

1 **Functional ultrasound speckle decorrelation-based velocimetry of the brain**

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12 **Keywords:** functional ultrasound velocimetry, field autocorrelation function, brain imaging,  
13 cerebral blood flow velocity

14  
15 **Abstract:**

16 A high-speed, contrast free, quantitative ultrasound velocimetry (vUS) for blood flow velocity  
17 imaging throughout the rodent brain is developed based on the normalized first order temporal  
18 autocorrelation function of the ultrasound field signal. vUS is able to quantify blood flow velocity  
19 in both transverse and axial directions, and is validated with numerical simulation, phantom  
20 experiments, and *in vivo* measurements. The functional imaging ability of vUS is demonstrated by  
21 monitoring blood flow velocity changes during whisker stimulation in awake mice. Compared to  
22 existing power Doppler and color Doppler-based functional ultrasound imaging techniques, vUS  
23 shows quantitative accuracy in estimating both axial and transverse flow speeds and resistance to  
24 acoustic attenuation and high frequency noise.

## 25 **1. Introduction**

26 Functional quantitative *in vivo* imaging of the entire brain with high spatial and temporal resolution  
27 remains an open quest in biomedical imaging. Current available methods are limited either by  
28 shallow penetration of optical microscopies that only allow imaging of superficial cortical layers,  
29 or by low spatiotemporal resolution such as functional magnetic resonance imaging or positron  
30 emission tomography. Ultrasound-based blood flow imaging techniques hold the promise to fulfill  
31 the unmet needs<sup>[1,2]</sup>, particularly with the emerging implementation of ultrafast ultrasound plane  
32 wave emission<sup>[3]</sup> which paves the way for ultrasound to be applied for functional cerebral  
33 hemodynamic imaging of the entire rodent brain with 10-100  $\mu m$  resolution.

34 Since the introduction of ultrafast plane wave emission-based Power Doppler functional ultrasound  
35 imaging (PD-fUS)<sup>[4]</sup>, an increasing number of studies are exploiting the capabilities of PD-fUS for  
36 functional brain imaging studies<sup>[5-7]</sup>. However, the exact relationship between the PD-fUS signal  
37 and the underlying physiological parameters is quite complex as the PD-fUS signal is also affected  
38 by the acoustic attenuation, beam pattern, clutter rejection and flow speed, in addition to the blood  
39 volume fraction and hematocrit<sup>[8,9]</sup>. On the other hand, ultrasound Color Doppler (CD-fUS) is able  
40 to measure a specific physiological parameter of the axial blood flow velocity but suffers from  
41 unstable estimations of mean speed due to the presence of noise and from incorrect estimation if  
42 opposite flows exist within the measurement voxel<sup>[2,4,10-12]</sup>. The microbubble tracking-based  
43 ultrasound localization microscopy (ULM<sup>[13]</sup>) method is able to map the whole mouse brain  
44 vasculature (coronal plane) and quantify the in-plane blood flow velocity (vULM<sup>[13,14]</sup>) with  $\sim 10$   
45  $\mu m$  resolution. However, it suffers from a fundamental limitation of low temporal resolution as it  
46 requires extended data acquisition periods ( $\sim 150$  seconds for 75,000 images<sup>[13]</sup>) to accumulate

47 sufficient microbubble events to form a single vascular image and corresponding velocity map,  
48 limiting its potential for functional brain imaging studies.

49 Here, we report a novel ultrasound speckle decorrelation-based velocimetry (vUS) method for  
50 blood flow velocity image of the rodent brain that overcomes the aforementioned limitations. We  
51 derived vUS theory which shows that the ultrasound field signal decorrelation in small vessels is  
52 not only determined by flow speed but also the axial velocity gradient and a phase term due to axial  
53 movement. We further developed a comprehensive experimental implementation and data  
54 processing methodology to apply vUS for blood flow velocity imaging of the rodent brain with  
55 high spatiotemporal resolution and without the need for exogenous contrast. We validated vUS  
56 with numerical simulations, phantom experiments, and *in vivo* measurements, and demonstrated  
57 the functional imaging ability of vUS by quantifying blood flow velocity changes during whisker  
58 stimulation in awake mice. We further show its advantage over PD-fUS and CD-fUS in terms of  
59 quantitative accuracy in estimating axial and transverse flow speeds and its resistance to acoustic  
60 attenuation and high frequency noise through phantom and *in vivo* measurements.

## 61 2. Results

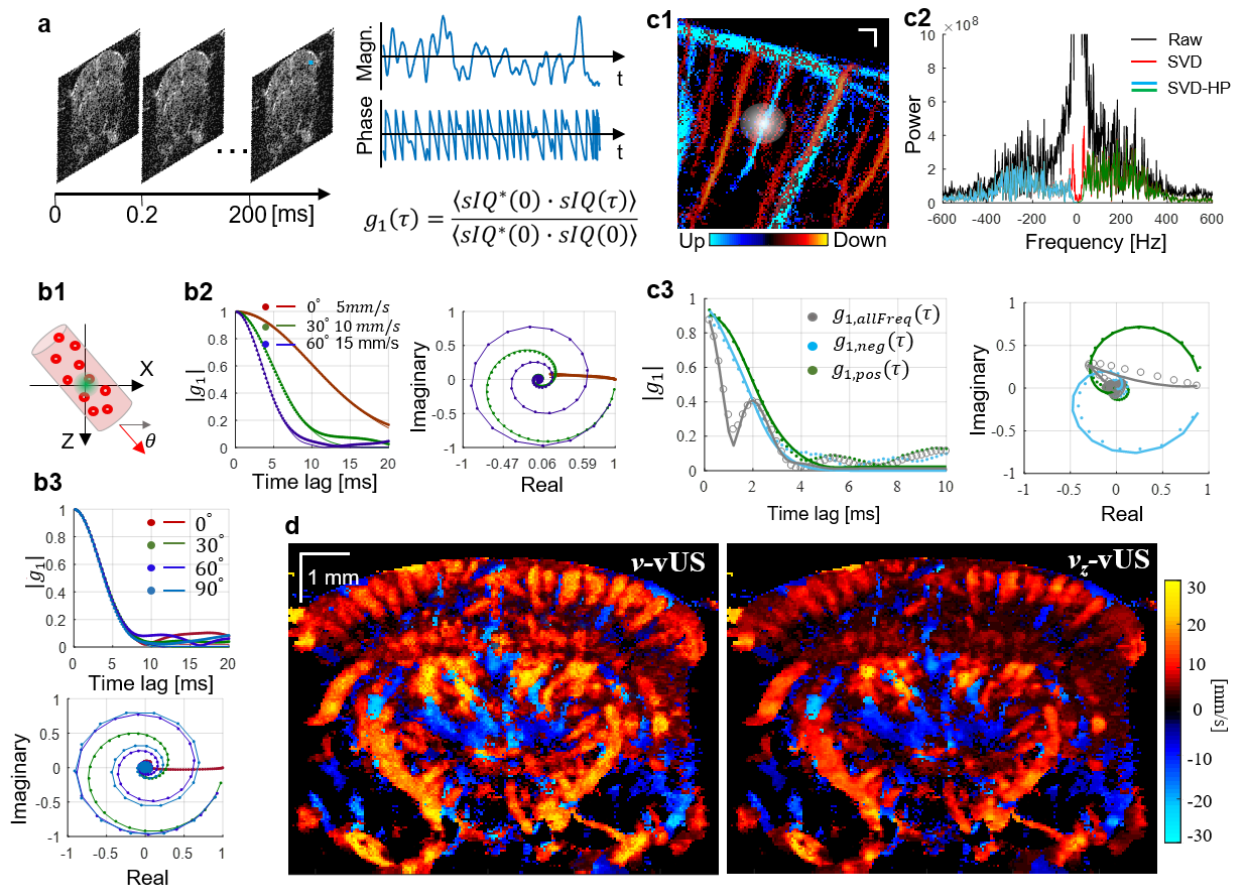
### 62 2.1. vUS theory

63 The time varying ultrasound signal detected from a measurement voxel at time  $t$  can be considered  
64 as the integration of all moving point scatters within the voxel, and the ultrasound pressure arising  
65 from a given voxel can thus be written as,

$$66 \quad sIQ(x_0, y_0, z_0, t) = R \sum_{i_s}^{N_s} e^{-\frac{(x_{i_s}(t)-x_0)^2}{2\sigma_x^2} - \frac{(y_{i_s}(t)-y_0)^2}{2\sigma_y^2} - \frac{(z_{i_s}(t)-z_0)^2}{2\sigma_z^2}} e^{i2k_0(z_{i_s}(t)-z_0)} \quad (1)$$

67 where, sIQ is the complex ultrasound quadrature signal of the moving particles of the voxel;  $R$  is  
68 the reflection factor;  $i_s$  is the index of the  $i^{th}$  scatterer;  $N_s$  is the total number of scatterers within

69 the voxel;  $(x_{i_s}, y_{i_s}, z_{i_s})$  is the position of the  $i_s$  scatter;  $(x_0, y_0, z_0)$  is the central position of the  
 70 measurement voxel;  $\sigma_x, \sigma_y$ , and  $\sigma_z$  are the Gaussian profile width at the  $1/e$  value of the maximum  
 71 intensity of the point spread function (PSF) in  $x, y$ , and  $z$  directions, respectively; and  $k_0$  is the  
 72 wave number of the central frequency of the transducer. In **Equation 1**, we assumed that all scatter  
 73 points have the same reflection factor.



75 **Figure 1** Principle of ultrasound field speckle decorrelation-based velocimetry (vUS). (a) A time series of  
 76 a high frame rate complex ultrasound quadrature signal after bulk motion rejection ( $sIQ(t)$ ) was used for  
 77  $g_1(\tau)$  calculation. (b) Characteristics of  $g_1(\tau)$ ; (b1) Scatterers flow through the measurement voxel at an  
 78 angle  $\theta$ ; Magnitude decorrelation of  $|g_1(\tau)|$  and field decorrelation of  $g_1(\tau)$  in the complex plane at (b2)  
 79 different angles with different speeds and (b3) different angles with the same speed ( $v_0 = 15$  mm/s). (c1)  
 80 ULM measurement shows the microvasculature network in the brain; the white diffuse spot illustrates the

81 ultrasound point spread function; (c2) Frequency power spectrum from *in vivo* data where descending and  
82 ascending vessels were observed in the same measurement voxel; (c3)  $g_1(\tau)$  calculated using whole  
83 frequency signal (gray circles), negative frequency signal (cyan dots), and positive frequency signal (green  
84 dots), respectively. (d) Representative total velocity map and axial velocity map reconstructed with vUS of  
85 a mouse brain; descending flow map is overlapped on the ascending flow map. The solid lines in (b&c) are  
86 the fitted  $g_1(\tau)$  using **Equation 3**.

87 As shown in **Figure 1a**, the movement of particles will cause the detected ultrasound field signal  
88 to fluctuate in both magnitude and phase. This movement can be quantified based on the dynamic  
89 analysis theory of the normalized first-order field temporal autocorrelation function ( $g_1(\tau)$ ).  $g_1(\tau)$   
90 of a time varying ultrasound signal for a measurement voxel is given by,

$$91 \quad g_1(\tau) = E \left[ \frac{\langle sIQ^*(t)sIQ(t+\tau) \rangle_t}{\langle sIQ^*(t)sIQ(t) \rangle_t} \right] \quad (2)$$

92 where,  $\tau$  is the time lag;  $E[\dots]$  indicates the average over random initial positions;  $\langle \dots \rangle_t$  represents  
93 an ensemble temporal average; sIQ is the clutter rejected ultrasound quadrature signal; and \* is the  
94 complex conjugate. **Figure 1b** illustrates the major characteristics of  $g_1(\tau)$ . Briefly, 1)  $g_1(\tau)$   
95 decays faster for scattering particles flowing with higher speeds, 2)  $g_1(\tau)$  rotates and decays to (0,  
96 0) in the complex plane, and 3) different flow angle has different decorrelation path in the complex  
97 plane, as shown in **Figure 1b2**. The rotating decorrelation in the complex plane is caused by the  
98 phase change due to axial movement. As shown in **Figure 1b3**, flows with the same total speed but  
99 in different angles have the same magnitude decorrelation (left panel) but different ‘rotation paths’  
100 in the complex plane (right panel). This feature gives  $g_1(\tau)$  analysis the ability to recover both  
101 axial velocity component and total flow speed.

