

1 **SOL3D: Soft-lithography on 3D vat polymerised moulds for fast,** 2 **versatile, and accessible high-resolution fabrication of customised** 3 **multiscale cell culture devices with complex designs**

4 ***Cathleen Hagemann*^{1,2,7+}, *Matthew C. D. Bailey*^{1,2+}, *Eugenia Carraro*^{1,2,7}, *Valentina Maria*
5 *Lionello*^{2,3}, *Noreen Khokhar*^{2,3,6}, *Pacharaporn Suklai*^{1,2,7}, *Carmen Moreno-Gonzalez*^{1,2,7}, *Kelly*
6 *O'Toole*^{1,2,7}, *George Konstantinou*², *Sudeep Joshi*^{1,2}, *Eleonora Giagnorio*^{2,3,5}, *Mads Bergholt*¹,
7 *Albane Imbert*², *Francesco Saverio Tedesco*^{2,3,4}, *Andrea Serio*^{1,2,7,*}**

8 1. Centre for Craniofacial & Regenerative Biology, King's College London, London SE1 9RT, UK

9 2. The Francis Crick Institute, London NW1 1AT, UK

10 3. Department of Cell and Developmental Biology, University College London, London WC1E6DE, UK

11 4. Dubowitz Neuromuscular Centre, UCL Great Ormond Street Institute of Child Health & Great
12 Ormond Street Hospital for Children, London, UK

13 5. Neurology IV - Neuroimmunology and Neuromuscular Diseases Unit, Fondazione IRCCS Istituto
14 Neurologico Carlo Besta, Milan 20133, Italy.

15 6. Randall Centre for Cell and Molecular Biophysics, King's College London, London SE1 1UL, UK

16 7. Dementia Research Institute (UK DRI)

17 * = *corresponding author*

18 + = *these authors contributed equally*

19 **Abstract.**

20 Cell culture devices, such as microwells and microfluidic chips, are designed to increase the
21 complexity of cell-based models whilst retaining control over culture conditions and have
22 become indispensable platforms for biological systems modelling. From microtopography,
23 microwells, plating devices and microfluidic systems to larger constructs for specific
24 applications such as live imaging chamber slides, a wide variety of culture devices with
25 different geometries have become indispensable in biology laboratories. However, while their
26 application in biological projects is increasing exponentially, due to a combination of the
27 techniques and tools required for their manufacture, and the physical science background
28 sometimes needed, the design and fabrication of such devices directly by biological labs
29 remains a relatively high investment in terms of costs, use of facilities, needed collaborations
30 and time. Whilst commercially available systems are available, these are also often costly,
31 and importantly lack the potential for customisation by each single lab. This combination of
32 factors still limits widespread application of microfabricated custom devices in most biological
33 wet labs.

34 Capitalising on recent important advancements in the fields of bioengineering and
35 microfabrication, and taking advantage of low-cost, high-resolution desktop resin 3D printers
36 combined with PDMS soft lithography, we have developed an optimised low-cost and highly
37 reproducible microfabrication pipeline, capable of generating a wide variety of customisable
38 devices for cell culture and tissue engineering in an easy, fast reproducible way for a fraction
39 of the cost of conventional microfabrication or commercial alternatives. This protocol is
40 designed specifically to be a resource for biological labs with little to none prior exposure to
41 these fields technique and enables the manufacture of complex devices across the µm to cm
42 scale.

1 We provide a ready-to-go pipeline for the efficient treatment of resin-based 3D printed
2 constructs for PDMS curing, using a combination of curing steps, washes and surface
3 treatments. Together with the extensive characterisation of the fabrication pipeline, we show
4 the utilization of this system to a variety of applications and use cases relevant to biological
5 experiments, ranging from micro topographies for cell alignments to complex multi-part
6 hydrogel culturing systems.

7 This methodology can be easily adopted by any wet lab, irrespective of prior expertise or
8 resource availability and will enable the wide adoption of tailored microfabricated devices
9 across many fields of biology.

10 **1. Introduction**

11 Stem cell-based models are an invaluable resource, which allows the study of nearly
12 any cell type *in vitro*¹⁻⁴. The advent of cellular reprogramming and subsequent
13 access to patient-derived stem cell models have also galvanised their position as an
14 ideal tool to investigate cellular processes in health and disease⁵⁻⁹. While stem cell
15 models offer significant control over the identity of cultured cell types, the
16 conventional culture systems used for them typically lack the ability to control key
17 parameters of the culture itself, which greatly influence the analyzed biological
18 processes. These parameters include the relative position of the cultured cells,
19 grouping, cell-cell and cell-material interactions. Although some commercially
20 available devices allow for some control over culture conditions, they are often non-
21 customizable and limited in their application to different research questions.
22 Therefore, it is desirable for biologists to design and manufacture their own custom
23 cell culture devices.

24 Several bioengineering strategies have been developed to create custom-
25 engineered culture environments that direct the cell's environment^{10,11}. To achieve
26 this, two main requirements are necessary: a suitable cell culture material and a
27 method for shaping it into the desired form. PDMS (polydimethylsiloxane) is one of
28 the most used materials for cell culture devices due to its numerous advantages.
29 These include optical clarity, making it suitable for microscopy, and tunable stiffness
30 ranging from 800 kPa to 10 MPa. PDMS also allows for a wide range of chemical
31 modifications. However, PDMS is a porous material that absorbs small molecules
32 and growth factors, necessitating single usage of PDMS constructs and frequent
33 preparation of new devices. For this reason, fast and reliable manufacturing of these
34 devices is often a crucial limit step in several experimental pipelines.

35
36 Most microdevices used in cell culture experiments require features ranging from
37 several millimeters to micrometers, depending on the size of the cells, the required
38 volume of the culture medium and needed experimental paradigm.

39 Several microfabrication techniques have been adapted over the years to the needs
40 of the biology research community, and as a result the use of micropatterned
41 substrates, microchamber devices and other engineered substrates has increased
42 exponentially. One of the most versatile combination of techniques to obtain PDMS
43 devices for biological experiments is photolithography coupled with soft-

1 lithography^{12,13}. Briefly, photolithography is based on the deposition of layers of UV-
2 sensitive photoresist of desired thickness, which is then exposed to a UV source with
3 either a photomask or by direct laser writing to create the desired design, before
4 developing the exposed photoresist. This process can be repeated for multiple layers
5 and allows to create 2.5D designs (i.e. different planar structure of different thickness
6 stacked to form one single set of features)

7 While they can be used to create advanced *in vitro* culture systems with micron-
8 scaled features, photolithography based pipelines also present some limitations; for
9 example, they can only create a single layer at a time with a given height determined
10 by the photoresist layer's properties, and are generally limited in the aspect ratio of
11 the features that they can create. As a result, features are limited to 2.5D designs
12 with defined thickness, lacking 3D volumes, curves, or interconnected shapes
13 (Diagram 1B). Moreover, generating multi-layer constructs for complex features
14 involves multiple photolithographic steps, which can be time-consuming, prone to
15 errors, and costly (Supplement Diagram 1 A-B).

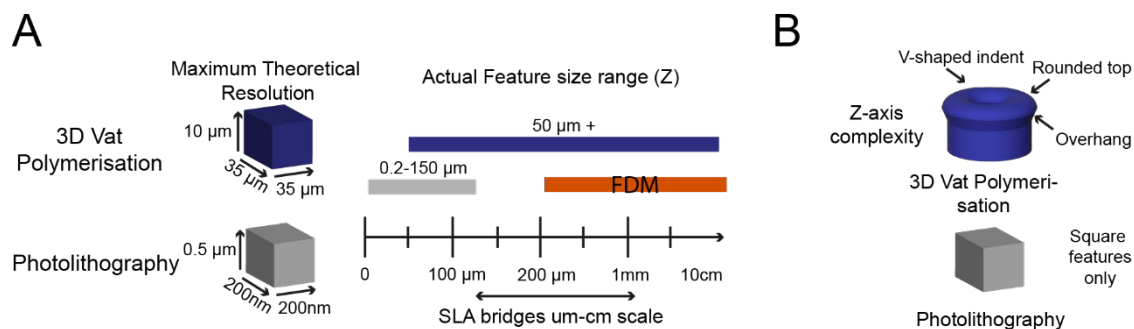


Diagram 1: Comparison between feature constructing techniques; photolithography and UV resin vat polymerisation

(A) Scale comparison of 3D printing methods UV resin vat polymerisation, FDM and photolithography. Comparison of maximal resolution achieved with UV resin vat polymerisation, with current printers, and photolithography. (B) Representation of feature designs achievable with UV resin vat polymerisation and photolithography. UV resin vat polymerisation offers a wide range of feature dimensions and complexity compared to photolithography which underlies technical limitations for designs.

16 While these limitations can be obviated by recent improvements and optimisations in
17 photolithography, such as grey scale photoresist^{14,15} and high resolution 2-photon
18 based lithograph¹⁶, the result is often increased complexity in the fabrication process,
19 and in costs or availability of the necessary instruments.

20 Consequently, it remains challenging for wet labs to perform rapid prototyping of
21 user-handleable macroscale devices with microscale features for cell culture
22 applications. Additionally, specialized facilities and expertise are often required for
23 these techniques, limiting access for many biology focused groups and potentially
24 creating a bottleneck for wider adoption of microfabrication. (e.g., imaging chambers
25 for microscopy with fixed geometry or volume).
26

27 3D printing technology has emerged as an accessible and adaptable tool for fast
28 prototyping and fabrication of small objects. Alongside their increasing availability,
29 rapid technological advancements in 3D printers have led to the development of
30 several open-source projects aiming to enable any wet lab to create and adopt critical

1 and innovative modeling strategies^{17–22}. This is particularly important when
2 considering the challenges experienced by laboratories in less developed countries
3 in sourcing equipment or specific consumables, or the sometimes-steep practical
4 barrier that some labs encounter when venturing into cell culture and biology from a
5 different field.

6 There are a variety of different 3D printing techniques, ranging from filament
7 deposition to vat polymerisation of resins. Most of these basic techniques are
8 commercially available but more complex and intricate techniques have been
9 developed over time, for example two-photon based microfabrication^{23,24}. Although
10 these custom-built, high-resolution setups offer significant advancements, our focus
11 here will be on vat polymerization as it represents the most accessible and cost-
12 effective form of 3D printing with a μm -scale resolution.

13 UV resin vat polymerisation is a specific type of 3D printing based on light-curable
14 resin, that with recent advancements in maximal resolution and pricing, shows the
15 potential to bridge the gap between μm -resolution photolithography and mm-
16 resolution fused deposition modelling (FDM) 3D printers (**Diagram 1A,**
17 **Supplementary 17**), whilst remaining economically accessible to any lab (**Figure**
18 **S1**). Because of the positive characteristics UV vat polymerisation provide while
19 remaining accessible, coupled with the rapid and easy fabrication of complex shapes
20 in 3D, UV resin vat polymerisation represents in theory an ideal technique to create
21 bespoke culture vessels, inserts and other devices to increase complexity within
22 biological experiments without sacrificing control over culture conditions^{25,26}.

23 Unfortunately, most commercially available resins for UV resin vat polymerisation are
24 cytotoxic and cannot be used for cell culture applications²⁷. Additionally, the
25 composition of these resins is often proprietary, and conversion or production of
26 biocompatible resins requires skills limited to dedicated chemistry laboratories²⁸.
27 Some biocompatible resins are commercially available; however, they tend to be sold
28 at a much higher cost than even high-resolution resin, and more than the actual
29 printers in some cases (e.g Phrozen sonic mini 4K printer = GBP 365²⁹, 1L Zortrax
30 Raydent Crown and Bridge resin = GBP 392³⁰), undermining the applicability of 3D
31 SLA printing for cell culture purposes (**Figure S1**), even though these prices can be
32 variable and might change over time but are here used to exemplify the lower cost.
33 Moreover, unlike PDMS and other silicon-based materials used for soft-lithography
34 resins do not have tuneable stiffness and generally are not optically clear and cannot
35 be used for microscopy studies.

36 One possible solution to these problems would be to combine PDMS soft lithography
37 with UV resin vat polymerised 3D printed moulds, and effectively employ 3D printing
38 in lieu of photolithography in conventional pipelines. However, curing of PDMS on
39 vat polymerisation resin prints can be quite challenging as acrylates and
40 triorganophosphate photo-initiators, constituents of most commercially available
41 resins, inhibit PDMS polymerisation^{31–34}. Furthermore, vat polymerisation -resin-
42 induced PDMS curing inhibition makes demoulding difficult and can result in leaching
43 of cytotoxic uncured PDMS monomers into the cell culture medium of even

1 successfully demoulded designs³⁵, making the devices unusable for cell culture
2 applications.

3 To overcome these challenges and facilitate the production of complex 3D constructs
4 suitable for cell culture, several successful post-processing and coating approaches
5 have been attempted^{36–38}. However, these protocols generally involve either long
6 heat and detergent treatments³⁹, which often cause print deformation, or expensive
7 techniques⁴⁰, not accessible to every lab. One example of the latter, coating of UV
8 resin vat polymerised prints with parylene is effective in creating usable moulds, and
9 is sufficient to overcome curing inhibition of PDMS⁴¹, but require the use of
10 specialised equipment and adds another potentially technically challenging step to
11 optimise.

12 Driven initially by our own experience with adapting microfabrication techniques to
13 hard biological questions, and inspired by the many recent technical advancements
14 by different groups, we aimed to create an optimized and universally effective
15 pipelines that would include the production and post-processing protocol for **soft**
16 **lithography on 3D vat polymerised moulds (SOL3D)**, using a low-cost commercially
17 available printer and materials.

18 To demonstrate the applicability of this method to several different biological
19 experiments and provide an effective blue-prints for other labs that don't have
20 expertise in microfabrication, we demonstrated its use to develop customisable
21 culture devices ranging from μm to mm and cm scale, with complex 3D shapes or
22 and micro topographies. Together with the detailed protocols, we also provide the
23 designs for each device showcased, which can be customised to fit different
24 experimental needs.

25

26 **2. Results**

27

28 ***2.1 Optimisation of PDMS curing on 3D SLA printed moulds***

29 To overcome the current barriers preventing the integration of 3D vat polymerisation
30 for the fabrication of tissue culture constructs in biology labs, we aimed to optimise an
31 easy-to-implement and widely applicable protocol to enable efficient PDMS curing on
32 vat polymerised moulds using commercially available equipment. We, therefore,
33 tested a variety of commercially available resins (**Table 3**) subsampling different
34 manufacturers together with a commercially available high-resolution 3D vat printer
35 (300-400 GBP retail price, Phrozen 4K Sonic Mini or Anycubic Photon S equivalent to
36 approx. 2 batches of a monoclonal antibody for immunostaining).

37 First, we verified the previously reported cytotoxicity of each resin following
38 conventional post-processing steps (isopropanol washing, UV curing), either in an
39 untreated state or with supplementary heat treatment, washing and UV sterilisation,
40 by co-culturing chips of resin with induced pluripotent stem cells (iPSC)-derived motor
41 neurons (MNs) (**Figure S2**). Additionally, we tested a grad 2a biocompatible resin
42 used for dental implants. After 4 days of coculture with this resin, the iPSC-derived

1 MNs show despite different washing protocols toxic effects, and a clear visual increase
2 in debris compared to the control well (Figure S16). As none of the resins were suitable
3 for cell culture applications in direct use, we then focused on optimising the post-print
4 processing protocol for resin moulds testing different parameters across three main
5 steps: resin washing, print coating, and PDMS heat treatment curing (**Figure 1A**), to
6 find an easy and fast method overcoming PDMS curing inhibition, as no standardised
7 post-processing protocol exists (**Figure 1B**). Resins were printed using modified
8 manufacturer's settings for the recommended printer (either Anycubic or Phrozen)
9 (**Table 3**) (**Figure 1C**). We tested PDMS curing on the moulds at 6 different time points
10 (2h, 4h, 6h, 18h, 22h, 24h) and considered the sample conditions not optimal for curing
11 if the process took over 30h.

12 The isopropanol washing step is designed to remove excess uncured resin from the
13 printed moulds. We tested two different methods for removal, sonication and stirring,
14 alone or in combination, each for 10 minutes, and found that post-printing washing
15 conditions in isolation have a modest effect on PDMS curing time, but a combinatorial
16 treatment was beneficial. Therefore, all subsequent experiments were performed
17 using sequential treatment with sonication and washing (10 minutes each).
18 Interestingly, we found that resin selection had more impact on curing time than
19 washing itself, with resins A and F performing the best (**Figure 1D**). Washing of resin
20 E and D was unsuccessful in most conditions, due to the amount of uncured resin
21 adhering to the print from improper printing, and subsequent analysis of PDMS curing
22 on these samples would bias the curing time if curing can take place at all.

23 It has been suggested that curing inhibition on resin can result from vaporised acrylate
24 monomers³⁶, which are components of most resins, released into the PDMS during
25 heating. We reasoned that either blocking the contact sites between acrylates and
26 PDMS or reducing the release of acrylates from the resin during curing could be
27 sufficient to allow efficient curing of PDMS on the moulds. To test these hypotheses,
28 we used commercially available enamel paint to homogeneously coat the washed 3D
29 prints with an airbrushing system, forming a protective barrier between the PDMS and
30 resin. We then compared the PDMS curing time of coated prints to uncoated prints at
31 3 different temperatures (60, 75 and 90°C), which allowed us to identify the role of
32 temperature on acrylate release and PDMS curing. These experiments showed that
33 enamel paint coating enabled PDMS curing not only on the surface but throughout the
34 whole cast, and decreased PDMS curing times for all resins. It is important to note that
35 Resin A is a special case, as it showed good PDMS curing performance with and
36 without coating (**Figure 1E**), permitting the use of our post-processing protocol with
37 and without enamel paint. These two protocols differ not only in the coating but also in
38 the curing temperature used, which impacts the overall manufacturing times. The
39 benefit of the missing paint layer of the non-coating protocol is that it allows the
40 manufacture of detailed PDMS moulds (features <300 µm) (**Figure 1G**). Overall, lower
41 temperatures improved PDMS curing times on resins and the variation in the effect of
42 temperature on coated samples was negligible. Additionally, we observed that high
43 temperatures (90°C) resulted in a significant warping of the print. These unwanted
44 effects were less prominent at lower temperatures (60-75 °C), which were still effective
45 enough to cure PDMS.

1 It has also been reported that acrylate monomers and photo-initiators, which are resin
2 components, can leach from the resins into PDMS, impacting the biocompatibility of
3 cast constructs³⁵. To verify that the cured PDMS samples did not have leachates of
4 resins or enamel paint, we used Raman spectroscopy to characterise the chemical
5 composition of samples from each post-processing condition and compared them to
6 cured and uncured PDMS (**Figure S3**). This spectral analysis revealed no detectable
7 carryover of resin constituents or paint into the casted PDMS and high similarity of
8 resin casts to cured PDMS. To further validate these findings, we cocultured resin print
9 cast PDMS substrates with iPSC-derived MNs. These co-cultures demonstrated good
10 biocompatibility over longer culturing periods (**Figure S4**).

11 As introducing a layer of enamel coating on the mould devices could negatively impact
12 fine feature sizes, we used SEM imaging on printed moulds with resin A to quantify
13 whether print dimensions and surface roughness were significantly affected. Analysis
14 showed that coated prints exhibited a thin layer of paint <100 µm and greater surface
15 roughness compared to uncoated ones (**Figure S5**). This limits the application of this
16 method to features larger than 100 µm in any dimension (**Figure 1F**).

17 Overall, we established a fast and robust post-processing pipeline, identified suitable
18 resins and provide a ready-to-use protocol for 3D vat printing. We provide two modified
19 versions of an effective post-processing protocol for **soft-lithography** on **3D** vat
20 polymerised moulds, depending on the design and feature size (**Figure 1G**).

21

22

23

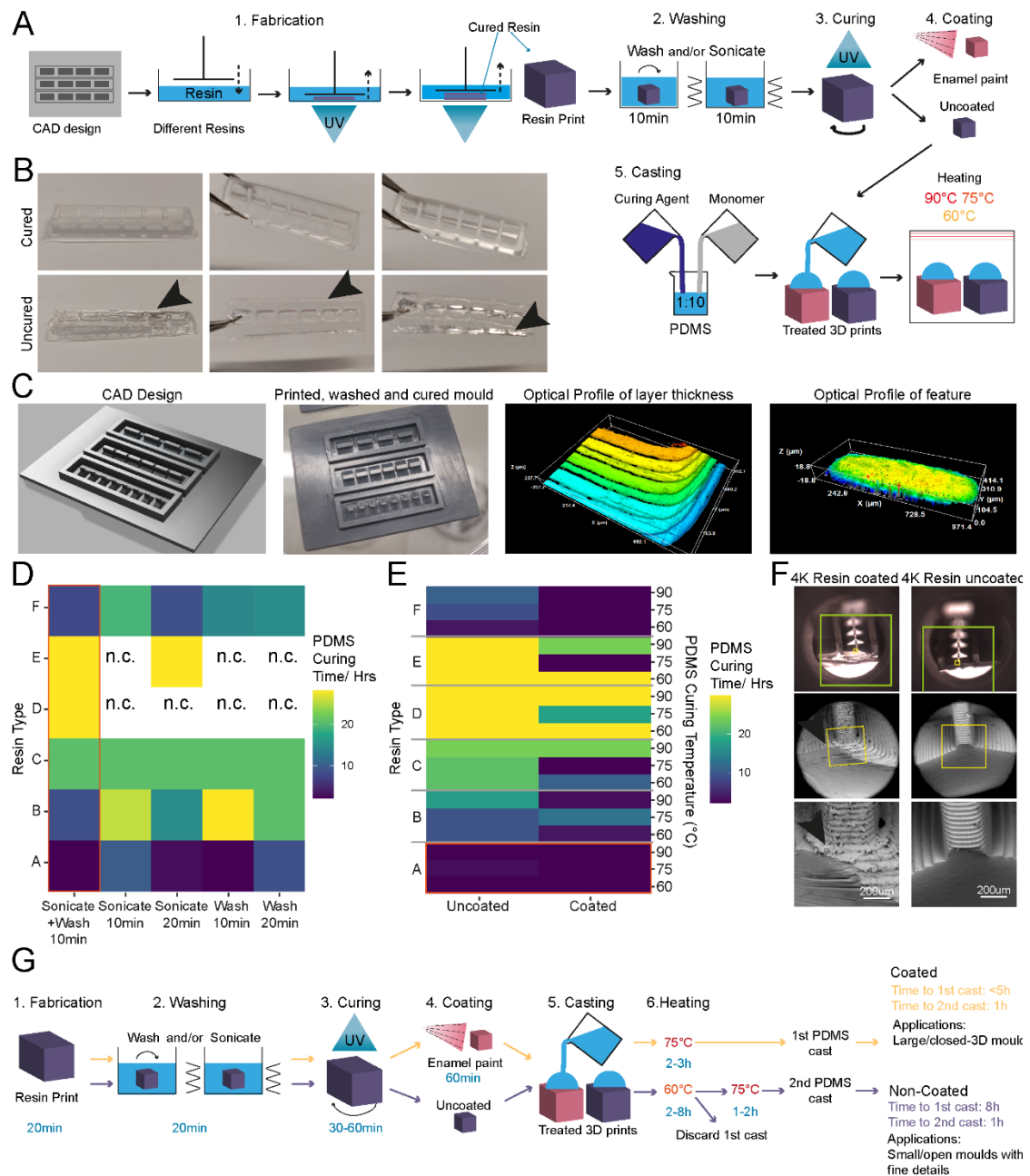


Figure 1: Enamel paint coating facilitates rapid PDMS curing on 3D printed moulds

(A) Schematic overview of the investigation strategy to establish a protocol for PDMS curing on 3D printed moulds (B) Representative images of PDMS casts removed from printed devices classified as cured or uncured. Arrows highlight liquid PDMS. (C) Representative images of a CAD of 3D printed moulds, the completed print, and surface optical profiles of layer thickness and feature dimensions. (D) Heatmap of PDMS curing time by resin type for different washing and curing conditions. (E) Heatmap of PDMS curing time by resin type for different PDMS curing temperatures (right y-axis) and different SLA print coatings. (F) Representative SEM images of uncoated (right) and enamel paint coated prints (left), arrows highlight the paint layer. (G) Schematic overview of optimised fabrication, post processing and PDMS casting protocols with (yellow) and without (purple) enamel coating.

