated feedback
168 intensity profile peaks early in the movement (blue line). These simulated feedback intensities do
169 not appropriately capture the modulation of visuomotor feedback intensities in our experimental
170 results. Specifically they predict a temporal shift in the peak intensity that is not present in our
171 participants data, and predict similar peak levels of feedback intensities across all three conditions.
172 While the simulated feedback intensities are qualitatively similar to the experimental results within
173 each condition, overall this model cannot appropriately capture the modulation of visuomotor
174 feedback responses across the conditions.

175 For the time-to-target OFC model, we extended the classical model to account for the different
176 movement durations for each perturbation location (and movement condition) that is seen in the
177 experimental results. After a perturbation, the remaining time-to-target was adjusted to match the
178 experimentally recorded times-to-target for this specific movement, while before the perturbation

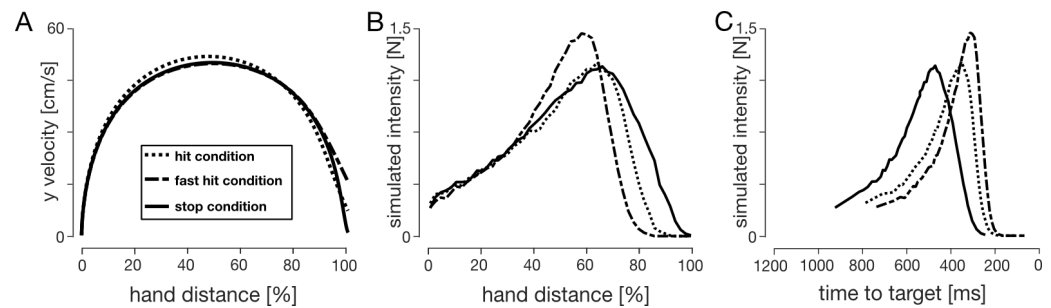


Figure 8. Comparisons between hit and stop instructions. **(A)** Velocity profiles for the stop, hit and fast-hit conditions. **(B)** Simulated feedback intensity profiles as a function of hand position. **(C)** Simulated feedback intensities of **(B)** re-mapped as a function of time-to-target at the time of target perturbation.

179 both the classical model and the time-to-target model were identical. After adjusting for the
180 individual durations of each perturbation condition we are now able to qualitatively replicate the
181 general regulation of feedback intensity profiles for different kinematics using OFC (Figure 6C). In
182 the late-velocity peak condition we predict a general increase in the feedback responses throughout
183 the movement compared to the baseline condition, whereas in the early velocity peak condition we
184 predict a general decrease in these feedback responses compared to the baseline condition. Thus
185 we show that within the OFC the time-to-target is critical for the regulation of feedback responses,
186 and when we take this into account we are able to replicate the feedback intensity modulation of
187 our participants.

188 While in our experiment, we manipulated the time-to-target through skewing the velocity profiles,
189 time-to-target is naturally modified through changing the peak velocity. Therefore, we can further
190 analyse the effect of the time-to-target by calculating the feedback intensities for movements
191 with different peak velocities (Figure 7A). The simulated feedback intensities vary widely across
192 peak velocities, with a shift of peak feedback intensities towards the earlier locations for faster
193 movements (Figure 7B). However, when these distinct simulated feedback intensity profiles are
194 re-mapped as a function of time-to-target, the simulated feedback intensities follow a consistent,
195 albeit non-monotonic, relationship (Figure 7C). This relationship is also consistent over a range of
196 peak velocities across all three kinematic conditions and is well described by a combination of a
197 square-hyperbolic and logistic function (Figure 7D). The squared-hyperbolic arises from the physics
198 of the system: the lateral force necessary to bring a point mass to a target is proportional to $1/t^2$
199 (Materials and Methods, Equation 9). The logistic function simply provides a good fit to the data.
200 Overall our models show that the feedback intensity profiles under OFC are independent of the
201 peak velocity or movement duration. Instead, our simulations suggest that time-to-target is a key
202 variable in regulating visuomotor feedback responses.

203 It has been shown that the optimal controller gains (*Liu and Todorov (2007)*), as well as the
204 visuomotor feedback intensities (*de Brouwer et al. (2017)*; *Knill et al. (2011)*) are influenced by task
205 definition (e.g. instruction to hit the target or stop at the target). Here we simulated the hit, fast
206 hit and stop instructions for our classical model in order to test how it influenced the relation
207 between simulated feedback intensity and time-to-target. Our previous simulations represent the
208 stop instruction. We modified the ω_v and ω_f to simulate the baseline equivalent of hit and fast
209 hit instructions. Specifically, we set $\omega_{v,hit} = \omega_v/4 = 0.05$, $\omega_{f,hit} = \omega_f/4 = 0.005$ for hit instruction,
210 and $\omega_{v,fasthit} = \omega_v/10 = 0.02$, $\omega_{f,fasthit} = \omega_f/10 = 0.002$ for fast hit instruction. As changing the
211 terminal costs also results in a change in peak velocity, we further reduced the desired movement
212 times to $N = 800$ ms for the hit instruction and $N = 750$ ms for fast hit instruction, such that
213 all three peak velocities match (Figure 8A). According to our simulations, such modification of
214 task demands produced different simulated feedback intensity profiles (Figure 8B). However, the
215 intensity relationship with time-to-target maintained the same structural profile independent of
216 the task demand (Figure 8C). Specifically, both the squared-hyperbolic and logistic segments of the