102 When imaging the cerebral vasculature, the blood vessel diameter is usually less than the ultrasound  
103 system point spread function as indicated by **Figure 1c1**. In this case, the group velocity and  
104 velocity distribution must be taken into account as the relative movement of the scattering particles

105 will result in additional decorrelation<sup>[15]</sup>. To simplify the derivation, we used a Gaussian speed  
106 distribution where,  $v_{gp}$  is the group velocity; and  $\sigma_v$  describes the velocity distribution, and we  
107 finally arrive at,

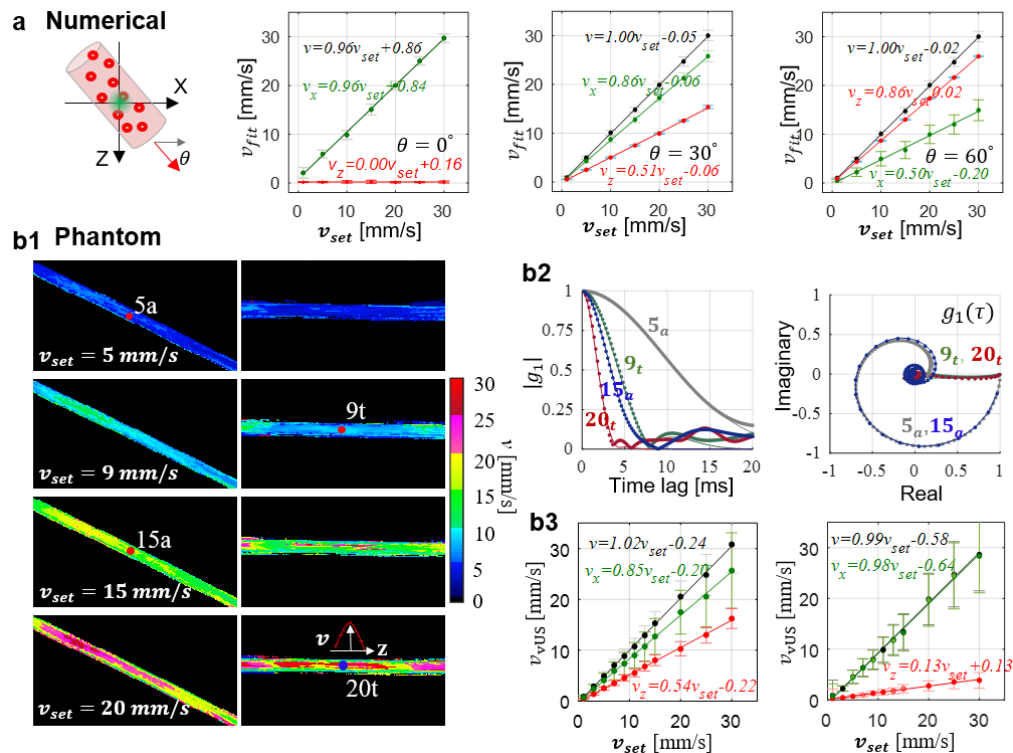
$$108 \quad g_1(\tau) = e^{-\frac{(v_{xgp}\tau)^2}{4\sigma_x^2} - \frac{(v_{ygp}\tau)^2}{4\sigma_y^2} - \frac{(v_{zgp}\tau)^2}{4\sigma_z^2}} e^{-\sigma_{vz}^2(k_0\tau)^2} e^{i2k_0\tau v_{zgp}} \quad (3)$$

109 From **Equation 3**, we note that in addition to flow speed, the axial velocity distribution  $\sigma_{vz}$  also  
110 contributes to the magnitude decorrelation, and the axial velocity component leads to a phase term  
111 in  $g_1(\tau)$  decorrelation. For details regarding the theoretical derivation, please refer to the  
112 **Experimental Section-vUS theory derivation**.

113 In addition, we noticed from the *in vivo* data that it's common to have opposite flows present in the  
114 same measurement voxel when imaging the rodent brain, as shown in **Figure 1c1**. In this case,  
115  $g_1(\tau)$  is a mix of dynamics of opposite flows and behaves very differently from that of the single  
116 direction flow as can be observed from **Figs. 1b2 vs c3** (gray circles). In addition, we observed that  
117 the majority of the mouse cerebral blood vessels contain an axial velocity component to the flow.  
118 This axial flow component causes the frequency spectrum to shift to negative values if the flow is  
119 away from the transducer, and positive if the flow is towards the transducer. Thus, we used a  
120 directional filter (positive-negative frequency separation) method to obtain the positive frequency  
121 and negative frequency signals for the  $g_1(\tau)$  calculation, as shown in **Figure 1c2**.

122 To implement the vUS technology, we developed a comprehensive vUS data acquisition and  
123 processing method (**Materials and Methods-vUS implementation** and **Figure S1**). **Figure 1d**  
124 shows representative in-plane total velocity and axial velocity maps of a mouse brain reconstructed  
125 by vUS. The descending flow velocity map which is reconstructed from the negative frequency  
126 component ( $SIQ_{neg}$ ) is overlapped on the ascending flow velocity map which is obtained from the  
127 positive frequency component ( $SIQ_{pos}$ ). Like the existing PD-fUS and CD-fUS techniques, vUS

128 has an in-plane spatial resolution of  $\sim 100 \mu\text{m}$  which is determined by the ultrasound system  
 129 acquisition parameters. **Figure S2** shows more vUS results at different coronal planes.  
 130 **2.2. Validation of vUS**  
 131 The numerical simulation validation (details in **Materials and Methods**) results shown in **Figure**  
 132 **2a** suggest that the vUS reconstructed total velocity ( $v$ ), transverse velocity component ( $v_x$ ) and  
 133 axial velocity component ( $v_z$ ) agree well with preset speeds and angles. It is worth noting that vUS  
 134 is capable of measuring transverse flows (i.e.  $\theta = 0^\circ$ ) and differentiating the axial velocity  
 135 component from the transverse velocity component for the angled flows, as shown by results from  
 136 flow angle  $\theta = 30^\circ$  and  $\theta = 60^\circ$ . For all simulation results, the correlation coefficient between  
 137  $v_{set}$  and  $v_{fit\_mean}$  were  $r > 0.99$  with  $p < 0.001$ .



138  
 139 **Figure 2** vUS numerical and phantom validation. (a) Numerical simulation validation with different flowing  
 140 angles and speeds. Error bars: standard deviation. (b) Phantom validation of blood flowing through angled

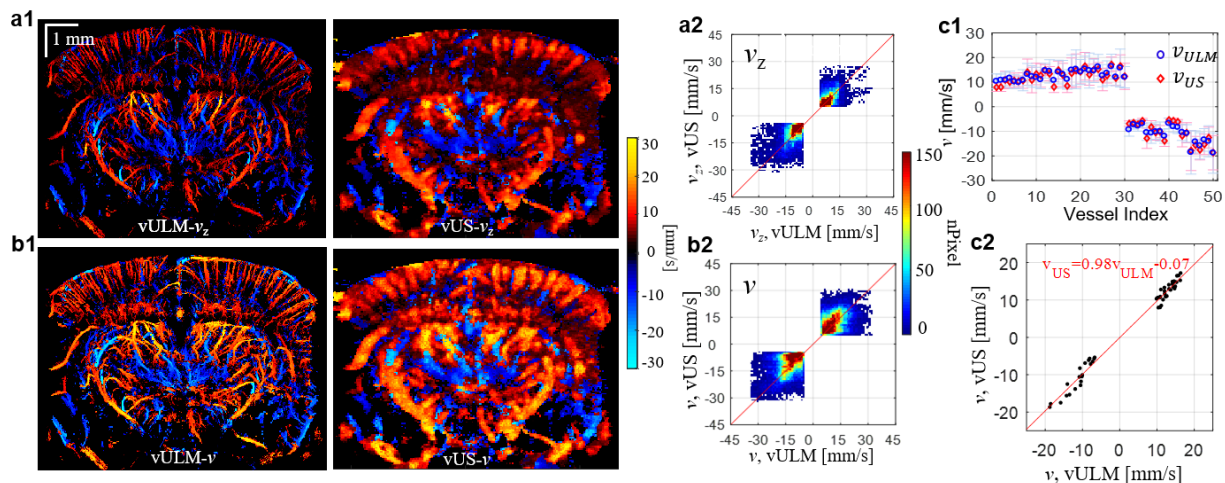
141 and transverse positioned micro tubes (inner diameter  $580\ \mu\text{m}$ ). (b1) vUS reconstructed velocity maps of  
142 angled and transverse flows at different speeds. The inset in the right bottom panel shows the cross sectional  
143 laminar velocity profile of the transverse flow. (b2) Experimental  $g_1(\tau)$  (dots) and corresponding vUS  
144 fit results (solid lines) for both angled and transverse flows at different speeds. (b3) Results of vUS  
145 ( $v$ ,  $v_x$  and  $v_z$ ) for transverse flow ( $\theta \approx 0^\circ$ , left) and angled flow ( $\theta \approx 30^\circ$ , right) . Error bars: standard  
146 deviation.

147 The phantom validation experiments (details in **Materials and Methods**) were performed with  
148 blood samples flowing through a micro plastic tube buried within a static agarose phantom, as  
149 shown in **Figure 2b**. **Figure 2b1** shows the velocity maps of both angled and transverse flows at  
150 preset speeds of 5, 9, 15, and 20 mm/s. A laminar velocity profile was observed, particularly for  
151 higher flow speeds, as indicated in the inset of **Figure 2b1**. **Figure 2b2** shows the experimental  
152 (dots) and vUS fitted  $g_1(\tau)$ , from which we see that  $g_1(\tau)$  decays faster for higher speeds, and, as  
153 shown in the complex plane,  $g_1(\tau)$  rotates and decays to (0, 0) for angled flows ( $5_a$  and  $15_a$ ) which  
154 is due to the axial velocity component inducing a phase shift as indicated in **Equation 3**. Different  
155 flow angles will have different ‘rotation paths’ in the complex plane. **Figure 2b3** shows the vUS  
156 reconstructed results compared to preset speeds, from which we note that the vUS measurements  
157 of total speed agree well with the preset speeds even for speeds as low as 1 mm/s for both transverse  
158 and angled flows. The correlation coefficient between  $v_{set}$  and  $v_{fit\_mean}$  for transverse and angled  
159 flows were  $r > 0.99$  with  $p < 0.001$ . **Figure S3** presents all phantom experiment results obtained with  
160 the vUS, CD-fUS, and PD-fUS analysis methods.

161 We further performed *in vivo* validation by comparing the velocity measured with ultrasound  
162 localization microscopy velocimetry (vULM, **Materials and Methods**) against vUS, as shown in  
163 **Figure 3**. We note that the measured axial velocity (**Figure 3a1**) and total velocity (**Figure 3b1**)  
164 agree well between vUS and vULM. The weighted scatter plots of all nonzero pixels between vUS



165 and vULM in **Figure 3a2&b2** indicate that the vUS measurement is highly correlated with the  
166 vULM measurement. We further compared the mean velocity of 50 vessels marked in **Figure S4**  
167 between vULM and vUS. **Figure 3c1** shows the mean velocity and standard deviation measured  
168 with vULM (blue) and vUS (red) of the 50 vessels. **Figure 3c2** shows the scatter plot of the mean  
169 velocity of the 50 vessels measured with vULM and vUS. We note that the mean value of the 50  
170 vessels agree well between vULM and vUS measurements with a linear relationship of  $v_{z_{vUS}} =$   
171  $0.98v_{z_{vULM}} - 0.07$  mm/s, indicating the accuracy of vUS for *in vivo* blood flow velocity imaging  
172 within the rodent brain.

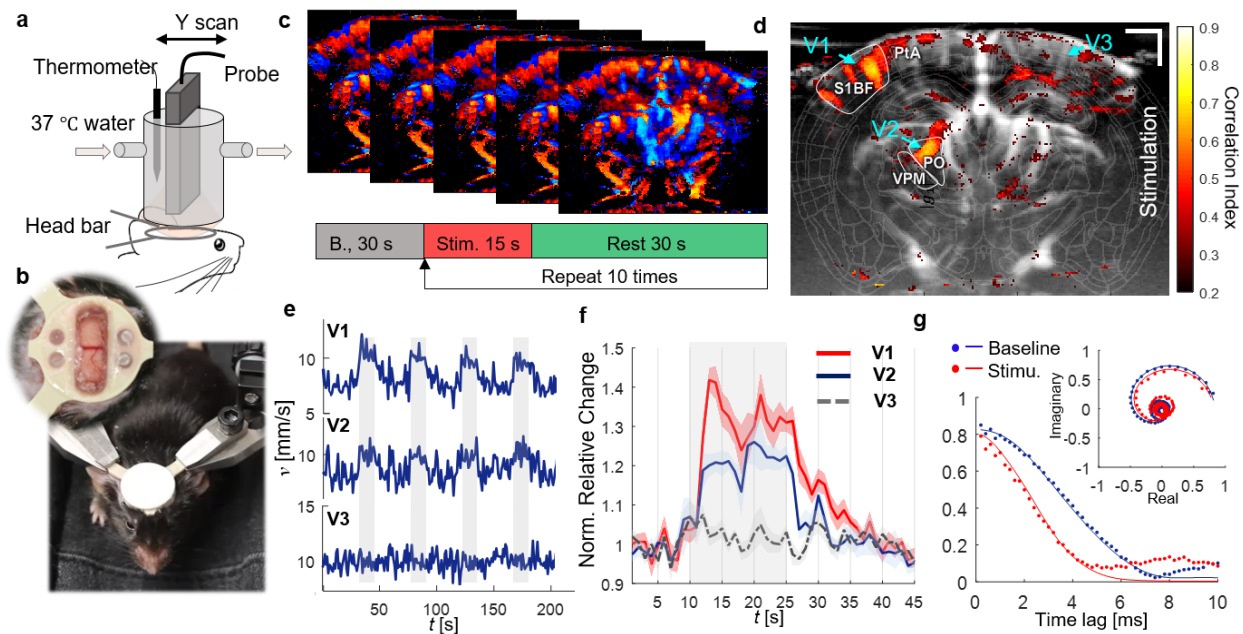


173  
174 **Figure 3** *in vivo* validation between vULM and vUS of axial velocity (a) and total velocity (b). (a2) and (b2)  
175 are pixel-to-pixel weighted scatter plot of common pixels of vULM and vUS with value  $|v| > 3$  mm/s. (c1)  
176 Mean velocity and standard deviation measured with vULM (blue) and vUS (red) of 50 vessels marked in  
177 Supplementary Figure 4a. (c2) Cross correlation of the mean total velocity of the 50 vessels between vULM  
178 and vUS ( $r=0.984$ ,  $p<0.001$ ).