1 **2.2 SOL3D fabrication allows the generation of complex 3D-**
2 **shaped stencils for precise control of cell positioning and**
3 **grouping within open wells.**

4 *3D printed stencil-aided dry plating devices to control cell location and*
5 *number within standard well plates*

6 Conventional open well culture systems generally do not allow control over cell
7 position, grouping, and numbers in an easy and reproducible fashion, limiting the
8 complexity of *in vitro* modelling experiments. Several techniques are available to
9 overcome these limitations and to create precise arrangements of cells within culture
10 vessels -from microfluidic devices to cell bioprinting-, however, most rely on creating
11 compartmentalised structures which limit the manipulation of the cells granted by the
12 open well systems.

13 A different approach that allows both to increase complexity within conventional
14 culture vessels and to maintain an open well system are stencil-like plating devices
15 ^{42,43}. These systems are temporary structures that guide the organisation of cells within
16 an open well, although at present they suffer from the same fabrication limitations as
17 the above-mentioned strategies. Moreover, this method is especially affected by the
18 technical limitations of feature sizes and aspect ratios dictated by photolithography,
19 resulting in thin devices that are difficult to handle and have limited customisation
20 possibilities (**Figure S6**).

21 We decided to use these types of devices, using human induced pluripotent stem cell-
22 derived motor neurons (MNs) as a cell model system, for an initial proof-of-principle of
23 our optimised SOL3D protocol, based on an engineered platform we recently
24 developed for MN cultures using a micropatterned substrate to facilitate axonal
25 elongation ⁴⁴.

26 We combined and optimised this platform with our SOL3D moulding protocol to create
27 a tailored plating strategy for investigating hiPSC-derived MN behaviour with control
28 over cell location and orientation. We designed moulds for casting PDMS stencil-well
29 devices, rectangular extruded features with funnel-shaped media reservoirs as
30 complex 3D features to ease cell seeding. This optimised design permits rapid and
31 facile manual seeding as cells can settle into micro-sized wells in a suitable volume of
32 medium to avoid excessive evaporation and cell death (**Figure 2 A-B**).

33 PDMS stencils from these 3D moulds allow seeding by “dry plating”, whereby a stencil
34 is placed in a dry conventional tissue culture plastic vessel and cells in suspension are
35 manually pipetted in the stencil device, isolating the cell bodies from the residual well
36 and allowing them to adhere at these specific positions. With the cell bodies secured,
37 the stencil device can be removed and the whole well filled with culture medium, while
38 the adhered cells remain in their specified position. For this “dry plating” process, a
39 strong fluidic seal surrounding the PDMS stencil wells is necessary, requiring a flat
40 surface between the stencil and substrate below. Without specific steps to adjust the
41 surface roughness of prints, PDMS casts from 3D printed moulds are inherently
42 rougher than those from micropatterned silicon wafers used for casting

1 microfabricated PDMS devices (**Figure S7**). We, therefore, implemented an additional
2 clamping step before PDMS curing, using a silanised glass slide (see *M&M*) to cover
3 the PDMS surface, which is in contact with air, taking advantage of the flat surface
4 provided by the glass (**Figure S8A**). We evaluated the efficiency of clamp-cured
5 stencil fluid seals when placed on a PDMS micropatterned surface with 10 x 10 μ m-
6 grooves using a blue dye. An effective seal was achieved in all stencils cured using
7 the additional clamping, denoted by dye reaching the microgroove substrate in the well
8 area only and spreading within these specific grooves. Stencils cast without clamping
9 showed uncontrolled dye spreading throughout the devices, verifying a lack of fluid
10 seal (**Figure S8B**).

11 We were then able to use the optimised stencil devices to answer a biological question
12 and investigate the minimum number of iPSC-MNs required to form a self-organised
13 3D neural aggregate on microgrooves for axonal elongation, a process determined by
14 chemotaxis and topography. To achieve this, we used the above-described stencils
15 with a funnel shaped reservoir and rectangular wells, varying in Y-dimension to reduce
16 the stencil well size and control cell amount. The well dimensions were homogenous
17 and faithful to CAD specifications throughout the print sizes down to 50 μ m in Y
18 (**Figure S9**). These PDMS stencil-well devices were placed on the extra cellular matrix
19 (ECM) coated and dried micropatterned surface with axonal guidance grooves⁴⁴, and
20 the iPSC-derived MN cell suspension was manually pipetted into the dry wells of the
21 device. To avoid potential air pockets in the smaller wells, as it is common for non-
22 functionalised PDMS, we performed oxygen plasma treatment on stencils prior to cell
23 “dry plating” (**Figure S10**). Compact rectangular “aggregoids” (i.e. 3D cell clusters
24 generated by reaggregating single cells from a culture) with decreasing size were
25 achieved during seeding and were maintained following device removal. Staining with
26 β -III-tubulin after 7 days in differentiation medium revealed that wells with a size of
27 down to 150 μ m provide suitable cell numbers for aggregate formation. However, the
28 two smallest well sizes did not provide the environment for aggregate formation and
29 cells migrated across the topography (**Figure 2C-D**). Subsequent staining with
30 compartment specific markers showed a clear separation between dendrites and
31 axons in the open well devices of compact aggregoids (**Figure 2E**).

32 In summary, stencil-well devices cast with SOL3D can be used to control cell location
33 in an open well, facilitate control over different cell numbers in the same device, and
34 enable cell compartment specific investigations.

35

36

37

38

39

40

41

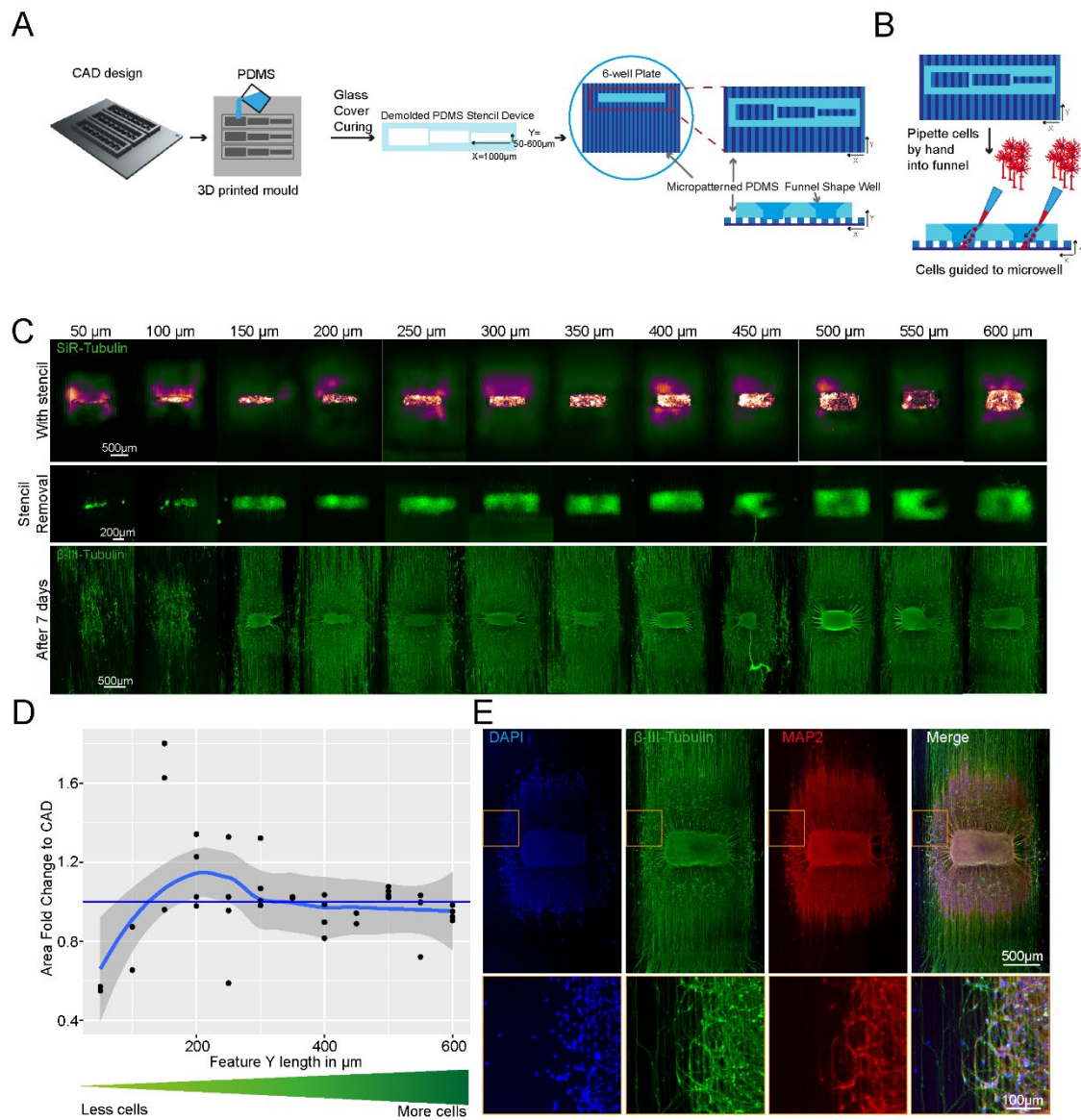


Figure 2: SLA 3D printing enables control over cell location and number in an open well

(A) Schematic overview of the investigation dry plating strategy to combine PDMS casts from 3D printed molds with PDMS microgroove substrate to control cell body location and number. Well sizes range from 600 μm x 1000 μm to 50 μm x 1000 μm in 50 μm intervals (B) Schematic overview of funnel shape well for easy manual seeding in microwells. (C) Representative images of stencil devices filled with pre stained (Silicon Rhodamine-tubulin) MN progenitors with device still in place (top), after device removal (middle), and axonal β -III Tubulin following fixation after 7 days of culture (bottom). (D) Comparison of seeded cell area after stencil removal to CAD specified values by fold change (E) Representative images of 3D aggregoid with 2D axon elongation stained with DAPI (1st image), axonal β -III Tubulin (2nd image), and Dendritic MAP-2 (3rd image) simultaneously (4th image).

1
2
3
4
5

1 *Spatial, temporal and morphological control over cell-cell interaction using*
 2 *tailored plating devices.*

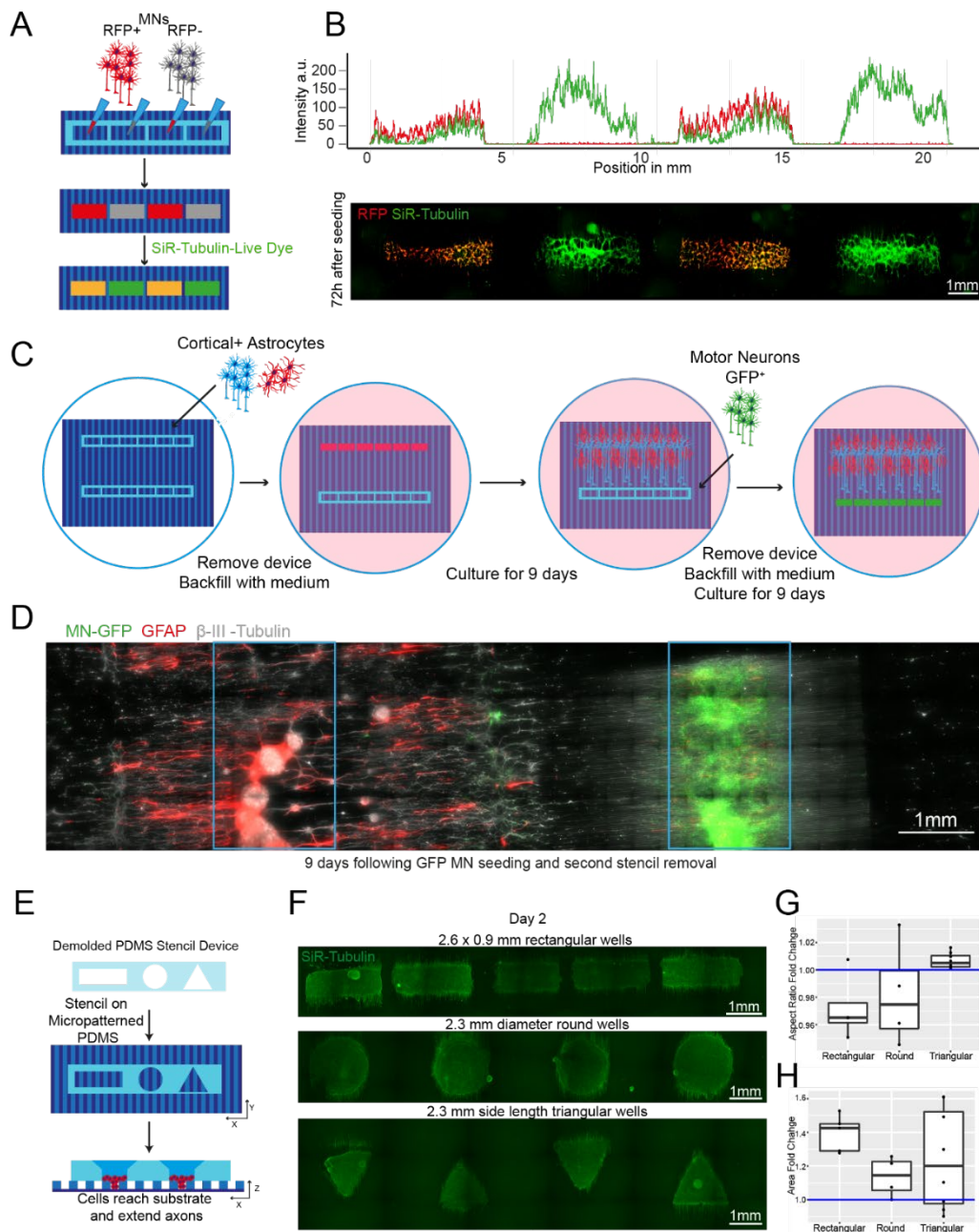


Figure 3: Plating devices enable spatiotemporal control of cell plating with different geometries for construction of complex neural circuits

(A) Schematic overview of alternate seeding of RFP and non-RFP+ motor neurons in the same device and the following live cell staining (B) Representative line profile of stained across the well showing segregation of individual populations to their designated wells – RFP+ only in wells 1 and 3, but SiR-tubulin+ (here in green) in all wells (top). Representative fluorescence images of stained RFP+/- motor neurons (bottom) (C) Schematic overview of the multidevice protocol for constructing a neural circuit using 2 stencil devices and 3 different cell types (MNs, cortical and astrocytes) with seeding performed at different time points (D) Composite of the complete circuit after 19 days of culture. GFP transfected motor neurons = green, Glial Fibrillary Acidic Protein (GFAP) identifies astrocytes, β -III – Tubulin identifies motor neurons and the tubulin in GFP+ motor neurons. Blue device well shapes overlaid for illustrative purposes. (E) Schematic overview of protocol for manipulating aggregate geometry in combination with existing microgroove (F) Representative images of SiR-tubulin live-cell stained motor neuron aggregoids at day 2. (G) Boxplot of aggregoid aspect ratio fold change by shape between CAD (blue line) and day 2 of culture from β -III-Tubulin channel (top). (H) Boxplot of aggregoid area fold change by shape between CAD (blue line) and day 2 of culture from β -III Tubulin channel.

1 We next explored the potential to use SOL3D for more complex cultures, incorporating
2 different cell types and plating timepoints.

3 First, to plate multiple cell populations within the same devices we sought to take
4 advantage of PDMS natural hydrophobicity coupled with the large rectangular well
5 design and funnel shaped well profile showed in **Figure 2A**. The high contact angle
6 between media and hydrophobic PDMS allows to achieve confinement of the different
7 cell suspension droplets, which generates enabling complete fluidic separation
8 between adjacent wells containing different cell populations, even with manual plating.
9 We sought to utilise this strategy to simultaneously plate different iPSC-derived MNs
10 populations within the same tissue culture well in different spatially separate pockets
11 of the PDMS device. For this we used fluorescent RFP⁺ and untransfected MNs, which
12 we plated manually within adjacent pockets in the same device placed on an ECM
13 coated well of a 6-well plate. The different cell populations were left to adhere for 2h
14 before the plating device was removed. After removing the device and further cell
15 culture for 72 hours, all MNs were stained with a silicon rhodamine tubulin dye (here
16 depicted in green for visualisation), to visualise all neurites and cell bodies. A line
17 graph analysis across the whole device showed that all wells contained MNs (RFP⁺
18 and RFP⁻/ Tubulin⁺) and in every second well, RFP⁺ cells were present (**Figure 3A-**
19 **B**), demonstrating multi cell type seeding in confined predetermined spatial groups
20 within a single device.

21 We then sought to further increase the complexity of our *in vitro* cultures by seeding
22 multiple cell types at different time points within the same well, taking advantage of the
23 efficient and reversible fluid seal between our devices and the culture plate. For this,
24 we placed two rectangular plating devices, approximately 2mm apart from each other
25 on an ECM-coated micropatterned surface within a well of a 6-well plate, as described
26 above. Initially, one device was used to dry plate iPSC-derived cortical neurons⁴⁵ and
27 astrocytes⁴⁶ in a 1:1 ratio and removed after 24h, while the other device was kept
28 empty. The whole tissue culture well was then filled with differentiation medium and
29 cultured for 9 days. During this time, cortical axons guided by the microtopography
30 extended toward the empty device, which maintained its initial fluidic seal even
31 surrounded by medium. On day 9, GFP⁺ MNs were seeded in the second device by
32 first lowering the level of the medium within the well to be below the edge of the plating
33 device, and then seeding the MNs in suspension directly within it. After allowing for
34 cell attachment, the second device was also removed, the well refilled with fresh
35 medium and cells cultured for further 9 days. The position of the different cell types
36 was then verified using immunocytochemistry (ICC) for astrocytes (GFAP) and
37 neurons (both MNs and cortical neurons, β -III-Tubulin), as cortical neurons could be
38 identified by the overlap of GFP and β -III-Tubulin. Using these tailored removable
39 SOL3D-generated plating devices we were able to easily plate 3 different cell types at
40 2 different time points within the same culture well, creating a complex neural circuit
41 and demonstrating true spatiotemporal control over cell seeding in a cost-effective and
42 highly adaptable fashion (**Figure 3C-D, Supplementary 11**). Additionally, we
43 demonstrated also multiple time point seedings within the same well using large format
44 “nesting” plating devices which can be used to construct large-scale cell and tissue
45 arrangements (**Figure S12**).

1 Next, we tested whether the ease of available prototyping using our optimised SOL3D
2 protocol could enable investigation and manipulation of the fundamental behaviour of
3 complex iPSC-derived MN cultures. It has been shown that aggregation of cells using
4 different geometries has an influence on the signalling environment and patterning of
5 aggregates⁴⁷. We therefore designed and fabricated moulds for PDMS stencils with 3
6 different well shapes: rectangular, circular, and triangular, to create geometrically
7 constrained neural aggregates. With the advantage of volumetric 3D printing, we were
8 able to preserve the funnel reservoir and straight well design from previous moulds
9 (**Figure 3E**). Using these multi-shaped stencils, we seeded motor neuron progenitors
10 (MNPs) as before on our micropatterned substrate and allowed axons to extend for 11
11 days (**Figure 3E**). Here, MN aggregates maintained faithful area and aspect ratios to
12 CAD specifications on day 2 after stencil removal. After 11 days, the groups also
13 retained their specific geometry although showed slight changes in the aspect ratio
14 and area over time (**Figure 3F-H**). Next, we used these PDMS stencils on
15 nonpatterned and uncoated tissue culture plastics to avoid cell adherence, directing
16 self-organisation of aggregate-like structures (**Figure S13 A**). Here, we seeded
17 cortical progenitors in Matrigel and were able to generate differently shaped
18 aggregates demonstrated by SiR-tubulin live dye images after 24 hours (**Figure**
19 **S13B**). SOL3D fabrication can therefore be used as a valid method of fabricating
20 constructs for controlling cellular interactions in complex cultures of multiple
21 geometries for both 2.5 (i.e. partially tridimensional adherent cultures) and 3D non-
22 adherent cultures (e.g. aggregates) depending on the seeding substrate.

23

24

25

26

27

28

29

30

31

32

33

34

35

1 **2.3 SOL3D fabrication allows the generation of micro** 2 **topographies**

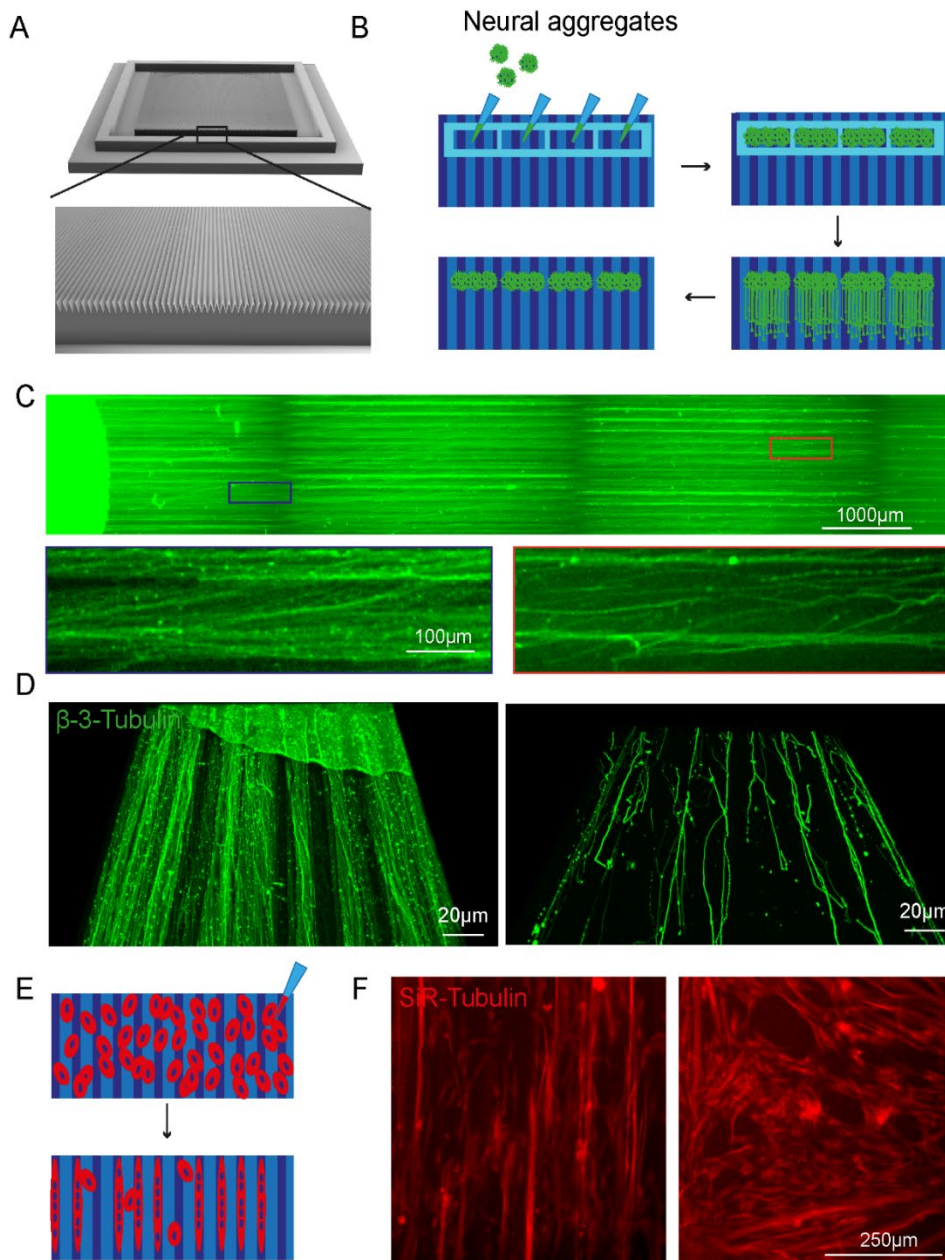


Figure 4: SOL3D fabricated grooves guide axonal elongation and alignment of muscle fibres

(A) CAD design of triangular grooves 100 μ m wide and 200 μ m deep with 75° triangular spacing in between (B) Schematic overview of 'dry' neural aggregate seeding in PDMS stencil devices on the 3D printed grooves and axonal elongation. (C) Representative overview image of axons(β -III-Tubulin) on the SOL3D fabricated grooves with magnifications of axons aligning with the topography in the proximal (blue) and distal (orange) compartment. (D) Representative 3D reconstruction of axons (β -III-Tubulin) on grooves in the proximal (left) and distal (right) compartment. Across compartment axonal alignment to the topography is given. (E) Schematic representation of myoblast seeding and differentiation on SOL3D grooves. (F) At day 3 of differentiation myotubes (SiR-Tubulin) align to the given topography(left) compared to cells cultured on a non-patterned surface (right).