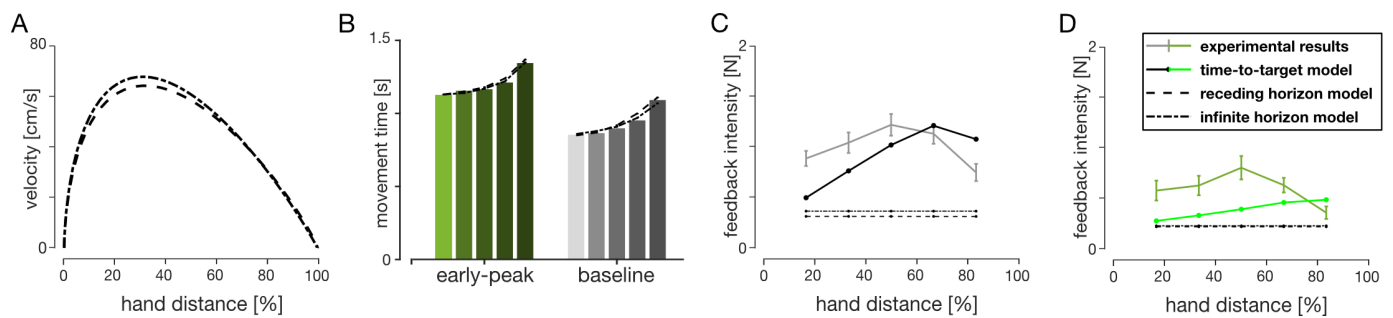


Figure 9. Receding horizon and infinite horizon model simulations. **(A)** Simulated velocity profiles of receding horizon (dashed) and infinite horizon (dot-dashed) models. Both models naturally produce positively skewed velocity profiles, more closely resembling early-peak velocity, rather than the baseline condition. **(B)** Mean experimental movement durations (bar chart) compared to the receding and infinite horizon model predictions. Both models accurately simulate the variations in the reach durations with perturbation location. **(C)** Baseline and **(D)** Early-peak velocity condition simulations for receding horizon, infinite horizon and time-to-target (dot-solid lines) models, compared to the experimental data. Only the time-to-target model predicts different visuomotor feedback response intensities for different perturbation onset locations, while receding and infinite horizon models predict constant intensities. Note that models were not fit to match the intensities, only to qualitatively demonstrate the behaviour.

217 control are still present, although we observe the shift in the temporal location of the crossover
218 point. While each task requires a different pattern of feedback gains (and will therefore produce
219 different responses), variations of the kinematic requirements within a task do not change these
220 gains and therefore do not require recalculation.

221 Receding horizon and infinite horizon control

222 A limitation of the finite-horizon implementation used in classical and time-to-target models is that
223 the variable movement duration (Figure 5) is the model input rather than output. Therefore, in
224 addition to finite-horizon models we also modelled our task in receding and infinite horizon for a
225 single movement condition. Specifically, for the infinite horizon model both state-dependent and
226 regulator costs were kept constant throughout the simulated movement. For the receding horizon
227 model the regulator cost was kept constant, while the state-dependent cost was zero for all but last
228 “foreseeable” state. Such models were expected to simulate the baseline experimental condition,
229 however the resultant velocity profile better resembled the early-peak condition (Figure 9A). As a
230 result, we compared these simulations with both baseline and early-peak velocity condition data
231 and with the time-to-target model simulations (Figure 9B-D).

232 Both receding horizon and infinite horizon LQG models were able to successfully capture the
233 non-linear change in trial durations for different perturbation onsets (Figure 9B) matching the
234 experimental results. In addition, these models also predicted variable times-to-target for the five
235 perturbation onset locations: (700 ms, 660 ms, 620 ms, 600 ms, 580 ms) for the infinite horizon
236 and (690 ms, 640 ms, 610 ms, 610 ms, 600 ms) for the receding horizon. However, neither model
237 showed variation of the simulated feedback intensities for different perturbation onset locations
238 (Figure 9CD) – a result that was present in the experimental data and captured by our time-to-target
239 model. Instead both models predicted constant feedback intensities for all perturbations locations.
240 Therefore neither the receding nor the infinite horizon models are able to explain our experimental
241 results. While both of the approaches can accurately capture the variability in movement duration,
242 only the time-to-target model well describes the behavioural variation in visuomotor feedback
243 responses.

244 Validation of the time-to-target model

245 Overall our simulations suggest that independent of movement kinematics — different temporal
246 position, velocity, and acceleration profiles — the visuomotor feedback intensities follow the same
247 profile with respect to the time-to-target. We further verified how our time-to-target prediction

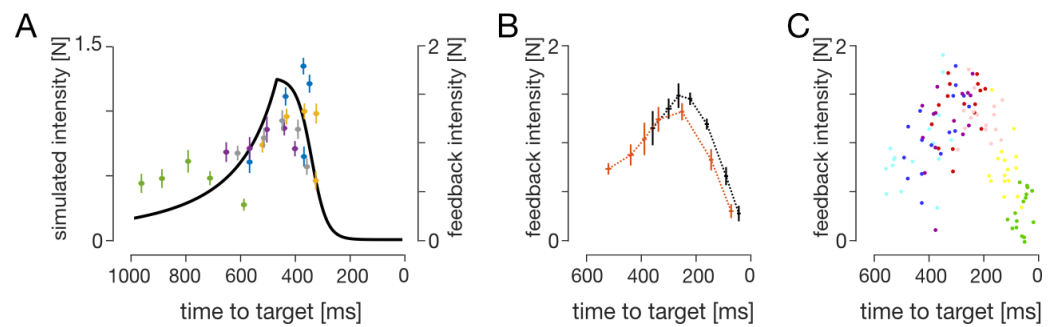


Figure 10. Validation of the time-to-target model. **(A)** Experimental visuomotor feedback intensities for all five experimental conditions (scatter plot) overlaid with the OFC model for the baseline condition, as a function of time-to-target. Error bars represent 1SEM **(B)** Experimental data of the visuomotor feedback intensities of *Dimitriou et al. (2013)*, mapped against the time-to-target. Black and orange traces represent mean participant data for 17.5 cm and 25 cm movement conditions respectively. **(C)** A scatter plot of individual subjects' data from **(B)**. Different colours represent different perturbation onset distances as in *Dimitriou et al. (2013)*.