### 179 2.3. Blood flow velocity change evoked by whisker stimulation

180 To demonstrate the functional imaging capability of vUS, we measured the blood flow velocity  
181 response to whisker stimulation. We developed an animal preparation protocol using a

182 polymethylpentene (PMP) film<sup>[6]</sup> with a custom designed headbar for chronic ultrasound imaging  
183 in awake mice (**Materials and Methods**), as shown in **Figure 4a&b**. Following the published  
184 whisker stimulation protocol used in a previous PD-fUS study<sup>[4]</sup>, we used a stimulation pattern that  
185 consists of 30 s baseline followed by 10 trials of 15 s stimulation and with a 45 s interstimulus  
186 interval, as shown in **Figure 4c**. The vUS images were acquired at a rate of 1 frame/s.



187  
188 **Figure 4** vUS of functional brain activation in awake mice. (a) Experimental setup. (b) Photos showing the  
189 trained mouse for awake-head fixed ultrasound imaging; inset: a PMP film protected cranial window was  
190 prepared in the center of the head bar for ultrasound imaging. (c) Whisker stimulation protocol and the vUS  
191 images were acquired at 1 frame/s. (d) Activation map in response to the mouse's left whisker stimulation.  
192 S1BF: Primary somatosensory barrel field; PO: Posterior complex of the thalamus; VPM: Ventral  
193 posteromedial nucleus of the thalamus; PtA: Posterior parietal association. The ROIs were identified  
194 according to Allen Mouse Brain Atlas<sup>(16)</sup>. (e) First 4 trials of blood flow velocity time course of vessels  
195 V1, V2, and V3 as marked in (d). The voxels of the three vessel ROIs were selected with absolute velocity  
196 value greater than 3 mm/s. Gray shades indicate when stimulation was on. (f) Average blood flow velocity  
197 relative change of the 10 trials for the three vessels. Error bar: standard error of the mean. (g) Representative

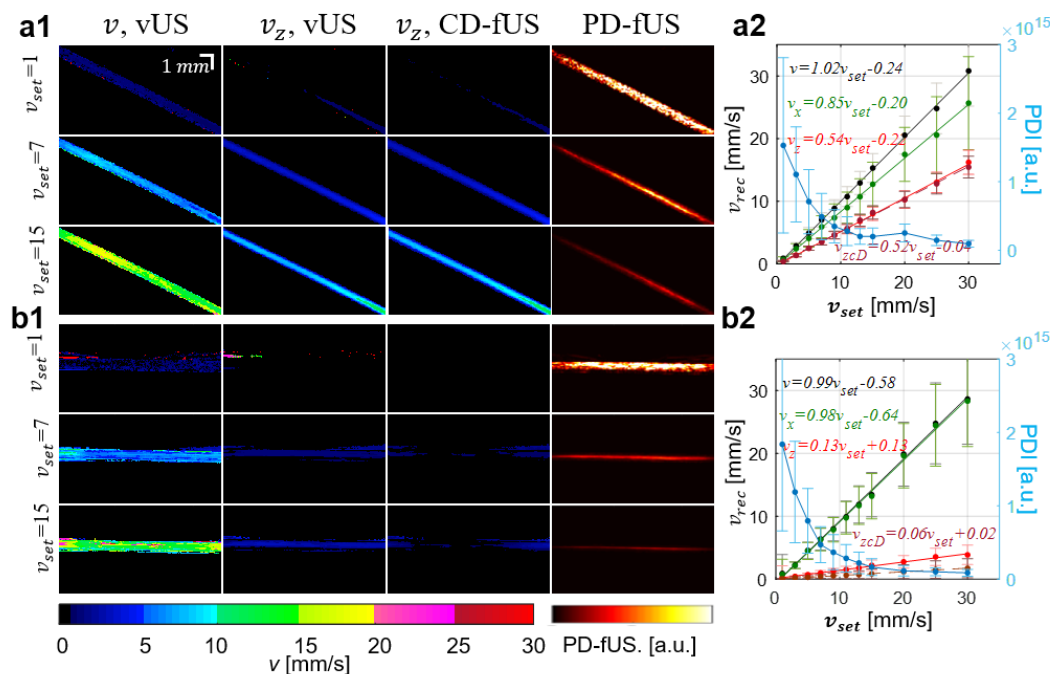
198  $g_1(\tau)$  from baseline (blue) and under stimulation (red) for the same pixel within V1. Solid lines: vUS fitted  
199  $g_1(\tau)$ . Inset:  $g_1(\tau)$  in complex plane.

200 **Figure 4d** shows the correlation coefficient map between the blood flow velocity measured with  
201 vUS and the stimulation pattern. We note that in addition to the significant activation of vessels in  
202 the primary somatosensory barrel field (BF), the blood vessel flowing through the posterior  
203 complex (PO) and ventral posteromedial nucleus (VPM) of the thalamus also exhibited activation.  
204 Importantly, in addition to identifying significantly activated regions, vUS goes further and  
205 provides quantitative estimates of the evoked changes in the absolute flow velocity. The velocity  
206 time courses and velocity relative change averaged over the 10 trials of vessels V1 and V2 indicate  
207 robust blood flow velocity increases in response to the stimulation as shown in **Figs. 4e&f**. The  
208 time course of vessel V3 on the ipsilateral cortex of the stimulation was plotted as a control region,  
209 which shows no correlation with the stimulation. The **Supplemental Video 1** shows the relative  
210 blood flow velocity changes of the whole recording. We further compared the  $g_1(\tau)$  for baseline  
211 and under stimulation of the same spatial pixel in V1, as shown in **Figure 4g**. It is evident that  
212  $g_1(\tau)$  decays faster when under stimulation compared to that during the baseline, indicative of  
213 faster dynamics, i.e. elevated blood flow speed in response to whisker stimulation. **Figure S5** shows  
214 more results of whisker stimulation experiments. Following the stimulation pattern commonly used  
215 in optical functional studies<sup>[16]</sup>, we used vUS to detect the cerebral blood flow velocity change in  
216 response to a 5 s whisker stimulation with a 25 s interstimulus interval, as shown in **Figure S5b**,  
217 and see that the measured blood flow velocity increases in response to the 5 s stimulation, indicating  
218 vUS is also sensitive to short duration stimulation evoked cerebral hemodynamic changes.

#### 219 **2.4. Comparison of vUS with PD-fUS and CD-fUS**

220 The data set acquired for the vUS calculation can also be used for PD-fUS and CD-fUS data  
221 processing, so there can be a direct comparison of the different approaches. The advantages of vUS

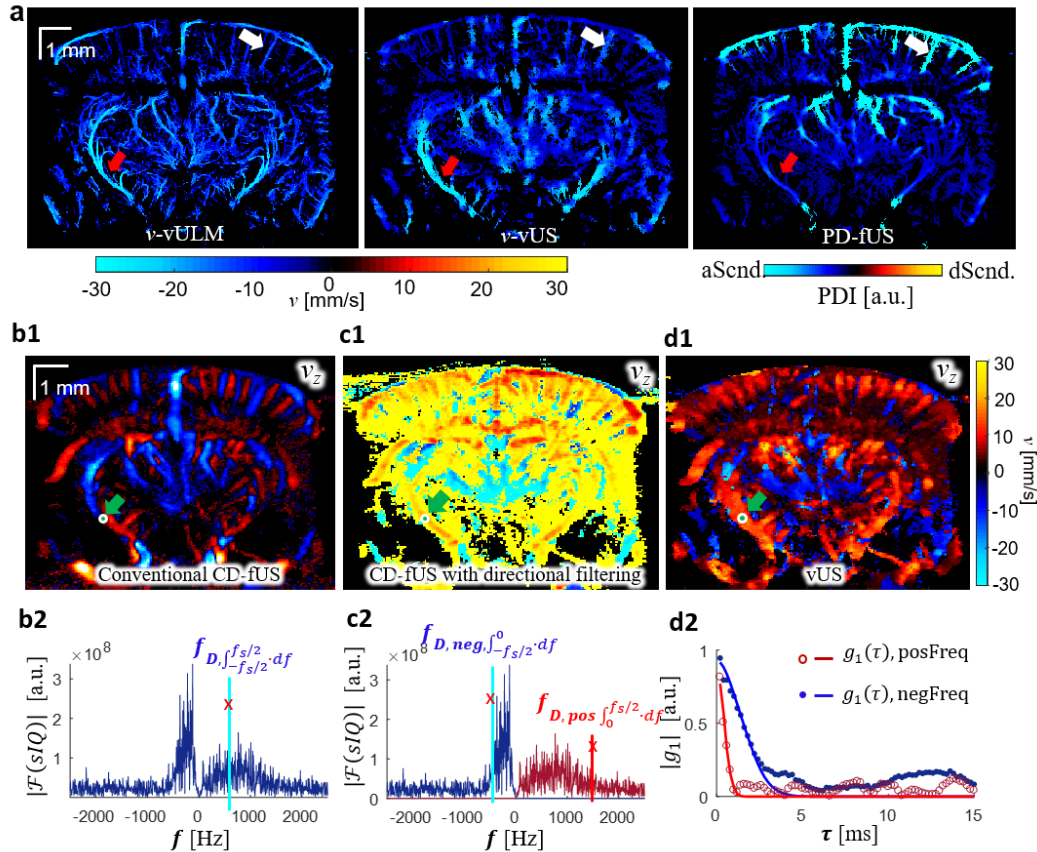
222 processing are apparent as shown in **Figure 5**. We see that 1) CD-fUS is only able to measure the  
 223 axial velocity component (**Figure 5a**); 2) the signal intensity of PD-fUS is not linearly related to  
 224 total speed but nonlinearly decreases with increasing speed (**Figure 5a2&b2**); and 3) vUS is able  
 225 to measure the blood flow velocity of both angled (**Figure 5a**) and transverse (**Figure 5b**) flows  
 226 and differentiate the axial velocity component from the transverse velocity component (**Figure**  
 227 **5a2**), indicating the advantages of vUS in quantitatively imaging flow speeds in both axial and  
 228 transverse directions.



229 **Figure 5** | Phantom results comparison of vUS with Power Doppler-based fUS (PD-fUS) and Color  
 230 Doppler-based fUS (CD-fUS). Angled (a) and transverse (B) flow phantom experiment results obtain with  
 231 vUS ( $v$  and  $v_z$ ), CD-fUS ( $v_z$ ), and PD-fUS.

233 **Figure 6a** compares the *in vivo* measurements of ascending flow (positive frequency component)  
 234 obtained with vUS and PD-fUS. Using the vULM measurement as the comparison standard of flow  
 235 velocity, we note that vUS agrees well with vULM, while PD-fUS has high signal intensity in

236 superficial layers and low signal intensity in deep regions, as indicated by the white and red arrows,  
237 indicating the strong dependence of the PD-fUS signal on acoustic attenuation. In contrast, vUS is  
238 not affected by acoustic attenuation as the normalization processing cancels the heterogeneous  
239 acoustic distribution. **Figure 6b1** shows the axial velocity maps obtained with conventional CD-  
240 fUS<sup>[4]</sup> (**Online Methods**). The conventional CD-fUS suffers from underestimation of Doppler  
241 frequency ( $f_D$ ) due to mutual frequency cancellation when opposite flows exist within a  
242 measurement voxel, as illustrated in **Figure 6b2**. For a fair comparison between vUS and the  
243 Doppler methods, we applied CD-fUS processing on the directional filtered data that we used for  
244 vUS processing. As shown in **Figure 6c**, we note that the blood flow speed is overestimated by the  
245 directional filtering-based CD-fUS. This overestimation happens because of high frequency noise  
246 causing overestimation of the Doppler frequency ( $f_D$ ) when a directional filter is applied and thus  
247 a higher speed bias, as shown in **Figure 6c2**. In comparison, vUS doesn't suffer from the high  
248 frequency noise as the high frequency noise is un-correlated and only causes  $g_1(\tau)$  to drop to a  
249 lower value at the first time lag but it doesn't affect the decorrelation rate of  $g_1(\tau)$  at longer time  
250 lags, which is determined by the correlated motion of flowing red blood cells, as shown in the  
251 bottom panel of **Figure 6d2**. Thus, by fitting the decorrelation of  $g_1(\tau)$  the blood flow velocity can  
252 be accurately reconstructed by vUS, as shown in **Figure 6d1**.