3
4 In the initial experiments presented in **Figures 2 and 3**, we employed SOL3D-
5 fabricated devices on top of microgrooves generated with conventional

1 photolithography. As this method is not available to all labs, we then focused on
2 achieving the same level of organisation within the culture but on a platform purely
3 based on SOL3D-manufactured devices. While the 3D vat polymerisation printers do
4 not have the same resolution as photolithographic equipment, we could not simply
5 recreate the 10 μ m grooves.
6 Moreover, with current LCD-based illumination, repetitive patterns in close proximity
7 to each other and close to the minimal resolution pose a challenge for 3D vat
8 polymerisation printing, due to the illumination pattern and diffraction of the light.
9 However, the key parameter is the biological organisation rather than the material
10 geometry, and we, therefore, focused on obtaining a design that can both be printed
11 with SOL3D and achieves the same neurite orientation. We developed a design with
12 different groove geometry and dimensions (**Figure 4A**), with a groove depth of 200 μ m
13 and width of 100 μ m. Optical profiling of the 3D prints reveals that the grooves are
14 shallower than the CAD design, around 60 μ m, and less wide, as expected (**Figure**
15 **S13**). Despite these limitations, we tested if the topography is sufficient to align axonal
16 elongation. We plated MN neural aggregates⁴⁴ in a SOL3D-manufactured stencil
17 device on SOL3D-manufactured grooves following the 'dry plating' protocol (**Figure**
18 **4B**). Visualisation of axons (β - III-Tubulin) after 7 days of culture revealed an alignment
19 with the topography throughout the axonal length (**Figure 4C-D**).
20 Another process benefitting from alignment to topographies is the formation of
21 myotubes⁴⁸. We seeded myoblasts on the SOL3D grooves and a flat control surface
22 (**Figure 4E**). Cells were differentiated for 3 days and then visualised using SiR-
23 Tubulin. Myoblasts cultured on the patterned surface show alignment to the
24 topography, compared to the control conditions where cells are randomly positioned
25 (**Figure 4F**). While the cells follow the given topography, the differences in size and
26 shape of the SOL3D grooves compared to the photolithography pattern, might evoke
27 different interaction and biological responses, making the two different groups not
28 entirely comparable, but Sol3D manufactured grooves provide a suitable alternative
29 to microfabricated grooves and provide guidance and cell alignment in some
30 circumstances. As a resource, the SOL3D grooves provide a suitable alternative to
31 microfabricated grooves and provide guidance and cell alignment. Taken together with
32 the SOL3D stencil-like devices, a whole on-chip platform can be generated using
33 SOL3D.

34

35 **2.4 Customisable SOL3D fabrication as a tailored alternative to** 36 **standardised commercially available culture platform.**

37 The ability to create customisable devices and substrates suitable for cell culture or
38 other biological experiments, with μ m to cm sized features, in a fast, reliable and cost-
39 efficient manner would be particularly useful in any wet lab, granting independence
40 from high costs, delivery times and availability of the equivalent commercial products,
41 while enabling substantial customisation. For example, most cell culture vessel layouts
42 are standardised and not tailored to the need of an individual laboratory or a specific
43 cell type, causing higher costs and potential compromises in experimental setups. We
44 therefore aimed to test whether our optimised SOL3D mould protocol could be used
45 to reproduce and further customise relevant features from popular commercially

1 available cell culture products. These constructs can be customised in dimensions
2 and/or shapes for individual experimental aims, while remaining cost-effective,
3 highlighting the versatility and accessibility of our system to enhance biological
4 investigations.

5 *PDMS bonding for chamber slide devices.*

6 Chamber slide systems and other microscopy-ready hybrid culture devices are
7 commercially available systems that allow cells to be cultured within neighbouring
8 wells directly on cover slides for high resolution imaging, providing small well sizes
9 and imaging-compatible set-ups for high throughput and convenience. To ascertain if
10 our SOL3D protocol could be applied to mimic these constructs, we designed a
11 chamber slide system which can be permanently bonded to an imaging coverslip
12 either using oxygen plasma treatment or a UV sensitive resin adhesive. Importantly,
13 the adaptation of our construct for use with UV resin makes this method accessible to
14 labs without a plasma cleaning system (**Figure 5A**). Our design was fabricated using
15 the SOL3D protocol and was size matched to a 60 mm x 24 mm microscopy coverslip
16 with 12 circular wells with funnel shapes. As described above, we generated a fluidic
17 seal by clamping the device with a glass slide during PDMS curing to isolate
18 neighbouring wells. This extremely flat PDMS surface allows fusion of PDMS to the
19 glass slide using oxygen plasma bonding, or the simple application of a UV adhesive.
20 It is important to note that the UV adhesive is resin based and therefore cytotoxic and
21 cannot be used on any medium-facing area. Astrocyte progenitors were then seeded
22 into selected wells at different concentrations (**Figure 5B**). Staining with a live dye
23 (SiR-Tubulin) revealed an intact fluidic seal in both devices, liquids maintained in the
24 respective wells, and healthy astrocyte progenitor populations. We further
25 demonstrated the high-resolution imaging compatibility (**Figure 5C**), as cells are
26 seeded on a glass slide. Ostensibly, we have demonstrated that both oxygen plasma
27 and UV resin are suitable for PDMS bonding of a chamber slide device and highlighted
28 the capabilities of 3D printing for the fabrication of bespoke chamber slides in a fast
29 and cost-effective way.

1

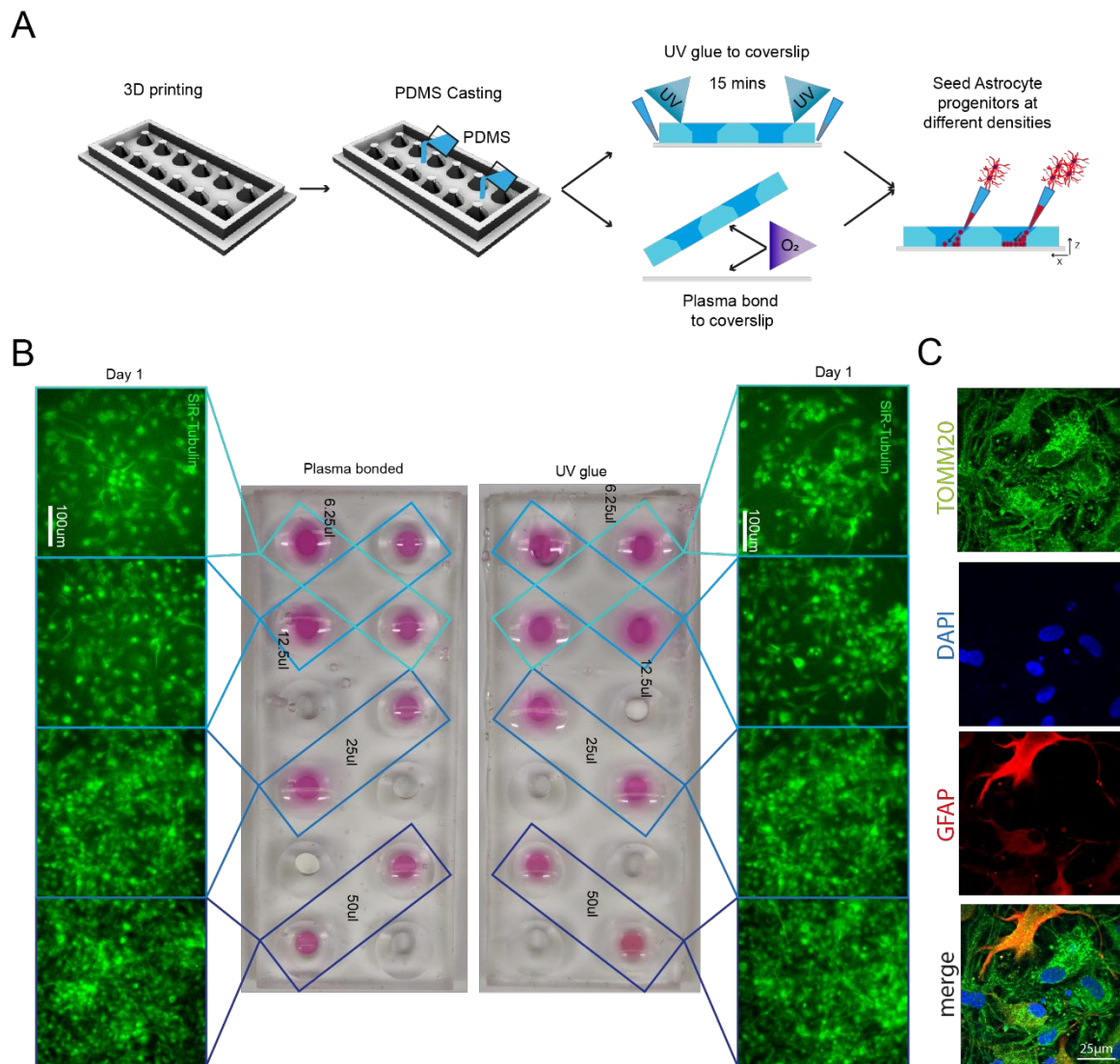


Figure 5: 3D printing can create fully customisable imaging chambers with complex well geometry suitable for cell culture via two different methods of PDMS bonding

(A) Schematic overview of design and manufacture of chamber slide device with large wells with (1) UV glue or (2) oxygen plasma bonding to a glass coverslip to seal the wells. (B) As demonstration of the seal quality and viability for cell culture astrocyte progenitors were seeded in different densities in non-adjacent wells and cultured in chamber slide device. Representative images of SiR-tubulin live dye-stained astrocyte progenitors 1 day after seeding in chamber slides bonded with different methods. (C) High-resolution imaging of astrocytes (GFAP) and mitochondria (TOMM20) cultured in custom made SOL3D PDMS chambers.

2 Custom microwell arrays for embryoid body formation.

3 The first design we tested for this purpose was an array of pyramidal-shaped
 4 microwells (390 x 350 x 150 µm) which we fabricated using the optimised protocol with
 5 no coating step, as it is required for this small feature size (<500 µm) (**Figure 6A-B**).
 6 These microwells have become essential for induction of specific cell lineages from
 7 iPSCs and for aggregate research^{49,50}. One of the most important functions of these
 8 wells is to ensure homogenous aggregate size for reproducible results, for example,
 9 generating embryoid bodies (EBs) of regular size and shape. We used our moulded
 10 microwell arrays to form EBs from an iPSCs suspension (**Figure 6C**) and quantified

1 their size after 4 days of culture on the devices. In our microwells, iPSCs formed EBs
2 with consistent diameters, verifying the suitability of our custom PDMS moulds to
3 create small regular arrays of features (**Figure 6D**). The microwells generated by our
4 protocol are therefore suitable for generation of homogenous EBs with the benefit of
5 substantial customisation of well shape and size at a low cost.

6
7

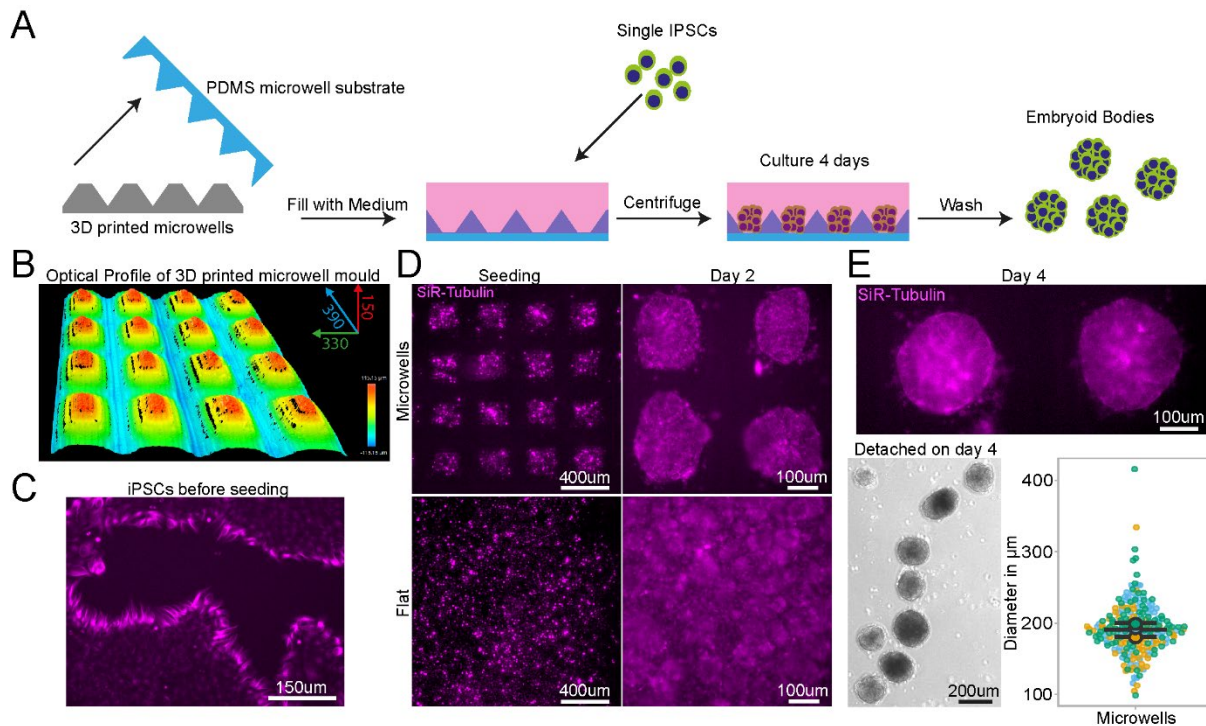


Figure 6: PDMS substrates cast from 3D printed devices permit regular sized embryoid body

(A) Schematic of design, manufacturing and seeding of iPSCs on microwells (B) Representative optical profile of 3D printed microwell device with well sizes of 390 μm length x 350 μm width x 150 μm height. (C) Representative SiR-tubulin live cell dye images of iPSCs before seeding in microwell mould cast. (D) Representative SiR-tubulin live cell dye images of iPSCs seeded on PDMS cast from 3D printed microwell device compared to flat PDMS substrate after seeding (left) and 2 days culture (right). (E) Representative SiR-tubulin image of fused embryoid bodies on microwell PDMS mould prior to detachment after 4 days in culture (top) and embryoid bodies following washing off the PDMS microwell substrate (bottom left). Quantification of embryoid body diameter detached from microwell PDMS mould demonstrates homogenous size of embryoid bodies (bottom right).

8

9 Large tissue engineered devices with complex designs.

10 Generating complex devices for tissue engineering often combines relatively small
11 features within large constructs and has so far proven challenging to implement in
12 most laboratories, as construction processes are complex and time-consuming,
13 requiring dedicated expertise. Most devices of this kind are therefore sourced from
14 commercially available suppliers, with limited possibility of customisation and at a high
15 cost. For example, tissue-engineered 3D muscle constructs use a variety of devices
16 for suspending large cell laden hydrogels during culture using thin suspension posts
17 ^{51,52}. They are comprised of small pillars with complex shaped end feet, which serve to
18 suspend the hydrogel construct and provide mechanical stiffness to aid differentiation.

1 As these posts are difficult to manufacture and arrive pre-made of a single size and
2 shape, no customisation is available, e.g. miniaturization or altered substrate stiffness.
3 Successful 3D adaptations have been implemented for smaller and less complex
4 muscle post, however with low ease of production for 3D SLA printing ⁵³.

5 We used our SOL3D protocol to fabricate a device for suspended 3D muscle culture
6 with customisable post size and overall dimensions. The challenge, in this case, stems
7 from the fact that these devices do not have large flat faces, they present thin complex
8 features and need ideally to be produced as a single component to avoid complex
9 assembly steps that can introduce variability. A single mould system would in this case
10 not be sufficient, as the lack of air in contact with the complex shapes would prohibit
11 the successful demoulding of the structure. We created a two-part mould/injection
12 system using SOL3D, which can easily be assembled by clamping for curing after
13 PDMS is poured into the mould. Optimisation of the moulds showed that an unequal
14 distribution of the design between the two parts (70/30) is beneficial for successful
15 demoulding (**Figure S15**), resulting in a reproducible single device with the desired
16 dimensions, in this case twice as large as the commercial alternative – a 2cm muscle
17 compatible with 12-well plates (**Figure 7 A**). We compared our 12-well plate 3D posts
18 to the commercially available 24-well adapted equivalent (see M&M, *Muscle culture*),
19 using immortalised myoblasts.

20 Following the protocol to generate 3D bioengineered muscle constructs described by
21 Maffioletti and co-workers⁵², we first created a pouring mould by filling liquid agarose
22 around a 3D printed rectangular spacer which was removed after the agarose has set
23 (**Figure S9**). Subsequently, myoblasts were seeded in fibrin hydrogels within the
24 agarose mould, and the SOL3D fabricated posts (or commercially available devices ⁵⁴
25 used in Maffioletti et al.) were inserted within the still-settling fibrin constructs⁵². After
26 2 weeks of differentiation, we performed electrical micro stimulation to measure
27 muscle contractility – a hallmark of successful 3D muscle culture- on both constructs
28 at 20mV with 0.5Hz frequency (**Figure 7 B**), which showed periodic contractions for
29 both SOL3D and control devices. Immunostaining of the muscle tissue showed the
30 presence of terminally differentiated myosin heavy chain (MyHC) and titin positive
31 multi-nucleated fibres in both constructs. Directionality analysis revealed that
32 myofibres were preferentially aligned along the posts (**Figure 7 C, D**). After showing
33 the suitability of our 3D posts for muscle cell culture, we wanted to further demonstrate
34 the customisation of such devices. We first focussed on miniaturisation of the posts,
35 which would allow fewer cells to be used and an increased throughput. We designed
36 and manufactured with the SOL3D protocol insets for 12 (i.e. original size) 24 and 48
37 well plates (Figure 7E). Moreover, as PDMS stiffness can be tuned by changing the
38 ratio between monomer and curing agent, we were also able to produce 24-well plate
39 format muscle devices with different stiffnesses by varying the components ratio
40 (Figure 7 F). As expected, the storage and loss modulus are higher for 1:10 PDMS
41 compared to the 1:20 formulation (Figure 7 G).

42 In summary, our protocol allows for complex and small features to be easily moulded
43 in PDMS comparable to commercially available 3D muscle systems with the additional
44 benefit of customisation in all aspects of design for improved function.

1

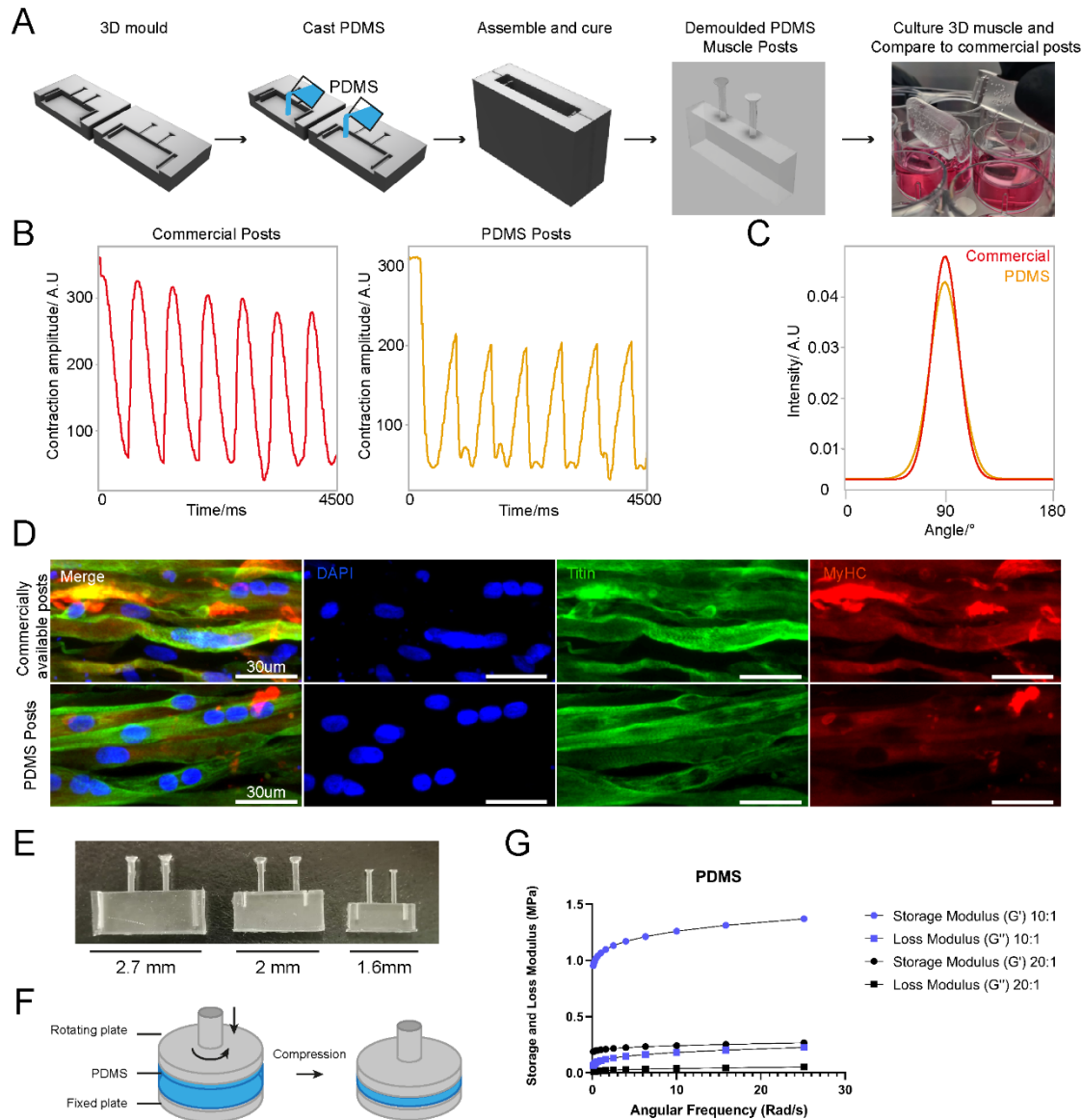


Figure 7: 3D sandwich moulds for PDMS casting to generate complex cell culture devices

(A) Schematic overview of design and PDMS casting strategy for a 3D sandwich mould. Immortalised myoblast hydrogels were then formed around PDMS posts, differentiated and cultured for 2 weeks. (B) Comparative contractility analysis with microstimulation at 20mV with 0.5Hz frequency of differentiated 3D muscle between crafted PDMS posts and commercially available posts. (C) Directionality analysis of fiber alignment in differentiated 3D muscle fibers between PDMS posts and commercially available posts after 2 weeks differentiation. (D) Representative images of myoblast differentiation (Titin) and developmental stage (MyHC) on PDMS posts and commercially available posts after 2 weeks differentiation. (E) Images of posts with different dimensions suited for 12, 24 or 48 well plate (from left to right). (F) Illustration of compressing PDMS to measure the modulus through a lateral and rotating movement. (G) The Storage and Loss Modulus of PDMS with different formulations (1:10 or 1:20) at changing angular frequency.