248 matches our actual experimental results by plotting participants' visuomotor feedback intensities
249 against the average time-to-target for the respective perturbation locations and movement condi-
250 tions (Figure 10A). While we did not specifically fit our time-to-target model to our experimental data,
251 we still see the qualitative similarities between the two. Specifically, the intensities monotonically
252 increase with decreasing time-to-target until the peak (following the squared-hyperbolic function)
253 and then reduce (the logistic function range).

254 Finally, we also compared the prediction of the time-to-target model to independent results
255 from an external data set (*Dimitriou et al. (2013)*). In the article the authors could not rigorously
256 encapsulate both conditions within a simple relationship to movement distance, movement fraction
257 or movement velocity. We plotted visuomotor feedback intensities against time-to-target for
258 two experimental conditions: goal directed reach of 17.5 cm and of 25 cm (Figure 10BC). Two
259 observations can be made from these results. First, the time-to-target model prediction and
260 the experimental data follow the same qualitative features, independent of the target distance
261 (experimental condition). Second, the feedback intensities for both conditions are well explained
262 by a single relationship with time-to-target. All together, both our data and *Dimitriou et al. (2013)*
263 data strongly support our time-to-target model.

264 Discussion

265 Here we examined how movement kinematics regulate visuomotor feedback responses. Partic-
266 ipants extended their movement duration after perturbations to successfully reach the target.
267 In addition, visuomotor feedback responses were modulated when the hand followed different
268 kinematics, but not when the cursor followed different kinematics. In order to better understand
269 this modulation we built four normative models using OFC: a classical finite-horizon OFC (*Liu and*
270 *Todorov (2007)*), a finite-horizon time-to-target adjusted OFC, a receding-horizon OFC (*Guigon et al.*
271 *(2019)*) and an infinite-horizon OFC (*Qian et al. (2013)*). While the classical, receding and infinite
272 horizon models failed to predict the experimental visuomotor feedback response intensities, the
273 time-to-target model qualitatively replicated the visuomotor feedback intensity profile of our par-
274 ticipants. Overall, optimal feedback control models suggested that feedback intensities for each
275 perturbation location depended on the time-to-target rather than distance or velocity. Moreover,
276 this explains why any mismatch between visual and haptic kinematics had no effect on the feedback
277 intensities, as these manipulations did not affect the time-to-target. Simulated feedback intensities
278 under all movements followed the same profile with respect to time-to-target, suggesting a critical
279 role in the regulation of visuomotor feedback responses.

280 Experimentally, our participants exhibited a temporal evolution of visuomotor feedback in-
281 tensities for each condition, confirming the findings of *Dimitriou et al. (2013)*. In addition, we

282 also showed the regulation of visuomotor feedback responses across conditions, allowing us to
283 investigate the underlying mechanism of this temporal evolution. Specifically, our experimental
284 results demonstrated strong regulation of visuomotor feedback intensity profiles with different
285 hand kinematics, but not with different cursor kinematics (Figure 2C). Compared to the baseline
286 condition, in the matched-cursor early-peak velocity condition participants produced longer times-
287 to-target at each perturbation location (Figure 5B), resulting in weaker feedback responses based
288 on the relationship between time-to-target and visuomotor feedback intensities (Figure 10A). The
289 opposite is true for the matched-cursor late-peak velocity condition. As the two matched-hand
290 conditions produced similar times-to-target as the baseline due to similar hand kinematics, we
291 did not observe a different regulation in feedback responses. Therefore, the condition-dependent
292 visuomotor feedback response modulation exhibited by our participants meshes nicely with a
293 control policy whereby the time-to-target regulates the feedback responses.

294 It has long been suggested that we select movements that minimize the noise or endpoint
295 variability (*Harris and Wolpert (1998)*). Within the framework of optimal control, this idea has been
296 expanded to the corrective movements – that is, optimality in reaching movements is achieved
297 in part by minimizing the noise during any corrective response (*Todorov and Jordan (2002)*). As
298 motor noise scales proportionally to muscle activation (*Jones et al. (2002); Hamilton et al. (2004)*),
299 one way of minimising such noise is reducing the peak levels of muscle activation during the
300 correction. Mathematically, the optimal solution to correct any perturbation approximates a
301 constant activation, resulting in a constant force for the whole duration between perturbation
302 onset and target interception. Such a solution assumes that the brain is capable of estimating
303 the remaining duration of the movement (*Benguigui et al. (2003); McIntyre et al. (2001); Zago et al. (2004)*)
304 and that the force follows the squared-hyperbolic relationship to this duration (Equation.
305 9). The parallel can be drawn here between our results and the results of *Oostwoud Wijdenes*
306 *et al. (2011)*, where the authors showed a similar temporal evolution of peak acceleration against
307 the time-to-target in a single forward velocity condition. Our results further show that time-to-
308 target strongly modulates visuomotor feedback responses across a range of different kinematics,
309 consistent with the idea that human participants aim to behave optimally. More specifically, we
310 suggest that, among different optimality variables, the temporal evolution of visuomotor feedback
311 response intensities serves to reduce effects of system noise.

312 Finite-horizon OFC predicts a time beyond which feedback responses are suppressed. Beyond
313 this critical time, a logistic function well describes the relation between time-to-target and feedback
314 responses, with response intensities reducing as the time-to-target decreases. The controller gains
315 at this stage are the most sensitive to acceleration, suggesting a more “behavioural” outcome
316 – the controller is trying to stop, rather than correct errors. The neural recordings in rhesus
317 macaque monkeys’ supplementary motor area and M1 (*Russo et al. (2019)*) show that SMA can
318 signal movement termination as far as 500 ms before the end of the movement. This further
319 suggests that there may be multiple stages within a movement, where our control system might
320 “care” more about error correction in one or movement termination in another. On the other hand,
321 the suppression of responses close to the target leads to undershooting the target. Our participants,
322 however, had to bring the cursor to the target in order to advance to the next trial. As a result, they
323 extended the movement durations post-perturbation to return to the squared-hyperbolic range
324 of control. The control performance of such behaviour is well accounted for by our time-to-target
325 model. Moreover, our time-to-target model also well explained the modulation of visuomotor
326 feedback intensities from an external data set (*Dimitriou et al. (2013)*). However, an important
327 distinction from our study is that in *Dimitriou et al. (2013)* the suppression of feedback responses
328 towards the end of movements would not interfere with reaching the target as perturbation trials
329 were always in a mechanical channel so that no corrections were required. As a result, the times-to-
330 target were shorter and the data clearly exhibits both logistic and squared-hyperbolic segments of
331 the control.