253  
 254 **Figure 6** | *in vivo* results comparison. (a) *in vivo* ascending flow results obtained with vULM, vUS, and  
 255 PD-fUS, where vULM is used as the comparison standard and the ULM spatial mask was applied to both  
 256 vUS and PD-fUS. (b1) Axial velocity ( $v_z$ ) map obtained with conventional CD-fUS; (b2) Doppler frequency  
 257 ( $f_D$ ) is underestimated with conventional CD-fUS. (c1) Axial velocity map obtained with directional  
 258 filtering-based CD-fUS; (c2) Doppler frequencies ( $f_{D,neg}$  and  $f_{D,pos}$ ) are overestimated with the directional  
 259 filtering-based CD-fUS. (d1) Axial velocity map obtained with vUS; (d2)  $g_1(\tau)$  calculated with positive  
 260 frequency component and negative frequency component after directional filtering; dots: experimental data;  
 261 solid line: theoretical fitting. Descending flow velocity maps were overlapped on ascending flow velocity  
 262 maps in (c1) and (d1).

263 **3. Discussion**

264 The development of robust blood flow velocity measurement technologies has been of great  
265 importance in neuroscience research as quantifying blood flow alterations enables the assessment  
266 of brain disease<sup>[17–19]</sup> and interpretation of regional neural function according to neurovascular  
267 coupling<sup>[20]</sup>. In this work, we introduced vUS based on the first-order temporal field autocorrelation  
268 function analysis of the ultrasound speckle fluctuations to quantify cerebral blood flow velocity  
269 with a temporal resolution of 1 frame/s (up to 5 frames/s in theory), with a greater than 10 mm  
270 penetration depth, and  $\sim 100 \mu\text{m}$  spatial resolution. vUS provides much deeper penetration  
271 compared to optical velocimetry methods which are usually restricted to superficial layers of less  
272 than 1 mm depth<sup>[21]</sup> while maintaining high spatial and temporal resolution compared to magnetic  
273 resonance imaging-based phase contrast velocity mapping<sup>[22]</sup>.

274 Using ultrasound signal decorrelation analysis to estimate flow speed dates back to the 1970s.  
275 Atkinson and Berry<sup>[23]</sup> have shown that the motion of moving scatterers is encoded in the  
276 fluctuations of the ultrasound signal and Bamber et al.<sup>[24]</sup> demonstrated that the ultrasound signal  
277 decorrelation could be used to image tissue motion and blood flow. Wear and Popp and others<sup>[8,9,25–</sup>  
278 <sup>28]</sup> showed that the decorrelation of ultrasound signal decays following a Gaussian form. In this  
279 paper, we showed that the ultrasound signal field decorrelation is governed by three terms,  
280 including the flow speed, the gradient of the axial velocity, and an axial velocity-dependent phase  
281 term. This phase term gives vUS the ability to differentiate the axial velocity component from the  
282 transverse velocity component.

283 The high frame rate ultrafast ultrasound plane-wave emission and acquisition paves the way for  
284 vUS implementation, which permits the speckle decorrelation caused by the moving scattering  
285 particles to be resolved with sufficiently high temporal resolution required to capture the speckle  
286 decorrelation within the small measurement voxels. The combination of spatiotemporal singular

287 value decomposition and high pass filtering plays an important role in rejecting bulk motion which  
288 enables the decorrelation of  $g_1(\tau)$  to represent the dynamics of the motion of red blood cells and  
289 to not be confounded by bulk motion. For blood flow velocity imaging of the brain, vUS  
290 reconstructs both descending and ascending flow velocities from the negative frequency  
291 component and positive frequency component by applying directional filtering, respectively. We  
292 further developed a comprehensive fitting algorithm to reconstruct axial and transverse blood flow  
293 velocities. The proposed vUS technique was validated with numerical simulation, phantom  
294 experiments, and in vivo blood flow velocities obtained with vULM. The functional whisker  
295 stimulation experiment result agrees with previous rodent functional studies that mechanoreceptive  
296 whisker information reaches the barrel cortex via the thalamic VPM nuclei<sup>[29]</sup>, and the PO is a  
297 paralemniscal pathway for whisker signal processing<sup>[30]</sup>. This experiment demonstrates that vUS is  
298 sensitive to quantify the cerebral blood flow velocity change in response to functional stimulation  
299 and can be applied for brain imaging in awake mice.

300 Compared to PD-fUS (Power Doppler), vUS is a quantitative imaging modality for assessing blood  
301 flow velocity while the PD-fUS signal decreased with increasing speed and is strongly affected by  
302 the acoustic attenuation. Compared to CD-fUS (Color Doppler), vUS is able to measure both axial  
303 and transverse flow velocities and is resistant to high frequency noise compared to the directional  
304 filtering-based CD-fUS which suffers from large or random values in regions with a low signal-to-  
305 noise ratio. Compared to vULM, vUS has lower spatial resolution but has much higher temporal  
306 resolution (up to 5 Hz of vUS compared to 2 mins/frame of vULM) and is applicable for awake  
307 functional studies in rodents requiring high temporal resolution. In addition, it measures the flow  
308 velocity of the intrinsic contrast of red blood cells while vULM measures the speed of microbubbles.  
309 One important application that will be enabled by the absolute blood flow velocity measured with  
310 vUS is that the metabolic rate of oxygen can be quantitatively estimated if vUS measurements are



311 combined with quantitative oxygenation measurements using multispectral photoacoustic  
312 tomography<sup>[31,32]</sup>, providing a new high resolution biomarker for neuroscience research.

313 A limitation is that vUS is not sensitive to measuring blood flow velocity in small vessels with low  
314 flow speeds due to the use of the spatiotemporal filter which rejects slow dynamics from the signal.  
315 Also, limited by the spatial resolution of the ultrasound system, the reconstructed blood flow  
316 velocity of a measurement voxel may represent integrated dynamics of multiple vessels that flow  
317 through the measurement voxel. For the results presented in this work, vUS was simplified to  
318 estimate in-plane 2D velocities (i.e.,  $v_x$  and  $v_z$ ), ignoring decorrelation from flow in the y-direction  
319 (see **Materials and Methods** for justification). This simplification, however, results in a moderate  
320 overestimation of the transverse velocity ( $v_x$ ) as  $v_x$  tends to compensate for the decorrelation  
321 caused by  $v_y$ . Nevertheless, we note that the measured total velocity is very close to that obtained  
322 with vULM as shown in **Figure 3**. In the future, with the development of fast 3D ultrasound  
323 imaging technology using a 2D transducer matrix, vUS can be easily adopted for 3D velocimetry  
324 of the whole rodent brain.

## 325 **4. Experimental Section**

### 326 **4.1. vUS theory derivation**

327 The complex ultrasound quadrature signal of particles moving at the same speed in a measurement  
328 voxel can be written as,

$$329 \quad sIQ(x_0, y_0, z_0, t) = R \sum_{i_s}^{N_s} e^{-\frac{(x_{i_s}(t)-x_0)^2}{2\sigma_x^2} - \frac{(y_{i_s}(t)-y_0)^2}{2\sigma_y^2} - \frac{(z_{i_s}(t)-z_0)^2}{2\sigma_z^2}} e^{i2k_0(z_{i_s}(t)-z_0)} \quad (4)$$

330 Considering the basic scenario that all scatters have identical dynamics, i.e. the scatters are moving  
331 in the same direction with same speed, the ultrasound pressure of the resolution voxel at time lag  $\tau$   
332 can be written as,

333 
$$sIQ(x_0, y_0, z_0, t + \tau) = R \sum_{i_s}^{N_s} e^{-\frac{(x_{i_s}(t)+v_x\tau-x_0)^2}{2\sigma_x^2} - \frac{(y_{i_s}(t)+v_y\tau-y_0)^2}{2\sigma_y^2} - \frac{(z_{i_s}(t)+v_z\tau-z_0)^2}{2\sigma_z^2}} e^{i2k_0(z_{i_s}(t)+v_z\tau-z_0)} \quad (5)$$

334 According to **Equation 2**,  $g_1(\tau)$  for particles flowing identically within the ultrasound  
335 measurement voxel can be derived to be,

336 
$$g_1(\tau) = e^{-\frac{v_x\tau^2}{4\sigma_x^2} - \frac{v_y\tau^2}{4\sigma_y^2} - \frac{v_z\tau^2}{4\sigma_z^2}} e^{i2k_0v_z\tau} \quad (6)$$

337 For microvasculature imaging of the rodent brain, the group velocity and velocity distribution must  
338 be taken into account as the relative movement of scatters will result in additional decorrelation.  
339 To simplify the derivation, we used a Gaussian distributed velocity model to describe the velocity  
340 distributed flow,

341 
$$P(v_x, v_y, v_z) = \frac{1}{\pi\sqrt{\pi}\sigma_{v_x}\sigma_{v_y}\sigma_{v_z}} e^{-\frac{(v_x-v_{xgp})^2}{\sigma_{v_x}^2} - \frac{(v_y-v_{ygp})^2}{\sigma_{v_y}^2} - \frac{(v_z-v_{zgp})^2}{\sigma_{v_z}^2}} \quad (7)$$

342 where,  $P(v_x, v_y, v_z)$  is the velocity distribution probability;  $v_{gp}$  is the group velocity; and  $\sigma_v$   
343 describes the velocity distribution.

344  $g_1(\tau)$  for the Gaussian speed distribution flow is derived to be,

345 
$$g_1(\tau) = \sqrt{\frac{64\sigma_x^2\sigma_y^2\sigma_z^2}{(4\sigma_x^2+\sigma_{v_x}^2\tau^2)(4\sigma_y^2+\sigma_{v_y}^2\tau^2)(4\sigma_z^2+\sigma_{v_z}^2\tau^2)}} e^{-\frac{(v_{xgp}\tau)^2}{4\sigma_x^2+\sigma_{v_x}^2\tau^2} - \frac{(v_{ygp}\tau)^2}{4\sigma_y^2+\sigma_{v_y}^2\tau^2} - \frac{(v_{zgp}\tau)^2+4\sigma_z^2\sigma_{v_z}^2(k_0\tau)^2}{4\sigma_z^2+\sigma_{v_z}^2\tau^2}} e^{i2k_0\tau\frac{4\sigma_z^2v_{zgp}}{4\sigma_z^2+\sigma_{v_z}^2\tau^2}} \quad (8)$$

346 From our observations, the typical decorrelation time ( $\tau_c$ ) for blood flow with a speed around 10  
347 mm/s is ~5 ms. Therefore,  $\sigma_{v_{\leftrightarrow}}^2\tau^2 < 6.25 \times 10^{-4} \text{ mm}^2$  which is more than 8 times smaller than  
348  $4\sigma_{\leftrightarrow}^2 \geq 50 \times 10^{-4} \text{ mm}^2$ , where ' $\leftrightarrow$ ' represents the coordinate direction (i.e., x, y or z). Thus, the  
349 theoretical equation of  $g_1(\tau)$  can be further simplified to be,

350 
$$g_1(\tau) = e^{-\frac{(v_{xgp}\tau)^2}{4\sigma_x^2} - \frac{(v_{ygp}\tau)^2}{4\sigma_y^2} - \frac{(v_{zgp}\tau)^2}{4\sigma_z^2}} e^{-\sigma_{v_z}^2(k_0\tau)^2} e^{i2k_0\tau v_{zgp}} \quad (9)$$

351 where,  $\sigma_x$ ,  $\sigma_y$ , and  $\sigma_z$  are the Gaussian profile width at the  $1/e$  value of the maximum intensity of  
352 the point spread function (PSF) in  $x$ ,  $y$ , and  $z$  directions, respectively;  $v_{gp}$  is the group velocity; and  
353  $\sigma_{vz}$  describes the axial velocity distribution; and  $k_0$  is the wave number of the central frequency of  
354 the transducer.

## 355 **4.2. vUS implementation**

### 356 *4.2.1. Coherent plane wave compounding-based data acquisition*

357 The ultrasound signal was acquired with a commercial ultrafast ultrasound imaging system  
358 (Vantage 256, Verasonics Inc. Kirkland, WA, USA) and a linear ultrasonic probe (L22-14v,  
359 Verasonics Inc. Kirkland, WA, USA). The Vantage 256 system has 256 parallelized emission and  
360 receiving channels, and can acquire planar images at a frame rate up to 30 kHz when the imaging  
361 depth is  $\sim 15$  mm. The L22-14v ultrasonic probe has 128 transducer elements with a pitch of 0.1  
362 mm and a center frequency of 18.5 MHz with a bandwidth of 12.4 MHz (67%, -6 dB). It has an  
363 elevation focus at  $z=6$  mm.