2 **2.5 Entirely SOL3D fabricated hydrogel moulding, culture and** 3 **imaging system**

4 Hydrogel cultures offer a great opportunity for in vitro 3D modelling, as they are easy
5 to produce, can be tailored to specific applications and provide an *in vivo*-like
6 environment with a complex architecture, and mechanical properties that more align
7 with specific tissues. The low stiffness is a particular advantage for neuronal cultures
8 as the brain is one of the softest matters in the human body, but it also creates

1 challenges in the handling of these hydrogel cultures. Bioprinters can be used to
2 directly form hydrogel cultures with specific shapes and positions of cells within the
3 gel, however, due to the complexity and engineering effort required, accessibility is
4 limited for many labs. Moreover, the use of 3D cultures also presents challenges in
5 adapting conventional culture vessels and plates to the specifics of the hydrogel
6 constructs.

7 We sought to provide a 3D culture system for hydrogels that allows ease of handling
8 and culture of hydrogels, is entirely customisable and cost-effective, requiring no more
9 than the equipment needed for SOL3D to be implemented.

10 We started by designing and manufacturing a PDMS mould for shaping hydrogels.
11 This mould is manufactured using the SOL3D protocol and our clamping system for a
12 flat bottom surface so that the mould stays at the desired position. Once placed,
13 pipetting the hydrogel into the mould and seeding of MNs progenitors is performed
14 manually (**Figure 8A**). To further avoid detachment of the gel from the mould and
15 control medium flow to the construct, we developed a chamber system that can be
16 placed on top of the hydrogel with the mould. The design includes a chamber for the
17 hydrogel and mould that is connected with a funnel to a reservoir on the top. This
18 restricts the movements of the hydrogel and at the same time offers the opportunity to
19 provide medium from the top (**Figure 8B**). The chamber has two round-shaped
20 openings that provide a flow of medium from the respective side of the well (**Figure**
21 **8C**). We also matched the size of the chamber to the size of a 6-well plate, this allows
22 for providing different media from both sides and the top of the device (**Figure 8D**).
23 We used IPSC-derived MNs in a custom-made hydrogel and cultured the construct for
24 7 days (**Figure 8E**). Visualisation of axonal outgrowth in the hydrogel requires
25 fluorescent imaging with a higher magnification. The size of hydrogel constructs limits
26 the simplicity of imaging approaches and usually requires more complicated and
27 expensive setups. We designed an imaging holder which is custom fitted to the size
28 of the hydrogel mould. After staining for axons (β -III-Tubulin), the hydrogel chamber is
29 removed and the mould containing the gel can be easily transferred to the holder. Due
30 to the tailored dimensions, only a small amount of mounting medium is required to
31 cover the sample and then a cover slip is placed on top of the holder (**Figure 8F**). This
32 results in a very tight mounting of the sample, where MNs are close to the glass slide,
33 and minimal disturbance of the sample itself, maintaining the complex architecture
34 (**Figure 8G**). Fluorescent imaging with a low magnification (4x) shows the overall
35 structure of the MN aggregate, and higher resolution images (20x) show that MNs
36 extend long axons in the hydrogel construct (**Figure 8H**). This SOL3D fabricated
37 hydrogel moulding, culturing and imaging system provides an easy and inexpensive
38 system, that is not limited to hydrogels but can be adapted for any 3D system.

39

40

1

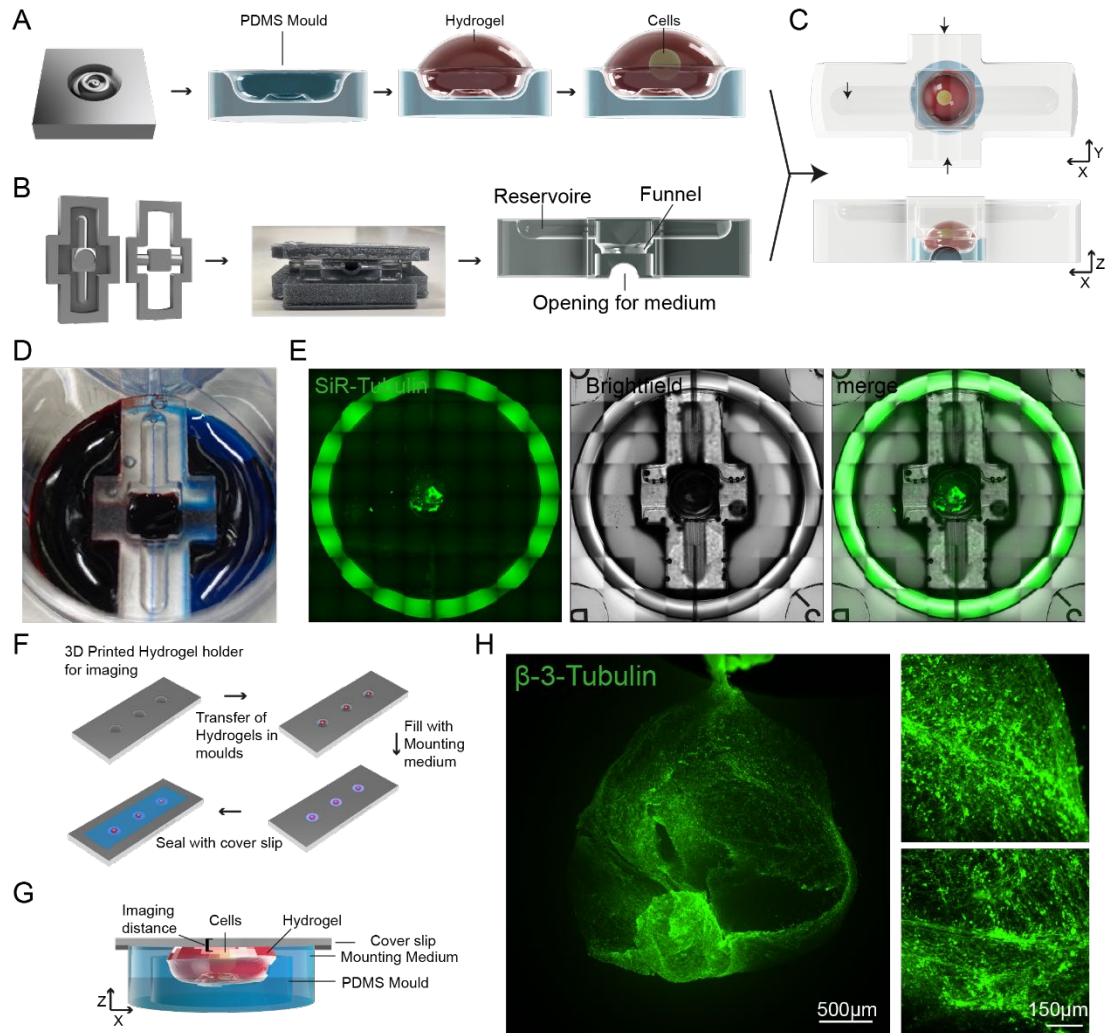


Figure 8: Entirely SOL3D-manufactured hydrogel moulding and culturing chamber system with customised imaging chamber.

(A) Schematic overview of PDMS mould generation for hydrogel moulding and MN seeding. Cells are manually pipetted into a preformed hydrogel moulded in the SOL3D fabricated PDMS mould. (B) Schematic overview of the PDMS chamber manufacturing process using SOL3D. The chamber has a complex design with a funnel shape within the structure and multiple openings. We used a two-part design for ease of demoulding. (C) Schematic overview of the combined hydrogel with MNs placed in the mould (A) and a diffusion chamber around the construct (B), arrows indicate the flow of medium. (D) Optional media compartments highlighted using food colouring (blue, red) and PBS (top). (E) Representative images of the SOL3D chamber system (Brightfield) with MNs (SiR-Tubulin) in culture in a 6-well plate. (F) Schematic overview of the mounting process of the complex hydrogel samples for fluorescent imaging. A SOL3D manufactured holder allows the transfer of whole constructs without disturbance and mounting close to the coverslip for imaging. (G) Schematic overview of the imaging chamber. The PDMS mould sits in the bottom of the well with the hydrogel and cells on top. The sample is surrounded by mounting medium and covered with a thin glass coverslip for imaging. Due to the custom holder system, the distance between sample and glass is minimised allowing for fluorescent imaging. (H) Representative fluorescent images of MNs cultured for 7 days in the SOL3D hydrogel chamber system and mounted in the SOL3D chamber. MNs (β -III-Tubulin) seeded in the hydrogel extend many axonal processes.

1

2 **3. Discussion**

3 In this study, we have developed a fast, high resolution and cost-effective protocol to
4 quickly prototype highly versatile cell culture compatible devices that can be applied
5 to a range of different applications, from live cell imaging to microfluidics and even
6 advanced tissue engineering, which we have called **Soft-lithography with 3D Resin**
7 **moulds using vat polymerisation (SOL3D)**. This methodology allows any lab, even
8 those with very minimal prior expertise in the field or without dedicated resources, to
9 effectively set up a complete microfabrication prototyping system and produce culture
10 devices tailored to their specific biological experiments with minimum expenditure.

11

12 The widespread commercialisation of 3D printing has led to a significant development
13 of resolution and accessibility, which accompanied by free repositories and software
14 packages, have significantly lowered the entry barrier for the adoption of this
15 technique. As a result of this rapid development and the sheer number of new resins
16 and printers becoming available, it is difficult to get an overview of the suitable
17 protocols and materials for a given application. A general protocol for printing and
18 fabrication using any commercially available product is therefore highly desirable.

19

20 We have capitalised on these technological and community developments to
21 overcome one of the primary barriers to complex microfabrication in a biology-focused
22 lab by developing and testing a robust pipeline of fabrication for 3D vat polymerisation,
23 post-processing and PDMS casting, which enables for complete customisation of any
24 cell culture device without further establishment or optimisation. We tested resins from
25 various manufacturers and identified one suitable for PDMS casting and high-
26 resolution prints. In particular, one of the resin compositions performed optimally
27 without the application of a paint layer for high-resolution prints. This feature allows
28 users to exploit the full potential of high-resolution prints, making ink coating for small
29 details redundant³⁸. Interestingly, this resin was originally developed for high-
30 resolution printing and has a noticeably lower viscosity than other resins we tested,
31 parameters to consider when evaluating different resin compositions for this method.
32 However, enclosed prints such as the large tissue culture constructs (**Figure 7**) would
33 still not be able to cure sufficiently without a coating layer which isolates the PDMS
34 from the mould. We also tested Resin A with a different commercially available mid-
35 price SL printer and found no observable difference in print quality, PDMS curing, or
36 biocompatibility, showing easy transfer of optimised parameters for resins to multiple
37 printer systems and designs (data not shown).

38

39 When considering microfabricated devices for biological experiments, especially with
40 cell culture and other *in vitro* set-ups, the topographical features one might want to
41 add can range roughly from sub-cellular scale (<5 µm, e.g. nanoindentations⁵⁵ and
42 other nanostructures⁵⁶), cellular scale (10-100µm e.g. microgrooves⁵⁷ and other
43 microwells⁵⁸), multicellular (200-1000µm e.g. microfluidic channels⁵⁹) or tissue scale
44 (>1mm e.g. aggregate culture devices⁶⁰). In the vast majority of microfabrication
45 pipelines, there is a practical gap at the interface between the cellular and multicellular
46 scale, as conventional photolithography is mostly suited for precise features on the
47 smaller scales and is less suited for multicellular scales. Moreover, combining
48 efficiently multiple fabrication rounds across scales is sometimes challenging, time

1 consuming and error prone. Instead, methodologies such as SOL3D are capable of
2 simultaneously combining cellular, multicellular and tissue scale features within the
3 same fabrication round, effectively filling a gap in the potential toolkits currently
4 available.

5
6 Another advantage here is that SOL3D is not tied to any particular printer or resin, and
7 as such can work for any combination (we have tested several resins over 3 different
8 printers) and with the advent of higher resolution printers this gap will become
9 significantly smaller. We have also demonstrated the versatility of our pipeline by
10 successfully developing cell culture devices of different designs targeted to a wide
11 range of applications, which either confers new capabilities to conventional culture
12 systems (e.g. easily plating multiple cell types on precise spatiotemporal relationships)
13 or customisation of bioengineered culture systems.

14
15 While a number of studies have already proposed similar protocols (e.g. heat curing⁶¹,
16 UV light⁶², micro-diamond coating⁶³), they all generally tend to either have a
17 considerably lower resolution or in some cases require obligatory steps with very
18 expensive specialised equipment that is not generally available to most biological labs.
19 Moreover, the chemicals and materials used in several of these processes require a
20 much higher degree of training and expertise compared to the pipeline presented here,
21 which requires no hazardous processes or chemicals, but only non-toxic and easily
22 handleable components, and could therefore be implemented in a lab without risk.

23
24 In its most minimal implementation, SOL3D requires only a high-resolution (~50µm)
25 desktop vat polymerisation printer, a suitable resin, PDMS and everyday cell culture
26 and microscopy components. All of these resources can be obtained with an initial
27 investment below the cost of 2 vials of monoclonal antibodies and at an estimated
28 running cost of <300USD per year to produce regular medium size batches of devices,
29 which would be affordable to any lab that has an ongoing budget for cell culture
30 consumables. For context, a commercially available single-use 8-well chamber slide
31 suitable for live microscopy with fixed dimensions and no possibility of customisation,
32 ranges between 10 and 15 USD, while a single microfluidic device costs from 50 to
33 120 USD, both of which can be easily replaced by SOL3D.

34
35 One caveat to the capability of the method, which is a limitation due to the properties
36 of PDMS rather than the fabrication process, is that while it is possible to create
37 complex devices without any specialised equipment to effectively use smaller features
38 (**Figure 2**), a step of oxygen plasma treatment was necessary. However, plasma
39 etchers are not available to all labs, potentially limiting the applicability of this protocol.
40 Wang and colleagues tested alternatives to plasma treatment of PDMS persorption of
41 fibronectin sufficient for Caco-2 cells⁶⁴, hence plasma treatment might not be
42 necessary for all cell types and has to be assessed individually.

43
44 Unfortunately, the low compatibility of most UV resins with cell culture experiments
45 also poses limitations to the potential application of this method and vat polymerisation
46 in general. We have characterised several different commercially available resins and
47 found that all of them, in a treated or untreated state, are cytotoxic (**Figure S1**). There
48 are some biocompatible alternatives available on the market (although the extent to
49 which biocompatibility, as defined for dental implants, can be directly applied to stem
50 cell cultures and other more sensitive biological systems needs to be verified) to

1 overcome this fundamental limitation of 3D vat polymerisation, but for a far higher price
2 than any standard resin. Additionally, the fact that resin composition is generally
3 proprietary limits the possible customisations that end-users can achieve. Some
4 providers have recently started publishing their resin composition as well as
5 customised resins generated from a number of research groups that can be recreated,
6 although the burden of adoption of these unique formulations is likely to prevent their
7 use in most cases⁶⁵⁻⁶⁷. Alternatively, modifications of PDMS to be printable can lead
8 to decreased resolution of the print, undermining the strong advantage of high-
9 resolution printers for microfabrication using resins⁶⁸. The solution we implemented for
10 the well-known curing inhibition issues with resin moulds and PDMS is to extract and
11 cure completely the resin first with a multistep preparation (see **Figure 1**) and then
12 further shield the PDMS with a layer of enamel coating.

13
14 The use of PDMS in cell culture experiments has a long history and we have decades
15 of experience with its use with cells and in microscopy applications, however it also
16 has some potential drawbacks. In particular, several groups have reported that PDMS
17 can retain organic molecules and adsorb other substances, which can severely impact
18 biological and biochemical experiments in particular cases^{35,69-71}. However, one
19 advantage of this setup is that it can be used for any soft-lithography material, for
20 example, polymers such as Flexdym, polymethylmetacrylate, or poly(DL-lactide-co-
21 glycolide), as well as with any hydrogel or cure-forming material with a temperature
22 below 70 degrees.

23
24 With this system we aim to empower any lab, regardless of its capabilities, access to
25 resources or prior expertise, to create customised microdevices with features tailored
26 to their specific biological experiments and designed with their biological question in
27 mind, which will significantly lower the barrier for experimentation with microfabrication
28 and tissue engineering applications in any field.

29

30 **4. Materials & Methods**

31 **Cell culture**

32 Control hiPSC motor neuron and cortical neuron progenitors were derived as described⁷² from
33 multiple donors (Table 2). These cells were cultured on Matrigel (Corning) coated plates in
34 base medium, comprised of 50% NeuroBasal (Gibco), 50% advanced DMEM (Gibco),
35 supplemented with B27 and N2 (Gibco), 100 µg/ml Pen-Strep (Gibco), and 2mM L-alanyl-L-
36 glutamine dipeptide (Gibco). For expansion of progenitors, FGF (20 ng/ml) (Gibco) was added
37 to base medium. Differentiation of MN progenitors was achieved using base medium with
38 compound E (Enzo) (0.1 µM) and the growth factors BDNF (10 ng/ml) and GDNF (10 ng/ml)
39 unless stated. Astrocytes were generated from iPSC using a modified protocol described in
40 Hall et al⁷². Derived astrocyte progenitors were cultured in neuronal base medium with FGF
41 (20 ng/ml) (Gibco) and EGF (20 ng/ml) (Thermo). For differentiation astrocytes were cultured
42 in base medium without growth factor supplements. All cells were cultured with 5% CO₂ in
43 humidified atmosphere at 37°C (Table 1).

44 **Transfection of MNPs**

45 For transfection of cells a plasmid based *Piggybac* transposon system was used with pgK-
46 Puro-CMV-GFP and pPb-CAG-RFP-Hygro construct cloned in the lab and a *PiggyBac* vector

1 containing the transposase. Motor neuron progenitors were sparsely cultured on a 24-well
2 plate and one day after passaging transfected using Mirus LT1 (Mirus Bio) transfection
3 reagent. Plasmids were added at total 0.5 µg per well (GFP/RFP+ transposase containing
4 plasmid) in 200 µl of Pen-Strep free growth medium. This solution was gently mixed before
5 addition to the wells which also contained 200 µl of Pen-Strep free medium. The medium
6 containing the transfection reagent was exchanged with growth medium after 24h. Cells were
7 cultured to confluency and then pooled into a 6-well plate for further expansion.

8 **Fabrication**

9 3D printing

10 3D printed moulds were designed using fusion 360⁷³ and tinkercad⁷⁴ computer aided design
11 software, then exported as .stl (stereolithography) files to either Chitubox or Photon workshop
12 slicing software. These software were used to define print parameters such as layer thickness,
13 layer UV exposure time, and lifting/retract speeds for each resin. All resins, printers and print
14 settings can be found in Table 3 and Table 4.

15 Post processing

16 After printing, constructs were washed in fresh isopropanol (IPA) using either/or/both an
17 ultrasonic cleaner and stirring washing bath (Anycubic). Washing method and time were varied
18 as part of the protocol establishment. To ensure fair comparison, washing IPA was filtered for
19 every resin for a given washing condition to remove resin components from previous washes.
20 After washing, all prints were cured in a commercially available curing chamber (Anycubic) for
21 60 mins. Constructs were then selectively coated with a layer of enamel paint (Plastikote)
22 using a hobbyist airbrushing system (Timbertech) diluted 70:30 with water as per manufacture
23 instructions. Painted casts were left to dry at room temperature on the bench for at least an
24 hour before PDMS casting (Table 5).

25 Microfabrication of patterned substrates

26 Microgroove substrates were manufactured from silicon masters patterned using
27 photolithography as previously described ⁷⁵. Briefly, SU-8 2002 (Kayaku) was spun on a silicon
28 wafer for 40s at 1000 rpm on a spin coater (Polos) and prebaked at 95 °C for 2 minutes. A
29 microgroove pattern designed in CleWin5 and containing 10x10 µm grooves with 250 µm
30 plateaus every 5 mm was then etched into the SU-8 via UV exposure and an aligned
31 photomask with the design (Kiss MA6 mask aligner). Excess SU-8 was cleaned with PEGMA,
32 then soft and hard baked at 95°C for 5 mins, before being silanized with trichlorosilane
33 (C₈H₄Cl₃F₁₃Si) in a vacuum chamber for 1 hour. Excess silane was then washed off from
34 masters with 100% acetone. An unpatterned silicon wafer was used for flat substrates. For
35 comparison of surface roughness between 3D printed casts and microfabricated substrates,
36 etching was achieved by a single photolithographic step using a MicroWriter ML3 (Durham
37 Magneto Optics) to form a pattern designed to mimic the potential capabilities of 3D printing
38 in microfabrication. Following the photolithographic step, PDMS casts (prepared as above)
39 were made of the flat or micropatterned silicon wafers, spin coated at 300 rpm for 40s on a
40 spin coater (Polos) to ensure uniform thickness and cured on a hotplate at 100 °C for 5-10
41 minutes (Table 6).

42 PDMS

43 Sylgard-184™ silicone elastomer kit PDMS pre-polymer was well mixed (5 mins) with curing
44 agent at a 10:1 w/w ratio using a digital balance (Sartorius BP610) prior to vacuum desiccation
45 and casting at various temperatures (60-90°C).

1

2 Biofunctionalisation

3 Biofunctionalisation of PDMS substrates and casts from 3D printed moulds was achieved
4 using oxygen plasma treatment (30s, 50%, 7sccm – unless stated otherwise) (Henniker
5 Plasma). Additional biofunctionalisation of micropatterned PDMS substrates to facilitate
6 cellular attachment was achieved using a coat of poly-D-Lysine 0.01% (PDL) (Gibco) for 15
7 min and laminin (Sigma) overnight (unless stated otherwise) (Table 7).

8 Cell Seeding

9 Cells were detached from culture using Accutase (Stem Cell Technologies) and seeded in
10 oxygen plasma treated PDMS constructs cast from 3D printed moulds bound to either tissue
11 culture plastic, flat PDMS, or micropatterned PDMS substrates. Cells were concentrated to
12 300 μ l per detached well and seeded in differentiation media with Compound E (Millipore).
13 Following initial plating, cells were left to settle for 2 hours in constructs. Cells were then
14 washed 2x with PBS to remove unattached cells from constructs and wells filled with
15 differentiation media supplemented with Compound E with constructs left in place. After 24
16 hours in culture, cells were washed with PBS and constructs removed before a 1:100 Matrigel
17 spike for >2 hours and culturing cells (as above) in differentiation media supplemented with
18 Compound E for 7 days (or as stated). For longer term experiments media was selectively
19 supplemented with additional BDNF and GDNF growth factors depending on the experiment.

20

21 Immunostaining

22 Prior to staining cells were fixed in 4% PFA (Boster) for 15 min (unless stated otherwise) and
23 washed 3x with PBS. Cells were then permeabilized with 0.1% Triton-X for 10 min and blocked
24 with 3% goat serum (GS) (Sigma) for 30 mins at room temperature (unless stated otherwise).
25 Antibodies diluted in 0.05% Triton-X and 1.5% GS in PBS were then used to stain cells for
26 markers of interest. Antibodies and their concentrations can be found in Table 10. Primary
27 antibodies were incubated for 1 hour at room temperature in the dark, before washing 3x with
28 PBS. Secondary antibodies were then incubated for 30 min at room temperature in the dark,
29 before washing 3x with PBS. All secondary antibodies were incubated at a final concentration
30 of 2 μ g/ml (Table 11). For some experiments, stained cells were then mounted on glass slides
31 using FluorSave (Millipore). Otherwise, cells were kept in PBS at 4°C until imaging. For live
32 cell imaging cells were incubated with 1:10,000 (100nM) silicon rhodamine tubulin (SiR) live
33 cell dye (Spirochrome) for 1 hour before removal of the dye and imaging.