332 A limitation of our time-to-target model is that it takes time-to-target as an input in order to

333 generate feedback intensity predictions, rather than obtain the time-to-target as a model output.
334 As a result, our time-to-target model does not describe exactly how the change in movement geom-
335 etry after the perturbation influences this time-to-target, which in turn regulates the visuomotor
336 feedback responses. On the other hand, both receding and infinite horizon models did predict the
337 movement duration change after perturbations very well, but could not at all describe the changes
338 in visuomotor response intensity. However, utility of movement has recently been used within
339 optimal control to characterise reaching movements (*Rigoux and Guigon (2012); Shadmehr et al.*
340 *(2016)*) in which optimal movement time falls out automatically from a trade-off between reward
341 and effort. With respect to our models, this adds additional complexities to capturing the different
342 movement conditions. Future approaches could attempt to model these results within the utility of
343 movement framework.

344 In addition, our time-to-target model does not directly show the causality of the time-to-target
345 as a control variable for the visuomotor feedback intensities. Particularly, the time-to-target
346 relation to feedback intensity could be a by-product of a more sophisticated control scheme.
347 Additional arguments for the time-to-target control scheme could be two-fold. First, there is
348 evidence that humans are well capable of estimating the time-to-target of a moving stimulus, even
349 if it is accelerating (*Benguigui et al. (2003); McIntyre et al. (2001); Zago et al. (2004)*), indicating that
350 time-to-target is at least an available input for such a controller. Second, while we have tested
351 finite-horizon OFC and two other (receding and infinite horizon) OFCs, only the finite horizon
352 controllers had any effect on the variation of simulated feedback intensities. Importantly, neither
353 the receding nor infinite horizon models use time-to-target as an input to the controller. We posit
354 that this time-to-target control input is the one key difference between the finite and non-finite
355 models and is therefore the simplest explanation for our results.

356 Rapid feedback responses scale with the temporal urgency to correct for mechanical pertur-
357 bations (*Crevecoeur et al. (2013)*). Here we have shown that visuomotor feedback responses also
358 follow a similar regulation, suggesting that these two systems share the same underlying control
359 policy. Our work further extends this finding of Crevecoeur by not just showing that temporal
360 urgency affects feedback responses, but explaining the manner in which these responses are
361 regulated with respect to urgency. That is, here we have shown that for visual perturbations
362 the feedback intensities scale with a squared-hyperbolic of the time-to-target, which is a direct
363 measure of urgency. Moreover, the feedback intensities were rapidly adjusted due to the change in
364 urgency as the task changed. Specifically, when the cursor jumps close to the target, the expected
365 time-to-target is prolonged, and therefore the optimal visuomotor feedback response needs to
366 be adjusted appropriately to this increase in time. Our results show that participants produce a
367 visuomotor response consistent with the actual, post-perturbation, time-to-target, as opposed to
368 the expected time-to-target prior to the perturbation. Therefore, our results not only suggest that
369 similar computations might occur for both stretch and visuomotor feedback response regulation,
370 but also that this regulation originates from task-related optimal feedback control.

371 Our work has shown that simulated feedback intensities from OFC exhibit the same underlying
372 pattern as a function of time-to-target over a wide range of movement kinematics, matching
373 well the feedback intensities of our human participants (Figure 6). As expected, changes in the
374 task goals (e.g. hit versus stop) changed the relation between feedback responses and time-to-
375 target. However, the qualitative features – the squared-hyperbolic and logistic function – remained
376 consistent across these tasks. These results suggest that, for a specific task and known dynamics,
377 we do not need to recalculate the feedback gains prior to each movement, but instead can access
378 the appropriate pattern as a function of the estimated time-to-target in each movement. Therefore
379 gain computation in reaching movements may not be a computationally expensive process, but
380 instead could be part of an evolutionary control strategy that allows for rapid estimation of the
381 appropriate feedback gains. Moreover, the fact that both stretch reflex and visuomotor feedback
382 systems exhibit similar control policies despite different sensory inputs, perhaps only sharing
383 the final output pathway, suggests that this simple feedback pathway may be an evolutionary

384 old system. Indeed, several studies have suggested that visuomotor feedback is controlled via
385 a pathway through the colliculus (*Reynolds and Day (2012); Gu et al. (2018); Corneil et al. (2004)*).
386 Such a system would then only need to be adapted as the dynamics or overall task goals change,
387 allowing for fine tuning of the feedback gains according to changes in the environment (*Franklin*
388 *et al. (2017)*).

389 Our results have shown the connection between the visuomotor feedback response regulation
390 and the time left to complete the movement. Specifically, in our human participants we recorded
391 the increase in the time-to-target after the perturbation onset, which consequently increased the
392 movement durations (Figure 5). This increase was also longer for later perturbations, consistent
393 with previous studies (*Liu and Todorov (2007)*). According to our normative time-to-target OFC
394 model, the time-to-target alone is enough to successfully regulate visuomotor feedback responses
395 as observed in humans. This result was independent of the kinematics of the movement or the
396 onset times of the perturbations. This suggests that there is no recalculation of a control scheme
397 for the rest of the movement after the perturbation, but rather a shift to a different state within
398 the same control scheme. Such findings are consistent with the idea that visuomotor feedback
399 gains are pre-computed before the movement, allowing for faster than voluntary reaction times
400 (*Franklin (2016)*). Moreover, through our results, we gain a deeper insight into how optimal feedback
401 control governs these feedback gains – through a straightforward relationship to the estimated
402 time-to-target, based on physics.