364 To ensure sufficient temporal resolution, the ultrasound plane wave frame rate was set to 30 kHz  
365 which was mainly limited by the transmit time of the ultrasound signal in the sample through the  
366 intended imaging depth, as shown in **Figure S1a**. To enhance the signal-to-noise ratio while  
367 preserving sufficient temporal resolution, we further employed coherence plane wave  
368 compounding<sup>[33]</sup> at five emitting angles ( $-6^\circ, -3^\circ, 0^\circ, 3^\circ, 6^\circ$ ) to form a compounded image whose  
369 frame rate was 5 kHz, as shown in **Figure S1b**.

370 In addition, to acquire sufficient ensemble averaging of the US speckle fluctuations for the vUS  
371 analysis, we acquired 200 ms of data, i.e. 1,000 compounded images, to calculate  $g_1(\tau)$  over a  
372 range of  $0 < \tau < 20$  ms. Therefore, the maximum vUS frame rate is 5 frames/s. However, for extended

373 data acquisition (i.e. >1 mins) the maximum vUS frame rate was reduced to 1 frame/s due to limit  
374 data transfer and saving requirements.

#### 375 4.2.2. Clutter rejection

376 For the phantom data processing, we used a spatiotemporal filtering method (singular value  
377 decomposition, SVD, **Equation 10**<sup>[34]</sup>) to remove the first two ( $N_c=3$ ) highest singular value signal  
378 components. To reject the bulk motion signal from the *in vivo* data, we used a combination of SVD  
379 and high pass filtering. The first 20 highest singular value signal components were removed  
380 ( $N_c=21$ ), followed by a fourth order Butterworth high pass filtering with a cutoff frequency of 25  
381 Hz corresponding with a 1 mm/s speed cutoff.

$$382 \quad sIQ = \sum_{i=N_c}^N S(z, x) \lambda_i V(t) \quad (10)$$

383 where, sIQ is the dynamic signal;  $N_c$  is the cutoff rank for SVD processing;  $S(z, x)$  is the spatial  
384 singular matrix;  $\lambda_i$  is the singular value corresponding with the  $i^{\text{th}}$  rank; and  $V(t)$  is the temporal  
385 singular vector.

#### 386 4.2.3. vUS fitting algorithm

387 **Figure S1d** summarizes the vUS data processing algorithm. Based on the developed vUS theory  
388 for *in vivo* brain imaging, the clutter rejected sIQ data of a measurement voxel,  $sIQ(z, x)$ , was first  
389 directionally filtered to obtain the negative frequency signal component (descending flow) and the  
390 positive frequency signal component (ascending flow) using the directional filtering processing  
391 (**Equation 11&12**).

$$392 \quad \mathcal{F}(sIQ) = \mathcal{F}_{neg}(sIQ) + \mathcal{F}_{pos}(sIQ) \quad (11)$$

$$393 \quad sIQ_{neg} = \mathcal{F}^{-1}[\mathcal{F}_{neg}(sIQ)], \quad sIQ_{pos} = \mathcal{F}^{-1}[\mathcal{F}_{pos}(sIQ)] \quad (12)$$

394 where,  $sIQ_{neg}$  and  $sIQ_{pos}$  are the complex ultrasound quadrature signal of the negative frequency  
395 and positive frequency, respectively;  $\mathcal{F}$  denotes the Fourier transform; and  $\mathcal{F}^{-1}$  denotes the inverse  
396 Fourier transform.  $g_{1neg}(\tau)$  and  $g_{1pos}(\tau)$  for  $sIQ_{neg}$  and  $sIQ_{pos}$  are obtained using **Equation 2**,  
397 respectively.

398 We used criteria including the ratio of positive/negative frequency power to whole frequency power  
399 (**Equation 13**) and the absolute value of  $g_1(\tau)$  at the first time lag (**Equation 14**) to control signal  
400 quality for data processing.

$$401 \quad R_{pos} = \frac{\sum \mathcal{F}(sIQ)_{f>0}}{\sum \mathcal{F}(sIQ)_{all\ freq.}} > 0.2, \quad R_{neg} = \frac{\sum \mathcal{F}(sIQ)_{f<0}}{\sum \mathcal{F}(sIQ)_{all\ freq.}} > 0.25 \quad (13)$$

$$402 \quad |g_1(1)| > 0.2 \quad (14)$$

403 where,  $\mathcal{F}$  denotes the Fourier transform. These criteria enable us to skip the poor quality data,  
404 which also greatly reduces the processing time.

405 Then, the fitting procedure is applied for both  $sIQ_{neg}$  and  $sIQ_{pos}$ , respectively. In practice, random  
406 noise results in a prompt ‘drop’ of  $g_1(1)$ , i.e. the change of  $g_1(0)$  to  $g_1(1)$  is not a smooth  
407 transition compared to  $g_1(1)$  to the end of the decorrelation as the noise is uncorrelated. We  
408 therefore modified the  $g_1(\tau)$  equation by using an ‘F’ factor to account for this ‘drop’. Also, it is  
409 worth noting that when using a linear transducer array the ultrasound PSF is anisotropic in the  
410 transverse directions, i.e.  $\sigma_x \neq \sigma_y$ . In our experimental setup,  $\sigma_y$  was more than 3 times larger than  
411  $\sigma_x$  which results in a more than 9 times slower signal decorrelation rate from  $v_{ygp}$  compared to  
412 that from  $v_{xgp}$ . Therefore, we omitted the y component from the  $g_1(\tau)$  fitting to simplify the data  
413 processing. In addition, in the case of Gaussian velocity distribution,  $\sigma_{vz}$  is proportional to the  
414 maximum speed in the center line and also linearly related to the group velocity  $v_{zgp}$ . Thus  $\sigma_{vz}$  in

415 **Equation 3** can be replaced with  $\sigma_{vz} = p \cdot v_{zgp}$  where  $p$  is a linear factor with a range of [0 1].

416 Thus the theoretical  $g_1(\tau)$  model used for fitting the experimental data is,

$$417 \quad g_1(\tau) = F \cdot e^{-\frac{(v_{xgp}\tau)^2}{4\sigma_x^2} - \frac{(v_{zgp}\tau)^2}{4\sigma_z^2}} e^{-(p \cdot v_{zgp} \cdot k_0 \cdot \tau)^2} e^{i2k_0\tau v_{zgp}} \quad (15)$$

418 where  $F$  represents the correlated dynamic fraction which accounts for the  $g_1(\tau)$  value drop at the  
 419 first time lag due to uncorrelated signal fluctuations (e.g. noise);  $v_x$  and  $v_z$  are the flow speed in  
 420 the  $x$  and  $z$  directions respectively;  $\sigma_{vz} = p \cdot v_z$  accounts for the speed distribution within the  
 421 measurement voxel where  $p$  is a linear factor with a range of [0 1];  $\sigma_x$  and  $\sigma_z$  are the US voxel  
 422 Gaussian profile width at the  $1/e$  value of the maximum intensity of the point spread function (PSF)  
 423 in the  $x$  and  $z$  directions, respectively; and  $k_0 = 2\pi/\lambda_0$  is the wave number of the central frequency  
 424 of the transducer.

425 A proper initial guess of the unknown parameters (i.e.,  $F$ ,  $v_{xgp}$ ,  $v_{zgp}$ , and  $p$ ) is important to achieve  
 426 high fitting accuracy and efficiency. The initial guess of  $F_0$  was set to be  $F_0 = |g_1(1)|$ . As the axial  
 427 movement caused the phase change of  $g_1(\tau)$ , we used the phase information of  $g_1(\tau)$  to determine  
 428  $v_{zgp0}$  by finding the time lag  $\tau_V$  when  $g_1(\tau)$  reaches the first minimum.

$$429 \quad v_{zgp0} = \frac{\lambda_0}{4\tau_V} \quad (16)$$

430 We tested a mesh of  $v_{xgp}$  and  $p$  values to determine the initial guess of  $v_{xgp0}$  and  $p_0$  by finding the  
 431 pair of  $v_{xgp0}$  and  $p_0$  that maximizes the coefficient of determination,  $R$ .  $R$  is defined in **Equation**  
 432 **17** and was also used in the final fitting process as the objective function for a constrained least  
 433 squares regression non-linear fitting procedure to estimate the values for  $F$ ,  $v_{xgp}$ ,  $v_{zgp}$ , and  $p$  based  
 434 on the initial guesses.

$$435 \quad R = 1 - \frac{\langle |g_{1exp}(\tau) - (F \cdot e^{-\frac{(v_{xgp}\tau)^2}{4\sigma_x^2} - \frac{(v_{zgp}\tau)^2}{4\sigma_z^2}} e^{-(p \cdot v_{zgp} \cdot k_0 \cdot \tau)^2} e^{i2k_0\tau v_{zgp}})|^2 \rangle}{\langle |g_{1exp}(\tau) - \langle g_{1exp}(\tau) \rangle|^2 \rangle} \quad (17)$$

436 where,  $g_{1_{exp}}(\tau)$  is the experimental  $g_1(\tau)$  calculated with **Equation 2**;  $\langle \dots \rangle$  indicates temporal  
 437 ensemble averaging; and  $|\dots|$  indicates the absolute value.

438 Finally, the axial and total velocity maps were obtained for both descending and ascending flows,  
 439 as shown in **Figure S1e**.

### 440 **4.3. Power Doppler-fUS and Color Doppler-fUS calculation**

441 The Power Doppler image (PD-fUS) was calculated as<sup>[4]</sup>,

$$442 \quad PDI = \frac{1}{N} \sum_{i=1}^N sIQ^2(t_i) \quad (18)$$

443 where,  $N$  is the number of samples and  $sIQ$  is the complex ultrasound quadrature signal of the  
 444 moving particles.

445 The axial velocity based on the conventional Color Doppler calculation is obtained with<sup>[10]</sup>,

$$446 \quad v_{cz} = -\frac{c}{2f_0} \frac{\int_{-f_s/2}^{f_s/2} f \cdot |\mathcal{F}(sIQ)|^2 df}{\int_{-f_s/2}^{f_s/2} |\mathcal{F}(sIQ)|^2 df} \quad (19)$$

447 where,  $c$  is the sound speed in the medium and  $c= 1540$  m/s was used in this study;  $f_0$  is the  
 448 transducer center frequency;  $f_s$  is the frame rate; and  $\mathcal{F}$  denotes the Fourier transform.

449 Further, for a fair comparison with vUS which obtains velocity map based on the directional filtered  
 450 data ( $sIQ_{neg}$  and  $sIQ_{pos}$ ), we used Color Doppler to process the same directional filtered data to  
 451 obtain descending and ascending speeds (**Figure 6c1**),

$$452 \quad v_{cz,dsnd} = -\frac{c}{2f_0} \frac{\int_{-f_s/2}^0 f \cdot |\mathcal{F}(sIQ)|^2 df}{\int_{-f_s/2}^0 |\mathcal{F}(sIQ)|^2 df}, \quad v_{cz,asnd} = -\frac{c}{2f_0} \frac{\int_0^{f_s/2} f \cdot |\mathcal{F}(sIQ)|^2 df}{\int_0^{f_s/2} |\mathcal{F}(sIQ)|^2 df} \quad (20)$$

### 453 **4.4. Ultrasound Localization Microscopy**

454 The ultrasound localization microscopy (ULM) images and the ULM-based velocity maps (vULM)  
 455 were obtained based on a microbubble tracking and accumulation method described in<sup>[13,14]</sup>. Briefly,  
 456 a frame-to-frame subtraction was applied to the IQ data to get the dynamic microbubble signal.

457 The images of the microbubble were rescaled to have a pixel size of  $10 \mu m \times 10 \mu m$ . The centroid  
458 position for each microbubble was then identified with  $10 \mu m$  precision by deconvolving the  
459 system point spread function. By accumulating the centroid positions over time, a high resolution  
460 image of the cerebral vasculature image (ULM) is obtained. Further, by identifying and tracking  
461 the same microbubble's position, the in-plane flow velocity of the microbubble can be calculated  
462 based on the travel distance and the imaging frame rate. The final velocity for coordinates  $(z, x)$   
463 consists of descending and ascending flows, and the speed for each direction was obtained by  
464 averaging the same directional flow speed at all time points when the absolute value was greater  
465 than 0, respectively.