34 Microscopy

35 Cells were imaged using an encased Nikon eclipse TE2000-E fluorescence microscope
36 running Micromanager software with 4x, 20x LWD and 20x SWD objectives, cool LED pE-
37 4000 16 LED light source, and a Prior controlled stage. An LED driver Arduino controlled light
38 source provided illumination for brightfield imaging. To allow longitudinal and live imaging, the
39 microscope chamber was humidified and heated to 37.0°C with 5% CO₂ using a CAL3300
40 incubator temperature regulator (Solent Scientific) and CO₂ regulator (Okolab). Humidity, CO₂
41 balance, and temperature were regulated by further encasing the plate in a sealed custom 3D
42 printed chamber with humidified CO₂ inlet.

43

44

1

2 **Surface Characterisation**

3 Optical profilometry

4 Quantification of 3D printed mould dimensions and surface roughness was achieved using a
5 Sensofar S Neox optical profilometer to measure features in X and Y, and layer thickness.
6 Multi-image z-stacks were captured over stitching areas with 25% overlap using a 20x Nikon
7 EPI objective and surface-variation scanning mode. For analysis of patterned silicon master
8 feature dimensions and PDMS cast surface roughness from both 3D printed moulds and
9 silicon masters, multi-image z-stacks were captured of stitching areas with 25% overlap using
10 a 20x Nikon DI objective and confocal scanning mode. Analysis of features was conducted
11 using in-built analysis tools. Plane correction was conducted on all images to reduce bias
12 within imaged ROIs.

13 SEM

14 Samples of coated and uncoated 3D printed moulds were sputter coated with a 10 nm thick
15 layer of Platinum using a Quorum Q150R coater and imaged by a Phenom ProX Desktop
16 SEM (Thermo Scientific) at an acceleration voltage of 10kV (unless noise was too high, then
17 5kV was used). Images of the surface and cross section of prints was captured to investigate
18 the thickness of applied paint and identify changes in surface roughness/topography. Images
19 were processed in ImageJ FIJI ⁷⁶(Table 8).

20 **Image analysis**

21 All image analysis was conducted in ImageJ FIJI software, processed using R, and presented
22 with R or super-plots-of-data app ⁷⁷ unless stated otherwise.

23 Line Graph Analysis

24 To quantify cellular segregation within the same device/multiple devices threshold
25 fluorescence intensity was adapted to improve signal-to-noise ratio. A rectangular area was
26 then drawn over the cells of interest and fluorescence intensity plots were obtained for each
27 point.

28 Area and aspect ratio

29 Measurements of seeded cell area and aspect ratios were compared to either CAD
30 specifications or 3D printed mould feature dimensions. Cell measurements were taken from
31 the borders of aggregates using tubulin markers Silicon-Rhodamine tubulin (live) and β III-
32 tubulin (fixed). 3D printed mould dimensions were obtained using SensoScan software in-built
33 analysis tools.

34 **Resin biocompatibility**

35 Chips from each of the 6 resins printed using 50 μ m layer thickness printer settings (Table 4)
36 and post processed as above (20 mins sonication & wash, 60 mins UV cure) without enamel
37 coating. Chips were then either sterilised with UV for 15 mins, or baked for 4 hours at 75°C,
38 washed in PBS for 72 hours at 50°C, and UV sterilized for 15 mins before being added to
39 cultures of motor neuron progenitors pre-stained with SiR-tubulin cytoskeletal live dye. Cells
40 incubated with untreated chips were left for 48 hours before imaging. Cells incubated with
41 treated resin chips were live imaged for the first 24 hours in culture, then again at 48 hours
42 with control wells not containing any resin. Investigation of the Ortho dental clear resin, was
43 performed on cylinder shaped resin prints, that can be used as an inset to tissue culture wells.

1 The resin prints were either treated using our SOL3D protocol or the washing protocol
2 suggested by the manufacturer. The processed resin tubes were then inserted into wells
3 containing a known number of iPSC-derived MNs and cocultured for 4 days.

4

5 **Microwell arrays**

6 Microwell arrays of repeating 400 μm x 400 μm x 150 μm pyramids were 3D printed at 10 μm
7 layer thickness (Table 4) and post processed as above (20 mins sonication & wash, 60 mins
8 UV cure) without enamel coating. PDMS (prepared as above) was casted and left un-
9 biofunctionalised to enhance EB formation through PDMS hydrophobicity. Single iPSCs pre-
10 stained with SiR-Tubulin live dye were then seeded on microwell arrays or flat PDMS in E8
11 flex medium (Thermo) and centrifuged for 1 min at 100 rpm to settle cells into microwells. Cells
12 were cultured for 4 days, imaged directly after seeding, and at day 2 and 4 of culture. After
13 imaging on day 4 the regular EBs were detached from microwells and imaged to measure
14 their size.

15 **Chamber slide**

16 **Manufacture**

17 A 3D design with 12 wells with 5 mm diameter funnel and 3 mm diameter 1 mm deep straight
18 well was 3D printed with Resin A at 50 μm layer thickness (Table 3) on the Phrozen Sonic
19 mini 4K and post processed as above (20 mins sonication & wash, 60 mins UV cure) with
20 enamel coating. PDMS (prepared as above) casts were made of the arrays and bonded to
21 glass coverslips with two methods.

22 **PDMS bonding**

23 **Oxygen Plasma**

24 The surface of PDMS casts from 3D printed moulds and glass coverslips were oxygen plasma
25 treated (30s, 50%, 7sccm) (Henniker Plasma), sealed together, and baked at 75°C for 15
26 mins.

27 **UV glue**

28 The surface of PDMS casts from 3D printed moulds was sealed on glass coverslips and clear
29 photopolymerisable resin was applied round the exterior of the PDMS. Through visual
30 inspection we verified that the glue is only applied on the outside of the device and cannot
31 physically leak into the wells. This was verified though live cell imaging on the chamber device,
32 a uv resin is highly toxic for cells and would have resulted in immediate cell death. Resin was
33 cured via 1 minute UV exposure with a 365nm UV torch (Alonefire).

34 **Biofunctionalisation**

35 Plasma and UV bonded PDMS chamber slide devices were then sterilised with UV for 15 mins
36 (Analytik Jena UV light) and biofunctionalized with a coat of poly-D-Lysine 0.01% (PDL)
37 (Gibco) for 15 min and laminin (Sigma) overnight in each well.

38 **Seeding**

39 Control 3 astrocyte progenitors pre-stained with SiR-tubulin live dye were then seeded (as
40 defined in methods section – Cell Seeding) after concentration (1 confluent well in 400 μl
41 media) in expansion media with decreasing density in alternate wells of the chamber slide
42 device. Cells were seeded in 50 μl , 25 μl , 12.5 μl , 6.25 μl fractions of the concentrated cell

1 stock, left to settle for 10 mins, before additional media was added. Cells were cultured as
2 before (Methods – Cell Culture) and imaged after 24 hours to qualitatively assess viability at
3 different densities.

4

5

6

7 **3D muscle**

8 Preparation, differentiation and culture

9 3D muscle constructs were prepared as previously described^{52,78}. Rock inhibitor (Cell
10 guidance systems) at a concentration of 10 μ M was added to cells 2 hours prior to preparing
11 gels. Per construct 1 x 10⁶ AB1190 myoblast cells were used in a total volume of 120 μ l
12 comprised of 3.5 mg/ml of human fibrinogen (Baxter, TISSEELDUO 500), 3 U/ml of thrombin
13 (Baxter, TISSEELDUO 500), 10% Matrigel (Corning, 356231), and inactivated myoblast
14 medium (20-30 mins at 56°C) (PromoCell skeletal muscle cell growth medium, C-23060). The
15 mix was pipetted into agarose moulds containing posts and placed at 37°C, 5% CO₂ for 2
16 hours allowing hydrogels to polymerise. These moulds were prepared in 12-well plates using
17 2% UltraPure agarose (ThermoFisher Scientific, 16500500) (**Figure S8B**). A ring was placed
18 underneath the arms of the posts and inserted onto a 12-well plate to determine the distance
19 the posts can be pushed down into the agarose (**Figure S8C**). DMEM (Sigma, D5671) was
20 then added to the construct and the posts containing the muscle construct was removed from
21 the agarose mould and placed into a new 12-well plate with myoblast medium containing 33
22 μ g/ μ l aprotinin (Sigma, A3428) at 37°C, 5% CO₂. After 48 hours, the muscle construct was
23 placed in differentiation media (DMEM with 0.01 mg/ml insulin (Sigma, 10516) and 33 μ g/ μ l
24 aprotinin), media was changed every other day.

25 Contractility analysis

26 Artificial muscle contractility on 3D print moulded PDMS and commercially available posts⁵⁴
27 was achieved via microstimulation using an in-house stimulator system with a pair of
28 autoclaved pacing carbon electrodes (EHT-technology) mounted in the well containing the 3D
29 muscles dipped gently into the media. The stimulator was set to deliver 5 ms bipolar square
30 pulses of 20mV with 0.5Hz frequency. Muscle contraction and post holder movements were
31 recorded over a period of 5 seconds during stimulation via DinoLite Edge microscope
32 (DinoLite) mounted underneath the posts of each device. Analysis of footage was conducted
33 in Imagej using the MuscleMotion plugin.

34 Immunocytochemistry

35 After contractility recordings, 3D muscle constructs were fixed in 1% PFA overnight before
36 removal from posts. Constructs were then permeabilised and blocked for 6 hours in TBS
37 0.05M (1X) pH7.4, 10% FBS, 1% BSA, 0.5% Triton X-100 at 4°C. Prior to overnight incubation
38 with primary antibodies for Titin and MyoH (Table 10) at 4°C in TBS 0.05M (1X) pH7.4, 1%
39 BSA, 0.5% Triton X-100. The following day constructs were washed 6 times in PBS before
40 overnight incubation with secondary antibodies and DAPI at 4°C in TBS 0.05M (1X) pH7.4,
41 1% BSA, 0.5% Triton X-100. Finally, constructs were mounted on Brand™ Cavity Slides with
42 Fluoromount G (Thermo) prior to imaging.

43 Differentiation and directionality analysis

1 Images of 3D muscle constructs were captured using an inverted Zeiss confocal with a 40x
2 objective. Z-stacks were taken across the constructs and projected using the SUM function in
3 ImageJ. Single images were isolated, and directionality measured from titin signal using the
4 directionality plugin in ImageJ.

5 **Rheometric analysis**

6 PDMS 1:10 and 1:20 rheological properties were measured after 60 min of curing at 75°C, by
7 means of the Discovery HR20 rheometer (TA instrument). Samples were analysed at room
8 temperature (25°C), using an 8 mm plate geometry, with a frequency sweep of 1 and an
9 angular frequency from 25.12-0.1 rad/s. Storage (G') and loss (G'') moduli were measured for
10 the entire period. Young modulus (E) was calculated following the equation⁷⁹.

$$11 \quad E = 2G'(1 + \nu)$$

12 Where G' is the storage modulus and ν is the Poisson ratio (0.5).

13

14 **Hydrogel culture system**

15 Hydrogel composition:

16 Preparation steps started by measuring neuronal culture medium (4 mL) and homogenously
17 mixed with Matrigel (Corning) (1 mL). Hyaluronic acid (5 mg/mL) from Sigma Aldrich was
18 mixed in the above solvent and stirred for overnight (12 hours) at ambient temperature. This
19 was followed by addition of Fibrinogen (45 mg/mL) from Sigma Aldrich and stirred for 5 hours
20 at room temperature. As a final step, Alginate (5% (w/v)) from Sigma Aldrich is added to the
21 above mixture and was allowed to be stirred overnight to obtain a homogenous hydrogel
22 matrix. Motor neuron progenitors were dissociated from a 6-well plate using EDTA in PBS and
23 were gently mixed with the hydrogel matrix (4-5 Million cells/mL) by pipetting them up-down
24 gently for homogenous distribution of cells throughout the hydrogel, this led to the formation
25 of bio-ink. This bio-ink is crosslinked by a 50:50 solution consisting of calcium chloride (CaCl_2)
26 (1.5% (w/v)) and thrombin (25 U/mL in 0.1% BSA Solution). Bio-ink is allowed to be
27 crosslinked for the duration of 15 minutes at room-temperature. After crosslinking, the bio-ink
28 was washed with PBS solution for 3 times. This was followed by flooding the wells gently
29 through the walls of cell plate with neuronal culture media supplemented with Compound E
30 and kept in incubator at 37 °C with 5% CO_2 .

31

32 **2.2 Materials**

33

34 **Table 1: Cell culture**

Supplier	Reagent/apparatus	Catalogue number	Stock concentration/mass
Gibco	B27 supplement	17504044	50x
Gibco	N2 supplement	17502048	100x
Gibco	Pen/Strep	15070063	5,000 U/mL

Gibco	Neurobasal medium	21103049	N/A
Gibco	Advanced DMEM/F-12	12634028	N/A
Corning	Matrigel	354230	N/A
Stem Technologies	Cell Accutase	A6964-100ML	N/A
Gibco	GlutaMAX™ Supplement	35050061	N/A
Millipore	Compound E	ALX-270-415-C250	250 µg/ml
Invitrogen	EDTA	15575-038	0.5M
Gibco	DPBS	14190-094	N/A
Gibco	FGF	PHG6015	50 µg/ml
Thermo Fisher	EGF	PHG0311	50 µg/ml
Beckman Coulter	Allegra centrifuge 21R	BE-A21R	N/A
PHCHD	CO ₂ Incubator	MCO-230AICUV	N/A
Thermo Fisher	BDNF	PHC7074	10 µg/ml
Thermo Fisher	GDNF	PHC7045	10 µg/ml
Baxter	Thrombin	TISSEELDUO 500	3 U/ml
Baxter	Fibrinogen	TISSEELDUO 500	3.5 mg/ml
Thermo Fisher	UltraPure Agarose	16500500	2%
Cell guidance systems	ROCK inhibitor (Y-27632)	SM02-5	10uM
Promocell	Skeletal muscle growth medium	C-23060	N/A
Sigma	aprotinin	A3428	33 µg/µl
Sigma	Insulin	10516	0.01 mg/ml
Sigma	DMEM	D5671	N/A
Thermo Fisher	E8 flex	A2858501	N/A
Mirus Bio	Mirus LT1 reagent	MIR 2300	See description
Sigma	BSA	A2153-10G	N/A

1

2

3

Cell lines	Name	Donor Age	Donor Sex	Mutations present
iPSC/ Motor neuron/ cortical/ astrocyte progenitors	Control 1	78	Male	None
iPSC/ Motor neuron/ cortical/ astrocyte progenitors	Control 2	64	Male	None
iPSC/ Motor neuron/ cortical/ astrocyte progenitors	Control 3	unknown	Female	None

iPSC/ Motor neuron/ cortical/ astrocyte Progenitors	Control 5	51	Male	None
AB1190 Human immortalised myoblasts	Paravertebral muscle	16	Male	None

1 **Table 2: Cell lines**

2

3

4

5 **Table 3: Resins**

Supplier	Resin	Synonym
Phrozen	Aqua Gray 4K	A
Elegoo	ABS-like	B
Anycubic	Clear	C
Liqcreate	Flexible X	D
Liqcreate	Premium Tough	E
Phrozen	Water-washable model Gray	F
NextDent	Ortho Clear	

6

7

8

9

10

1 **Table 4: 3D Printer Fabrication**

Supplier	Resin	Printer	Layer thickness (μm)	Layer exposure time (s)	Bottom Exposure time (s)	Bottom Layers	Transition layers	Light off delay (s)	Z Lift Distance (mm)	Lift speed (mm/min)	Retract speed (mm/min)
Phrozen	Aqua Gray 4K	Phrozen sonic mini 4K	50	6.0	50	6	0	9	5	65	150
Phrozen	Water-washable model Gray	Phrozen sonic mini 4K	50	2.5	25	4	0	9	5	65	150
Elegoo	ABS-like	Anycubic Photon S	50	9.0	60	6	0	1.5	6	180	180
Anycubic	Clear	Anycubic Photon S	50	10.0	50	8	0	1	6	180	180
Liqcreate	Premium Tough	Phrozen sonic mini 4K	50	6.0	75	1	6	9	5	65	150
Liqcreate	Flexible X	Phrozen sonic mini 4K	50	18.0	70	1	6	9	5	65	150
Phrozen	Aqua Gray 4K	Phrozen sonic mini 4K	10	1.8	37.5	6	0	10	5	55	150

Next Dent	Ortho Clear	Phrozen sonic mini 4K	50	4.6	30	6	6	10	6	60	150
-----------	-------------	-----------------------	----	-----	----	---	---	----	---	----	-----

1

2

3 **Table 5: Post Processing**

Supplier	Apparatus
Fisher Scientific	Molecular biology grade isopropanol
Anycubic	Wash and Cure 2.0
Life Basis	Ultrasonic cleaner 600ml
KNF	Laboport N86 mini diaphragm vacuum pump
Timbertech	Timbertech airbrush ABPST01 with air compressor
Plastikote	B35 chrome fast dry enamel paint
Thermo Fisher	HeraTherm oven

4

5 **Table 6: Microfabrication**

Supplier	Reagent/Apparatus	Catalogue code
Kayaku	SU8 - 2002	N/A
Karl Suss	MA6 mask aligner	N/A
Sigma Aldrich	Trichlorosilane	448931
Sigma Aldrich	PEGMA	409537
Fisher Scientific	Acetone	13277983
Fisher Scientific	Vacuum Desiccator	11852732
Durham Magneto Optics	MicroWriter ML3	N/A
Polos	200 NPP Spincoater	42839

6

7 **Table 7: PDMS soft lithography and biofunctionalisation**

Supplier	Reagent/Apparatus	Catalogue code
Dow Chemical	Sylgard 184 PDMS kit	01673921
Sartorius	BP610 balance	Z266906
Henniker Plasma	HPT-100	N/A
Gibco	Poly-D-lysine	A38904-01
Sigma Aldrich	Laminin	L2020-1MG
Analytik Jena	UV lamp	UVP XX-15S
Frenshion	Clear UV Resin	B0823HDLM8
Alonefire	SV003 10W 365nm UV torch	B07SWW5FHB

8

1 **Table 8: Surface characterisation**

Supplier	Reagent/Apparatus	Catalogue code
Phenom	ProX Desktop SEM	N/A
Sensofar	S Neox optical profiler	N/A
Quorum	Q150R coater	N/A

2

3

4 **Table 9: Immunocytochemistry**

Supplier	Reagent	Catalogue code
Sigma Aldrich	Goat serum	G9023-10ML
Invitrogen	1% Triton in PBS	HFH10
Millipore	Fluor Save	345789 – 20 ml
Fisher Scientific	1 mm microscope slides	15545650
Fisher Scientific	22x22 glass coverslips	12312128
Fisher Scientific	60x24 glass coverslips	10083957
Boster	4% Paraformaldehyde	AR1068 (500 ml)
Sigma Aldrich	Brand™ Cavity Slides	BR475535-50EA
Thermo Fisher	Fluoromount G	00-4958-02

5

6

7

8

9 **Table 10: Primary antibodies/Stains**

Supplier	Antigen	Species	Isotype	Clone	Catalogue Code	Dilution
Sigma Aldrich	βIII-Tubulin	Mouse	IgG2b	SDL.3D10	T5076	1:1000
Thermo Fisher	MAP2	Mouse	IgG1	M13	13-1500	1:500
Abcam	GFAP	Chicken	Polyclonal	Polyclonal	ab4674	1:500
Thermo Fisher	DAPI	N/A	N/A	N/A	62248	1:5000
Spirochrome	Silicone Rhodamine-tubulin kit	N/A	N/A	N/A	SC002	1:10,000
DSHB	MF-20	Mouse	IgG2b	MYH1E	MF-20	1:9
DSHB	Titin	Mouse	IgM	TTN	9 D10	1:20

1

2 **Table 11: Secondary Antibodies**

Supplier	Host species	Target species	Isotype	Conjugate	Catalogue Code	Dilution
Invitrogen	Goat	Mouse	IgG2b	Alexa Fluor 647	A-21242	1:1000
Invitrogen	Goat	Mouse	IgG1	Alexa Fluor 555	A-21127	1:1000
Invitrogen	Goat	Chicken	Polyclonal	Alexa Fluor 555 (H+L)	A-21437	1:1000
Invitrogen	Goat	Mouse	IgG2b	Alexa Fluor 546	A-21143	1:1000
Invitrogen	Goat	Mouse	Polyclonal	Alexa Fluor 488	A-21042	1:1000

3

4

5 **Table 12: Microscope hardware**

Supplier	Apparatus	Catalogue code
Nikon	TE-2000-E	N/A
Solent Scientific	CAL3300 incubator temperature regulator	N/A
Cool LED	pE-4000 16 LED light source	N/A
Okolab	CO ₂ regulator	N/A
Zeiss	LSM710 Inverted Confocal microscope	N/A

6

7

8

9 **Table 13: Microstimulation Hardware**

10

Supplier	Reagent/Apparatus	Catalogue code
EHT Technologies	Silicone posts	C0001
EHT Technologies	Carbon pacing electrodes	P0001
DinoLite	USB microscope	AM73915MZT

11

1

2 **5. Acknowledgments**

3 The Serio lab wishes to acknowledge the support of UK Biotechnology and Biological
4 Sciences Research Council [BB/T011572/1] and the Wellcome Trust [213949/Z/18/Z]. Work
5 in the Tedesco lab is supported by the European Research Council (759108 – HISTOID),
6 AFM- Telethon, BBSRC, Muscular Dystrophy and the NIHR (the views expressed are those
7 of the authors and not necessarily those of the National Health Service, the NIHR, or the
8 Department of Health). Human immortalised myoblasts were provided by the Myoline
9 platform of the Institut de Myologie, Paris, France to the Tedesco lab. This research was
10 funded in whole, or in part, by the Wellcome Trust. For the purpose of Open Access, the
11 author has applied a CC BY public copyright licence to any Author Accepted Manuscript
12 version arising from this submission for the work described here.

13 **6. Author Contributions**

14 C.H. and M.Ba. performed and analysed the majority of experiments, from 3D printing
15 establishment and protocol development, cell culture, image acquisition, data analysis and
16 moulds design. C.H., M.Ba., and A.S. wrote the manuscript with feedback from all authors.
17 M.Be. performed Raman spectroscopy experiments and respective data analysis. C.M.G
18 generated a fluorescent motor neuron line used in this project. P.S, K.O'T. contributed to
19 astrocyte and cortical cell culture for the multicellular experiments. V.L. performed culture,
20 stimulation and staining of 3D muscle constructs and collected the images with support from
21 N.K.. N.K. and E.G. contributed to the optimisation of 3D constructs design for muscle tissue
22 engineering. G.K. performed SEM imaging. F.S.T. and A.I. provided feedback on data analysis
23 and manuscript. Resources were provided by A.S., A.I, F.S.T. Funding for this project was
24 provided by A.S.