403 **Materials and Methods**

404 **Participants**

405 Eleven right-handed (*Oldfield (1971)*) human participants (5 females; 27.3 ± 4.5 years of age) with
406 no known neurological diseases took part in the experiment. All participants provided written
407 informed consent before participating. All participants except one were naïve to the purpose of
408 the study. Each participant took part in five separate experimental sessions, each of which took
409 approximately 3 hours. One participant was removed from analysis as their kinematic profiles
410 under the five experimental sessions overlapped. The study was approved by the Ethics Committee
411 of the Medical Faculty of the Technical University of Munich.

412 **Experimental setup**

413 Participants performed forward reaching movements to a target while grasping the handle of a
414 robotic manipulandum with their right hand. Participants were seated in an adjustable chair and
415 restrained using a four-point harness. The right arm of participants was supported on an air sled
416 while grasping the handle of a planar robotic interface (vBOT, *Howard et al. (2009)*). A six-axis force
417 transducer (ATI Nano 25; ATI Industrial Automation) measured the end-point forces applied by the
418 participant on the handle. Position and force data were sampled at 1kHz. Visual feedback was
419 provided in the plane of the hand via a computer monitor and a mirror system, such that this
420 system prevented direct visual feedback of the hand and arm. The exact onset time of any visual
421 stimulus presented to the participant was determined from the graphics card refresh signal.

422 Participants initiated each trial by moving the cursor (yellow circle of 1.0 cm diameter) into the
423 start position (grey circle of 1.6 cm diameter) located approximately 25 cm in front of the participant,
424 centred with their body. This start position turned from grey to white once the cursor was within
425 the start position. Once the hand was within the start position for a random delay drawn from
426 a truncated exponential distribution (1.0-2.0 s, mean 1.43 s), a go cue (short beep) was provided
427 signalling participants to initiate a straight reaching movement to the target (red circle of 1.2 cm
428 diameter, located 25.0 cm directly in front of the start position). If participants failed to initiate the
429 movement within 1000 ms the trial was aborted and restarted. Once the cursor was within 0.6
430 cm of the centre of the target, participants were notified by the target changing colour to white.
431 The movement was considered complete when the participants maintained the cursor within this

432 0.6 cm region for 600 ms. If participants did not complete the movement within 4 seconds from
433 first arriving at the start position (e.g. by undershooting or overshooting the target), the movement
434 timed-out and had to be repeated. After each trial, the participant's hand was passively returned by
435 the robot to the start position while visual feedback regarding the success of the previous trial was
436 provided (Figure 11). Movements were self-paced, and short breaks were enforced after every 100
437 trials.

438 **Experimental paradigm**

439 Participants performed the experiment under five different conditions, each performed in a sepa-
440 rate session. In the baseline condition the cursor matched the forward movement of the hand, with
441 a peak velocity in the middle of the movement. In the other four conditions, the cursor location
442 was scaled relative to the hand location in the forward direction, such that the cursor and the hand
443 location matched only at the start and end of the movements (Figure 1). In two of the conditions
444 (matched-hand velocity), the hand velocity matched the baseline condition throughout the move-
445 ment (with the peak in the middle of the movement) but the cursor velocity peaked either earlier
446 (33% of movement distance) or later (66% of movement distance). In the other two conditions
447 (matched-cursor velocity), the cursor velocity was matched to the baseline condition throughout
448 the movement (with the peak in the middle of the movement) but the hand velocity peaked either
449 earlier (33% of movement distance) or later (66% of movement distance). The difference between
450 the cursor velocity and the hand velocity was produced through a linear scaling of the cursor
451 velocity as a function of the forward position (Figure 1A). Specifically, for the two conditions where
452 the position of the peak cursor velocity is earlier than the position of the peak hand velocity (Figure
453 1 top), this scaling was implemented as:

$$\frac{v_c}{v_h} = -0.012d + 1.6, \quad (1)$$

454 where v_c and v_h are cursor and hand velocities respectively, and d is the distance along the
455 movement direction in %. The cursor velocity was therefore manipulated by a linear scaling function
456 such that its velocity is 160% of the hand velocity at the beginning of the movement, linearly
457 decreasing to 40% at the target location (Figure 1 top). For the two conditions where the position of
458 the peak cursor velocity is later than the position of the peak hand velocity (Figure 1 bottom), this
459 scaling was implemented as:

$$\frac{v_c}{v_h} = 0.012d + 0.4 \quad (2)$$

460 such that the velocity gain function linearly increased from 40% hand velocity at the start of the
461 movement to 160% at the end of the movement (Figure 1, bottom). Desired velocity profiles of both
462 the hand and the cursor are shown in Figure 1B for each condition.

463 **Feedback regarding movement kinematics**

464 In all conditions, one of the velocity modalities (cursor or hand) was required to be similar to the
465 baseline velocity profile. Feedback was always provided about this specific velocity modality. Ideal
466 trials were defined as trials in which this peak velocity was between 42 cm/s and 58 cm/s with the
467 peak location between 45% and 55% of the movement distance with no target overshoot. After
468 each trial, visual feedback about the peak velocity and the location at which this peak occurred was
469 provided to the participants graphically (Fig 11). The peak velocity was indicated on the right hand
470 side of the screen with the length of a bar and the velocity target. This bar changed colour from red
471 to green if the velocity was within the ideal range. The location of the peak velocity was indicated as
472 a horizontal line between home and target positions at the exact location it was achieved, along
473 with the ideal range. This line was green when the location of the peak velocity was within the
474 ideal range, and red otherwise. Overshooting the target was defined as the position of the cursor
475 exceeding the centre of the target in the y-coordinate by more than 0.9 cm. If participants reached