#### 466 **4.5. Numerical Simulation**

467 In this study, two dimensional (x-z) flow and ultrasound detection was simulated to validate vUS.  
468 Point scattering particles ( $5 \mu m$  in diameter) were randomly generated at the initialization segment  
469 which is outside the ultrasound measurement voxel. Then the flowing positions were calculated for  
470 all time points based on the preset flow speed and flow angle at a temporal rate of 5 KHz. The  
471 detected ultrasound signal ( $sIQ$ ) was obtained based on **Equation 1** for each time point. Then the  
472 simulated  $g_1(\tau)$  was calculated according to **Equation 2** with 1000 observation time points (i.e.  
473 200 ms) and 100 autocorrelation calculation time lags (i.e. 20 ms). Flow velocity was then  
474 reconstructed by applying vUS processing on the simulated  $g_1(\tau)$ .

#### 475 **4.6. Phantom experiment and data processing**

476 For the phantom validation experiment, a plastic micro tube (inner diameter  $580 \mu m$ , Intramedic  
477 Inc.) was buried in a homemade agar phantom with an angle of  $\sim 30^\circ$  (angled flow), and another  
478 plastic micro tube was aligned close to  $\sim 0^\circ$  (transvers flow) in another homemade agar phantom.  
479 A blood solution was pumped through the tubes with a syringe pump (Harvard Apparatus) at speeds



480 of 1, 3, 5, 7, 9, 11, 13, 15, 20, 25, and 30 mm/s. SVD was performed to filter the background signal  
481 clutter by removing the first two highest singular value components. Since the diameter of the tube  
482 is much larger than the ultrasound resolution, the red blood cell speed distribution can be considered  
483 uniform. Therefore, the linear value  $p$  in **Equation 15** was set to 0 (i.e.  $\sigma_{vz} = 0$ ) for the phantom  
484 data processing.

#### 485 **4.7. Animal preparation**

486 The animal experiments were conducted following the Guide for the Care and Use of Laboratory  
487 Animals, and the experiment protocol was approved by the Institutional Animal Care and Use  
488 Committees of Boston University.

489 In this study, 12-16-week old C57BL/6 mice (22-28g, male, Charles River Laboratories) were used.  
490 Animals were housed under diurnal lighting conditions with free access to food and water. Mice  
491 were anesthetized with isoflurane (3% induction, 1–1.5% maintenance, in 1L/min oxygen) while  
492 the body temperature was maintained with a homeothermic blanket control unit (Kent Scientific)  
493 during surgery and anesthetized imaging sessions. After removal of the scalp, a custom-made  
494 PEEK headbar was attached to the skull using dental acrylic and bone screws. The skull between  
495 lambda and bregma extending to temporal ridges was removed as a strip. A PMP film cut to the  
496 size of the craniotomy was then secured to the skull edges. Since the PMP is flexible, brain is  
497 protected by a cap attached to the head bar. The animal was allowed to recover for 3 weeks before  
498 the imaging sessions. During surgery and anesthetized imaging, heart rate and oxygen saturation  
499 was non-invasively monitored (Mouse Stat Jr, Kent Scientific) and all noted measurements were  
500 within the expected physiological range. For awake imaging, animals were trained to be head fixed  
501 for at least two weeks before the imaging session using sweetened condensed milk as treat.

#### 502 **4.8. *in vivo* experiment and data processing**

503 *4.8.1. Experimental setup*

504 Agarose phantom (no scattering) was used to fill the cranial window, which serves as the acoustic  
505 matching medium between a water container and the mouse brain. The bottom of the water  
506 container was covered with a thin clear film preventing water leakage. To maintain the brain  
507 temperature of experimental animal, degassed warm water ( $37^{\circ} \pm 1^{\circ}$ ) was circulating through the  
508 water container and, along with the agarose phantom, worked as the acoustic transmitting medium  
509 between the ultrasound transducer and the mouse brain, as shown in **Figure 4a**. An anteroposterior  
510 linear translating stage was used to carry the ultrasound probe to acquire data at different coronal  
511 planes.

512 For anesthetized imaging, the experimental animal was anesthetized by isoflurane through a nose  
513 cone while the body temperature was maintained at  $37^{\circ}$  with a homeothermic blanket control unit  
514 (Harvard Apparatus) and its head was fixed by a stereotaxic frame. For awake imaging, the  
515 experimental animal head was fixed by attaching the head-bar to a customized mount and the  
516 animal was treated with milk every ~30 min.

517 *4.8.2. In vivo validation*

518 For in vivo validation, animals were anesthetized with isoflurane and the body temperature was  
519 maintained at  $37^{\circ}$ . vUS data was first acquired at different coronal planes and followed by  
520 microbubble injection for ULM/vULM imaging for each coronal plane. 0.03 ml commercial  
521 microbubble suspension ( $5.0\text{-}8.0 \times 10^8$  microbubbles per ml, Optison, GE Healthcare, Milwaukee,  
522 WI) was administered through retro-orbital injection of the mouse eye. The vULM map was  
523 rescaled to have the same pixel size ( $25 \times 25 \mu\text{m}^2$ ) as vUS map. For a fair comparison, both the  
524 vULM and the vUS measurements were applied with a spatial mask that ensures nonzero valued  
525 pixels for both vUS and vULM measurements.

### 526 4.8.3. Whisker stimulation

527 N=3 mice were trained and used for the whisker stimulation experiment. An air puffer machine  
528 (Picospritzer III, Parker Inc.) was used for the whisker stimulation experiments. The outlet of the  
529 air tube was placed ~15 mm behind the whiskers. Two stimulation patterns were used in this study:  
530 the first stimulation pattern (**Figure 4** and **Figure S5a**) consisted of 30 s baseline and followed by  
531 10 trials of 15 s stimulation and with a 45 s interstimulus interval, and the second stimulation pattern  
532 (**Figure S5b**) consisted of 20 s baseline and followed by 10 trials of 5 s stimulation and with a 25  
533 s interstimulus interval. A motion correction method was used to replace the signal value at strong  
534 motion time points with the median value of adjacent time points. The stimulation frequency was  
535 3 Hz.

536 The whisker stimulation activation maps were calculated as the correlation coefficient  $r$  between  
537 the blood flow velocity  $v(z, x, t)$  and the temporal stimulus pattern  $S(t)$ .

$$538 \quad r(z, x) = \frac{\sum_{t=1}^N (v(z, x, t) - \overline{v(z, x)}) (S(t) - \bar{S})}{\sqrt{\sum_{t=1}^N (v(z, x, t) - \overline{v(z, x)})^2} \sqrt{\sum_{t=1}^N (S(t) - \bar{S})^2}} \quad (21)$$

539 where,

$$540 \quad \overline{v(z, x)} = \frac{1}{N} \sum_{t=1}^N v(z, x, t) \quad \text{and} \quad \bar{S} = \frac{1}{N} \sum_{t=1}^N S(t)$$

541 where,  $N$  is the total acquisition. The correlation coefficient was transformed to  $z$  score according  
542 to Fisher's transform (**Equation 16**) and the level of significance was chosen to be  $z > 4.43$  ( $P <$   
543  $0.001$ , one tailed test), which corresponds to  $r > 0.2$ .

$$544 \quad z = \frac{\sqrt{N-3}}{2} \cdot \ln \frac{1+r}{1-r} \quad (22)$$

### 545 **Supporting Information**

546 Supporting Information is available from the Wiley Online Library or from the author.

547

548

### 549 **Acknowledgements**

550 The authors acknowledge funding from NIH R01-EB021018, R01 NS108472, and R01-  
551 MH111359.

552

### 553 **Competing financial interests**

554 The authors declare no competing financial interests.

### 555 **Authors contributions**

556 J.T. and D.A.B. conceived of the technology and designed this study. J.T., D.D.P., T.L.S. and  
557 D.A.B. developed the theoretical model and analyzed the results. J.T. derived the theoretical  
558 formula, developed the data processing method, constructed the experimental setup, carried out  
559 experiments, and wrote the manuscript. K.K., E.E. and B.L. developed the surgical protocol for  
560 chronic imaging on awake mice, carried out animal experiments and analyzed the results. J.T.G  
561 designed the head bar. D.A.B. supervised this study. All authors discussed the results and  
562 contributed to the final version of the manuscript.

563

564 Received: ((will be filled in by the editorial staff))

565 Revised: ((will be filled in by the editorial staff))

566 Published online: ((will be filled in by the editorial staff))

567

568

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- 624
- 625

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627

628 Supporting Information

629

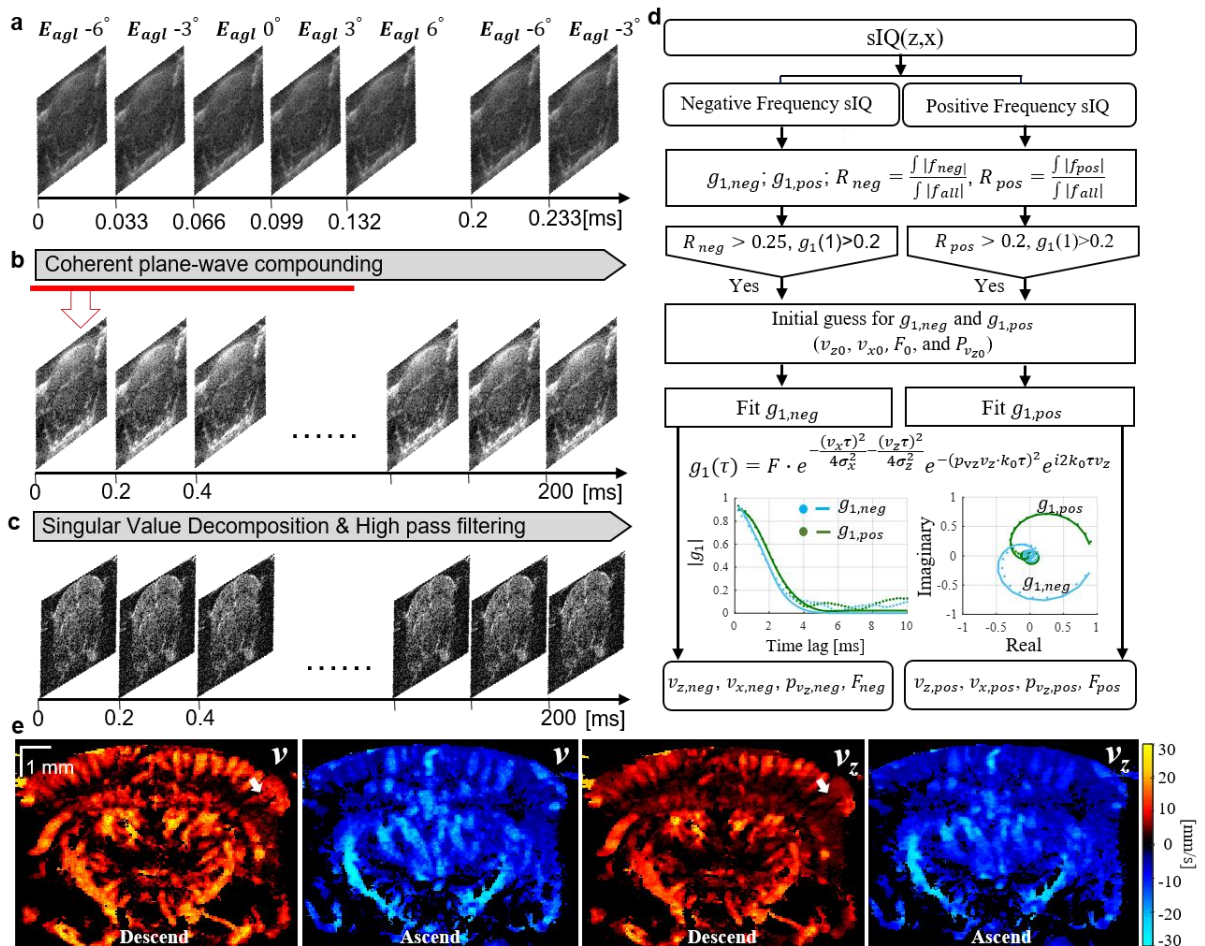
630 **Functional ultrasound speckle decorrelation-based velocimetry of the brain**

631 *Jianbo Tang<sup>1</sup>, Dmitry D. Postnov<sup>1,3</sup>, Kivilcim Kilic<sup>1</sup>, Sefik Evren Erdener<sup>1</sup>, Blaire Lee<sup>1</sup>, John T.*  
 632 *Giblin<sup>1</sup>, Thomas L. Szabo<sup>1</sup> & David A. Boas<sup>1,\*</sup>.*