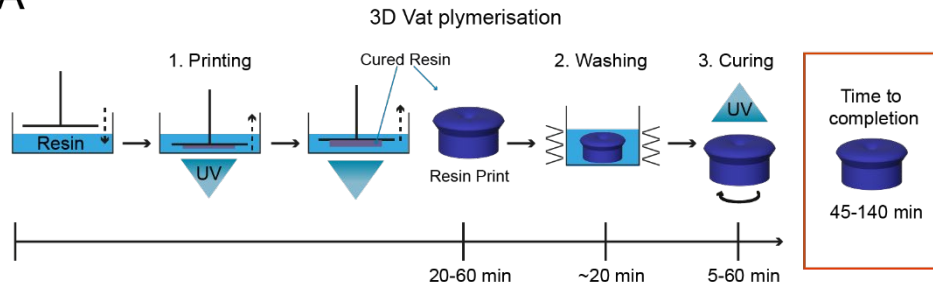
25 **7. Supplementary Information**

26

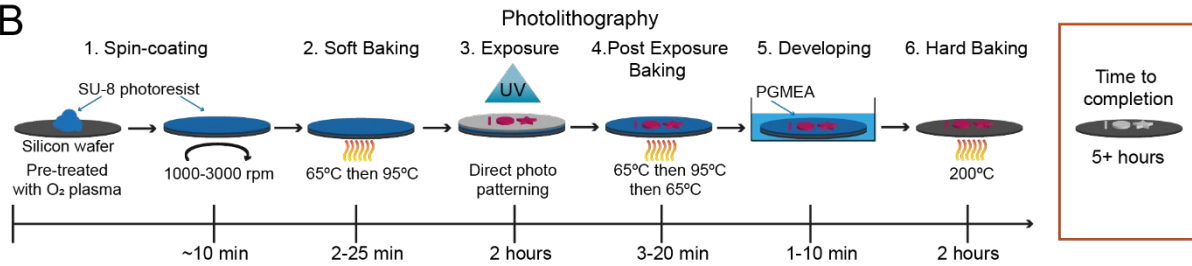
3D vat polymerisation		Photolithography	
Desktop printer	£300	Silicon Wafer (3 inch)	£14.50
Resin	£50/L	SU-8 photoresist	£871/500ml
IPA	£10/L	Spin-Coater	£4200
Ultrasonic cleaner/stirring bath	£75	Triple hot plates	£700
UV curing chamber	£100	Direct photo-patterning system	£100,000
		PGMEA	£23.67/L
		Plasma cleaner	£9440
		Fume Hood	Building specific
Total	£535	Total	>£115,250

Figure S1: Comparison of costs for 3D vat polymerization printing and photolithography with all the required equipment and materials but excluding personnel training costs.

1 A



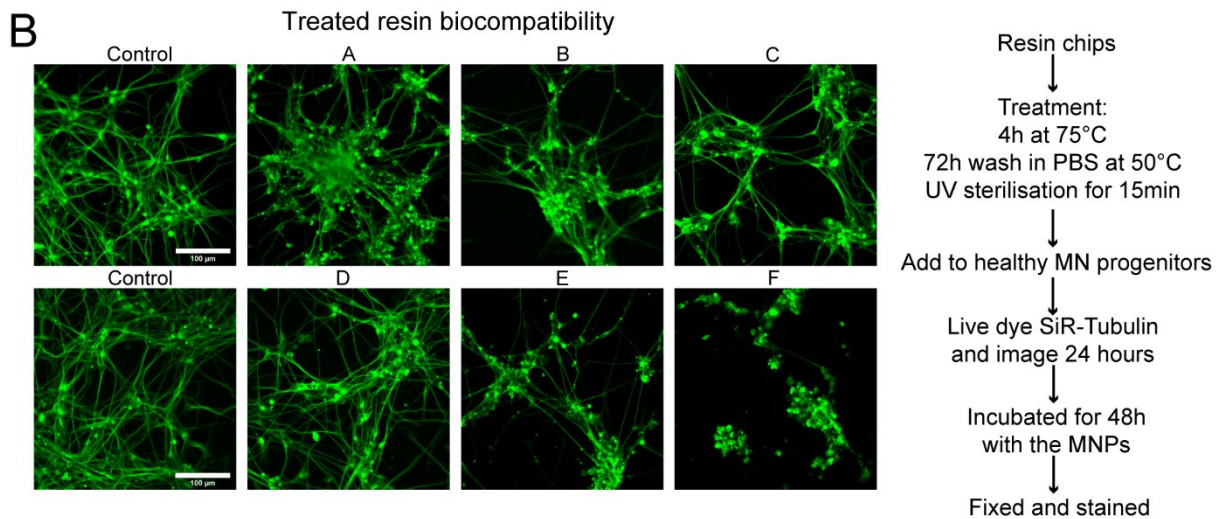
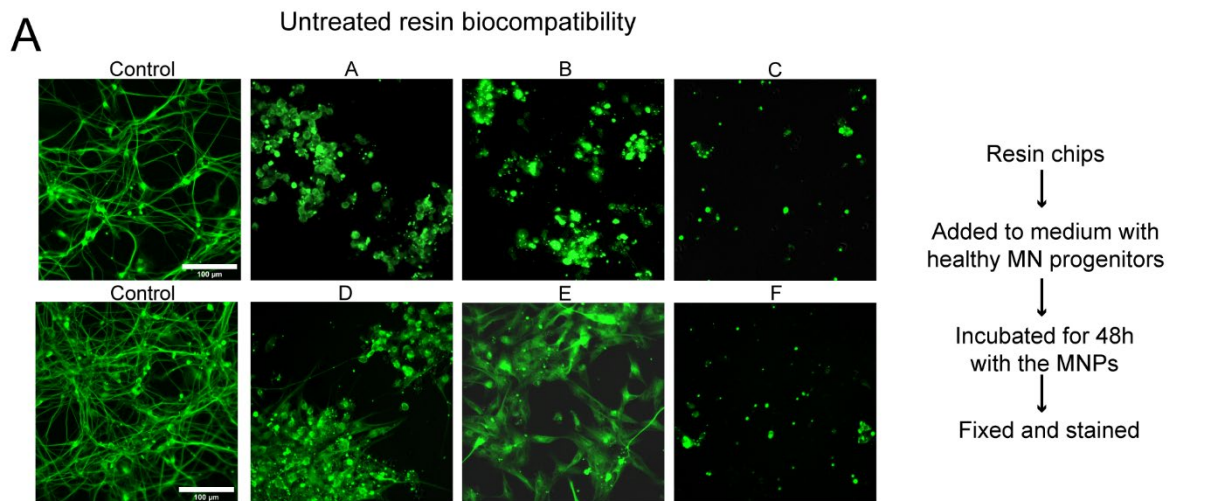
B



Supplementary Diagram 1: Description of 3D vat polymerization and soft lithography with estimated durations

(A) Schematic overview of the UV resin vat polymerisation process and post-processing with a time estimate for production. Printing times range depend on the printed volume but for cell culture device range from 10min to 1h. (B) Schematic overview of photolithography and an estimated time to completion of a print. Print time is a estimate for feature creation across the whole silicon wafer and alters in between prints, depending on the design. Overall, UV resin vat polymerisation is faster compared to photolithography, as it uses whole field illumination and not single point illumination as photolithography.

1



2

Figure S2: SLA resins themselves are toxic with and without pre-treatment

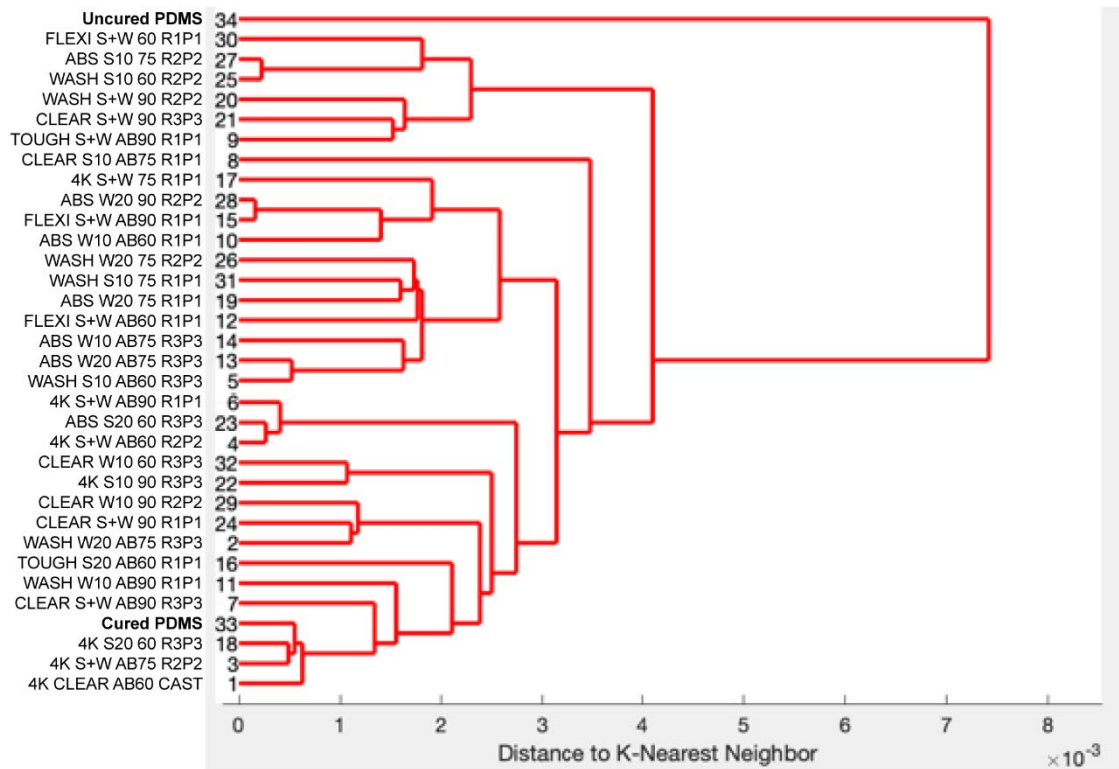
(A) Chips of 6 resins were added to cultures of motor neuron progenitors pre-stained with SiR – tubulin live dye, incubated for 48 hours before imaging. Representative images of SiR live dye-stained motor neurons after 48 hours in culture with resins compared to 2 control wells. (B) Chips of 6 resins were treated with extra processing steps to improve biocompatibility, bake 4 hours at 75°C, wash in PBS 72 hours at 50°C, UV sterilise 15 mins before being added to cultures of motor neuron progenitors pre-stained with SiR-tubulin cytoskeletal live dye, incubated for 48hrs before imaging. Representative images of SiR live dye-stained motor neurons after 48 hours in culture with treated resins compared to 2 control wells. (C) Representative time lapse videos of SiR live dye-stained motor neurons during the first 24 hours in culture with treated resin chips compared to 2 control wells.

3

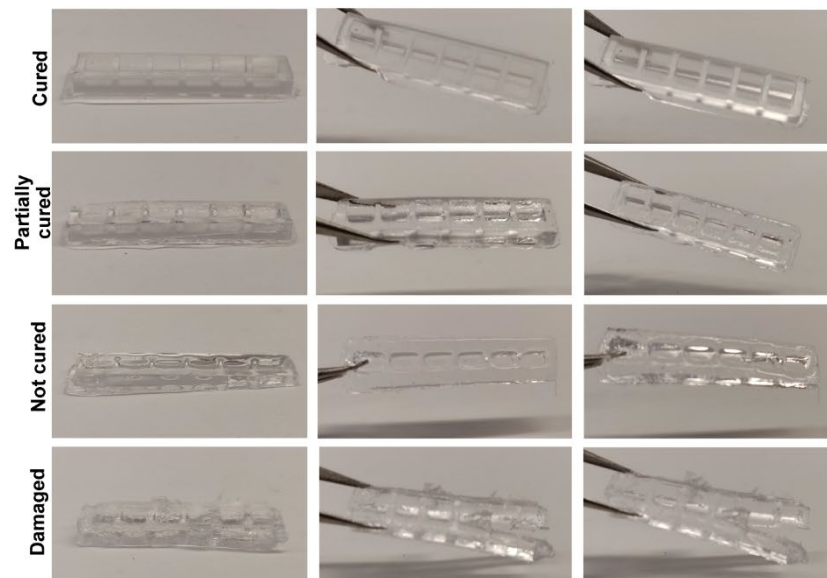
4

5

A



B



1

Figure S3: Quantitation of PDMS curing on 3D printed moulds

(A) Dendrogram of the spectral similarity of PDMS casts from 3D printed moulds fabricated with 6 commercially available resins, washed with 5 conditions (S+W = sonicate 10 mins, wash 10 mins, S10 = Sonicate 10 mins, S20 = sonicate 20 mins, W10 = Wash 10 mins, W20 = Wash 20 mins), either untreated or coated with airbrush (AB) and cured at 3 different temperatures (60), (75), (90), compared to samples of uncured and cured PDMS. Replicate and print number (RXPx) for each condition. (B) Heterogeneity of PDMS cast curing from 3D printed moulds by observation ranging from 'cured', 'partially cured', 'not cured', 'damaged'.

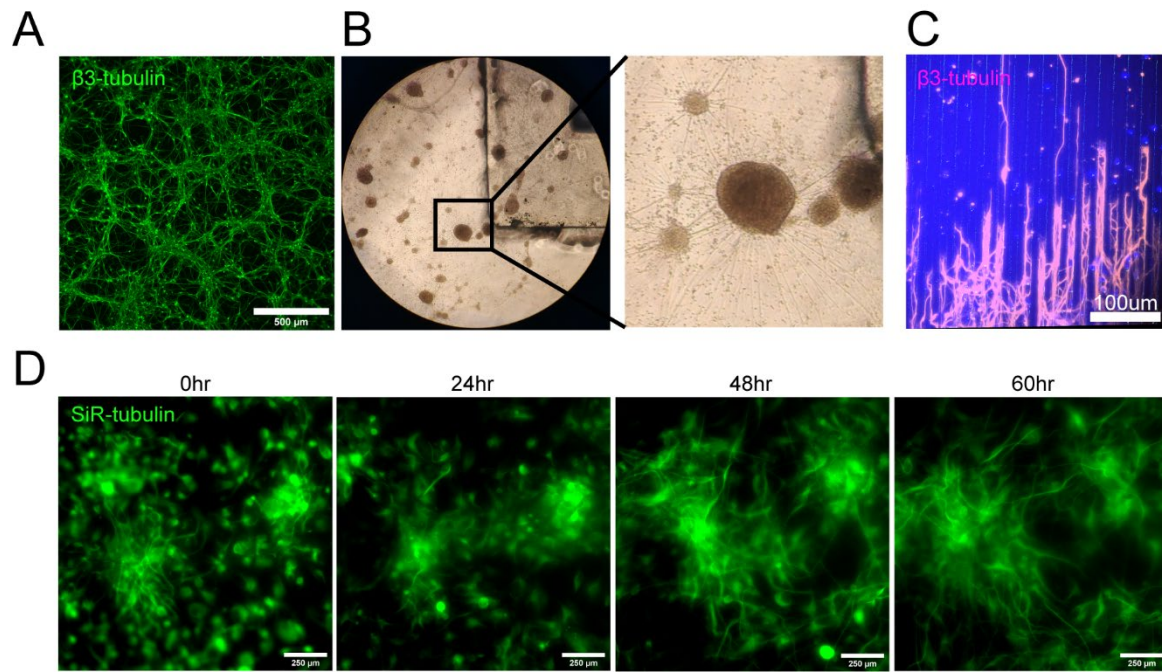


Figure S4: Biocompatibility of PDMS cast in 3D printed moulds with cells (timelapse and long axons)

(A) Representative β -III Tubulin stained differentiated motor neurons cultured on a flat substrate. (B) Brightfield images of differentiated motor neurons with a PDMS cast from a 3D printed mould in the culture medium. (C) β -III Tubulin stained motor neuron long axons seeded on PDMS microfabricated substrate. (D) Snapshots from 60-hour time-lapse of SiR – tubulin live dye stained motor neuron differentiation on PDMS substrate cast in a 3D printed mould.

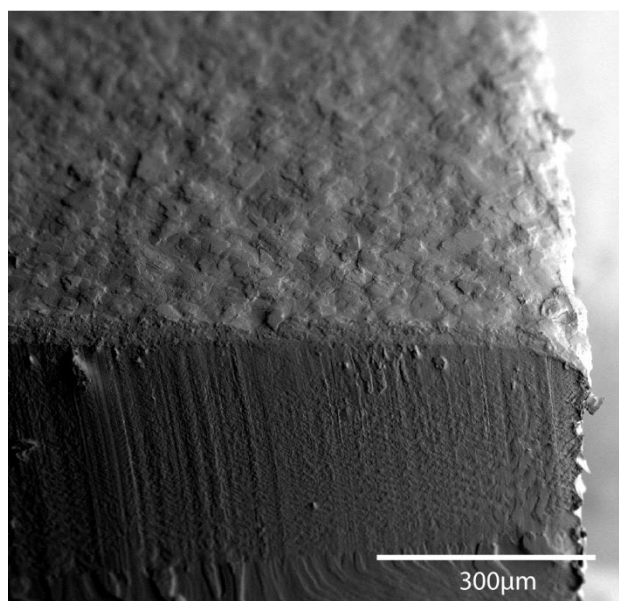
3

4

5

6

1 **A**



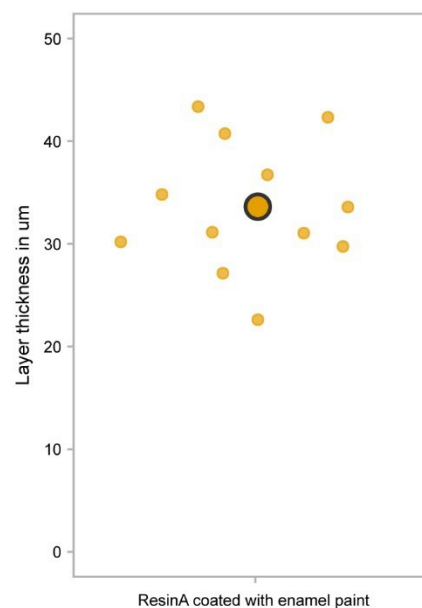
2

3 **Figure S5: Analysis of paint layer thickness**

4 (A) Representative SEM image of a resin A print with airbrushed enamel paint (B) Analysis of paint layer thickness
5 on 3D vat printed moulds

6

B



ResinA coated with enamel paint

1

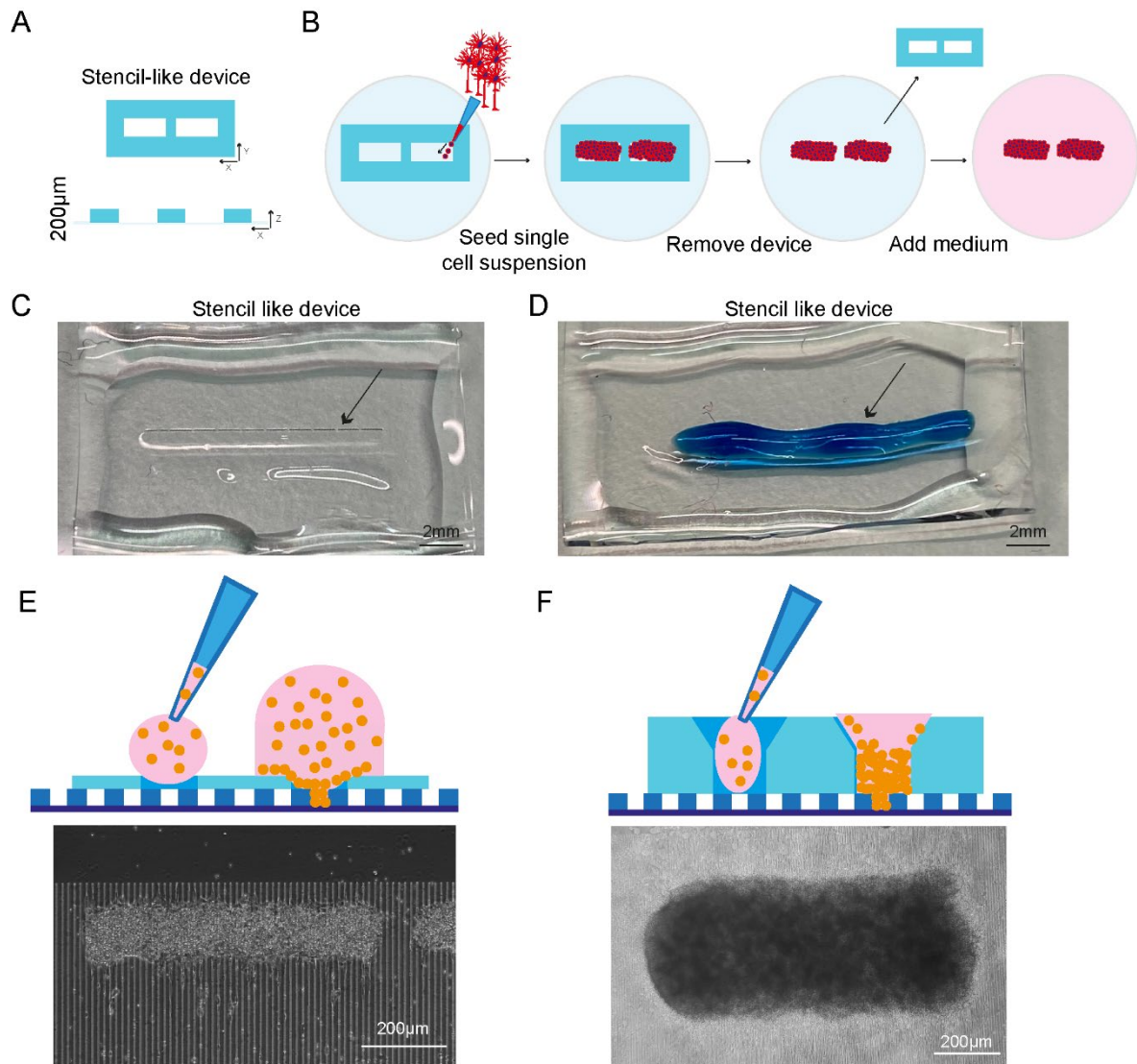


Figure S6: PDMS stencil devices manufactured using photolithography

(A) Dimensions of the stencil-like device with photolithography (B) Schematic overview of the seeding strategy with stencil-like devices (C) Representative image of a stencil-like device with pockets for cell seeding (arrow) (D) Demonstration of cell seeding using food coloring as a 'single-cell suspension'. The liquid was manually pipetted on the pockets of the device (arrow). Limited volume can be used. (E) Representative brightfield image of single motoneurons seeded using a stencil device manufactured using photolithography and a schematic showing the seeding process as well as the position of the cells. (F) Representative brightfield image of single motoneurons seeded using a plating device manufactured using SOL3D and a schematic showing the seeding process as well as the position of the cells.