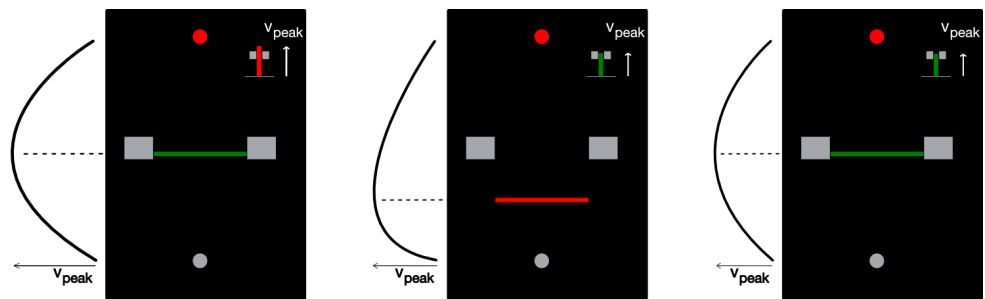


Figure 11. Examples of feedback presented to the participants. Feedback regarding the peak velocity and the timing of the peak velocity was provided after each trial. Large grey blocks indicate the velocity peak location target, while the bar chart at the top-right corner indicates peak y-velocity magnitude. Feedback was provided on the modality (cursor or hand) that matched the baseline. Left: velocity peak location is within the target, but the movement was too fast (unsuccessful trial); middle: velocity peak location is too early, but the movement speed is within the target (unsuccessful trial); right: successful trial.

476 the target while overshooting during the movement, a message indicating the overshoot was shown,
477 no points were scored and an error tone was played in order to discourage further overshoots.

478 Probe trials

479 During each session, probe trials were used to measure the visuomotor feedback intensity – the
480 average strength of corrective motor response to a change in the visual feedback of hand position.
481 To elicit these feedback responses (further visuomotor feedback responses), visual perturbations
482 were initiated laterally (± 2.0 cm) at five different hand distances (4.2, 8.3, 12.5, 16.7, and 20.8 cm)
483 from the start (Figure 2A). In addition a zero amplitude perturbation (cursor matched to the lateral
484 position of the hand) was included, resulting in eleven different probe trials. On these trials the
485 visual perturbations lasted 250 ms, after which the cursor was returned to the lateral location of the
486 hand. The lateral hand position was constrained in a simulated mechanical channel throughout the
487 movement, thereby requiring no correction to reach the target. The simulated mechanical channel
488 was implemented with a stiffness of 4000 N/m and damping of 2 Ns/m acting perpendicularly to the
489 line connecting the start position and the target (Scheidt et al. (2000); Milner and Franklin (2005)),
490 allowing measurement of any lateral forces in response to a visual perturbation.

491 In previous experiments, feedback response intensity gradually decreased during the course of
492 the experiment (Franklin and Wolpert (2008); Franklin et al. (2012)). However, it has been shown
493 that including perturbation trials where the perturbations were maintained until the end of the
494 movement, and where participants had to actively correct for the perturbation to reach the target,
495 prevents this decrease in the feedback intensity (Franklin et al. (2016)). Therefore half of the trials
496 contained the same range of perturbations as the probe trials but where these perturbations were
497 maintained throughout the rest of the trial and participants had to correct for this perturbation.
498 These maintained perturbations have now been used in several studies Franklin et al. (2016, 2017);
499 de Brouwer et al. (2017).

500 Session design

501 Prior to each session, participants performed 100 to 300 training trials in order to learn the specific
502 velocity profiles of the reaching movements. All training trials contained no visual perturbations
503 and were performed in the null force field. The training trials were stopped early once participants
504 achieved an accuracy of 75% over the last 20 trials, and were not used for the analysis.

505 Each session consisted of 40 blocks, where each block consisted of 22 trials performed in
506 a randomized order. Eleven of these 22 trials were probe trials (5 perturbation locations \times 2
507 perturbation directions + zero perturbation condition) performed in the mechanical channel. The
508 other eleven trials consisted of the same perturbations but maintained throughout the trial and

509 performed in the null field. Therefore in each of the five sessions participants performed a total 880
510 trials (440 probe trials). The order of the five different conditions (sessions) was pseudo-randomized
511 and counterbalanced across participants.

512 Data analysis

513 Data was analyzed in MATLAB R2017b and JASP 0.8.2. Force and kinematic time series were low-pass
514 filtered with a tenth-order zero-phase-lag Butterworth filter (40 Hz cutoff). The cursor velocity was
515 calculated by multiplying the hand velocity by the appropriate scaling function. The visuomotor
516 feedback response was measured for each perturbation location as the difference between the
517 force responses to the leftward and rightward perturbations within a block. To measure the
518 visuomotor feedback response intensity (mean force, produced as a response to a fixed-size visual
519 perturbation) this response was averaged over a time window of 180-230 ms, a commonly used time
520 interval for the involuntary visuomotor feedback response (*Franklin and Wolpert (2008); Dimitriou*
521 *et al. (2013); Franklin et al. (2012, 2016)*). In order to compare any differences across the conditions
522 a two-way repeated-measures ANOVA was performed with main effects of condition (5 levels)
523 and perturbation location (5 levels). As a secondary method to frequentist analysis we also used
524 the Bayesian factor analysis (*Adrian E. Raftery and Robert E. Kass (1995)*) to verify our statistical
525 results. Bayesian factor analysis is a method that in addition to the conventional hypothesis testing
526 (evaluating evidence in favour of the alternative hypothesis) allows us to evaluate evidence in favour
527 of the null hypothesis, therefore distinguishing between the rejection of the alternative hypothesis
528 and not enough evidence to accept the alternative hypothesis.