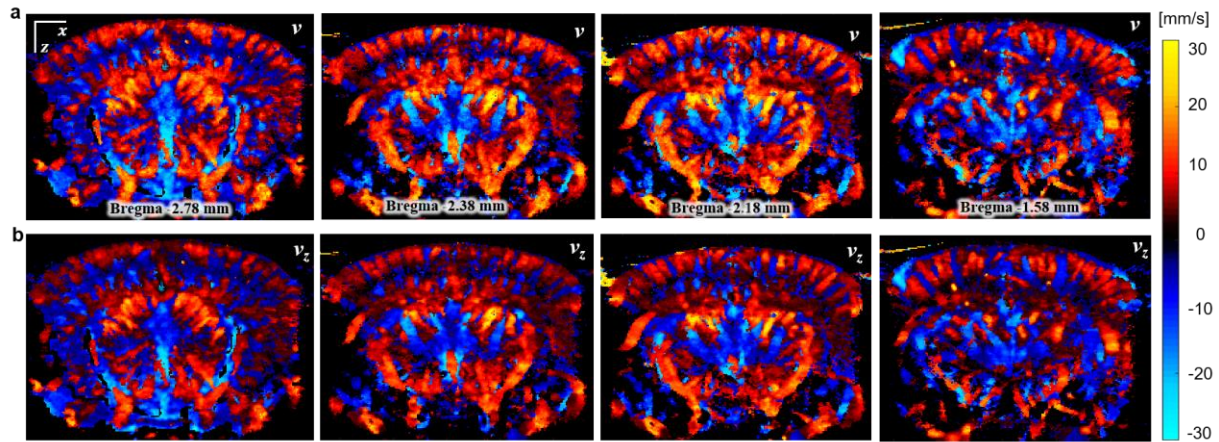
633

634 **I. Supplementary Figures**

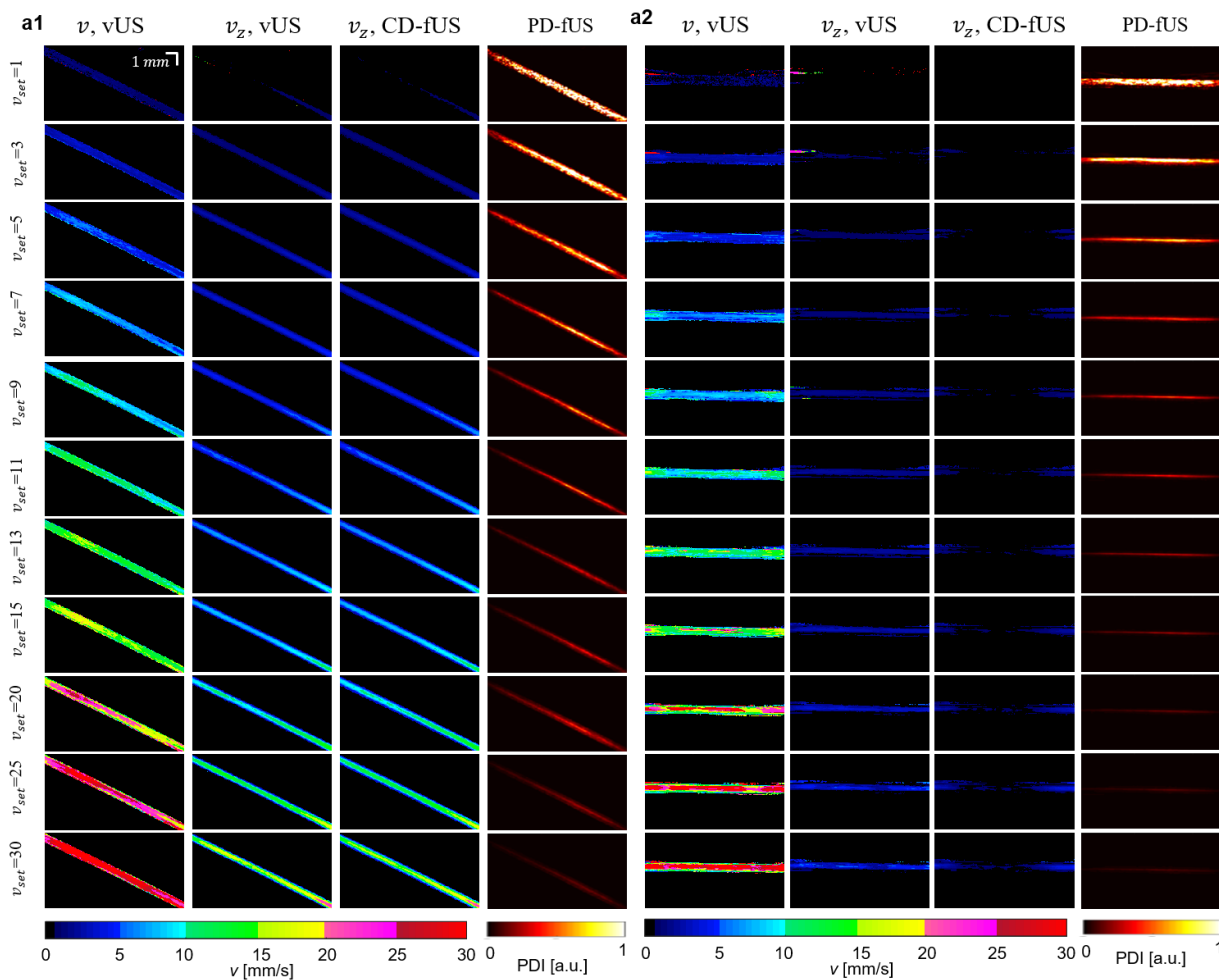
635



636 **Figure S1** | vUS implementation and data processing. (a) Ultrasound pulse & acquisition sequence. (b)  
 637 Coherent plane-wave compounding were performed on the 5 tilted emission angle frames and produced  
 638 a compounded image at a frame rate of 5 kHz. (c) Clutter rejection were performed to remove static  
 639 background and bulk motion signal components. (d) Negative and positive frequency components of a  
 640 measurement voxel are processed separately for *in vivo* data vUS processing; dots: experimental data;  
 641 solid lines: fitting results. (e) Descending and ascending blood flow velocity maps reconstructed by vUS  
 642 of a coronal plane ( $\sim$ Bregma -2.18 mm) of a mouse brain.



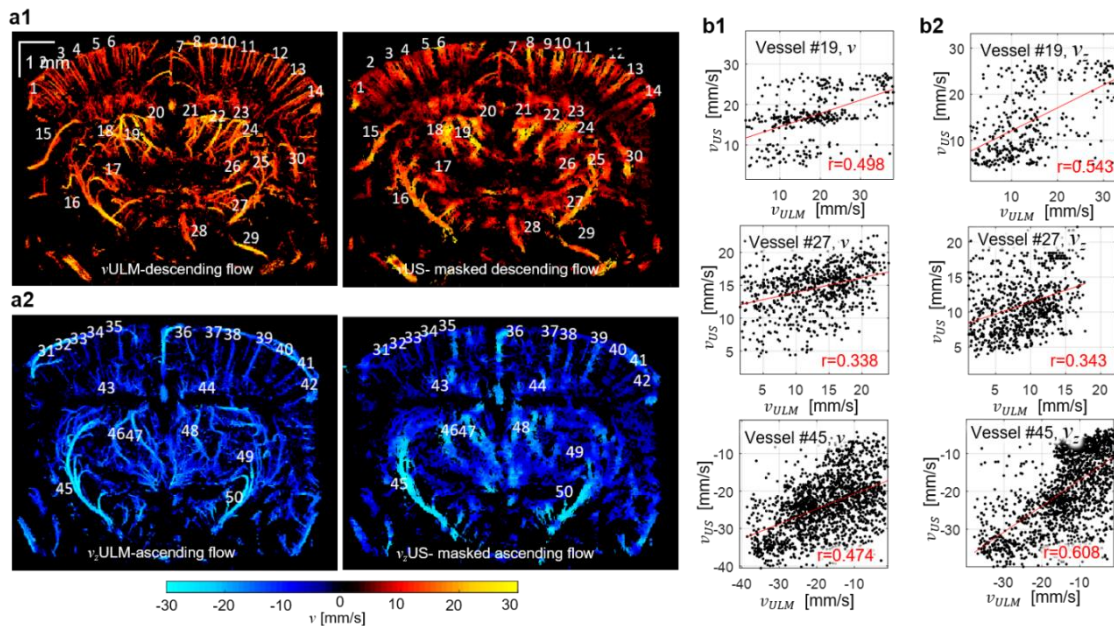
643  
 644 **Figure S2** | Total velocity (a) and axial velocity (b) obtained with vUS at different coronal planes of a mouse  
 645 brain. Descending flow velocity map was overlapped on ascending flow velocity map.



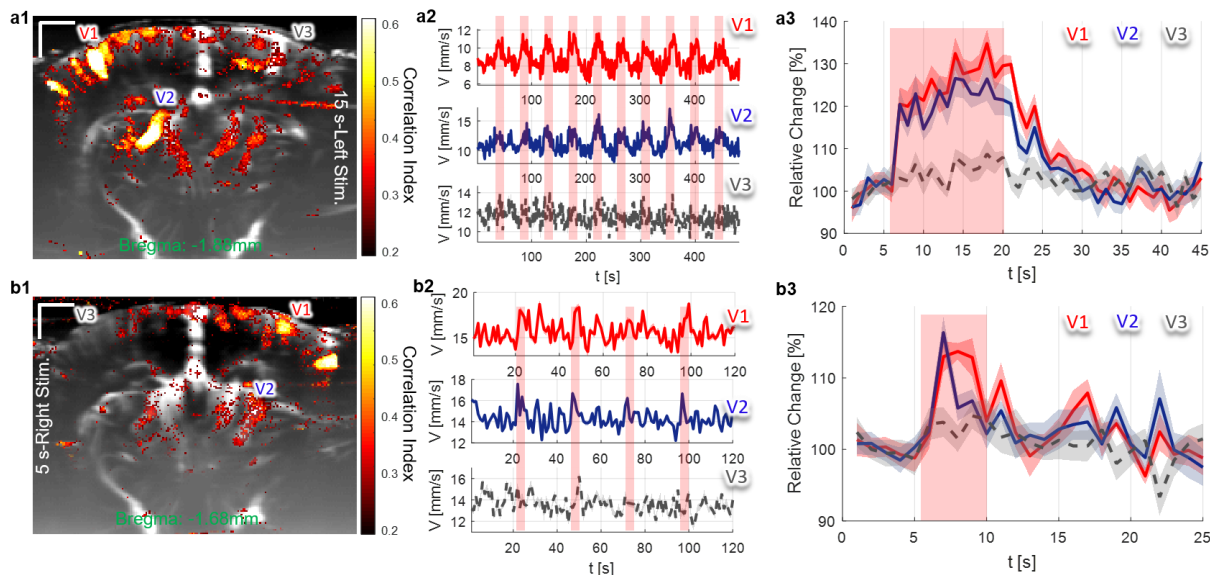
646  
 647 **Figure S3** | Phantom experiment validation and comparison. (a) Results for angled flow phantom  
 648 experiments. (b) Results for transverse flow phantom experiments. vUS is able to accurately measure both  
 649 axial and transverse velocity components while CD-fUS is not capable of measuring the transverse flow  
 650 velocity component. In addition, vUS is able to accurately differentiate the axial velocity component from



651 the transverse velocity component given its ability to determine flow direction. Compared to PD-fUS, vUS  
 652 measured velocity has a linear relationship with the preset speeds, while the PD-fUS measured signal  
 653 decreases nonlinearly with increasing preset speed.



654  
 655 **Figure S4** | *in vivo* validation by comparing vUS with vULM. (a) The numbers show the indices of selected  
 656 vessel for vessel-to-vessel comparison between vUS and vULM. (b1) Scatter plots of total velocity of three  
 657 representative vessels show the pixel-to-pixel correlation between vULM and vUS. (b2) Scatter plots of  
 658 axial velocity of three representative vessels show the pixel-to-pixel correlation between vULM and vUS.



659  
 660 **Figure S5** | Representative whisker stimulation results. (a) Results of 15 seconds left side whisker  
 661 stimulation; (a1) Activation map; (a2) Blood flow velocity time courses for the three vessels marked in (a1);  
 662 (a3) 10 trials averaged relative response of the three vessels. (b) Results of 5 seconds right side whisker  
 663 stimulation at Bregma ~ -1.58 mm; (b1) Activation map; (b2) Blood flow velocity time courses for the three  
 664 vessels marked in (b1); (b3) 10 trials averaged relative response of the three vessels.

## 665 II. Function description for vUS data processing

666 **Note:** vUS data processing code and example data is available from: [Supplementary](#)  
667 [Code](#).