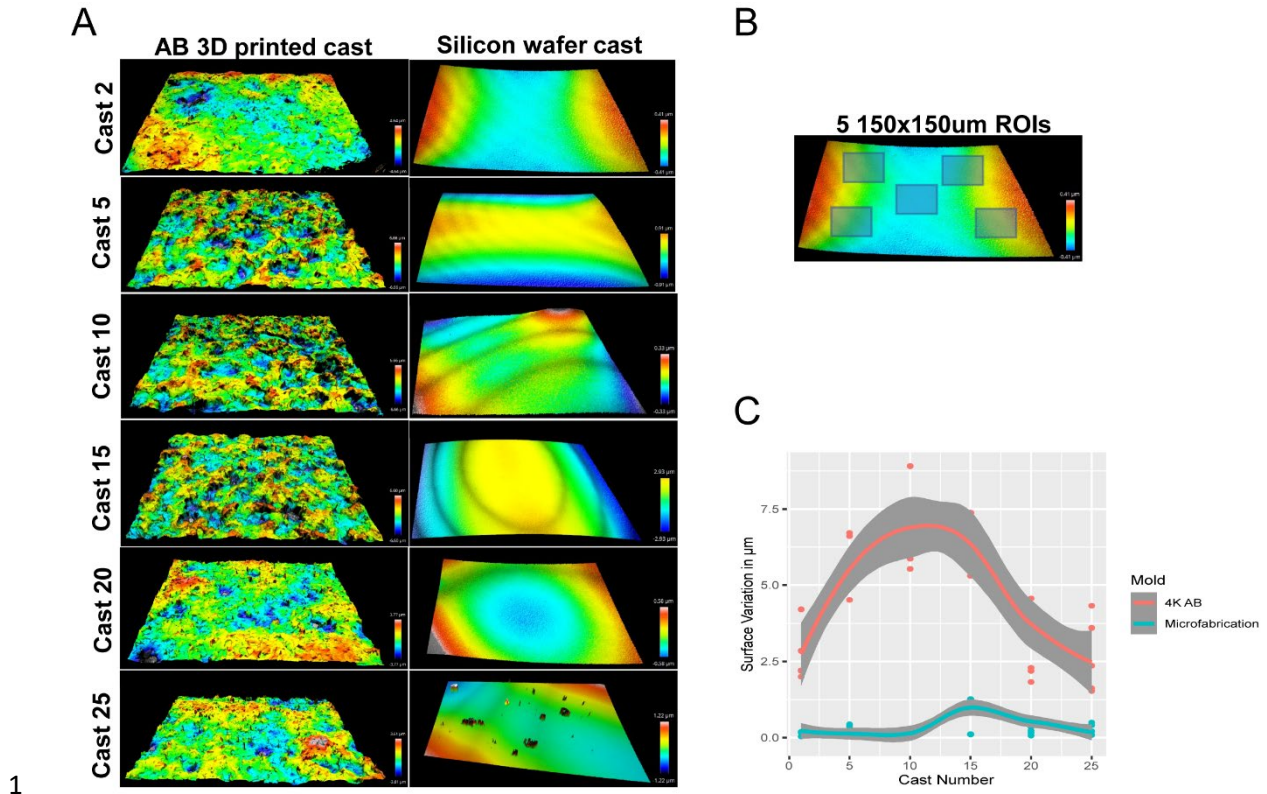


Figure S7: The surface of 3D prints is rough

(A) Representative optical profiles from PDMS casts demoulded from a single airbrushed 3D printed mould and a single microfabricated mould. (B) Representation of 5 ROI selection for quantification of surface roughness on PDMS casts. (C) Quantitation of surface roughness of PDMS casts from the same device over time (25 simultaneous casts) between an airbrushed 3D printed mould and a microfabricated mould.

2
3
4
5
6
7

1

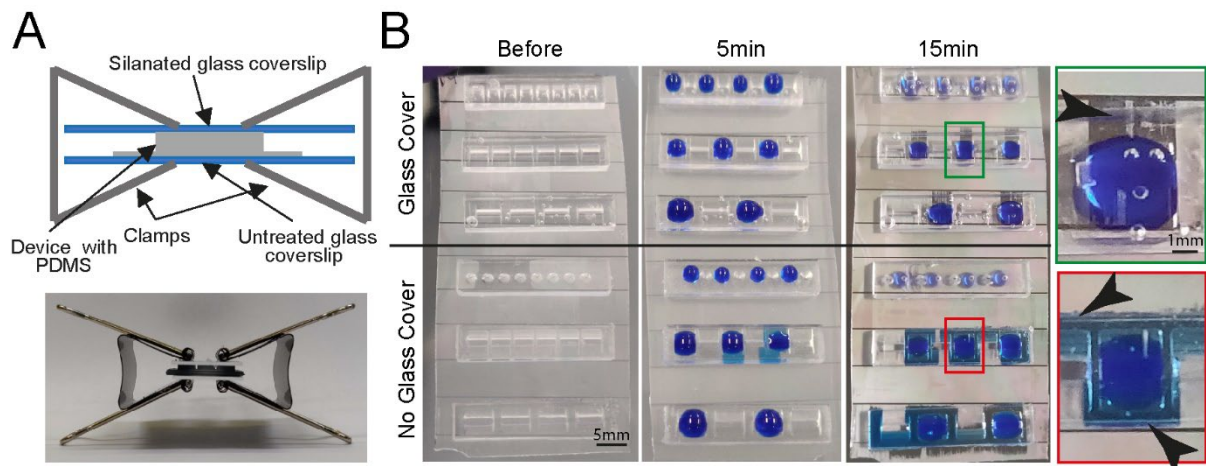


Figure S8: Fluidic seal for cell plating devices

(A) Schematic (top) and representative image (bottom) of clamping approach to ensure fluid seal when devices are placed on PDMS microgroove substrates. (B) Comparison of liquid seal integrity of clamping strategy (top) compared to open curing (bottom) on PDMS microgroove substrate with different well sizes and shapes using dyed liquid. Successful sealing of devices cast with a glass cover (**Green zoom**). Dye spreads throughout device and grooves using open cured (**Red zoom**). Arrows highlight liquid spreading.

1

2

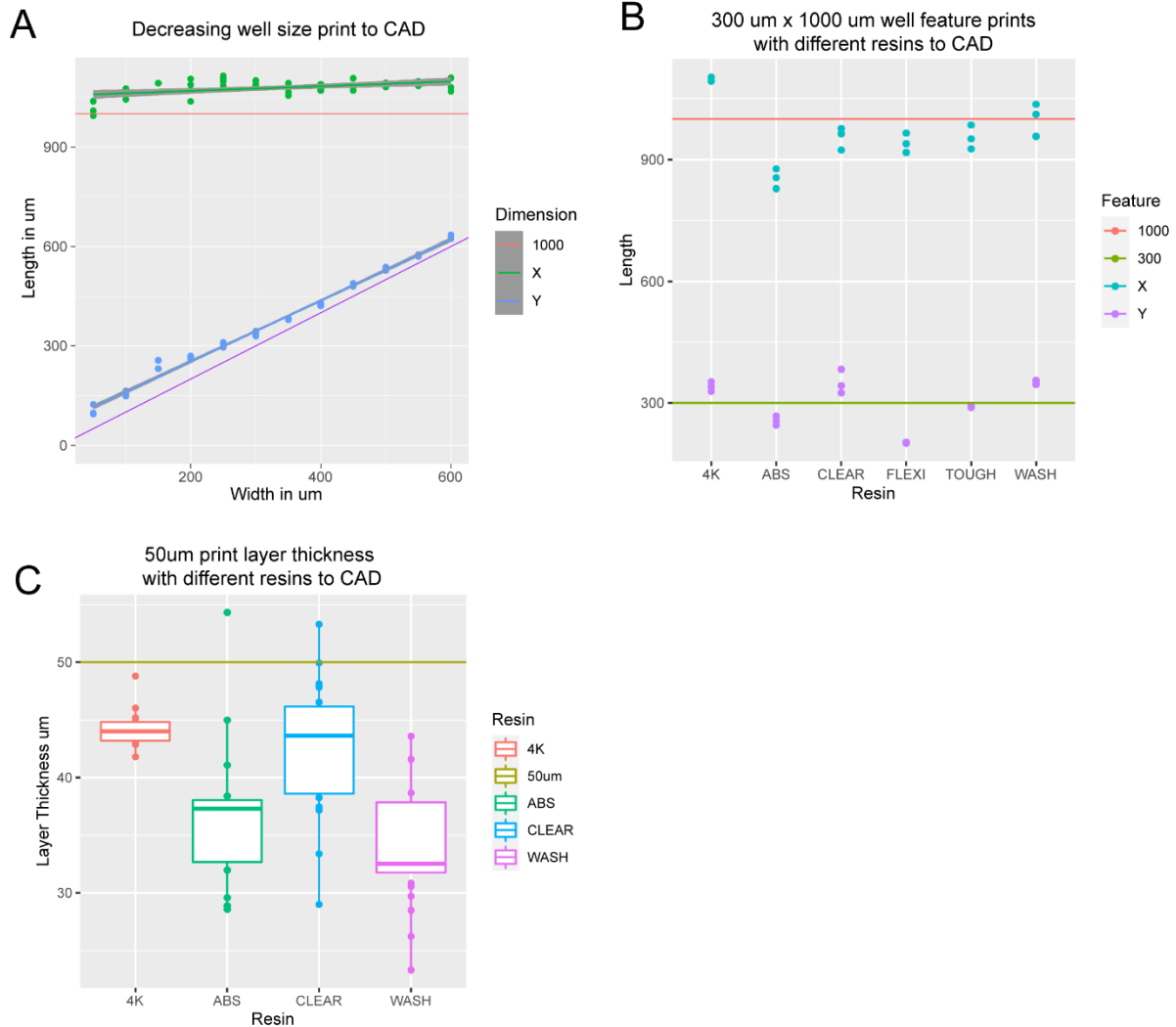


Figure S9: 3D print dimensions are homogenous

(A) Graph comparing X and Y dimensions of 3D printed constructs to CAD specifications in a single device with well dimensions ranging from 600 μm x 1000 μm to 50 μm x 1000 μm . (B) Graph comparing X and Y dimensions of 300 μm x 1000 μm features on 3D printed constructs to CAD specifications for 6 commercially available resins printed on 2 3D printers at manufacturer default settings with a 50 μm layer thickness. (C) Graph comparing the actual layer thickness of 3D printed constructs to CAD specifications for 6 commercially available resins printed on 2 SLA 3D printers at manufacturer default settings with a 50 μm layer thickness.

3

4

5

6

7

8

1

2

A

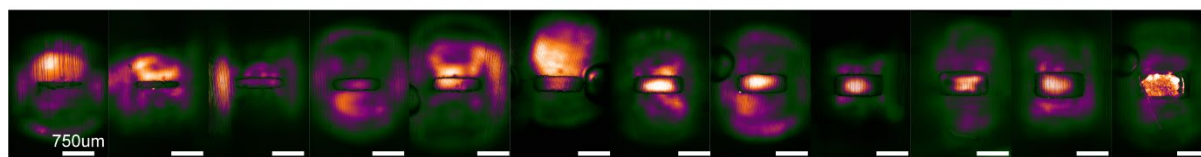


Figure S10: Non-Plasma devices cannot be used for seeding in microwells

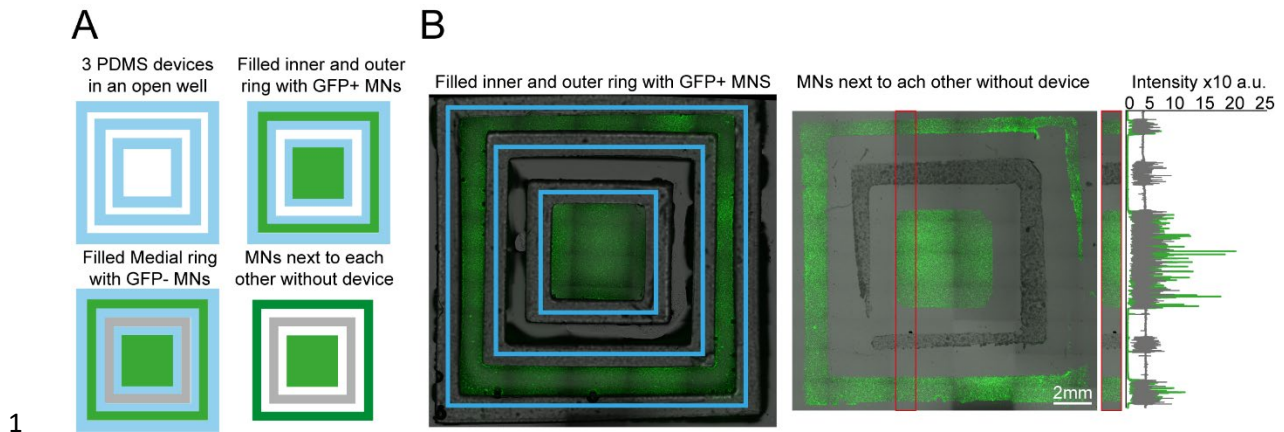
(A) Representative SiR-Tubulin images of motor neuron progenitors seeded in microwells ranging from 600 μm x 1000 μm to 50 μm x 1000 μm . Difference in colour indicates depth in focal plane where cells do not reach the micropatterned substrate below.

4

5

6

7



1

2

Figure S12: Plating devices enable manual segregated seeding of different cell types in the same well, device or multiple devices

(A) Multiple PDMS casts from 3D printed devices can be seeded in the same well and seeded with different cell types at different time points. Schematic overview of the multi-device protocol for seeding GFP and non GFP+ motor neurons at different time points in 3 devices in the same well. (B) Representative fluorescence images of cells GFP+ motor neurons seeded in the inner and outer rings of the 3 devices and imaged with devices still on (left) and after seeding of the second non-GFP+ motor neurons in the medial ring after device stripping (right), Representative line profile of imaged cell fluorescence showing segregation of individual populations to their designated rings

1

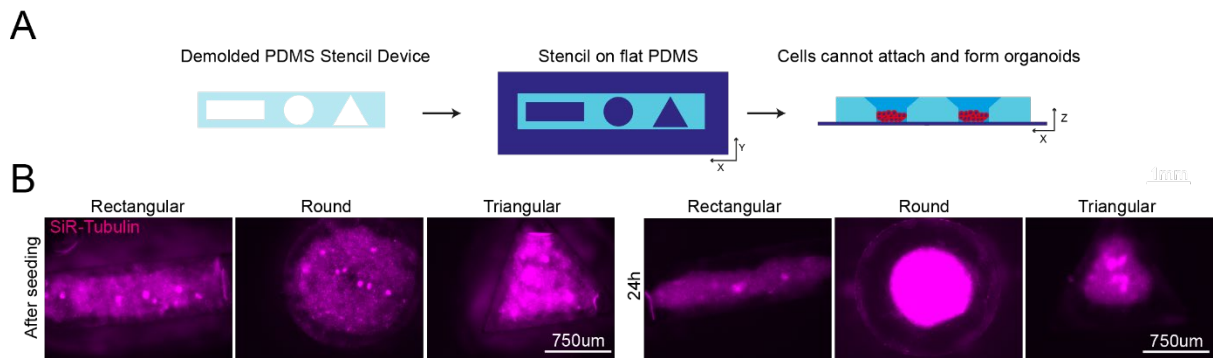


Figure S13: Plating devices enable geometric manipulation of aggregoid cultures in 2D and 3D

(A) Schematic overview of protocol for manipulating aggregate geometry in combination with existing microgroove and flat substrates. (B) Representative images of SiR-tubulin live-cell-stained motor neuron aggregoids at day 2 (top) and β -III Tubulin staining after 11 days (bottom) of culture. (C) Boxplot of aggregoid aspect ratio fold change by shape between CAD (blue line) and day 2 of culture from β -III-Tubulin channel (top) (D) Boxplot of aggregoid area fold change by shape between CAD (blue line) and day 2 of culture from β -III Tubulin channel. (E) Representative images of SiR-tubulin stained cortical aggregates after seeding and 24h later in different geometry stencil devices, round (left), triangular (middle) and rectangular (right).

1

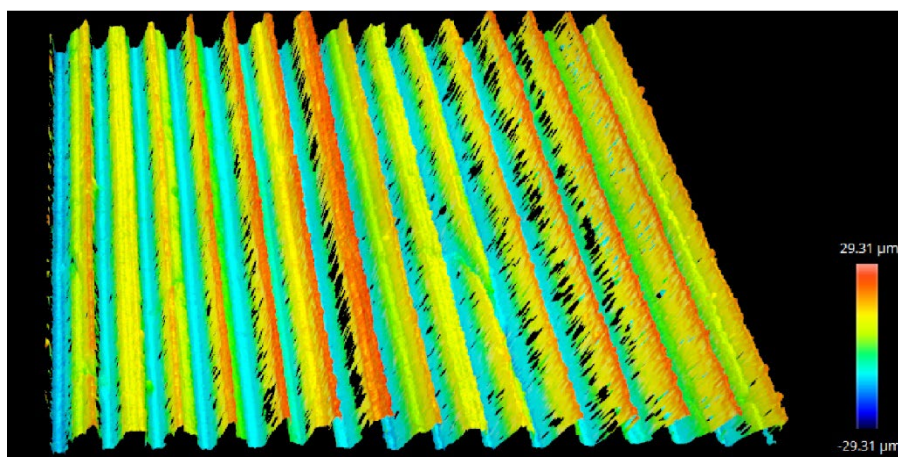


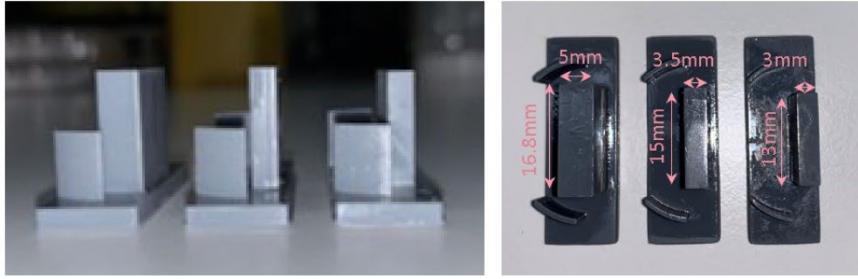
Figure S14: Representative image of an optical profile from SOLID manufactured triangular grooves

2

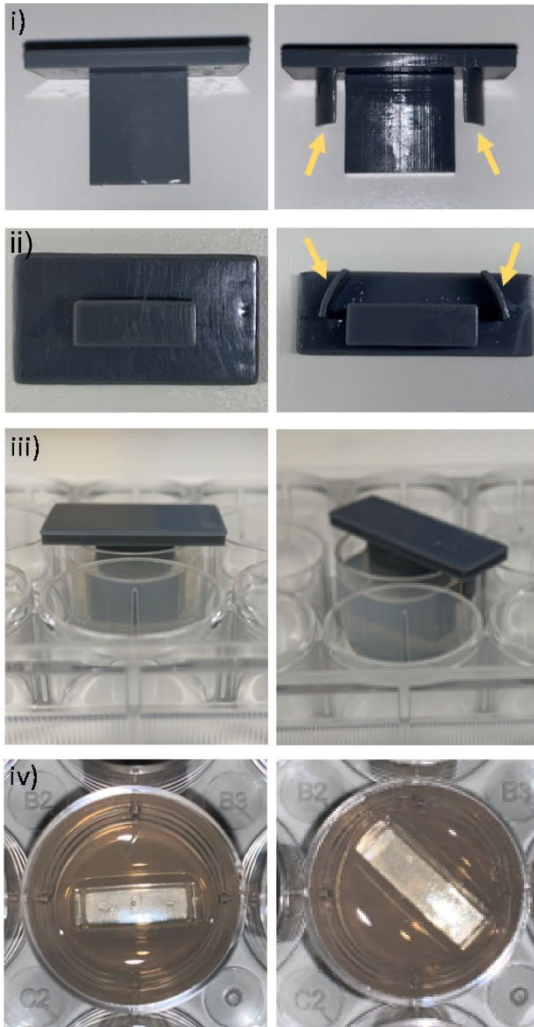
3

4

A



B



C

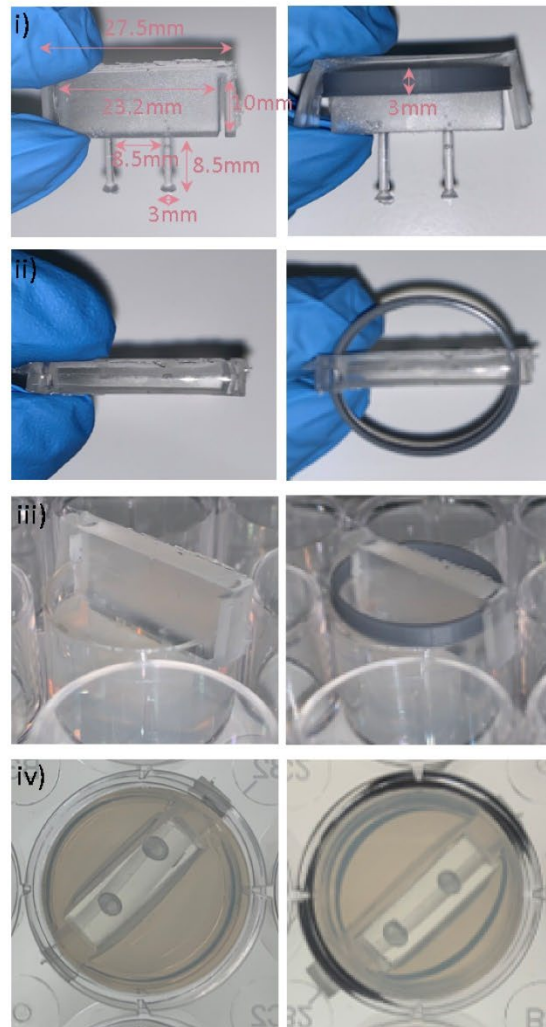


Figure S15: Optimisation and protocol for 3D muscle culture using PDMS constructs from 3D printed moulds

(A) Images show three different mould sizes tested to optimise the volume of the hydrogel mix at a side and bottom view. (Bi-iii) Images showing moulds with (yellow arrows) and without grooves at various perspectives. (Biv) Image shows top view of agarose once mould is removed. (Ci-i) Images show posts with and without a ring placed underneath the arms from a front and top view. Rings were designed to match the size of one well of a 12-well plate. (Cii) Images showing posts inserted into agarose moulds at a side view and bottom view from underneath the plate, rings allow posts to be inserted at a specific height.