529 Although we used the time window of 180-230 ms to estimate visuomotor feedback intensity,
530 we also verified whether the onset of the visuomotor feedback response in our data is consistent
531 with previously reported values. To estimate this onset time, we first estimated individual onset
532 times for each participant at each perturbation location and movement condition. To do so, we
533 used the Receiver Operator Characteristic (ROC) to estimate where the force reaction to leftwards
534 cursor perturbations deviated from the reaction to rightwards cursor perturbations (*Pruszynski*
535 *et al. (2008)*). For each type of trials we built the ROC curve for the two signals at 1 ms intervals,
536 starting from 50 ms before the perturbation, and calculated the area under this curve (aROC)
537 for each of these points until the aROC exceeded 0.75 for ten consecutive milliseconds. In order
538 to find where the force traces start deviating from each other we then fit a function of the form
539 $\max(0.5, k \times (t - \tau))$ to the aROC curve. The time point where the linear component of this function
540 first overtakes the constant component was taken as the threshold value. Overall, the mean onset
541 times across all conditions and perturbation locations were 138 ± 7 ms (mean + SD), with onset times
542 consistent among movement conditions ($F_{4,36} = 1.410$, $p = 0.25$, and $BF_{10} = 0.105$), perturbation
543 locations ($F_{4,36} = 1.582$, $p = 0.20$, $BF_{10} = 0.252$), and their interactions ($F_{16,144} = 1.350$, $p = 0.176$, and
544 $BF_{10} = 0.005$)

545 Modelling

546 Optimal feedback control

547 In addition to our linear models we implemented two different Optimal Feedback Control (OFC)
548 models: the classical model (*Liu and Todorov (2007)*) and the time-to-target model. In both models
549 we modelled the hand as a point mass of $m = 1.1$ kg and the intrinsic muscle damping as a viscosity
550 $b = 7$ Ns/m. This point mass was controlled in a horizontal plane by two orthogonal force actuators
551 to simulate muscles. These actuators were controlled by the control signal u_t via a first order
552 low-pass filter with a time constant $\tau = 0.05$ s. The state-space representation of the dynamic
553 system used to simulate the reaching movements can be expressed as

$$x_{t+1} = Ax_t + B(I + C)u_t + \xi_t, \quad (3)$$

554 where A is a state transition matrix, B is a control matrix, and C is a 2×2 matrix whose each element
555 is a zero-mean normal distribution representing control-dependent noise. Variables x_t and u_t are

556 state and control at time t respectively. State x_t exists in the Cartesian plane and consists of position
557 \mathbf{p} (2 dimensions), velocity \mathbf{v} (2), force \mathbf{f} (2) and target position \mathbf{p}^* (2). The presence of these four
558 states within the state vector means that the information about all of these states is eventually
559 used for the control. For our simulation purposes we treat the control-independent noise ξ_t as zero.

560 The state of the plant is not directly observable, but has to be estimated from noisy sensory
561 information. We model the observer as

$$y_t = Hx_t + D_t, \quad (4)$$

562 where $H = \text{diag}[1, 1, 1, 1, 1, 0, 0]$ is the observation matrix, and D_t is a diagonal matrix of zero-mean
563 normal distributions representing state-independent observation noise. Therefore, our observer
564 can infer the state information of position, velocity and applied force of the plant, consistent with
565 human participants.

566 The simulated movements were guided by the LQG controller with a state-dependent cost Q , an
567 activation cost R , a reaching time N , and a time step $t = 0.01$ s. However, due to the presence of the
568 control-dependent noise, the estimation and control processes are not anymore separable as in
569 the classic LQG theory. In order to obtain optimal control and Kalman gain matrices we utilised the
570 algorithm proposed by *Todorov and Li (2005)* where control and Kalman gain matrices are iteratively
571 updated until convergence.

572 For both the classical and time-to-target models we simulated three different movement kine-
573 matics representing three different conditions in our experiment – the baseline and the two
574 matched-cursor conditions. The state-dependent cost Q was identical for all three kinematics:

$$Q(t) = \begin{cases} 0, & \text{for } t \neq N \\ (\omega_p(\mathbf{p}(t) - \mathbf{p}^*(t)))^2 + \omega_v\|\mathbf{v}(t)\|^2 + \omega_f\|\mathbf{f}(t)\|^2, & \text{for } t = N \end{cases} \quad (5)$$

575 where $\omega_p = [0.5, 1]$, $\omega_v = 0.02$, and $\omega_f = 2$. The activation cost $R(t) = 0.00001$ was constant throughout
576 the movement for the baseline condition, but was modulated for the two matched-cursor conditions
577 by multiplying it elementwise by a scaling function:

$$R'(t) = \frac{\exp(p \frac{t+q}{r})}{\text{mean}(R')}, \quad (6)$$

578 where p , q and r are constants.

579 Thus, each movement condition only differed from the other two by the profile of this activation
580 cost R , but not by its magnitude. These modified activation costs shift the timing of the peak velocity
581 towards either the beginning or the end of the movement by penalising higher activations at either
582 the end or beginning of the movements respectively. The mean activation cost is kept constant
583 across the conditions resulting in each condition being equally “effortful”. All other simulation
584 parameters were kept constant across the three conditions.

585 Although LQG is a fixed time horizon problem, we did not pre-define the movement duration
586 N . Instead, we obtained the N , and constants p , q and r using Bayesian Adaptive Direct Search
587 (BADs, *Acerbi and Ma (2017)*) to maximise the log-likelihood of the desired peak velocity location
588 and magnitude. We did not fit any other parameters beyond this point. Rather, we analysed our
589 models’ qualitative behaviour compared to human participant data.

590 The classical and the time-to-target models only differed in the way the perturbations were
591 handled. For the classical model, we simulated perturbation trials at every time step t_p by shifting
592 the target x-coordinate by 2 cm at the time $t_p + 120$ ms. This 120 ms delay was used in order to
593 mimic the visuomotor delay in human participants, and was taken from *Liu and Todorov (2007)*. We
594 then averaged the force response of the controller over the time window $[t_p + 130, t_p + 180]$ as an
595 estimate of the simulated feedback responses, equivalent of visuomotor feedback responses in our
596 participants. This means that our simulated feedback responses arise due to separate contributions

597 from the controller position, velocity and acceleration gains. For perturbations occurring at times
598 where the movement is over before the end of this time window, the intensity of this simulated
599 feedback response is set to zero.