### 668 A. vUS data processing for *in vivo* data

#### 669 A.1. main function

```
670 %% IQ to vUS data processing for in vivo experiment
671 clear all; clc
672 addpath('./SubFunctions/');
673 %% Use GPU calculation or not
674 useGPU = questdlg('Use GPU for data processing?', 'Select', ...
675     'YES', 'NO', 'Cancel', 'Cancel');
676 %% Load data
677 disp(['Loading data, ', datestr(datetime('now'))]);
678 load('./DATA/invivoData.mat');
679 [nz,nx,nt]=size(IQ);
680 PRSSInfo.g1StartT=1;
681 PRSSInfo.g1nT=nt;
682 PRSSInfo.g1nTau=100;
683 PRSSInfo.rFrame=5000; % sIQ frame rate, Hz
684 PRSSInfo.SVDrank=[25, nt];
685 PRSSInfo.HPfc=25; % high pass frequency cutoff
686 PRSSInfo.FWHM=[125 100]*1e-6; % (X, Z) spatial resolution, Full Width at Half Maximum of point spread function, m
687 PRSSInfo.C=1540; % sound speed, m/s
688 PRSSInfo.f0=16.625*1e6; % Transducer center frequency, Hz
689 PRSSInfo.xCoord=interp(P.xCoord,PRSSInfo.rfnScale);
690 PRSSInfo.zCoord=interp(P.zCoord,PRSSInfo.rfnScale);
691 PRSSInfo.MpVz=1; % maximum p value for Sigma Vz
692 PRSSInfo.NEQ=0; % no noise equalization
693 %% 1. Clutter rejection
694 disp(['Clutter Rejection - ', datestr(datetime('now'))]);
695 [sIQ, sIQHP, sIQHHP, eqNoise]=IQ2sIQ(IQ(:,:,1:PRSSInfo.g1nT),PRSSInfo); % 0: no noise equalization
696 [nz,nx,nt]=size(sIQ);
697 clear IQ
698 %% 2. vUS data processing
699 disp(['g1-based vUS Processing - ', datestr(datetime('now'))]);
700 if strcmp(useGPU, 'YES')
701     disp('GPU-based vUS Processing ...(NOTE: it takes around 30 seconds);');
702     tic;[F, Vz, V, pVz, R]=sIQ2vUS_NPDV_GPU(sIQ, PRSSInfo);toc
703 else
704     disp('CPU-based vUS Processing ...(NOTE: it takes around 400 seconds);');
705     tic;[F, Vz, V, pVz, R]=sIQ2vUS_NPDV(sIQ, PRSSInfo);toc
706 end
707 %% 3. save results and plot V and Vz
708 [VzCmap]=Colormaps_fUS;
709 save(['vUS.mat'],'v7.3','F','Vz','V','R','pVz');
710 disp(['Results are saved! - ', datestr(datetime('now'))]);
711 % figure plot
712 Coord.x=PRSSInfo.xCoord; Coord.z=PRSSInfo.zCoord;
713 Fig=figure;
714 set(Fig, 'Position',[300 400 1300 400]);
715 subplot(1,2,1)
716 Fuse2Images(V(:,:,1),V(:,:,2),[-30 30],[-30 30],Coord.x,Coord.z,2.5);
717 title(['vUS, V [mm/s]']);
718 subplot(1,2,2)
719 Fuse2Images(Vz(:,:,1),Vz(:,:,2),[-30 30],[-30 30],Coord.x,Coord.z,2.5);
720 title(['vUS, Vz [mm/s]']);
```

#### 721 A.2. function IQ2sIQ

```
722 %% IQ to sIQ with SVD data processing, sIQ to sIQHP with high pass filtering on sIQ.
723 % Input:
724 % IQ: complex IQ data, obtained with RF2IQ, [nz,nx,nt]
725 % PRSSInfo.SVDrank: SVD rank [low high]
726 % PRSSInfo.HPfc: High pass filtering cutoff frequency, Hz
727 % PRSSInfo.NEQ: do noise equalization? 0: no noise equalization; 1: apply noise equalization
```

```
728 % PRSSinfo.rFrame: imaging frame rate, Hz
729 % output:
730 % sIQ: SVD clutter rejected data, [nz,nx,nt]
731 % sIQHP: SVD+HP clutter rejected data, [nz,nx,nt], cutoff frequency: PRSSinfo.HPfc
732 % sIQHHP: SVD+HHP clutter rejected data, [nz,nx,nt], cutoff frequency: 70 Hz
733 % subfunction:
734 % [sIQ, Noise]=SVDfilter(IQ,SignalRank)
735 function [sIQ, sIQHP, sIQHHP, eqNoise]=IQ2sIQ(IQ,PRSSinfo)

736 A.3. function sIQ2vUS_NP_DV

737 %% US g1 fit for in vivo data, fit negative and positive frequency signal separately
738 % input:
739 % sIQ: bulk motion removed data, [nz,nx,nt]
740 % PRSSinfo: data processing parameters, including
741 % PRSSinfo.FWHM: (X, Y, Z) spatial resolution, Full Width at Half Maximum of point spread function, m
742 % PRSSinfo.rFrame: sIQ frame rate, Hz
743 % PRSSinfo.f0: Transducer center frequency, Hz
744 % PRSSinfo.C: Sound speed in the sample, m/s
745 % PRSSinfo.g1nT: g1 calculation sample number
746 % PRSSinfo.g1nTau: maximum number of time lag
747 % PRSSinfo.SVDrank: SVD rank [low high]
748 % PRSSinfo.HPfc: High pass filtering cutoff frequency, Hz
749 % PRSSinfo.NEQ: do noise equalization? 0: no noise equalization; 1: apply noise equalization
750 % PRSSinfo.rfnScale: spatial refind scale
751 % PRSSinfo.MpVz: maximum pVz
752 % PRSSinfo.useMsk: 1: use ULM data as spatial mask; 0: no spatial mask
753 % PRSSinfo.ulmMsk: ULM-based spatial constrain mask
754 % output:
755 % F: dynamic component fraction, [nz,nx,2], 2: [real,imag]
756 % Vz: axial-direction velocity component, [nz,nx], mm/s
757 % V=sqrt(Vx.^2+Vz.^2), [nz,nx], mm/s
758 % pVz: Vz distribution (sigma-Vz), [nz,nx]
759 % R: fitting accuracy, [nz,nx]
760 function [F, Vz, V, pVz, R]=sIQ2vUS_NPDV_GPU(sIQ, PRSSinfo)
761 function [F, Vz, V, pVz, R]=sIQ2vUS_NPDV(sIQ, PRSSinfo)
```

## 762 B. vUS data processing (SV model) for phantom data

### 763 B.1. Main function

```
764 %% IQ to vUS data processing for ex vivo data using the basic model
765 clear all; clc
766 addpath('./SubFunctions');
767 %% Use GPU calculation or not
768 useGPU = questdlg('Use GPU for data processing?', 'Select', ...
769 'YES', 'NO', 'Cancel', 'Cancel');
770 %% Load data
771 disp(['Loading data, ', datestr(datetime('now'))]);
772 % load ('./DATA/phantomData5a.mat'); % angled flow, preset speed 5 mm/s
773 load ('./DATA/phantomData15a.mat'); % angled flow, preset speed 15 mm/s
774 % load ('./DATA/phantomData9t.mat'); % transverse flow, preset speed 9 mm/s
775 % load ('./DATA/phantomData25t.mat'); % transverse flow, preset speed 25 mm/s
776 % IQ: beamformed complex quadrature data
777 [nz,nx,nt]=size(IQ);
778 PRSSinfo.g1StartT=1;
779 PRSSinfo.g1nT=nt;
780 PRSSinfo.g1nTau=100;
781 PRSSinfo.rFrame=5000; % sIQ frame rate, Hz
782 PRSSinfo.SVDrank=[3, nt];
783 PRSSinfo.HPfc=25; % high pass frequency cutoff
784 PRSSinfo.FWHM=[125 100]*1e-6; % (X, Z) spatial resolution, Full Width at Half Maximum of point spread function, m
785 PRSSinfo.C=1540; % sound speed, m/s
786 PRSSinfo.f0=16.625*1e6; % Transducer center frequency, Hz
787 PRSSinfo.rfnScale=1;
788 PRSSinfo.xCoor=interp(P.xCoor,PRSSinfo.rfnScale);
789 PRSSinfo.zCoor=interp(P.zCoor,PRSSinfo.rfnScale);
790 PRSSinfo.NEQ=0; % no noise equalization
791 %% Clutter rejection
792 disp(['Clutter Rejection - ', datestr(datetime('now'))]);
793 [sIQ, sIQHP, sIQHHP, eqNoise]=IQ2sIQ(IQ(:, :, 1:PRSSinfo.g1nT),PRSSinfo); % 0: no noise equalization
794 [nz,nx,nt]=size(sIQ);
795 clear IQ
796 disp(['Power Doppler Processing - ', datestr(datetime('now'))]);
797 [PDI]=sIQ2PDI(sIQ); % PDI processing
798 disp(['Color Doppler Processing - ', datestr(datetime('now'))]);
799 Vcz0=(ColorDoppler(sIQ,PRSSinfo)); % color Doppler, all frequency
800 disp(['g1-based vUS Processing - ', datestr(datetime('now'))]);
801 if strcmp(useGPU, 'YES')
802     Dev=gpuDevice;
803     disp('GPU-based vUS Processing ...(NOTE: it takes around 4 seconds)');
804     tic;[F, Vz, Vx, V, R]=sIQ2vUS_SV_GPU(sIQ, PRSSinfo);toc
805 else
806     disp('CPU-based vUS Processing ...(NOTE: it takes around 30 seconds)');
807     tic;[F, Vz, Vx, V, R]=sIQ2vUS_SV(sIQ, PRSSinfo);toc
808 end
809 Vcz=imresize(Vcz0, [nz,nx]*PRSSinfo.rfnScale,'bilinear').*CR;
810 save(['./vUS.mat'],'-v7.3','F','Vz','Vx','V','Vcz','R','PRSSinfo','P');
811 disp(['Results are saved! - ', datestr(datetime('now'))]);
812 %% figure plot
813 [VzCmap,VzCmapDn, VzCmapUp, PhtmCmap]=Colormaps_fUS;
814 Coor.x=[1:nx]*0.05/PRSSinfo.rfnScale;
815 Coor.z=[1:nz]*0.05/PRSSinfo.rfnScale;
816 Fig=figure;
817 set(Fig,'Position',[400 400 1700 350])
818 subplot(1,3,1)
819 h1=imagesc(Coor.x,Coor.z,abs(V));
820 colormap(PhtmCmap);
821 caxis([0 30]);
822 colorbar
823 axis equal tight;
824 xlabel('x [mm]')
825 ylabel('z [mm]')
826 title('vUS-V [mm/s]')
827
828 subplot(1,3,2)
829 h2=imagesc(Coor.x,Coor.z,abs(Vz));
830 colormap(PhtmCmap);
```

```
831 caxis([0 30]);
832 colorbar
833 axis equal tight;
834 xlabel('x [mm]')
835 ylabel('z [mm]')
836 title('vUS-Vz [mm/s]')
837
838 subplot(1,3,3)
839 h3=imagesc(Coor.x,Coor.z,abs(Vcz));
840 colormap(PhtnCmap);
841 caxis([0 30]);
842 colorbar
843 axis equal tight;
844 xlabel('x [mm]')
845 ylabel('z [mm]')
846 title('Color Doppler-Vz [mm/s]')
```

847

## 848 B.2. function sIQ2vUS\_SV

```
849 %% US g1 fit, fit all frequency signal, for single flow direction scenario
850
851 % input:
852 % sIQ: bulk motion removed data
853 % PRSSinfo: data acquisition information, including
854 % PRSSinfo.FWHM: (X, Y, Z) spatial resolution, Full Width at Half Maximum of point spread function, m
855 % PRSSinfo.rFrame: sIQ frame rate, Hz
856 % PRSSinfo.f0: Transducer center frequency, Hz
857 % PRSSinfo.C: Sound speed in the sample, m/s
858 % PRSSinfo.gInT: g1 calculation sample number
859 % PRSSinfo.gInTau: maximum number of time lag
860 % PRSSinfo.SVDrank: SVD rank [low high]
861 % PRSSinfo.HPFc: High pass filtering cutoff frequency, Hz
862 % PRSSinfo.NEQ: do noise equalization? 0: no noise equalization; 1: apply noise equalization
863 % PRSSinfo.rfnScale: spatial refind scale
864 % PRSSinfo.MpVz=0; %
865 output:
866 % F: dynamic factor
867 % Vz: axial velocity component, mm/s
868 % Vx, transverse velocity component, mm/s
869 % V: total velocity, mm/s
870 % R: fitting accuracy
871 % CR: vUS data processing criteria mask
872
873 function [F, Vz, Vx, V, R, CR]=sIQ2vUS_SV_GPU(sIQ, PRSSinfo);toc
874 function [F, Vz, Vx, V, R, CR]=sIQ2vUS_SV(sIQ, PRSSinfo);toc
875
```

## 876 B.3. function ColorDoppler

```
877 %% color Doppler data processing to get axial blood flow velocity
878 % input:
879 % sIQ: bulk motion removed data
880 % PRSSinfo: data acquisition information, including
881 % PRSSinfo.rFrame: sIQ frame rate, Hz
882 % PRSSinfo.f0: Transducer center frequency, Hz
883 % PRSSinfo.C: Sound speed in the sample, m/s
884 % output:
885 % Vcz: axial velocity calculated with Color Doppler, mm/s
886 function [Vcz]=ColorDoppler(sIQ,PRSSinfo)
```