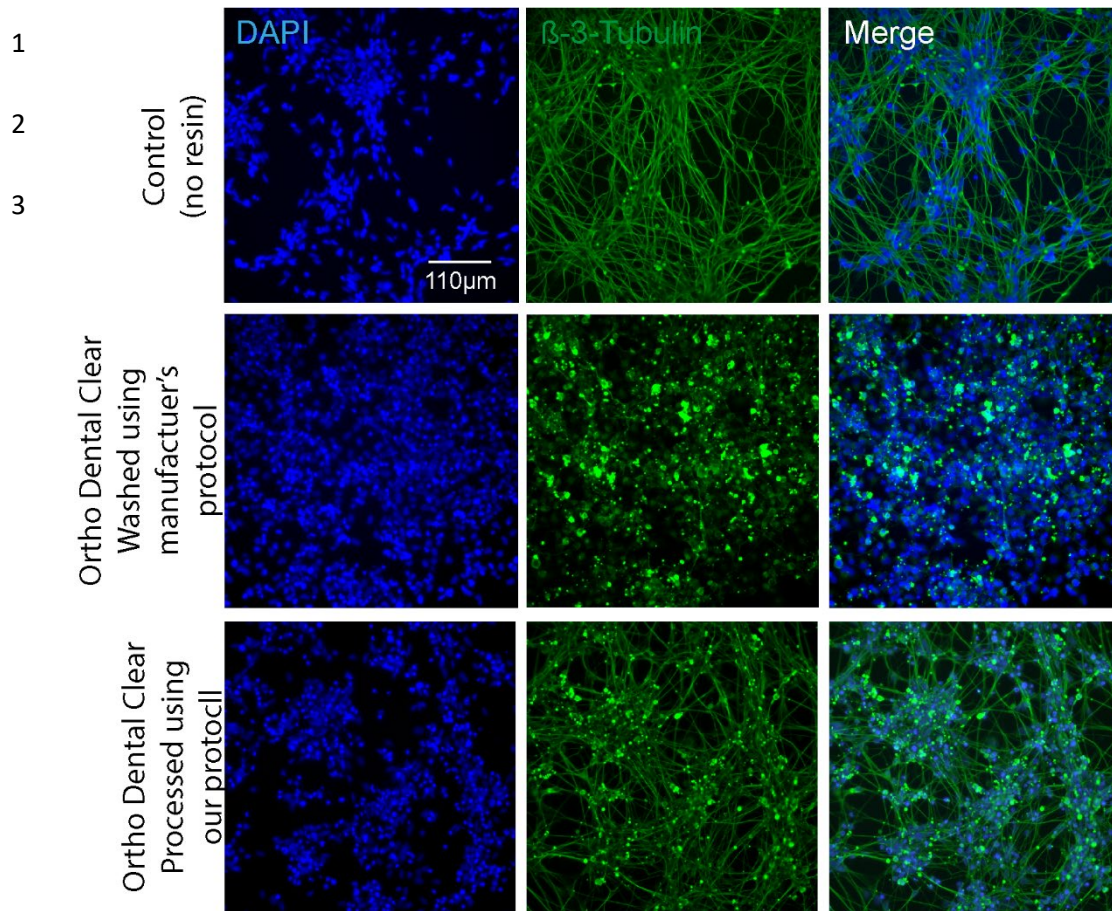
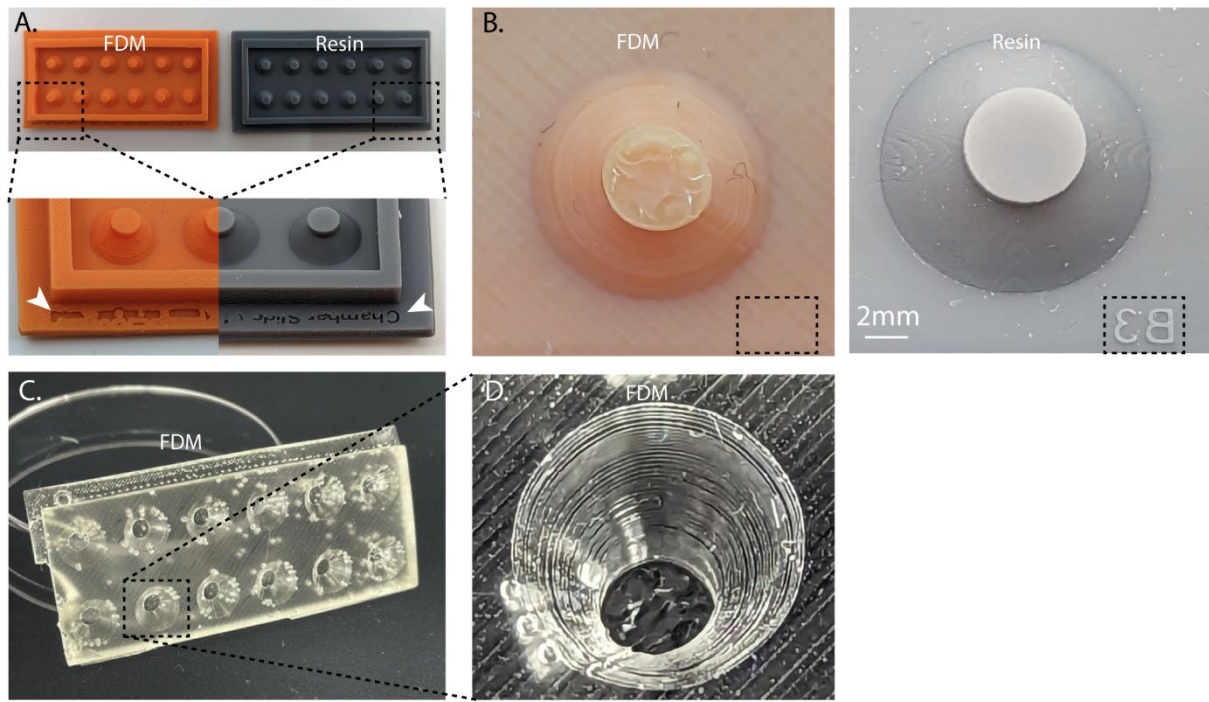


Figure S16: Effects of co-culture with a biocompatible resin on iPSC-derived MNs

iPSC-derived MNs were plated at equal densities. Then a 3D-printed well-sized cylinder of ortho-clear resin was added to the well and incubated for four days to identify the toxic effects of the biocompatible resin. The resin was either pretreated with the recommended manufacturer's protocol or our pipeline. Cells were stained for β -3-tubulin and DAPI.



1

Figure S17: Comparison of feature quality between FDM and Vat polymerized samples

(A) Chamber devices used in Figure 5 were manufactured using a FDM (Bambu Labs, 0.4mm nozzle with 0.16mm settings) printer and a 3D UV-resin printer (Phrozen mini 4k, 50um settings). Zoom in images show a clear constructed writing for the UV resin printer, lacking for the FDM sample. (B) Representative images highlight the flat surface of resin printed samples, especially on the flat top of the pillar. The dotted box highlights the absence of the well labelling in FMD prints, and a clear label in the resin sample. (C-D) PDMS cast of the FDM mould, clearly highlights the large print and build lines of the sample.

1 **8. References**

- 2
- 3 1. Gaspard, N. *et al.* An intrinsic mechanism of corticogenesis from embryonic stem cells.
4 *Nature* 455, 351–357 (2008).
- 5 2. Ying, Q.-L., Stavridis, M., Griffiths, D., Li, M. & Smith, A. Conversion of embryonic stem
6 cells into neuroectodermal precursors in adherent monoculture. *Nat Biotechnol* 21, 183–186
7 (2003).
- 8 3. Amit, M. *et al.* Clonally Derived Human Embryonic Stem Cell Lines Maintain
9 Pluripotency and Proliferative Potential for Prolonged Periods of Culture. *Dev Biol* 227, 271–
10 278 (2000).
- 11 4. Thomson, J. A. *et al.* Embryonic Stem Cell Lines Derived from Human Blastocysts.
12 *Science* 282, 1145–1147 (1998).
- 13 5. Takahashi, K. *et al.* Induction of Pluripotent Stem Cells from Adult Human Fibroblasts by
14 Defined Factors. *Cell* 131, 861–872 (2007).
- 15 6. Park, I. H. *et al.* Reprogramming of human somatic cells to pluripotency with defined
16 factors. *Nature* 451, 141–146 (2008).
- 17 7. Chanoumidou, K., Mozafari, S., Evercooren, A. B.-V. & Kuhlmann, T. Stem cell derived
18 oligodendrocytes to study myelin diseases. *Glia* 68, 705–720 (2020).
- 19 8. Hasselmann, J. & Blurton-Jones, M. Human iPSC-derived microglia: A growing toolset to
20 study the brain’s innate immune cells. *Glia* 68, 721–739 (2020).
- 21 9. Chang, C. Y. *et al.* Induced pluripotent stem cell (iPSC)-based neurodegenerative disease
22 models for phenotype recapitulation and drug screening. Preprint at (2020).
- 23 10. Weibel, D. B., Diluzio, W. R. & Whitesides, G. M. Microfabrication meets microbiology.
24 *Nat Rev Microbiol* 5, 209–18 (2007).
- 25 11. Qin, D., Xia, Y. & Whitesides, G. M. Soft lithography for micro- and nanoscale
26 patterning. *Nat Protoc* 5, 491–502 (2010).
- 27 12. Soft lithography for micro- and nanoscale patterning.
28 <https://www.nature.com/articles/nprot.2009.234.pdf>.
- 29 13. Qin, D., Xia, Y. & Whitesides, G. M. Soft lithography for micro- and nanoscale
30 patterning. *Nat Protoc* 5, 491–502 (2010).
- 31 14. Rammohan, A. *et al.* One-step maskless grayscale lithography for the fabrication of 3-
32 dimensional structures in SU-8. *Sens. Actuators B: Chem.* 153, 125–134 (2011).
- 33 15. Waits, C. M., Modafe, A. & Ghodssi, R. Investigation of gray-scale technology for large
34 area 3D silicon MEMS structures. *J. Micromechanics Microengineering* 13, 170 (2003).

- 1 16. Think big. Print nano. Your partner for high-precision additive manufacturing.
2 <https://www.nanoscribe.com/en/>.
- 3 17. Saggiomo, V. & Velders, A. H. Simple 3D Printed Scaffold-Removal Method for the
4 Fabrication of Intricate Microfluidic Devices. *Adv Sci* 2, 1500125 (2015).
- 5 18. Fichou, D. & Morlock, G. E. Open-Source-Based 3D Printing of Thin Silica Gel Layers
6 in Planar Chromatography. *Anal Chem* 89, 2116–2122 (2017).
- 7 19. Rosario, M. D., Heil, H. S., Mendes, A., Saggiomo, V. & Henriques, R. The Field Guide
8 to 3D Printing in Optical Microscopy for Life Sciences. *Adv Biology* e2100994 (2021)
9 doi:10.1002/adbi.202100994.
- 10 20. Baas, S. & Saggiomo, V. Ender3 3D printer kit transformed into open, programmable
11 syringe pump set. *HardwareX* 10, e00219 (2021).
- 12 21. Diederich, B. *et al.* A versatile and customizable low-cost 3D-printed open standard for
13 microscopic imaging. *Nat Commun* 11, 5979 (2020).
- 14 22. Collins, J. T. *et al.* Robotic microscopy for everyone: the OpenFlexure microscope.
15 *Biomed Opt Express* 11, 2447 (2020).
- 16 23. LaFratta, C. N. *et al.* Replication of Two-Photon-Polymerized Structures with Extremely
17 High Aspect Ratios and Large Overhangs. *J Phys Chem B* 108, 11256–11258 (2004).
- 18 24. Daicho, Y., Murakami, T., Hagiwara, T. & Maruo, S. Formation of three-dimensional
19 carbon microstructures via two-photon microfabrication and microtransfer molding. *Opt*
20 *Mater Express* 3, 875 (2013).
- 21 25. Balakrishnan, H. K. *et al.* 3D Printing: An Alternative Microfabrication Approach with
22 Unprecedented Opportunities in Design. *Anal Chem* 93, 350–366 (2021).
- 23 26. Kamei, K. *et al.* 3D printing of soft lithography mold for rapid production of
24 polydimethylsiloxane-based microfluidic devices for cell stimulation with concentration
25 gradients. *Biomed. Microdevices* 17, 36 (2015).
- 26 27. Waheed, S. *et al.* 3D printed microfluidic devices: enablers and barriers. *Lab Chip* 16,
27 1993–2013 (2016).
- 28 28. Weems, A. C., Arno, M. C., Yu, W., Huckstepp, R. T. R. & Dove, A. P. 4D
29 polycarbonates via stereolithography as scaffolds for soft tissue repair. *Nat Commun* 12, 3771
30 (2021).
- 31 29. Phrozen Sonic Mini 4K - 3DJake UK-[https://www.3djake.uk/phrozen/sonic-mini-](https://www.3djake.uk/phrozen/sonic-mini-4k?gclid=Cj0KCCQiAxc6PBhCEARIsAH8Hff0V1kZ0Ttq1RbiwsAtaU6Er7Aw3MK7xu6BFaIyEeOyLD8TOYQjX9e4aAgqoEALw_wcB-2022-01-28)
32 [4k?gclid=Cj0KCCQiAxc6PBhCEARIsAH8Hff0V1kZ0Ttq1RbiwsAtaU6Er7Aw3MK7xu6BFa](https://www.3djake.uk/phrozen/sonic-mini-4k?gclid=Cj0KCCQiAxc6PBhCEARIsAH8Hff0V1kZ0Ttq1RbiwsAtaU6Er7Aw3MK7xu6BFaIyEeOyLD8TOYQjX9e4aAgqoEALw_wcB-2022-01-28)
33 [IyEeOyLD8TOYQjX9e4aAgqoEALw_wcB-2022-01-28](https://www.3djake.uk/phrozen/sonic-mini-4k?gclid=Cj0KCCQiAxc6PBhCEARIsAH8Hff0V1kZ0Ttq1RbiwsAtaU6Er7Aw3MK7xu6BFaIyEeOyLD8TOYQjX9e4aAgqoEALw_wcB-2022-01-28). Preprint at
34 [https://www.3djake.uk/phrozen/sonic-mini-](https://www.3djake.uk/phrozen/sonic-mini-4k?gclid=Cj0KCCQiAxc6PBhCEARIsAH8Hff0V1kZ0Ttq1RbiwsAtaU6Er7Aw3MK7xu6BFaIyEeOyLD8TOYQjX9e4aAgqoEALw_wcB)
35 [4k?gclid=Cj0KCCQiAxc6PBhCEARIsAH8Hff0V1kZ0Ttq1RbiwsAtaU6Er7Aw3MK7xu6BFa](https://www.3djake.uk/phrozen/sonic-mini-4k?gclid=Cj0KCCQiAxc6PBhCEARIsAH8Hff0V1kZ0Ttq1RbiwsAtaU6Er7Aw3MK7xu6BFaIyEeOyLD8TOYQjX9e4aAgqoEALw_wcB)
36 [IyEeOyLD8TOYQjX9e4aAgqoEALw_wcB](https://www.3djake.uk/phrozen/sonic-mini-4k?gclid=Cj0KCCQiAxc6PBhCEARIsAH8Hff0V1kZ0Ttq1RbiwsAtaU6Er7Aw3MK7xu6BFaIyEeOyLD8TOYQjX9e4aAgqoEALw_wcB).

- 1 30. Zortrax Raydent Crown & Bridge Resin - 3DJake UK-
2 <https://www.3djake.uk/zortrax/raydent-crown-bridge-resin-2022-01-28>. Preprint at
3 <https://www.3djake.uk/zortrax/raydent-crown-bridge-resin>.
- 4 31. Oskui, S. M. *et al.* Assessing and Reducing the Toxicity of 3D-Printed Parts. *Environ Sci*
5 *Tech Let* 3, 1–6 (2016).
- 6 32. Kownacki, I. *et al.* Effect of triorganophosphites on platinum catalyzed curing of silicon
7 rubber. *Appl Catal Gen* 362, 106–114 (2009).
- 8 33. Bail, R. *et al.* The Effect of a Type I Photoinitiator on Cure Kinetics and Cell Toxicity in
9 Projection-Microlithography. *Proc Cirp* 5, 222–225 (2013).
- 10 34. Ikemura, K., Ichizawa, K., Yoshida, M., Ito, S. & Endo, T. UV-VIS spectra and
11 photoinitiation behaviors of acylphosphine oxide and bisacylphosphine oxide derivatives in
12 unfilled, light-cured dental resins. *Dent Mater J* 27, 765–74 (2008).
- 13 35. Ferraz, M. de A. M. M., Nagashima, J. B., Venzac, B., Gac, S. L. & Songsasen, N. 3D
14 printed mold leachates in PDMS microfluidic devices. *Sci Rep-uk* 10, 994 (2020).
- 15 36. Venzac, B. *et al.* PDMS Curing Inhibition on 3D-Printed Molds: Why? Also, How to
16 Avoid It? *Anal Chem* 93, 7180–7187 (2021).
- 17 37. Bazaz, S. R. *et al.* Rapid Softlithography Using 3D-Printed Molds. *Adv Mater*
18 *Technologies* 4, 1900425 (2019).
- 19 38. Comina, G., Suska, A. & Filippini, D. PDMS lab-on-a-chip fabrication using 3D printed
20 templates. *Lab Chip* 14, 424–430 (2013).
- 21 39. Woo, S. O., Oh, M. & Choi, Y. Fabricating self-powered microfluidic devices via 3D
22 printing for manipulating fluid flow. *STAR Protoc.* 3, 101376 (2022).
- 23 40. Chande, C. *et al.* Universal method for fabricating PDMS microfluidic device using SU8,
24 3D printing and soft lithography. *Technology* 08, 50–57 (2020).
- 25 41. O’Grady, B. J. *et al.* Rapid Prototyping of Cell Culture Microdevices Using Parylene-
26 Coated 3D Prints. *Biorxiv* 2021.08.02.454773 (2021) doi:10.1101/2021.08.02.454773.
- 27 42. Messner, J. J., Glenn, H. L. & Meldrum, D. R. Laser-fabricated cell patterning stencil for
28 single cell analysis. *Bmc Biotechnol* 17, 89 (2017).
- 29 43. Sahni, G., Yuan, J. & Toh, Y.-C. Stencil Micropatterning of Human Pluripotent Stem
30 Cells for Probing Spatial Organization of Differentiation Fates. *J Vis Exp Jove* (2016)
31 doi:10.3791/54097.
- 32 44. Hagemann, C. *et al.* Axonal Length Determines Distinct Homeostatic Phenotypes in
33 Human iPSC Derived Motor Neurons on a Bioengineered Platform. *Adv Healthc Mater* 11,
34 2101817 (2022).

- 1 45. Shi, Y., Kirwan, P. & Livesey, F. J. Directed differentiation of human pluripotent stem
2 cells to cerebral cortex neurons and neural networks. *Nat Protoc* 7, 1836–1846 (2012).
- 3 46. Serio, A. *et al.* Astrocyte pathology and the absence of non-cell autonomy in an induced
4 pluripotent stem cell model of TDP-43 proteinopathy. *Proc National Acad Sci* 110, 4697–
5 4702 (2013).
- 6 47. Sen, D., Voulgaropoulos, A. & Keung, A. J. Effects of early geometric confinement on
7 the transcriptomic profile of human cerebral organoids. *Bmc Biotechnol* 21, 59 (2021).
- 8 48. Suarez, A. M. A., Zhou, Q., Rijn, P. & Harmsen, M. C. Directional topography gradients
9 drive optimum alignment and differentiation of human myoblasts. *J Tissue Eng Regen M* 13,
10 2234–2245 (2019).
- 11 49. Bauwens, C. L. *et al.* Control of Human Embryonic Stem Cell Colony and Aggregate
12 Size Heterogeneity Influences Differentiation Trajectories. *Stem Cells* 26, 2300–2310 (2008).
- 13 50. Hwang, Y.-S. *et al.* Microwell-mediated control of embryoid body size regulates
14 embryonic stem cell fate via differential expression of WNT5a and WNT11. *Proc National*
15 *Acad Sci* 106, 16978–16983 (2009).
- 16 51. Hansen, A. *et al.* Development of a Drug Screening Platform Based on Engineered Heart
17 Tissue. *Circ Res* 107, 35–44 (2010).
- 18 52. Maffioletti, S. M. *et al.* Three-Dimensional Human iPSC-Derived Artificial Skeletal
19 Muscles Model Muscular Dystrophies and Enable Multilineage Tissue Engineering. *Cell*
20 *Reports* 23, 899–908 (2018).
- 21 53. Iuliano, A. *et al.* Coupling 3D Printing and Novel Replica Molding for In House
22 Fabrication of Skeletal Muscle Tissue Engineering Devices. *Adv. Mater. Technol.* 5, 2000344
23 (2020).
- 24 54. eht-technologies-<https://www.eht-technologies.com/products.html-2022-01-28>. Preprint
25 at <https://www.eht-technologies.com/products.html>.
- 26 55. Atae, A., Li, Y. & Wen, C. A comparative study on the nanoindentation behavior, wear
27 resistance and in vitro biocompatibility of SLM manufactured CP–Ti and EBM manufactured
28 Ti64 gyroid scaffolds. *Acta Biomater* 97, 587–596 (2019).
- 29 56. Choi, H. K., Kim, C.-H., Lee, S. N., Kim, T.-H. & Oh, B.-K. Nano-sized graphene oxide
30 coated nanopillars on microgroove polymer arrays that enhance skeletal muscle cell
31 differentiation. *Nano Convergence* 8, 40 (2021).
- 32 57. Otomo, A. *et al.* Efficient differentiation and polarization of primary cultured neurons on
33 poly(lactic acid) scaffolds with microgrooved structures. *Sci Rep-uk* 10, 6716 (2020).
- 34 58. Rizki-Safitri, A. *et al.* Efficient functional cyst formation of biliary epithelial cells using
35 microwells for potential bile duct organisation in vitro. *Sci Rep-uk* 8, 11086 (2018).

- 1 59. Osaki, T., Shin, Y., Sivathanu, V., Campisi, M. & Kamm, R. D. In Vitro Microfluidic
2 Models for Neurodegenerative Disorders. *Adv Healthc Mater* 7, 1700489 (2018).
- 3 60. Zhang, S., Wan, Z. & Kamm, R. D. Vascularized organoids on a chip: strategies for
4 engineering organoids with functional vasculature. *Lab Chip* 21, 473–488 (2021).
- 5 61. Chan, H. N. *et al.* Direct, one-step molding of 3D-printed structures for convenient
6 fabrication of truly 3D PDMS microfluidic chips. *Microfluid Nanofluid* 19, 9–18 (2015).
- 7 62. Hart, C., Didier, C. M., Sommerhage, F. & Rajaraman, S. Biocompatibility of Blank,
8 Post-Processed and Coated 3D Printed Resin Structures with Electrogenic Cells. *Biosensors*
9 10, 152 (2020).
- 10 63. Waheed, S. *et al.* Enhanced physicochemical properties of polydimethylsiloxane based
11 microfluidic devices and thin films by incorporating synthetic micro-diamond. *Sci Rep-uk* 7,
12 15109 (2017).
- 13 64. Wang, L., Sun, B., Ziemer, K. S., Barabino, G. A. & Carrier, R. L. Chemical and physical
14 modifications to poly(dimethylsiloxane) surfaces affect adhesion of Caco-2 cells. *J Biomed*
15 *Mater Res A* 93A, 1260–1271 (2010).
- 16 65. Hoffmann, A. *et al.* New stereolithographic resin providing functional surfaces for
17 biocompatible three-dimensional printing. *J Tissue Eng* 8, 2041731417744485 (2017).
- 18 66. Bacha, T. W., Manuguerra, D. C., Marano, R. A. & Stanzione, J. F. Hydrophilic
19 modification of SLA 3D printed droplet generators by photochemical grafting. *Rsc Adv* 11,
20 21745–21753 (2021).
- 21 67. Urrios, A. *et al.* 3D-printing of transparent bio-microfluidic devices in PEG-DA. *Lab*
22 *Chip* 16, 2287–2294 (2016).
- 23 68. Bhattacharjee, N., Parra-Cabrera, C., Kim, Y. T., Kuo, A. P. & Folch, A. Desktop-
24 Stereolithography 3D-Printing of a Poly(dimethylsiloxane)-Based Material with Sylgard-184
25 Properties. *Adv Mater* 30, e1800001 (2018).
- 26 69. Toepke, M. W. & Beebe, D. J. PDMS absorption of small molecules and consequences in
27 microfluidic applications. *Lab Chip* 6, 1484–1486 (2006).
- 28 70. Meer, B. J. van *et al.* Small molecule absorption by PDMS in the context of drug
29 response bioassays. *Biochem Bioph Res Co* 482, 323–328 (2017).
- 30 71. Regehr, K. J. *et al.* Biological implications of polydimethylsiloxane-based microfluidic
31 cell culture. *Lab Chip* 9, 2132–2139 (2009).
- 32 72. Hall, C. E. *et al.* Progressive Motor Neuron Pathology and the Role of Astrocytes in a
33 Human Stem Cell Model of VCP-Related ALS. *Cell Reports* 19, 1739–1749 (2017).
- 34 73. Fusion 360 | 3D CAD, CAM, CAE & PCB Cloud-Based Software | Autodesk.
35 <https://www.autodesk.com/products/fusion-360/overview>.

- 1 74. Tinkercad | Create 3D digital designs with online CAD | Tinkercad.
- 2 <https://www.tinkercad.com/>.
- 3 75. Gopal, S. *et al.* Biointerfaces: Porous Silicon Nanoneedles Modulate Endocytosis to
- 4 Deliver Biological Payloads (Adv. Mater. 12/2019). *Adv Mater* 31, 1970086 (2019).
- 5 76. Schindelin, J. *et al.* Fiji: an open-source platform for biological-image analysis. *Nat*
- 6 *Methods* 9, 676–682 (2012).
- 7 77. Goedhart, J. SuperPlotsOfData—a web app for the transparent display and quantitative
- 8 comparison of continuous data from different conditions. *Mol Biol Cell* 32, 470–474 (2021).
- 9 78. Hansen, A. *et al.* Development of a Drug Screening Platform Based on Engineered Heart
- 10 Tissue. *Circ Res* 107, 35–44 (2010).
- 11 79. Johnston, I. D., McCluskey, D. K., Tan, C. K. L. & Tracey, M. C. Mechanical
- 12 characterization of bulk Sylgard 184 for microfluidics and microengineering. *J.*
- 13 *Micromechanics Microengineering* 24, 035017 (2014).