600 For the time-to-target model we introduced an extension in the time-to-target after the onset of
601 any perturbation similar to that observed in our participants. Simulated feedback intensities were
602 modelled at five locations, matching the perturbation locations in our experiment to obtain the
603 appropriate increase in time-to-target after each perturbation. In order to simulate the response
604 to perturbations we first extracted the perturbation onset times from movement kinematics by
605 performing an unperturbed movement and recording the timepoint t_p at which this movement
606 passed the perturbation onset location. We then simulated the post-perturbation portion of the
607 movement as a new LQG movement with an initial state matching the state at $t_p + 120$ ms of the
608 unperturbed movement, and movement duration matching the time-to-target recorded in our
609 participants for the particular perturbation. Together this keeps our simulated reaches “naive”
610 to the perturbation prior to its onset and allows the time-to-target of the simulated reaches to
611 match the respective time-to-target of our human participants. Finally, we calculated the simulated
612 feedback intensities as described previously, using a time window [10 ms, 60 ms] of the post-
613 perturbation movement. As in the previous simulations, these simulated feedback responses arise
614 due to separate contributions from the controller position, velocity and acceleration gains.

615 Time-to-target tuning function

616 In order to understand the mechanisms that might underlie the consistent relationship between
617 the simulated feedback intensities and the time-to-target, we fit a mathematical expression to
618 the simulated feedback intensities. We modelled the relationship as the minimum of a squared-
619 hyperbolic function and a logistic function:

$$G(t) = \min \left(\frac{\beta}{(t - t_1)^2}; \frac{\alpha}{1 + \exp \left(-\frac{t - t_0}{\tau} \right)} \right) \quad (7)$$

620 and used BADS to fit this function to our time-to-target-simulated feedback intensity data (Fig. 7C)
621 by optimising the log-likelihood of this fit.

622 While the logistic function was chosen simply as it provided a good fit to the data, the squared-
623 hyperbolic arises from the physics of the system. Specifically, from the kinematic equations of
624 motion for a point mass (m) travelling a distance (d) under the influence of force F , the distance can
625 be expressed as:

$$d = \frac{Ft^2}{2m} + v_0t, \quad (8)$$

626 where $v_0 = 0$ is the lateral velocity at the start of perturbation correction. Rearranging gives:

$$F = \frac{2md}{t^2} \propto \frac{1}{t^2}. \quad (9)$$

627 Hence the lateral force necessary to bring a point mass to the target is proportional to $1/t^2$.

628 Receding horizon OFC

629 In addition to our finite horizon control we also implemented a receding horizon controller (**Guigon**
630 **et al. (2019)**). Irrespectively of the current state of the movement X_t , the receding horizon controller
631 is defined to aim to arrive at the target at time $t + T_h$. In essence, such controller is therefore not
632 different from the finite horizon controller in its implementation for a single state of the movement.
633 We implemented the receding horizon controller by iterating a finite horizon controller described
634 previously, but with the $T_h = 500$ ms, and Q and R costs scaled from the finite horizon model to fit
635 the movement duration. For each iteration we recorded the next movement state (10 ms away
636 from the initial state), and used that as the initial state for the next iteration. This process was

637 repeated until the cursor was within the distance of 0.4 cm from the target position, and remained
638 there without overshooting for 600 ms.

639 Simulating differently skewed velocity profiles within the framework of receding-horizon control
640 is non-trivial. As a result, we chose to only model one, the baseline, experimental condition, where
641 the activation cost R is constant within the movement. Therefore we chose the costs

$$Q(t) = \begin{cases} 0, & \text{for } t \neq T_h \\ \omega_p(\mathbf{p}(t) - \mathbf{p}^*(t))^2 + \omega_v\|\mathbf{v}(t)\|^2 + \omega_f\|\mathbf{f}(t)\|^2, & \text{for } t = T_h \end{cases} \quad (10)$$

642 where $\omega_p = [5, 5]$, $\omega_v = 0.05$, and $\omega_f = 5$. and the activation cost $R = 0.000003$. The values were
643 selected so that the movement durations, produced by the receding-horizon model would match
644 the experimental durations for the baseline condition (Figure 5A). However, the resultant velocity
645 profiles of this model more closely resembled those of the early-peak velocity condition, than those
646 of the baseline. To account for any effects of the velocity profile we also fit the costs so the model
647 prediction of movement durations matched the durations of the early-peak velocity condition.
648 For this simulation we selected $\omega_p = [0.7, 0.7]$, $\omega_v = 0.007$, and $\omega_f = 0.7$, while the activation cost
649 remained unchanged.

650 In this model we introduced the simulated perturbation by shifting the target position by 2 cm
651 at 120 ms after the y-coordinate of the movement passed the perturbation onset location. We only
652 simulated the perturbations matching our experimental conditions—lateral 2 cm cursor jumps, with
653 the onset at five evenly distributed forward distances. We calculated simulated feedback intensities
654 the same way as for the classical and time-to-target models.

655 Infinite horizon OFC

656 We implemented the infinite horizon OFC to control our simulated hand based on the previous
657 work of *Qian et al. (2013)*. Specifically, we calculated the control gain matrix L , and Kalman gain
658 matrix K to control the same system as in the previous models. We chose the state-dependent
659 costs $\omega_p = [1, 1]$, $\omega_v = 0.02$, and $\omega_f = 0$ for the baseline condition simulation, and $\omega_p = [0.35, 0.35]$,
660 $\omega_v = 0.007$, and $\omega_f = 0$ for the early-peak condition simulation. For both conditions the activation
661 cost $R=0.002$ was kept the same. The protocol of simulating the mean trajectories, feedback
662 responses and their intensities was otherwise identical to the receding horizon simulations.

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